



**HAL**  
open science

## Quantification of CO<sub>2</sub> uptake of concretes with mineral additions after 10-year natural carbonation

Akli Younsi, Philippe Turcry, Abdelkarim Aït-Mokhtar

► **To cite this version:**

Akli Younsi, Philippe Turcry, Abdelkarim Aït-Mokhtar. Quantification of CO<sub>2</sub> uptake of concretes with mineral additions after 10-year natural carbonation. *Journal of Cleaner Production*, 2022, 349, pp.131362. 10.1016/j.jclepro.2022.131362 . hal-03636490

**HAL Id: hal-03636490**

**<https://hal.science/hal-03636490>**

Submitted on 22 Jul 2024

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Distributed under a Creative Commons Attribution - NonCommercial 4.0 International License

## Quantification of CO<sub>2</sub> uptake of concretes with mineral additions after 10-year natural carbonation

Akli Younsi, Philippe Turcry\*, Abdelkarim Aït-Mokhtar

*La Rochelle University, LaSIE UMR CNRS 7356, Avenue Michel Crépeau, 17042 La Rochelle Cedex 1, France*

\* Corresponding author.

*E-mail address:* [philippe.turcry@univ-lr.fr](mailto:philippe.turcry@univ-lr.fr) (Ph. Turcry),

*Postal address:* La Rochelle University, LaSIE UMR CNRS 7356, Avenue Michel Crépeau, 17042 La Rochelle Cedex 1, France

*E-mail addresses:* [akli.younsi@univ-lr.fr](mailto:akli.younsi@univ-lr.fr) (A. Younsi), [philippe.turcry@univ-lr.fr](mailto:philippe.turcry@univ-lr.fr) (Ph. Turcry), [karim.ait-mokhtar@univ-lr.fr](mailto:karim.ait-mokhtar@univ-lr.fr) (A. Aït-Mokhtar)

### ABSTRACT

The CO<sub>2</sub> uptake of Portland cement, fly ash and blast furnace slag concrete cylinders was determined after 10-year natural carbonation. The purpose was to provide data to better assess the exchanges of CO<sub>2</sub> during the life cycle of structures. The CO<sub>2</sub> uptake of cylinders (mass of bound CO<sub>2</sub> per unit of surface) was calculated from profiles of CO<sub>2</sub> content determined by thermogravimetric and chemical analyses. The CO<sub>2</sub> binding capacity of concrete with high slag content was found much lower than that of Portland cement concrete, due to the low

degree of carbonation of CaO from slag. The CO<sub>2</sub> uptakes of the studied specimens were however rather close. High carbonation depth of slag concretes compensates partly their lower binding capacity. The experimental results were compared to predictions of the European Standard EN 16757 model. The Standard model underestimates the CO<sub>2</sub> uptake of concretes with mineral addition mainly because of an underestimation of the carbonation depth.

*Keywords:*

CO<sub>2</sub> uptake

Blended cement

Fly ash

Ground granulated blast-furnace slag

Natural carbonation

Sheltered/unsheltered natural exposure

Bound CO<sub>2</sub> content

Degree of carbonation

European Standard EN 16757

1 Wordcount : 10623 words

## 2 **1. Introduction**

3

4 Life cycle analyzes showed that cement production, responsible for 65 – 85 % of CO<sub>2</sub>  
5 emissions from concrete manufacturing, accounts for 5 – 8 % of global CO<sub>2</sub> emissions (Miller  
6 et al., 2016; Olivier et al., 2016; Andrew, 2019; Lim et al., 2019). Therefore, efforts to  
7 mitigate CO<sub>2</sub> emissions from concrete manufacturing have focused on: (i) using alternative  
8 fuels and raw materials during cement production, (ii) developing alternative low-carbon  
9 binders, (iii) substituting with raw or mineral materials a part of clinker during cement  
10 production or a part of cement during concrete manufacturing (Flower et al., 2007; Younsi et  
11 al., 2013; Gartner et al., 2015; Feiz et al., 2015; Elchalakani et al., 2017; Younsi et al., 2019;  
12 Costa et al., 2020; Ren et al., 2020; Esfahani et al., 2021; Younsi et al., 2021). However, to  
13 establish a more complete life cycle inventory of concrete in terms of carbon footprint, in  
14 addition to accounting for the CO<sub>2</sub> emissions due to its manufacture, it becomes essential to  
15 consider also the CO<sub>2</sub> uptake due to its carbonation (Lagerblad et al., 2005; Galan et al., 2010;  
16 Ashraf, 2016 ; Jang et al., 2016 ; Lee et al., 2016 ; Possan et al., 2016 ; Andrade et al., 2018;  
17 Andersson et al., 2019; Sanjuán et al., 2019; Sanjuán et al., 2020; Witkowski et al., 2020;  
18 Kwon et al., 2021). The CO<sub>2</sub> uptake is defined as the quantity of CO<sub>2</sub> bound by a concrete  
19 structure and expressed in mass of bound CO<sub>2</sub> per unit area of this structure. For instance, the  
20 study conducted by Pade and Guimaraes showed that, after 70 years, concrete structures  
21 produced in 2003 will bind about 28 % of the CO<sub>2</sub> emissions from cement production (Pade et  
22 al., 2007). (Yang et al., 2014) showed that concrete structure will bind 18 – 21 % of the CO<sub>2</sub>  
23 emissions from cement production, after 100 years. (Fitzpatrick et al., 2015) showed that  
24 structures built in 1972 will bind, after 100 years, about 16 % of the CO<sub>2</sub> emissions from  
25 cement production. The study of (Xi et al., 2016) showed that, due to their natural carbonation

1 occurring between 1930 and 2013, cementitious materials have bound 43 % of the CO<sub>2</sub>  
2 emissions from cement production for the same period. The authors concluded that  
3 carbonation is an important carbon sink which is not yet included in life cycle inventories.

4 Carbonation is a natural aging process during which atmospheric CO<sub>2</sub> diffuses into the  
5 pore network of concrete and chemically reacts with hydration products, forming mainly  
6 CaCO<sub>3</sub> (Papadakis et al., 1991). This phenomenon can be considered from two opposing  
7 points of view depending on how the role of chemical reactions involving CO<sub>2</sub> is considered:  
8 (i) from the point of view of durability of reinforced concrete structures, chemical reactions  
9 between CO<sub>2</sub> and hydration products can initiate the rebar corrosion by lowering the *pH* of the  
10 pore solution. Carbonation is thus considered as a degradation phenomenon expected to  
11 reduce the service life of structures, (ii) from the point of view of environmental impact, the  
12 chemical reactions involving CO<sub>2</sub> allow bounding CO<sub>2</sub> within the concrete. Carbonation is  
13 thus considered as a process contributing to the reduction of CO<sub>2</sub> emissions from concrete  
14 manufacturing and use.

15 As pointed out by Andrade, very few studies were devoted to the quantification of bound  
16 CO<sub>2</sub> (Andrade, 2020). The calculation of CO<sub>2</sub> uptake remains a very complex task since only  
17 approximate calculation methods and empirical models are used (Andersson et al., 2013). A  
18 standardized calculation method is presented in the Annex BB of the European Standard  
19 EN 16757 (EN16757, 2017). The standard allows assessing the CO<sub>2</sub> uptake at different life  
20 cycle stages by assuming a direct link between carbonation and amount of reactive CaO in  
21 concrete. To assess the CO<sub>2</sub> uptake occurring during a given period, EN 16757 refers to the  
22 concepts of: (i) carbonation rate, which is defined by considering both the compressive  
23 strength class and the exposure conditions, (ii) degree of carbonation (ratio between  
24 carbonated and available reactive CaO), (iii) maximum theoretical uptake of CO<sub>2</sub> in totally  
25 carbonated concrete which is correlated with the reactive CaO content in the binder. Results

1 from some published works, such as those carried out by (Yang et al., 2014) and (Fitzpatrick  
2 et al., 2015), are consistent with the calculations from EN 16757 in terms of CO<sub>2</sub> uptake.  
3 However, the findings provided by these studies remain theoretical long-term assessments (up  
4 to 100 years) that are difficult to validate with experimental data due to the lack of availability  
5 of the latter, as mentioned previously (Andrade, 2020). It thus appears interesting to compare  
6 experimental results obtained over a realistic and sufficiently long period exposure to natural  
7 carbonation with prediction of models such as the EN 16757 standard model. Moreover, there  
8 is also a lack of data on the CO<sub>2</sub> uptake of concrete made with blended binders that are  
9 increasingly used to the detriment of Ordinary Portland Cement (OPC) to reduce the footprint  
10 of concrete use.

11 In the view of these considerations, the present work aims at providing data on CO<sub>2</sub> uptake  
12 due to atmospheric carbonation of various concretes. There is still a lack of this type of data in  
13 the literature, especially for concretes with mineral additions. These data are necessary to  
14 better assess the real environmental footprint of the use of concrete in civil engineering  
15 structures with approach such as the one proposed by (Xi et al., 2016).

16 For this purpose, an experimental study was carried out on concretes designed with OPC,  
17 blended cements containing fly ash or ground granulated blast furnace slag (GGBFS), and  
18 partial substitutions of OPC with fly ash or GGBFS. The concretes were subjected to 10-year  
19 natural carbonation, under sheltered and unsheltered conditions. During the exposure period,  
20 the progress of carbonation was monitored by regular carbonation depth measurements. At the  
21 end of the exposure period, the CO<sub>2</sub> uptake was determined by Thermogravimetric analysis  
22 (TGA) coupled to chemical analysis by Inductively Coupled Plasma - Atomic Emission  
23 Spectroscopy (ICP-AES). In the following, the results of this experimental investigation are  
24 analyzed to assess the effect of both binder nature and exposure on CO<sub>2</sub> binding capacity,  
25 degree of carbonation and CO<sub>2</sub> uptake of the studied specimens. Finally, the experimental

1 results are compared to calculations using the EN 16757 model and its range of validity is  
2 discussed.

3

## 4 **2. Materials and methods**

5

### 6 *2.1. Materials*

7

8 The study was carried out on concrete mixtures designed with three cements as per the  
9 European Standard EN 197-1 ([EN197-1, 2011](#)): an Ordinary Portland Cement CEM I 52.5 N  
10 ~~from Lafarge France~~, a blended cement CEM II/B-V 32.5 R ~~from CCB Belgium~~, and a  
11 ground granulated blast-furnace slag cement CEM III/C 32.5 N ~~from Calcia France~~. Other  
12 constituents were used: a fly ash (FA) with low calcium content ~~from Surschiste France~~ as per  
13 the European Standard EN 450-1 ([EN15167, 2006](#)), a ground granulated blast-furnace slag  
14 (GGBFS) ~~from Ecocem Netherlands~~ as per the European Standard EN 15167-1 ([EN15167,](#)  
15 [2006](#)), a siliceous sand (0/4 mm) and two crushed diorite gravels (6.3/10 and 10/14 mm) ~~from~~  
16 ~~HeidelbergCement France~~ as per the European Standard EN 13139 ([EN13139, 2003](#)), and a  
17 polycarboxylate superplasticizer ~~Fluid-Optima 206<sup>®</sup> from Chryse France~~ as per the European  
18 Standard EN 934-2+A ([EN934-2, 2012](#)). [Table 1](#) shows the properties of the cementitious  
19 materials used. The chemical compositions of the binders were obtained by X-ray  
20 fluorescence (XRF) analysis. Note that the used sand is a sea sand which contains trace of  
21 limestone due to shell particles. Its mass content of CaCO<sub>3</sub> is equal to 6.9%.

22

### 23 **Table 1**

24 Physical, mineralogical, and chemical properties of the cementitious materials used.

Cements			Mineral additions	
CEM I	CEM II	CEM III	FA	GGBFS

<i>Physical properties</i>					
Density [kg/m <sup>3</sup> ]	3110	2890	2900	2210	2890
Blaine surface [cm <sup>2</sup> /g]	3400	3247	4280	4050	4500
<i>Composition [w%]</i>					
Clinker	95	73	15	0	0
Gypsum	5	4	3	0	0
Fly ash	0	23	0	100	0
GGBFS	0	0	82	0	100
Limestone	0	4	3	0	0
<i>Chemical composition [w%]</i>					
CaO	64.8	48.9	45.1	5.2	41.5
SiO <sub>2</sub>	20.5	27.4	32.0	55.3	33.3
Al <sub>2</sub> O <sub>3</sub>	4.5	9.0	10.3	25.2	12.5
Fe <sub>2</sub> O <sub>3</sub>	2.7	3.4	0.8	6.4	0.4
SO <sub>3</sub>	3.5	2.8	2.9	0.5	0.2
MgO	1.5	2.0	6.1	0.9	7.0
<i>Clinker mineralogical composition [w%]</i>					
C <sub>3</sub> S	67	69	66	-	-
C <sub>2</sub> S	13	10	13	-	-
C <sub>3</sub> A	7	9	11	-	-
C <sub>4</sub> AF	8	7	7	-	-

1

2 

## 2.2. Mixtures

3

4 The proportions used in the mixes are given in [Table 2](#). Three concrete mixtures were used  
5 as references: Ref I with CEM I, Ref II with CEM II and Ref III with CEM III. Three other  
6 concrete mixtures were designed with partial substitution of CEM I with FA (FA 30) or  
7 GGBFS (S 30 and S 75). Except for S 75, all the mixtures were designed as per the  
8 prescriptive requirements from the French annex of the European Standard NF EN 206/CN  
9 ([EN206/CN, 2014](#)) corresponding to the exposure class XC 3. These requirements are the  
10 following: a minimum strength class C25/30, a minimum equivalent binder content  
11 (Eq.binder) of 280 kg/m<sup>3</sup>, a maximum effective water-to-equivalent binder ratio  
12 (W/Eq.binder) of 0.6, and a maximum cement substitution ratio (A/(A+C)) of 30 % for FA 30  
13 and S 30. It should be noted that the requirements corresponding to XC 3 are equivalent to



1 those corresponding to XC 4. Moreover, the mixture S 75, which does not comply with the  
 2 prescriptive requirements of EN 206, was designed with a cement substitution ratio of 75 %  
 3 using the mix-design method suggested by (Khokhar et al., 2010). Its effective water-to-  
 4 binder ratio ( $W/(A+C)$ ) was optimized using the Bolomey's equation to obtain a 2-day  
 5 compressive strength of 10 MPa. Finally, for all the mixtures, the amount of superplasticizer  
 6 was adjusted to obtain a slump higher than 150 mm. Additional details on the mix-design  
 7 method used can be found in (Younsi et al., 2011). In summary, the six studied concretes are  
 8 equivalent in terms of site construction application, since they have the same workability and  
 9 mechanical performances at early age and 28 days.

10 The concrete mixtures were cast, according to the European Standard EN 12390-12  
 11 (EN12390-12, 2020), into Ø11X22 cm molds and stored in a room at  $20 \pm 1$  °C for 24 h.  
 12 Other physical, chemical and mechanical properties are given in Table 2. Especially, Table 2  
 13 gives the total mass of CaO from the  $\text{CaCO}_3$  of both sand and binder and from the anhydrous  
 14 elements of binder (e.g.,  $\text{C}_3\text{S}$ ,  $\text{C}_2\text{S}$ ). The parameter denoted  $\alpha$  is the fraction of CaO from the  
 15 binder to the total mass of CaO.

16

17 **Table 2**

18 Mix proportions per cubic meter of concrete and properties.

	Ref I	Ref II	Ref III	FA 30	S 30	S 75
CEM I 52.5 N [kg]	303	0	0	241	219	103
CEM II/B-V 32.5 R [kg]	0	321	0	0	0	0
CEM III/C 32.5 N [kg]	0	0	361	0	0	0
Fly ash [kg]	0	0	0	103	0	0
GGBFS [kg]	0	0	0	0	94	310
Gravel 10/14 [kg]	875	875	859	844	868	836
Gravel 6/10 [kg]	211	211	207	204	209	201
Sand 0/4 [kg]	855	855	839	824	848	816
Effective water [kg]	182	175	175	182	182	170
Superplasticizer [kg]	1.36	1.00	1.00	1.75	0.26	1.89
$W/(A+C)$ [-]	0.60	0.54	0.48	0.53	0.58	0.41
Binder content [%]	12.5	13.2	14.8	14.4	12.9	16.9

Eq.binder [kg]	303	321	361	303	304	223
W/Eq.binder [-]	0.60	0.54	0.48	0.60	0.59	0.76
Clinker [kg]	288	234	54	229	208	98
Total CaO from binder and sand [kg]	229	190	195	193	214	227
CaO from binder [kg]	196	157	163	161	181	195
$\alpha$ [-]	0.86	0.83	0.83	0.83	0.85	0.86
28-day water porosity [%]	13.8	12.6	16.7	14.4	13.5	13.7
28-day compressive strength [MPa]	36	32	34	33	36	40

*A = Mineral addition; C = Cement; W = Effective water; Eq.binder = Equivalent binder*

1

### 2 2.3. Carbonation conditions

3

4 Immediately after demolding at 1 day, the Ø11X22 cm specimens were subjected to natural  
5 carbonation under sheltered conditions (exposure class XC 3 as per EN 206) and unsheltered  
6 (XC 4) conditions for 10 years. This demolding at early age is not favorable for some  
7 concretes, such as GGBFS concrete (Ref III), but this makes the study conditions more  
8 representative of in working site conditions (i.e., poorly hydrated concrete cover), which  
9 interest the project managers. Table 3 gives the ranges of temperature and relative humidity at  
10 both exposure sites located in La Rochelle, France. In unsheltered conditions, the specimens  
11 were placed on the floor of an outside laboratory platform. So, they were subject to rain,  
12 wind, and solar radiation. Over the 10 years, the specimens were sometimes rotated, so that  
13 the effect of solar radiation is on all sides. In the sheltered conditions, the specimens were  
14 placed on shelves protected from external climatic conditions (rain and sun).

15

#### 16 **Table 3**

17 Temperature and relative humidity at both exposure sites: averages and ranges (minimum and  
18 maximum were obtained from 2-day moving averaging).

	Sheltered conditions	Unsheltered conditions
Temperature (°C)	18 (14 – 26)	13 (2 - 26)
Relative humidity (%)	70 (30 – 80)	77 (50 – 95)

1

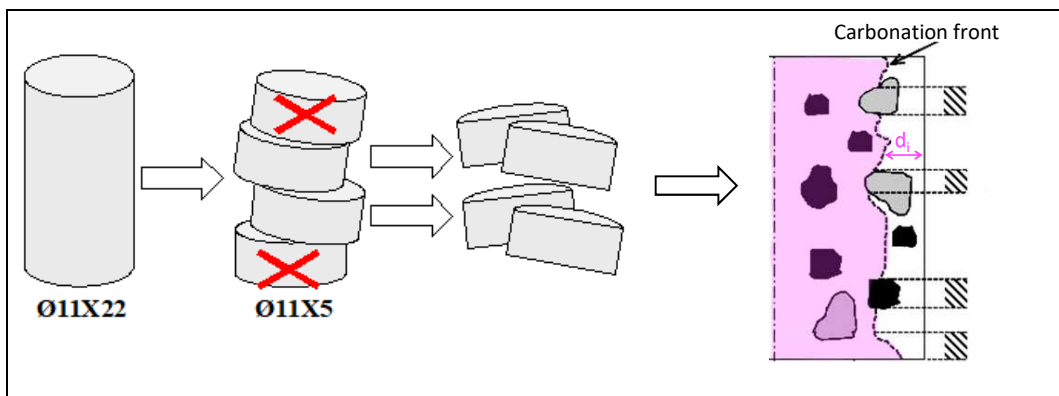
2 *2.4. Determination of carbonation depths by phenolphthalein spraying*

3

4 Carbonation depths were determined at 1, 2, 3, 6 and 10 years on Ø11X5 cm specimens  
5 saw-cut from the Ø11X22 cm specimens. The Ø11X5 cm specimens were split in half and a  
6 *pH* indicator solution, namely a solution of 1% phenolphthalein, was sprayed on the split  
7 sections to assess the carbonation depth as per the European Standard EN 12390-12  
8 (EN12390-12, 2020). Before spraying phenolphthalein, the top and the bottom of the  
9 Ø11X22 cm specimens were removed to only consider the carbonation depths due to radial  
10 CO<sub>2</sub> diffusion. The carbonation depth is the mean value of depths  $d_i$  determined as shown in  
11 Fig. 1. It should be kept in mind that phenolphthalein reveals area where *pH* is lower than 9  
12 and not strictly speaking a fully carbonated area.

13

14



15

16 **Fig. 1.** Schematic presentation of the carbonation characterization by phenolphthalein  
17 spraying: sawing of cylindrical specimen, then splitting of the obtained discs, and finally  
18 determination of carbonation depths ( $d_i$ ) after phenolphthalein spraying. Depths  $d_i$  are  
19 measured outside the hatched zones (EN12390-12, 2020).

20

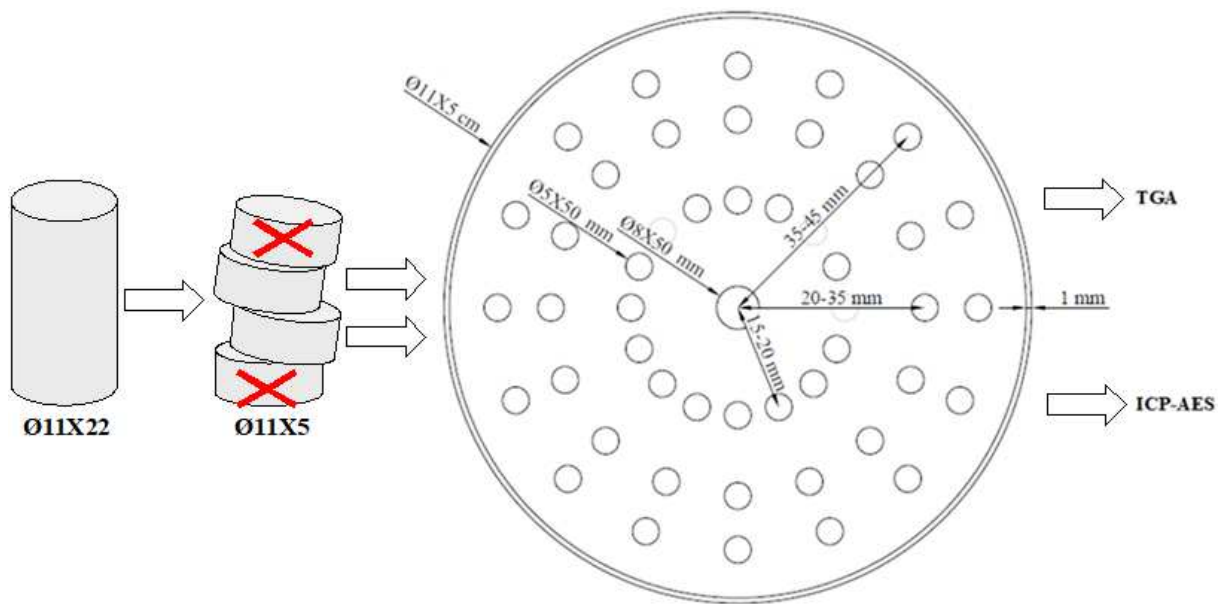
## 2.5. Carbonation characterization by TGA coupled to chemical analysis ICP-AES

Carbonation measurements were carried out after 10-year exposure by determining the bound CO<sub>2</sub> contents in concrete powders. The latter were obtained by drilling holes in Ø11X5 cm specimens, themselves saw-cut from the Ø11X22 cm specimens (Fig. 2). Before drilling holes, the top and the bottom of the Ø11X22 cm specimens were removed to only consider the radial carbonation. The centers of the holes were located at 4 different distances, from the core, chosen according to the carbonation depths revealed by phenolphthalein: 0; 15 – 20; 20 – 35 and 35 – 45 mm. For a given Ø11X5 cm specimen, a Ø8X50 mm hole was drilled through the core, and at each intermediate distance, 16 Ø5X50 mm holes were drilled. Moreover, the skin was removed to a depth of about 1 mm by planing. To avoid their carbonation, the powders were stored in a desiccator where the relative humidity was maintained at about 3 % by silica gel. The bound CO<sub>2</sub> contents were determined by thermogravimetric analysis (TGA) carried out on 210 ± 45 mg powders using a Setaram Setsys Evolution<sup>®</sup> device with a heating rate of 10 °C/min from 20 to 1000 °C in an argon atmosphere (Thiery et al., 2007; Bordy et al., 2017; Younsi et al., 2018). The mass of bound CO<sub>2</sub> corresponds to the loss of mass between 600°C and 900°C. In practice, this temperature range was refined by considering the derivative thermogravimetry (DTG) which reveals a peak at around 700°C due to the sample decarbonation. 2 to 3 replicates were used for TGA.

The bound CO<sub>2</sub> content determined by TGA is expressed in mg of CO<sub>2</sub> per mg of concrete powder. However, the powders are not enough homogenous and representative of the concrete. To express the bound CO<sub>2</sub> content as a function of a representative quantity of concrete, the binder content in each powder was assessed by chemical analysis (Turcry et al., 2014; Villain et al., 2007). The procedure consists of dissolving 100 ± 0.5 mg powder in 2 ± 0.01 mg nitric acid (HNO<sub>3</sub>) for 24 hours. After that, a solution of HNO<sub>3</sub>, with 1/50

1 dilution in pure water, is added. A week later, the suspension obtained is analyzed by  
 2 Inductively Coupled Plasma-Atomic Optical Emission Spectroscopy (ICP-AES), using a  
 3 Varian Vista device Pro<sup>®</sup>, to determine its CaO content. From the latter, it is possible to  
 4 deduce the binder content in each concrete powder, as explained in section 3.2. One replicate  
 5 for each sampling position was used for chemical analysis.

6



7

8

9 **Fig. 2.** Schematic presentation of the carbonation characterization by TGA/ICP-AES.

10

11 *2.6. Calculation of CO<sub>2</sub> uptake from Standard EN 16575*

12

13 An empirical model for the prediction of CO<sub>2</sub> uptake by cement-based products is proposed in  
 14 the European Standard EN 16757. In the following sections, the predictions of this model are  
 15 compared to our experimental results. To facilitate the comparison, we adopt the following  
 16 nomenclature.

17 The uptake of CO<sub>2</sub> is expressed by exposure surface [kg<sub>CO<sub>2</sub></sub>/m<sup>2</sup>] as follows:

18

$$\text{Uptake}(t) = \text{CBC} \cdot X_c(t) \quad (1)$$

1

2 Where: CBC is the CO<sub>2</sub> binding capacity of the carbonated zone [kg<sub>CO<sub>2</sub></sub> per m<sup>3</sup> of concrete]

3 and X<sub>c</sub>(t) is the carbonation depth [m] at an exposure time t [year].

4 In the model of European Standard, the carbonation depth is classically calculated as a

5 function of the square root of time:

6

$$X_c(t) = k\sqrt{t} \quad (2)$$

7

8 With: k the carbonation rate defined by considering the compressive strength class, the

9 exposure conditions (sheltered or unsheltered), and the type and the dosage of mineral

10 additions used.

11 The CO<sub>2</sub> binding capacity of the carbonated zone (CBC) is calculated with a conservative

12 approach assuming that only the calcium oxides from clinker can be carbonated (Eq. 3). This

13 approach is based on the point of view of the cement industry, since carbonation is seen in the

14 scope of CCUS (Carbon Capture, Utilization and Storage) as a way to use or consume the

15 CO<sub>2</sub> emitted during the production of clinker.

16

$$\text{CBC} = K \cdot U_K \cdot \text{DoC} \quad (3)$$

17

18 Where: CBC is the CO<sub>2</sub> binding capacity [kg<sub>CO<sub>2</sub></sub> per m<sup>3</sup> of carbonated concrete], K the clinker

19 content [kg<sub>K</sub>/m<sup>3</sup><sub>concrete</sub>], U<sub>K</sub> the maximum bound CO<sub>2</sub> by carbonation of CaO from the

20 clinker [kg<sub>CO<sub>2</sub></sub>/kg<sub>K</sub>], and DoC the degree of carbonation [-]. The latter is defined as the ratio

21 of the total bound CO<sub>2</sub> content for a given exposure and the theoretical maximum bound CO<sub>2</sub>.

22 Values of DoC are proposed for 3 exposures, i.e., indoor (0.40), outdoor sheltered (0.75),

1 outdoor unsheltered (0.85).  $U_K$  is usually taken equal to 0.5 kg<sub>CO2</sub>/kg<sub>K</sub> (for a CaO content in  
2 the clinker of around 65%).

3 To compare the model predictions with the experimental results, the model cannot be used as  
4 is, because the diffusion of CO<sub>2</sub> in our cylindrical specimens is radial. The square-root of time  
5 model given by Equation 2 is only valid for an axial diffusion. The calculated values of  $X_c$   
6 must be corrected with the method presented in Appendix 1, which considers the cylindrical  
7 geometry for a sharp front carbonation. Knowing the corrected  $X_c$ , the CO<sub>2</sub> uptake is then  
8 calculated as follows:

9

$$\text{Uptake} = \frac{1}{R} \int_{X_c}^R \text{CBC} \cdot r dr = \text{CBC} \left[ \frac{R^2 - (R - X_c)^2}{R} \right] \quad (4)$$

10

11 where:  $R$  [m] is the radius of the cylindrical specimen.

12

### 13 **3. Results**

14

#### 15 *3.1. Carbonation depths*

16

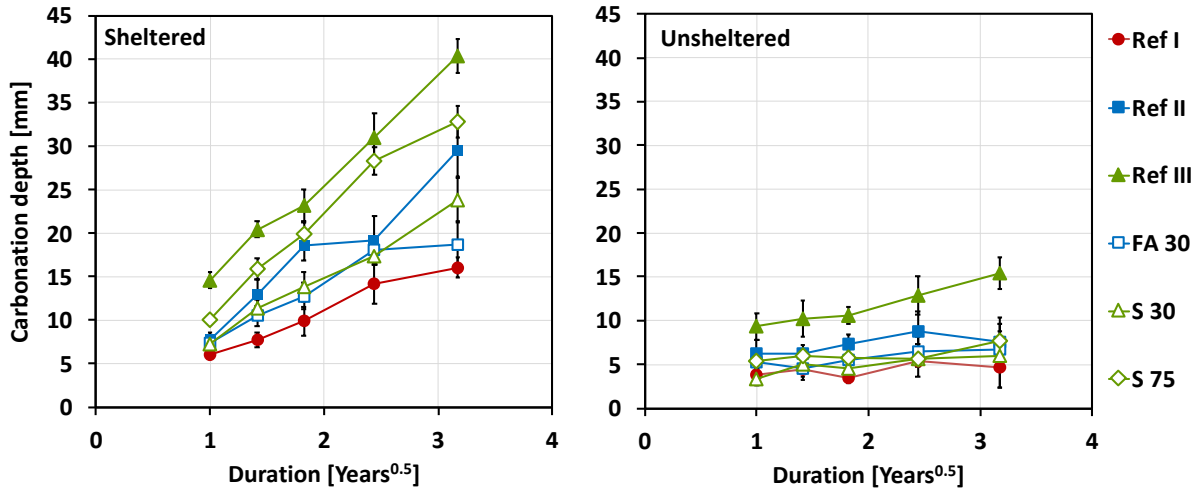
17 **Fig. 3** shows the time-evolution of the carbonation depths revealed after phenolphthalein  
18 spraying. For both sheltered and unsheltered conditions, FA 30 is more resistant against  
19 carbonation than Ref II, i.e. the reference with FA. S 30 and S 75 are more resistant than  
20 Ref III, i.e. the reference with GGBFS. In terms of natural carbonation, concretes with cement  
21 substitution thus exhibit a potential durability at least equivalent to that of the concretes with  
22 blended cements. By applying the concept of equivalent performance stated by the European  
23 Standard EN 206/CN, S 75, which does not comply with the prescriptive requirements of the  
24 standard, can replace at least Ref III. This result is consistent with previous studies on this

1 concrete mixture (Younsi et al., 2013; Younsi et al., 2019). Moreover, although Ref III  
2 complies with the prescriptive requirements of EN 206, it has the lowest resistance against  
3 carbonation. This is usually explained by the fact that, due to its very low clinker content, it  
4 has the lowest amount of carbonatable products and the highest water porosity (Table 2). Its  
5 CO<sub>2</sub> diffusion coefficient should be also the highest one because carbonation increases the  
6 CO<sub>2</sub> diffusivity of materials with high amount of GGBFS. For this kind of materials, recent  
7 papers give evidence of increase in gas diffusivity due to microstructural changes (Boumaaza  
8 et al., 2020a) or microcracking (Kangni-Foli et al., 2021) resulting from carbonation. Ref I  
9 has the lowest carbonation rate, because it contains the highest clinker content, thus the  
10 highest amount of carbonatable products (Table 2). In addition, its CO<sub>2</sub> diffusivity should be  
11 the lowest since carbonation tends to decrease the gas diffusivity of materials with high  
12 amount of clinker (Boumaaza et al., 2020a).

13 Concretes exposed to carbonation under unsheltered conditions exhibit lower carbonation  
14 depths than those exposed to carbonation under sheltered conditions (relative deviations from  
15 20 to 80 %). This result is expected because precipitation maintains the concrete pore network  
16 often close to saturation, what limits gas diffusion (Houst et al., 2002; Yoon et al., 2007;  
17 Ekolu, 2016 ; Huy Vu et al., 2019 ; Otieno et al., 2020). The diffusion of CO<sub>2</sub> is thus only  
18 possible through the pore solution, which considerably slows down, the carbonation progress  
19 since CO<sub>2</sub> diffusion coefficient in air is known to be 10<sup>4</sup> times higher than that in water  
20 (Thiery, 2005). Carbonation occurs mainly when the pore network is sufficiently dry up to the  
21 carbonation depth reached before precipitation. Carbonation process is then mainly controlled  
22 by the frequency and duration of the wetting/drying periods.

23





1

2 **Fig. 3.** Time-evolution of the carbonation depth in sheltered (left) and unsheltered conditions  
 3 (right).

4

5 *3.2. Binder content*

6

7 Powder samples were obtained from drilling at different locations in the Ø11X5 cm  
 8 specimens. Chemical analyzes allowed assessing the CaO content (%CaO) in these powder  
 9 samples. The CaO is obtained from both the binder and the marine sand (the CaO comes from  
 10 shells contains in the sand). Let us assume that the mass fraction  $\alpha$ , as defined in section 2.2  
 11 and given in Table 2, is the same for the powder sample than for the concrete mixture. In other  
 12 words, we consider that the powder samples contain the same proportions of sand and binder  
 13 as in the concrete. The content of CaO obtained from the binder is then equal to  $\alpha$  %CaO.

14 Knowing the CaO content in the binder used (%CaO<sub>B</sub>), it was then possible to deduce the  
 15 binder content in the powder as:

16

$$\%B = \frac{\alpha \%CaO}{\%CaO_B} \quad (5)$$

17

1 %CaO<sub>B</sub> was calculated from the CaO content of each binder (Table 1) and from the mix  
2 proportions (Table 2) as follows:

$$\%CaO_B = \%CaO_{CEM\ I, CEM\ II\ or\ CEM\ III} \text{ for Ref I, Ref II or Ref III} \quad (6)$$

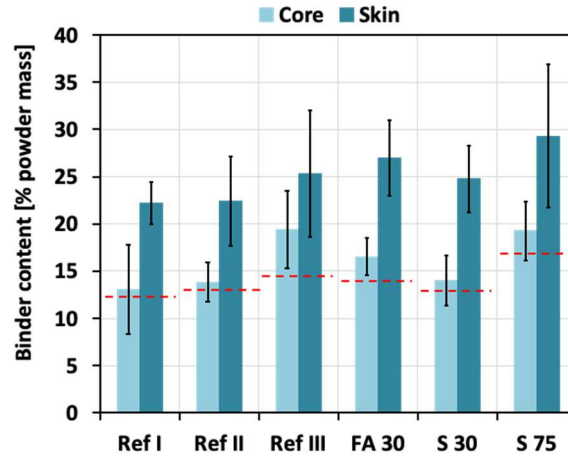
$$\%CaO_B = 0.70 \%CaO_{CEM\ I} + 0.30 \%CaO_{FA\ or\ GGBFS} \text{ for FA 30 or S 30} \quad (7)$$

$$\%CaO_B = 0.25 \%CaO_{CEM\ I} + 0.75 \%CaO_{GGBFS} \text{ for S 75} \quad (8)$$

3  
4 where: %CaO<sub>CEM I, CEM II or CEM III</sub> [%] are the CaO contents in CEM I, CEM II and CEM III,  
5 respectively. %CaO<sub>FA or GGBFS</sub> [%] are the CaO contents in FA and GGBFS, respectively.

6 For a given concrete, the binder contents of the powders taken between 0 and 45 mm, i.e., in  
7 the specimen core, were close, whatever the exposure conditions. Similarly, the binder  
8 contents of the powder samples taken at 55 mm, i.e., in the skin, were close. Fig. 4 shows the  
9 effect of the location (core versus skin) on the binder contents. The average %B are different  
10 from those calculated from the concrete composition given in Table 2 (relative difference  
11 from 18 to 59 %). This was expected since powder sampling by drilling or planing does not  
12 allow maintaining the initial composition. The binder content in the powders obtained by  
13 removing the skin by planing is higher than that in the powders taken by drilling the core. The  
14 observed relative difference of about 40 % is explained by the “skin-effect”, which leads to a  
15 surface layer richer in paste, thus in binder, than in the core (Kreijger, 1984). In the following,  
16 the average binder contents shown in Fig. 4 were used to calculate the bound CO<sub>2</sub> content per  
17 mass of binder. Different binder contents could have been used for each position. However,  
18 we distinguished only two cases: samples in the core (between 0 and 45 mm from the center)  
19 and samples in the skin (at 55 mm from the center). Let us recall that the sample is 110 mm  
20 diameter. This procedure was preferred for less inaccuracy, since only one replicate was used  
21 for chemical analysis.

22



1

2

3 **Fig. 4.** Average binder contents in the powder samples determined by chemical analysis, in  
 4 the specimen core (between 0 and 45 mm from the center) and in the skin (at 55 mm from the  
 5 center). The red dashed lines give the theoretical binder contents from the concrete  
 6 compositions (Table 2).

7

### 8 3.3. Profiles of bound CO<sub>2</sub> content per mass of binder

9

10 The bound CO<sub>2</sub> content at a location  $r$ , denoted  $(\%CO_2)_r$ , expressed by mass of binder was  
 11 determined from TGA on powders as follows (Eq. 9):

12

$$(\%CO_2)_r = 100 \cdot \left( \frac{\Delta m_{T_1 \rightarrow T_2}}{\%B \cdot m_P} \right)_r - 100 \cdot \beta \cdot \left( \frac{\Delta m_{T_1 \rightarrow T_2}}{\%B \cdot m_P} \right)_{r=0} \quad (9)$$

13

14 where:  $\Delta m_{T_1 \rightarrow T_2}$  [g] is the mass loss of the concrete powder during TGA in the temperature  
 15 range  $[T_1 - T_2]$ . Classically,  $T_1$  and  $T_2$  are close to 600°C and 900°C, respectively. %B [-] is the  
 16 binder content in the powder assessed by ICP-AES (section 3.2).  $m_P$  [g] is the mass of the  
 17 concrete powder tested by TGA.  $\beta$  is a correction factor accounting for the skin effect.

18 The center of the cylindrical specimen, i.e.,  $r = 0$ , is unaffected by carbonation. The CO<sub>2</sub>

1 content at this location results from the decarbonation of  $\text{CaCO}_3$  supplied by both sand and  
2 binder. By subtracting the value at  $r = 0$ , we obtain only the  $\text{CO}_2$  bound by carbonation. For  $r$   
3 lower than 55 mm, the correction factor  $\beta$  is taken equal to 0. On the skin of the specimen, the  
4  $\text{CaCO}_3$  content before carbonation is not the same than at  $r = 0$ . The difference is due to  
5 higher contents of sand and binder (as shown in section 3.2). Thus, to determine the bound  
6  $\text{CO}_2$  content at  $r = 55$  mm, the content of  $\text{CO}_2$  at  $r = 0$  in Equation 9 is corrected by  $\beta$ . The  
7 latter is calculated as the ratio of the binder content in the skin and the binder content in the  
8 core ( $\beta > 1$ ). Note that we assume that the proportions sand/binder are the same in the skin  
9 than in the core.

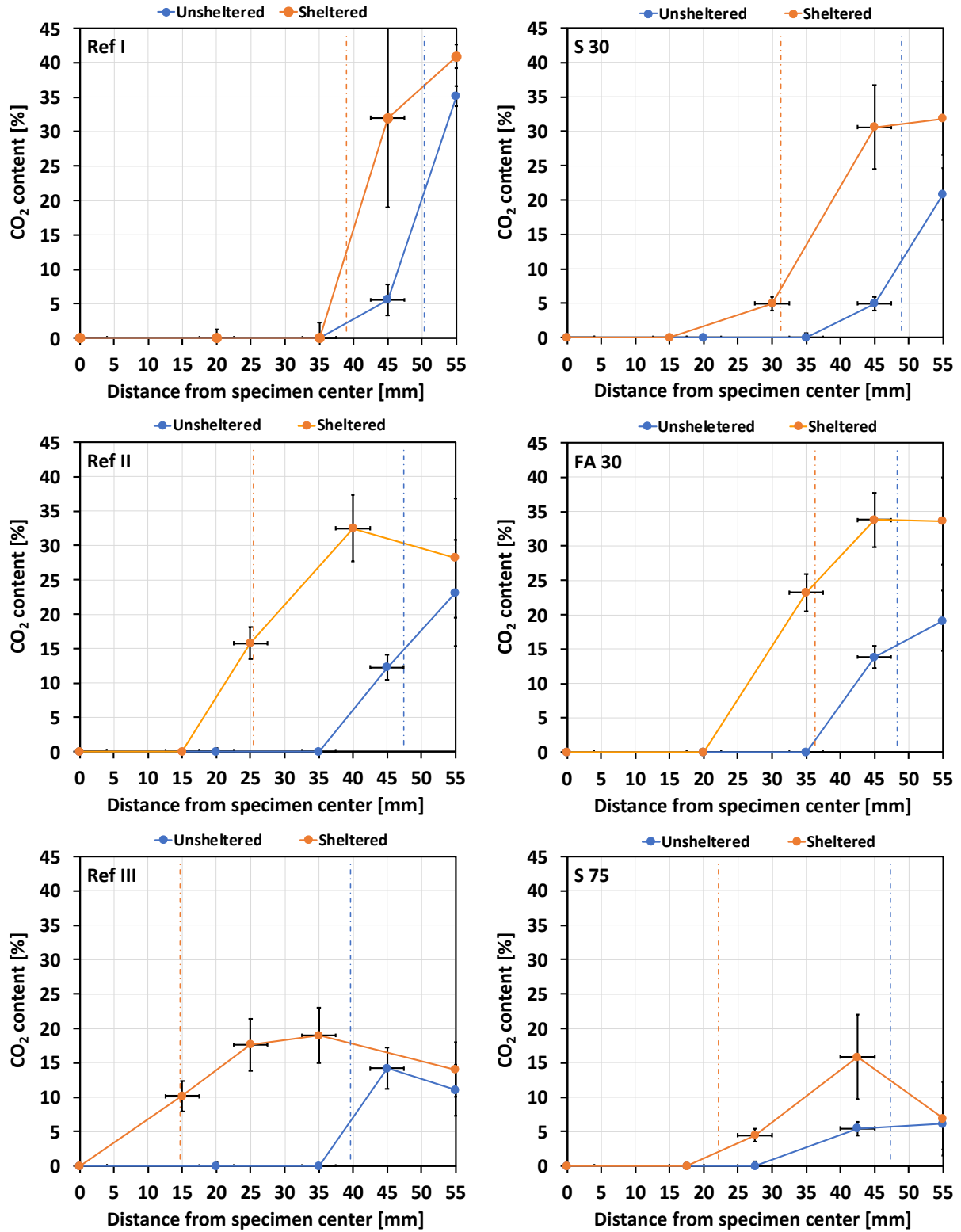
10 [Fig. 5](#) shows: (i) the carbonation fronts revealed by phenolphthalein spraying and (ii) the  
11 profiles of bound  $\text{CO}_2$  content. The carbonation fronts are rather close to that suggested by the  
12 bound  $\text{CO}_2$  content profiles determined by TGA/ICP-AES analysis. However, the latter shows  
13 that carbonation occurs more gradually, and in some cases more deeply than the pH front.  
14 This result is consistent with literature, e.g. ([Omikrine-Metalssi et al., 2009](#)).

15 In the area defined by the pH front, the profiles determined for the sheltered condition are up  
16 that for the unsheltered one. This suggests that unsheltered conditions, which strongly reduce  
17 the carbonation rate, also decrease the bound  $\text{CO}_2$  content. The result, which corresponds to  
18 that of Houst and Wittmann ([Houst et al., 2002](#)), is not consistent with other studies which  
19 report that, due to high humidity, unsheltered conditions slightly increase the bound  $\text{CO}_2$   
20 content ([Galan et al., 2010](#); [Andrade et al., 2018](#)). This result is discussed in section 4.1.

21 Ref III and S 75 exhibit maximum bound  $\text{CO}_2$  contents that are about two times lower than  
22 that of the other concretes, despite their higher carbonation depths. Moreover, these two  
23 concretes bound more  $\text{CO}_2$  in depth than in surface, although the binder content is higher in  
24 the specimen skin. This could be explained by the fact that these concretes, especially Ref III,  
25 are poorly hydrated in surface due to a too early demolding, as shown by numerical

1 computations in a previous study (Younsi et al., 2019). Anhydrous phases are less  
 2 carbonatable than hydrates (Boumaaza et al., 2020b).

3



4

1 **Fig. 5.** Profiles of bound CO<sub>2</sub> content per mass of binder after 10-year natural carbonation.  
2 Dash lines and colored areas indicate the locations of carbonation fronts determined by means  
3 of phenolphthalein spraying and the variation ranges of these fronts, respectively (blue for  
4 unsheltered conditions and orange for sheltered).

5

### 6 3.4. CO<sub>2</sub> uptake

7

8 The CO<sub>2</sub> uptake was assessed from the profiles of bound CO<sub>2</sub> content following the steps.  
9 First, the content of bound CO<sub>2</sub> at a distance r from the core was expressed by volume of  
10 concrete [kg<sub>CO<sub>2</sub></sub>/m<sup>3</sup>]:

11

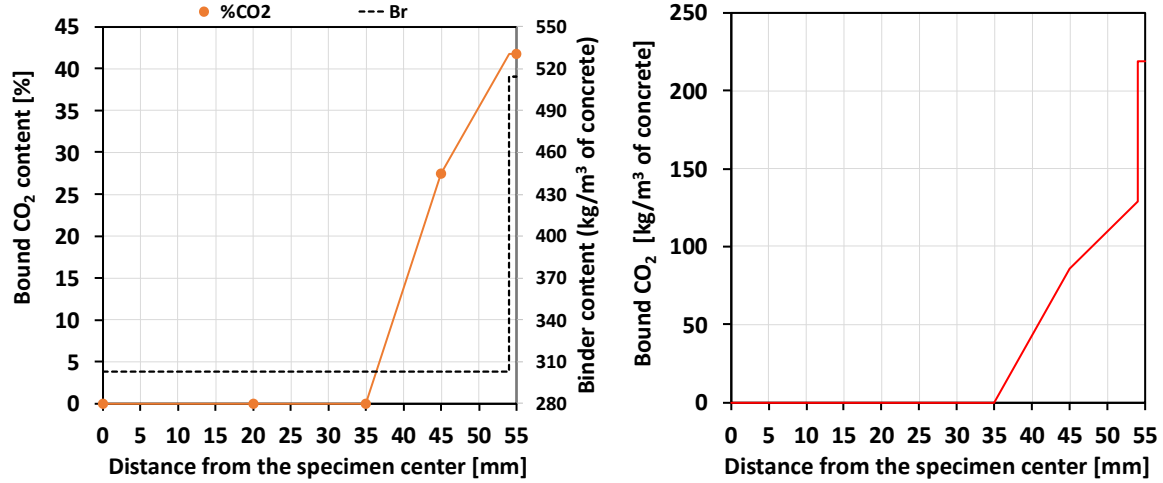
$$(CO_2)_r = B_r (\%CO_2)_r / 100 \quad (10)$$

12

13 where: (%CO<sub>2</sub>)<sub>r</sub> [%] is the bound CO<sub>2</sub> content at r expressed by mass of binder.  
14 B<sub>r</sub> [kg<sub>binder</sub>/m<sup>3</sup>] is the binder content at r expressed by volume of concrete.

15 At the first 4 distances from the core, i.e., 0, (15 – 20), (20 – 35) and (35 – 45) mm, B<sub>r</sub> was  
16 assumed to be equal to the binder content of the concrete mixture (Table 2). At 55 mm, B<sub>r</sub> was  
17 calculated from this binder content multiplied by the ratio between the binder content  
18 determined in the skin and that determined at the other distances. This ratio, deduced from the  
19 profiles shown in Fig. 5, accounts for the fact that in the specimen skin, the binder content is  
20 higher due to the “skin-effect”, which leads to a surface layer richer in binder (Kreijger,  
21 1984). Moreover, as the skin was sampled to a depth of about 1 mm, both (%CO<sub>2</sub>)<sub>r</sub> and B<sub>r</sub>  
22 were assumed to be constant between 54 and 55 mm. Examples of profiles of (%CO<sub>2</sub>)<sub>r</sub>, B<sub>r</sub>  
23 and (CO<sub>2</sub>)<sub>r</sub> obtained for Ref I under sheltered conditions are given in Fig. 8.

24



**Fig. 6.** Profiles of bound CO<sub>2</sub> content  $(\%CO_2)_r$  expressed by mass of binder and binder content  $B_r$  expressed by volume of concrete (left), and profile of bound CO<sub>2</sub> content  $(CO_2)_r$  expressed by volume of concrete (right): example of Ref I under sheltered conditions.

Second, the CO<sub>2</sub> binding capacity (CBC) of the carbonated zone revealed by phenolphthalein, expressed in  $kg_{CO_2}/m^3$ , was assessed by integration of the profile of  $(CO_2)_r$ :

$$CBC = \frac{2}{R^2} \int_{R-X_c}^R (CO_2)_r \, r \, dr \quad (11)$$

Table 4 gives the obtained value of CBC for each concrete. It should be noted that this value is an average CO<sub>2</sub> binding capacity of the carbonated zone, since the bound CO<sub>2</sub> is not necessarily uniform within this zone, as shown in Fig. 7. CBC as calculated is proposed because the depth  $X_c$  revealed by the pH indicator is usually the reference carbonation depth. It is also a comparison tool with the results of models such as that of standard EN 16757. Whatever the exposure condition, two sets of concretes can be distinguished: a set of

1 concretes with high CBC corresponding to concretes with binders of clinker content higher  
 2 than 70%, i.e., Ref I, Ref II, FA 30 and S 30, and a set with lower CBC (up to two times  
 3 lower), corresponding to concretes with clinker contents lower than 30%, i.e., Ref III and S  
 4 75.

5

6 In the third step, we determine the CO<sub>2</sub> uptake of the specimen expressed by exposure area  
 7 by integrating the profile of (CO<sub>2</sub>)<sub>r</sub>:

8

$$\text{Uptake} = \frac{1}{R} \int_0^R (\text{CO}_2)_r \, r \, dr \quad (12)$$

9

10 Table 4 gives for each concrete the value of uptake, which quantifies the CO<sub>2</sub> bound by the  
 11 cylindrical specimen after 10 years of exposure. The CO<sub>2</sub> uptake is at least 3 times higher in  
 12 sheltered conditions than in unsheltered ones. For a given exposure, the differences in uptake  
 13 between the studied concretes are rather low, especially for the unsheltered conditions.

14

15 **Table 4**

16 CO<sub>2</sub> binding capacity (CBC) of the carbonated zone revealed by phenolphthalein [kgCO<sub>2</sub>/m<sup>3</sup>]  
 17 and CO<sub>2</sub> uptake [kgCO<sub>2</sub>/m<sup>2</sup>] determined from the profiles of bound CO<sub>2</sub> content.

	Sheltered conditions						Unsheltered conditions					
	Ref I	Ref II	Ref III	FA 30	S 30	S 75	Ref I	Ref II	Ref III	FA 30	S 30	S 75
CBC	107	81	57	115	79	47	103	70	42	79	57	41
Uptake	1.47	1.74	1.46	1.79	1.47	1.08	0.46	0.49	0.56	0.50	0.32	0.30

18

19 **4. Discussion**

20



1 *4.1. Degree of carbonation*

2 The degree of carbonation (DoC) is defined as the ratio between the bound CO<sub>2</sub> content  
3 (%CO<sub>2</sub>) and the theoretical maximum bound CO<sub>2</sub> content (U<sub>B</sub>):

4

$$\text{DoC} = \frac{\%CO_2}{U_B} \quad (13)$$

5

6 U<sub>B</sub> can be assessed using Equation (14) assuming that all calcium oxides of the binder are  
7 converted by carbonation into CaCO<sub>3</sub>, except CaO reacting with SO<sub>3</sub> (Boumaaza et al.,  
8 2020b; Steinour, 1959):

9

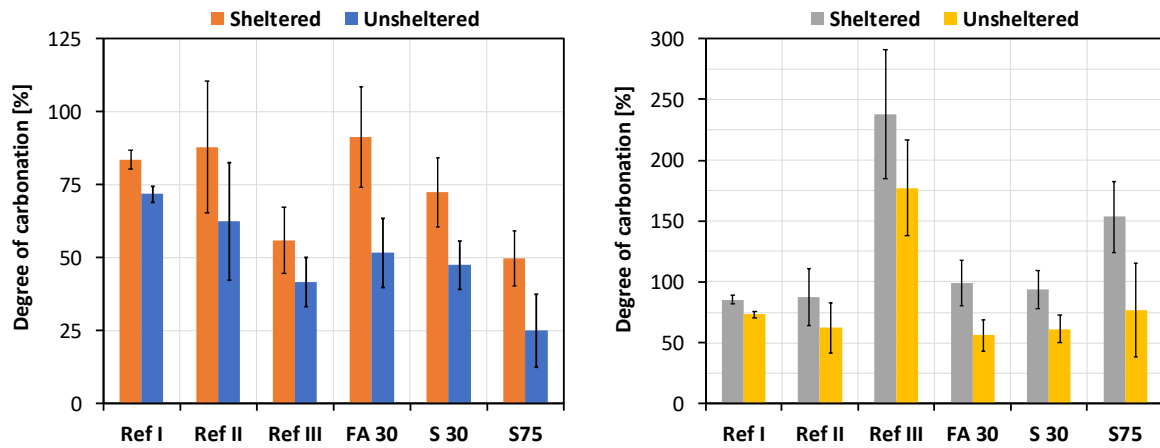
$$U_B = \%CaO_B \cdot \frac{M_{CO_2}}{M_{CaO}} - \%SO_3 \cdot \frac{M_{CO_2}}{M_{SO_3}} \quad (14)$$

10

11 Where: M<sub>CO<sub>2</sub></sub>, M<sub>CaO</sub> and M<sub>SO<sub>3</sub></sub> [g/mol] are the molar masses of CO<sub>2</sub>, CaO and SO<sub>3</sub>,  
12 respectively, %SO<sub>3</sub> the SO<sub>3</sub> content in the binder [%] provided by binder producers and  
13 determined by XRF analysis (Table 1).

14 The highest degree of carbonation was calculated for each concrete and each exposure from  
15 the profile of bound CO<sub>2</sub> content (Figure 7-left). Note that the highest DoC are in the  
16 specimen skin, except for the mixtures with high content of GGBFS (Ref III and S 75). As  
17 shown in section 3.3, the latter tend to be more carbonated in depth than in surface, especially  
18 in unsheltered condition. Two parameters controlling DoC can be discussed: exposure and  
19 nature of binder.

20

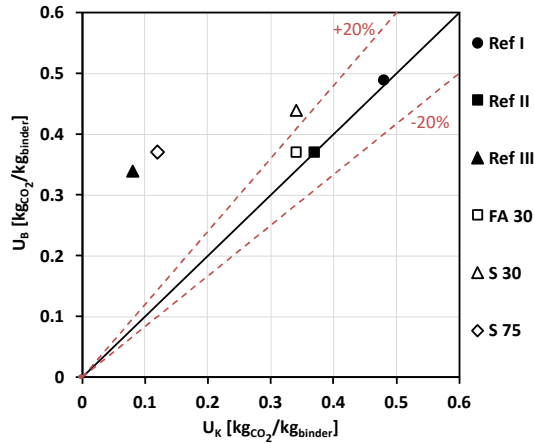


**Fig. 7.** The highest degrees of carbonation from the profiles of bound CO<sub>2</sub> content, calculated with the maximum bound CO<sub>2</sub> content considering carbonation of all CaO from binder (left) and with the maximum bound CO<sub>2</sub> content considering carbonation of CaO from the clinker only, as proposed by Standard EN1657 (right).

With respect to the effect of exposure conditions, DoC is found higher for sheltered specimens than for unsheltered ones. This result is a bit surprising since, in most of literature data, the degree of carbonation increases in the most wet conditions (Andrade, 2020; Andrade et al., 2018; Galan et al., 2010). This is usually explained by the fact that increasing the water saturation degree also increases the amount of available compounds for carbonation, since the carbonation reactions take place in the pore solution. As shown by (Boumaaza et al., 2020b; Steiner et al., 2020), ultimate DoC of hydrates depends strongly on the relative humidity. In our study, several reasons can be given to explain the lower degrees of carbonation in unsheltered conditions. First, it can be due to the sampling of powder at the specimen surface, especially in the case of Ref I, Ref II, FA 30 and S 30. The specimen skin not protected from rain was slightly degraded, probably due to leaching. It is therefore more difficult to have a precise determination of DoC at the specimen surface. It should be kept in mind that the carbonation depths determined for most of unsheltered specimens were low (around 5 mm)

1 and the profiles of bound CO<sub>2</sub> content rather sharp. Second, the oceanic climate of La  
2 Rochelle (France) is windy. Rapid and frequent drying due to sunshine and wind, followed by  
3 relatively short but heavy rainfall periods, could reduce the water content within the  
4 carbonated zone, which could slightly hamper the carbonation reactions. The water content  
5 however remains enough for slowing down the progress of the carbonation front. Under  
6 sheltered conditions, with an acceptable relative humidity of the environment, the concrete  
7 pore network remains partially saturated, perhaps even in equilibrium, which favors the  
8 carbonation reactions (Houst et al., 2002; Leeman et al., 2015; Ekolu, 2016). Third, the  
9 average temperatures of both exposure sites were not the same. The average temperature for  
10 the sheltered specimens was about 5°C higher and the temperature range narrower (Table 3).  
11 Although the influence of temperature on carbonation is difficult to understand because of  
12 contradictory effects on the involved mechanisms, it is recognized that carbonation rate  
13 increases when temperature increases, e.g., (Drouet et al., 2019). Finally, both exposure  
14 conditions used in the present study could lead to substantially equal degrees of carbonation.  
15 By way of comparison, note that Standard EN 16575 proposes close DoC values for the two  
16 types of exposure, i.e., 75% for sheltered condition and 80% for unsheltered one.  
17 The nature of binder is also a parameter which has a huge effect on the degree of carbonation.  
18 It clearly appears that concretes with a high substitution of clinker by GGBFS, i.e., Ref III and  
19 S 75, have much lower DoC, as defined by Equation 13, despite their higher carbonation  
20 depths. There is no relationship between the carbonation depth, determined by means of a pH  
21 indicator, and the degree of carbonation (Omikrine-Metalssi et al., 2009; Andrade, 2020).  
22 Ref III and S 75 exhibit the lowest average bound CO<sub>2</sub> contents although their CaO contents  
23 are close to those of FA 30 and Ref I, respectively (Table 2). To better understand this  
24 tendency, the degrees of carbonation were also calculated assuming that only calcium oxide  
25 from clinker can be carbonated. This approach is proposed by EN 16757, i.e., U<sub>B</sub> is taken

1 equal to  $U_K$ . Fig. 8 shows the difference between  $U_K$  from EN 16757 and  $U_B$  calculated with  
 2 the entire CaO content of the binder (Eq. 14). The highest differences are for mixtures with  
 3 GGBFS. In the case of mixtures with fly ash, i.e., Ref II and FA 30,  $U_K$  and  $\%CO_2max$  are  
 4 almost equal because of the very low CaO content of fly ash.  
 5



6  
 7  
 8 **Fig. 8.** Maximum theoretical bound CO<sub>2</sub> content as per the definition of this study ( $U_B$ ) *versus*  
 9 values obtained using EN 16757 ( $U_K$ ).

10  
 11 In [Figure 7 \(right\)](#), the degrees of carbonation so obtained for the mixtures with GGBFS are  
 12 much higher, and even higher than 100% (i.e., losing the physical sense of this parameter), as  
 13 shown by Andrade ([Andrade, 2020](#)). This result highlights that a part of the calcium oxides  
 14 supplied by GGBFS contributes to the uptake of CO<sub>2</sub>. To assess the degree of carbonation of  
 15 the calcium oxide from slag, the global DoC, as defined previously in Equation 13, was  
 16 rewritten as follows:

17

$$18 \quad DoC = 100 \frac{\%CO_2}{U_B} = 100 \frac{U_K \cdot DoC_K \cdot \%K + U_S \cdot DoC_S \cdot \%S}{U_B} \quad (15)$$

1 Where:  $U_i$  is the maximal content of  $\text{CO}_2$  bound by  $\text{CaO}$  of the constituent  $i$ ,  $\text{DoC}_i$  is the  
2 degree of carbonation of the constituent  $i$ , and  $\%i$  is the content of  $i$  in the binder.  $K$  and  $S$   
3 denote clinker and slag, respectively.  $U_i$  is calculated with the  $\text{CaO}$  content in the constituent  
4  $i$ , (Equation 14).

5 In Equation 15, all parameters, except  $\text{DoC}_S$ , are known if we assume that  $\text{DoC}_K$  is equal to  
6 the degree of carbonation found for Ref I, i.e., the mixture made with a Portland cement.  
7 Calculated values of  $\text{DoC}_S$  are given in Table 5. These values are only rough estimations due  
8 to the high standard deviations obtained for  $\text{DoC}$ . These orders of magnitude show that the  
9 degree of carbonation of  $\text{CaO}$  from slag is much lower than that of  $\text{CaO}$  from clinker, but not  
10 negligible, except in unsheltered conditions. Our estimations confirm recent results of (Saillo  
11 et al, 2021) obtained from an in-depth study of the mineral changes in cement pastes due to  
12 carbonation. The authors show that calcium from slag is less carbonatable than that of clinker.  
13 Moreover, a large amount of slag can remain unreacted even after a long-term water curing. In  
14 our case, the specimens were removed from the mold after 1 day and exposed to drying, what  
15 strongly disadvantages hydration (Younsi et al., 2019). From our data, it remains however  
16 difficult to propose a single empirical value to predict the degree of carbonation of slag.  
17 Moreover, the combination of  $\text{CO}_2$  with the cementitious elements is undoubtedly more  
18 complex than a simple separation of the binding capacity of  $\text{CaO}$  as a function of the  
19 constituent origin as proposed by Equation 15. The mineral assemblages of Portland cement  
20 and that of binders with GGBFS are quite different. GGBFS promotes calcium silicate  
21 hydrate (C-S-H) with lower  $\text{Ca/Si}$  ratio than that of Portland cement. Through experimental  
22 observations, (Steiner et al., 2020) confirms that the carbonation rate and the  $\text{CO}_2$  binding  
23 capacity of C-S-H decreases with the  $\text{Ca/Si}$  ratio.

24

25 **Table 5**

- 1 Calculated degrees of carbonation: degree as defined in Eq. 15 (DoC), degree of CaO from
- 2 Ref I binder (DoC<sub>K</sub>) and degree of CaO from slag (DoC<sub>S</sub>).

	Sheltered conditions			Unsheltered conditions		
	S 30	Ref III	S 75	S 30	Ref III	S 75
DoC (%)	72	56	50	47	42	25
DoC <sub>K</sub> (%)	83	83	83	72	72	72
DoC <sub>S</sub> (%)	31	48	32	~0	40	~0

3

#### 4 4.2. CO<sub>2</sub> uptake

5

6 To analyze the CO<sub>2</sub> uptake of the studied specimens, the results obtained for mixture Ref I

7 made with the high clinker content are used as reference values for comparison. The relative

8 differences in CBC, X<sub>c</sub> and CO<sub>2</sub> uptake are given in Figure 9. There is no clear correlation

9 between the CO<sub>2</sub> binding capacity of the material and the CO<sub>2</sub> uptake of the specimen. For

10 instance, Ref III has high relative differences in CBC (-50%) but CO<sub>2</sub> uptakes rather close to

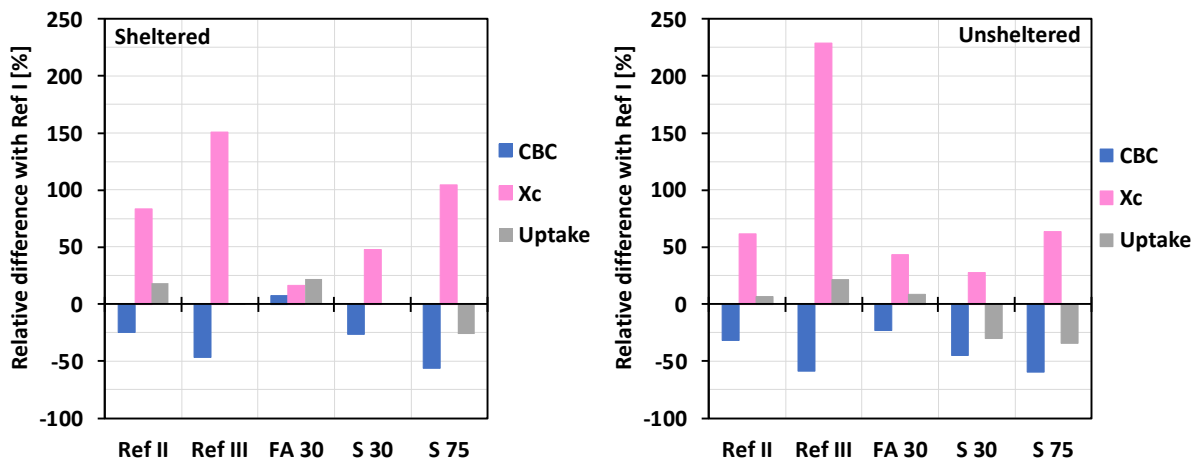
11 the uptake of Ref I (relative differences lower than 20%). In fact, as shown also in Figure 9,

12 the relative differences in carbonation depth of Ref III are very high. For this concrete, the

13 high carbonation depths partly compensate the lower binding capacity. A similar analysis can

14 be made for Ref II, FA 30, S 30 and S 75.

15

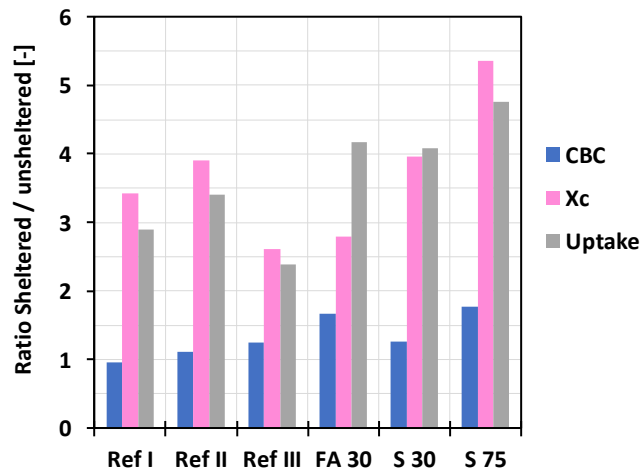


16

1 **Fig. 9.** Relative differences in CO<sub>2</sub> binding capacity (CBC), carbonation depth (X<sub>c</sub>) and CO<sub>2</sub>  
 2 uptake between Ref I and other studied concretes, for sheltered (left) and unsheltered (right)  
 3 exposure conditions after 10 years of natural carbonation.

4  
 5 To highlight the effect of exposure, the results from experiments are presented differently in  
 6 Figure 10. The latter gives the ratios of values for sheltered conditions and values for  
 7 unsheltered ones. These ratios are between 1 and 1.8 for CO<sub>2</sub> binding capacity while they are  
 8 much higher for carbonation depth and CO<sub>2</sub> uptake. This means that CBC is much less  
 9 impacted by the exposure for all studied materials, than X<sub>c</sub> and CO<sub>2</sub> uptake. Once again, the  
 10 role of X<sub>c</sub> is decisive for the CO<sub>2</sub> uptake at the specimen scale.

11



12  
 13 **Fig. 10.** Effect of exposure conditions on CO<sub>2</sub> binding capacity (CBC), carbonation depth  
 14 (X<sub>c</sub>) and CO<sub>2</sub> uptake: ratios of values for sheltered conditions and values for unsheltered ones.

15

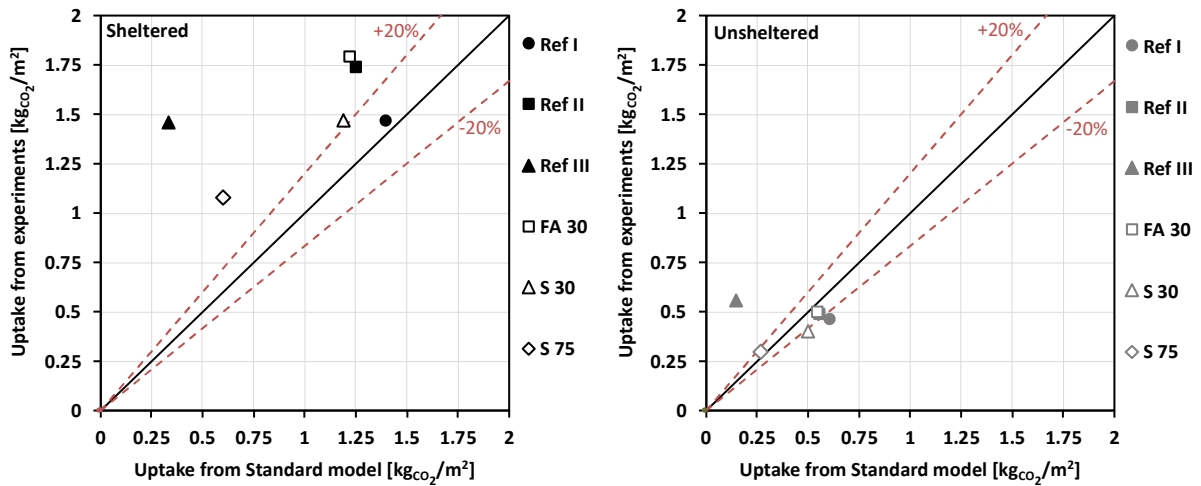
16 *4.3. Comparison with prediction of EN 16757 model*

17

18 Figure 11 compares the CO<sub>2</sub> uptakes obtained experimentally and values calculated using the  
 19 Standard EN 16757 model. The latter underestimates the uptake in sheltered conditions with

1 errors of at least 20% for most of concretes. The prediction is good only for Portland cement-  
 2 based concrete, i.e., Ref I. The predictions are better for unsheltered concretes with errors  
 3 lower than 20%, apart for Ref III whose predicted uptake is 3 times lower than that from  
 4 experiments. To understand the differences between experimental and computed values,  
 5 analysis can be made as previously, i.e., in terms of CBC and  $X_c$ .

6



7

8

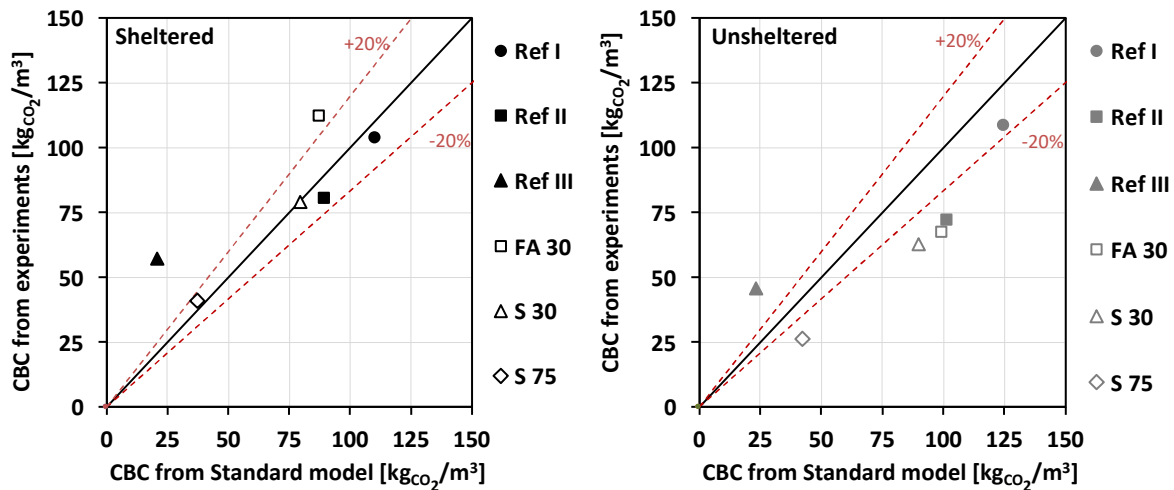
9 **Fig. 11.** CO<sub>2</sub> uptakes calculated from experimental data *versus* values calculated as per  
 10 EN 16757: sheltered (left) and unsheltered conditions (right).

11

12 Figure 12 shows that the standard model tends to overestimate the binding capacities of  
 13 concrete for unsheltered conditions, except for Ref III. The wrong estimation of CBC results  
 14 from errors in degree of carbonation (DoC) and theoretical bound CO<sub>2</sub> content ( $U_B$ ). In the  
 15 case of concrete with high clinker content (Ref I, Ref II, FA 30 and S 30), the latter is  
 16 correctly computed by the model, because  $U_B$  is equal to  $U_K$  (Fig. 8). Thus, the main error  
 17 comes from DoC which is significantly lower from experiments than from the model (see  
 18 section 4.1). In the case of Ref III, both DoC and  $U_B$  used by the model are not correct.  
 19 Standard DoC (75 or 80%) is higher than experimental DoC (around 50%) and  $U_B$  is taken



1 equal to  $U_K$  considering that only calcium oxides from clinker can be carbonated, while, as  
 2 shown previously, a part of CaO from slag also binds  $CO_2$ . However, the overestimation of  
 3 DoC compensates partly the underestimation of  $U_B$ . Globally, the differences in CBC between  
 4 experiments and model for Ref III are lower than the differences in  $CO_2$  uptake.  
 5



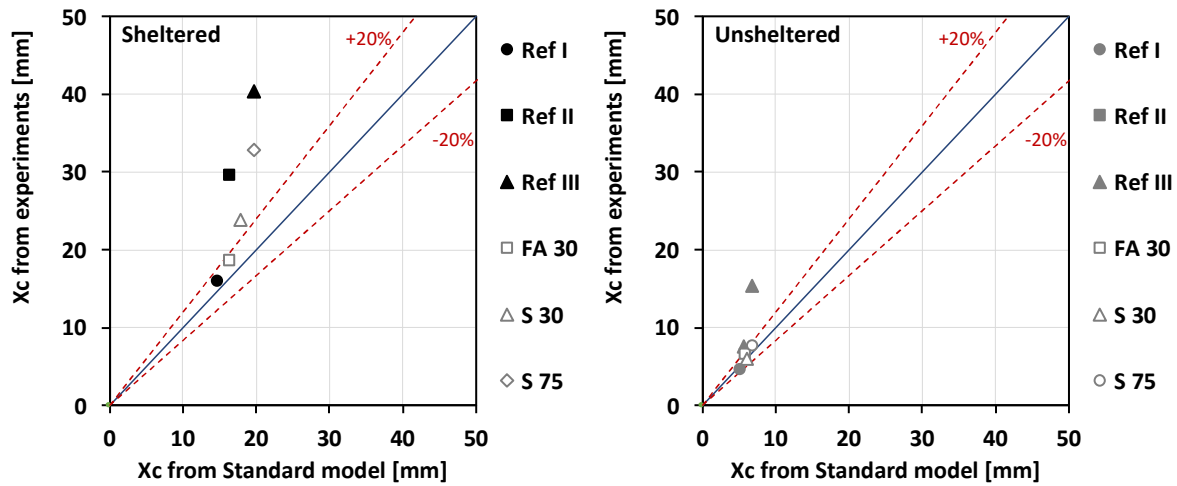
6  
 7  
 8 **Fig. 12.** CBC from experiments *versus* values calculated as per EN 16757: sheltered  
 9 conditions (left) and unsheltered conditions (right).

10  
 11 As revealed by Figure 13, lot of the difference between experimental and computed values  
 12 come from the underestimation of the carbonation depth by the model. Especially, for  
 13 sheltered conditions, the model error is high for most of concretes. Prediction is good only for  
 14 the Portland cement concrete. The model accuracy is better for the unsheltered conditions,  
 15 apart for Ref III.

16 Finally, these analyses show that efforts to improve predictions of  $CO_2$  uptake should focus  
 17 primarily on the carbonation rate, which is not predicted with sufficient accuracy for  
 18 concretes with low clinker content. As suggested by Andrade (Andrade, 2020), adjustments  
 19 per country for the carbonation rate should be proposed because of the diversity of cements

1 used and exposure conditions. Another solution could be the extrapolation of the carbonation  
 2 rate from results of accelerated carbonation tests, as proposed in models for service life  
 3 design, e.g. (fib, 2006).

4



5

6

7 **Fig. 13.** Carbonation depths from experiments *versus* values as per EN 16757: sheltered  
 8 conditions (left) and unsheltered conditions (right).

9

## 10 5. Conclusions

11

12 An experimental study of CO<sub>2</sub> uptake after 10 years natural carbonation was carried out on  
 13 concretes designed with Portland cement (OPC), blended cements containing fly ash (FA) or  
 14 ground granulated blast furnace slag (GGBFS) and partial substitutions of OPC with FA  
 15 (30 %) or GGBFS (30 and 75 %). These concretes were designed to have equivalent strengths  
 16 at early age and 28 days. 1 day after casting, concrete cylinders were subjected to a 10-year  
 17 natural carbonation, under sheltered and unsheltered conditions. The CO<sub>2</sub> uptake, i.e., the  
 18 bound CO<sub>2</sub> content per m<sup>2</sup> of exposed surface, was determined from profiles of bound CO<sub>2</sub>  
 19 obtained by TGA and chemical analyses. The main conclusions are the following.

- 1 • 10-year natural carbonation monitoring shows that the concretes with cement substitution  
2 with fly ash or GGBFS have carbonation depths close to those of concretes with blended  
3 cements containing the same additions. Thus, their potential durability is at least  
4 equivalent to that of the latter. This confirms prediction from previous studies based on  
5 accelerated carbonation tests.
- 6 • The concretes kept in sheltered conditions have higher CO<sub>2</sub> uptake than in unsheltered  
7 conditions. In sheltered conditions, the CO<sub>2</sub> uptake was between 1.1 and 1.8 kg/m<sup>2</sup> ( of  
8 exposure area) while in unsheltered ones it was between 0.3 and 0.6 kg/m<sup>2</sup>, depending on  
9 the concrete mixture. This is mainly due to the deeper ingress of CO<sub>2</sub> when concrete is  
10 sheltered from rain and remains under more stable moisture conditions.
- 11 • The CO<sub>2</sub> binding capacity, i.e., the bound CO<sub>2</sub> content in the carbonated depth, was found  
12 lower in the rainy conditions than in the sheltered one, what was somewhat unexpected  
13 with respect to literature. This tendency could be due to differences in parameters such as  
14 temperature or drying rate between both exposure conditions. The following conclusions  
15 are the same whatever the exposure conditions.
- 16 • CO<sub>2</sub> binding for concretes with high content of GGBFS consumes calcium oxides from  
17 both clinker and GGBFS. However, the degree of carbonation of CaO from GGBFS is  
18 much lower than the degree of carbonation of CaO from clinker. The low Ca/Si ratio of C-  
19 S-H produced by hydration of GGBFS and poor hydration degree of GGBFS could  
20 explain this finding. As a result, the CO<sub>2</sub> binding capacity is up to two times lower for the  
21 concretes with high content of GGBFS than for the other studied concretes.
- 22 • No correlation was found between the CO<sub>2</sub> binding capacity of the material and the CO<sub>2</sub>  
23 uptake of the specimen. Concretes with the lowest CO<sub>2</sub> binding capacity have also the  
24 highest carbonation depth. Since the CO<sub>2</sub> uptake can be assessed as the product of the CO<sub>2</sub>  
25 binding capacity and the carbonation depth determined from pH change (accounting for

1 the structure geometry), a low CO<sub>2</sub> binding capacity can be partly compensated by a high  
2 carbonation depth.

- 3 • The model from the Annex BB of the European Standard EN 16757 underestimates the  
4 CO<sub>2</sub> uptakes, especially for concretes under sheltered conditions and concretes with high  
5 content of GGBFS. The predictions were found correct mainly for the OPC concrete. The  
6 wrong estimation of the CO<sub>2</sub> uptake comes from wrong estimation of the CO<sub>2</sub> binding  
7 capacity but, above all, from misestimation of the carbonation depth.

8 Based on these results, some adjustments of the European Standard EN 16757 could be  
9 proposed to better assess the CO<sub>2</sub> uptake, especially for concretes with high GGBFS content.

10 In terms of carbonation rate, the adjustment factors defined by the standard to account for the  
11 effect of mineral additions should be increased. In the design phase of a project, the  
12 carbonation rate could be deduced from accelerated carbonation test, rather than assessed  
13 from tabulated values. In terms of CO<sub>2</sub> binding capacity of concrete with high GGBFS  
14 content, two approaches could be suggested. First, the CO<sub>2</sub> binding capacity can be calculated  
15 considering only CaO from clinker and high degree of carbonation, as proposed in the present  
16 model. This approach leads to an underestimation of the binding capacity, which could be  
17 viewed as a “safety approach”. Second, the CO<sub>2</sub> binding capacity could be calculated more  
18 realistically considering all the CaO from the binder, but with degree of carbonation at least  
19 two times lower than that proposed currently. Further in-deep research is needed to better  
20 define the degree of natural carbonation of hydrates produced by GGBFS.

21 Also, for a better representativeness, this study should be extended to concretes from old  
22 real structures but including different types of binders.

23  
24 **CRedit authorship contribution statement**

1       **Akli Younsi:** Conceptualization, Methodology, Validation, Investigation, Resources,  
2 Writing - Original Draft, Writing - Review & Editing, Visualization, Supervision. **Philippe**  
3 **Turcry:** Conceptualization, Methodology, Validation, Investigation, Resources, Writing -  
4 Review & Editing, Visualization. **Abdelkarim Aït-Mokhtar:** Validation, Resources, Writing  
5 - Review & Editing, Visualization.

6

## 7 **Declaration of Competing Interest**

8

9       The authors declare that they have no known competing financial interests or personal  
10 relationships that could have appeared to influence the work reported in this paper.

11

## 12 **Acknowledgments**

13

14       The authors would like to acknowledge the French National Federation of Public Works  
15 (FNTP) for funding the carbonation characterization by TGA/ICP-AES, the French National  
16 Research Agency (ANR) for funding the *EcoBéton* project during which the concrete  
17 mixtures studied were designed, and Carine Churlaud (La Rochelle University, LIENSs UMR  
18 CNRS 7266) for the chemical analyzes ICP-AES. The authors would like also to  
19 acknowledge Emmanuel Rozière (GeM, UMR CNRS 6183, Ecole Centrale Nantes) for  
20 supplying a sample of sand.

21

22

## 23 **Appendix – Calculation of the time-evolution of the carbonation depth in cylindrical** 24 **geometry**

25

1 First, let us recall how we obtain the time-evolution of the carbonation depth in axial  
2 geometry (i.e., the “classic” square-root of time model).

3 Several assumptions were made:

- 4 - The main parameters, i.e., the gaseous CO<sub>2</sub> diffusion coefficient (D), the content of  
5 carbonatable compounds in concrete (n<sub>c</sub>) and the ambient concentration of CO<sub>2</sub> (C<sub>0</sub>),  
6 were assumed to be constant.
- 7 - The chemical reactions were assumed to be much faster than the gas diffusion. As a  
8 result, the carbonation front progresses only when all the carbonatable compounds at  
9 the front are consumed. The front separates two zones, a “completely” carbonated  
10 zone where CO<sub>2</sub> diffuses and, more in depth, a non-carbonated zone where the  
11 concentration of CO<sub>2</sub> is null.

12 In the carbonated zone, the Fick’s second law can be applied:

13

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2} \quad (\text{A.1})$$

14

15 Where: C is the concentration of gaseous CO<sub>2</sub> at time t and depth x.

16 Due to the second assumption, the time variation of the concentration of CO<sub>2</sub> is very small  
17 ( $\partial C/\partial t \approx 0$ ). Thus, the profile of C is a linear function of the depth x:

18

$$C = C_0 \left(1 - \frac{x}{x_c}\right) \quad (\text{A.2})$$

19

20 Where: x<sub>c</sub> is the carbonation depth.

21 At the carbonation front, the amount of CO<sub>2</sub> diffusing through a surface S during a time dt is  
22 consumed by the carbonatable compounds in an elementary volume dV = Sdx<sub>c</sub>:

1

$$-SD \frac{\partial C}{\partial x} dt = n_c dV \quad \Leftrightarrow \quad D \frac{C_0}{n_c} dt = x_c dx_c \quad (\text{A.3})$$

2

3 By integrating Equation (A.3), the time evolution of the carbonation depth can be written as:

4

$$X_c = \sqrt{\frac{2DC_0}{n_c}} \sqrt{t} \quad (\text{A.4})$$

5

6 In the case of a cylindrical geometry with a radial diffusion, the previous model cannot be

7 applied because the Fick's second law takes a different form:

8

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial r^2} + \frac{D}{r} \frac{\partial C}{\partial r} \quad (\text{A.5})$$

9

10 Where  $r$  is the radial location, so as  $r = R - x$ , with  $R$  is the radius of the cylinder.11 With the same assumption than previously (very small time-variations), the profile of  $\text{CO}_2$ 12 concentration as a function of  $x$  can be written as a function of the depth  $x$ :

13

$$C = C_0 \left( \frac{\ln(R - x) - \ln(R - x_c)}{\ln(R) - \ln(R - x_c)} \right) \quad (\text{A.6})$$

14

15 Then, from the equality of the diffusing and the consumed amounts of  $\text{CO}_2$ :

16

$$-SD \frac{\partial C}{\partial x} dt = n_c dV \quad \Leftrightarrow \quad D \frac{C_0}{n_c} dt = (R - x_c)(\ln(R) - \ln(R - x_c)) dx_c \quad (\text{A.7})$$

17

1 By integrating Equation (A.7), we establish the following relationship between carbonation  
 2 depth and time:

$$D \frac{C_0}{n_c} t = -\frac{X_c^2}{4} - \ln(R) \frac{X_c^2}{2} + \ln(R - X_c) \frac{(R - X_c)^2}{2} + R \ln(R) X_c + R \frac{X_c}{2} + \frac{R^2 \ln(R)}{4} \quad (\text{A.8})$$

4  
 5 Equation (A.8) can be solved numerically to determine  $X_c$  at a given time  $t$ . The left-hand side  
 6 parameter  $DC_0/n_c$  can be deduced from empirical models giving  $X_c$  as a function of the  
 7 square-root of time (axial geometry), such as the model from standard EN16575:

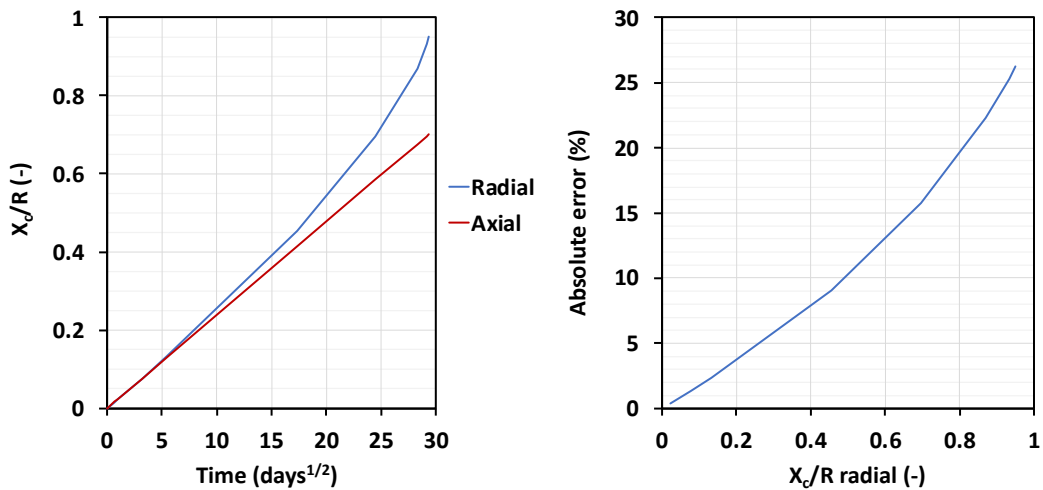
$$X_c = A\sqrt{t} \quad (\text{A.9})$$

9  
 10 From Equation (A.4),  $DC_0/n_c$  is thus equal to  $A^2/2$ .

11  
 12 Figure A.1 compares results obtained for both geometries, i.e., axial and cylindrical:  
 13 carbonation depths (related to the cylinder radius  $R$ ) as a function of time from Equation A.4  
 14 and A.8, respectively. These results were obtained for a cylinder of 55 mm in radius, a  $\text{CO}_2$   
 15 concentration of 500 ppm ( $2 \cdot 10^{-2} \text{ mol/m}^3$ ), a diffusion coefficient of  $5 \cdot 10^{-7} \text{ m}^2/\text{s}$  and a  
 16 concentration of carbonatable compounds of  $1000 \text{ mol/m}^3$ . The difference between values  
 17 from both geometries remains small when the carbonation depth  $X_c$  is lower than 40% of the  
 18 specimen radius, i.e., 22 mm for the present example. Beyond this ratio, the use of Equation  
 19 A.6 is necessary to calculate the time-evolution of  $X_c$  for a radial carbonation, instead of the  
 20 classical square-root of time model (with the same assumption than the latter, e.g., a constant  
 21  $DC_0/n_c$ ).

22





1  
2 **Fig. A.1.** Comparison of calculated values for axial and cylindrical geometries: ratio between  
3 carbonation depth and radius versus square root of time (left) and absolute error versus the  
4 ratio for the cylindrical geometry (right). Calculations were done using data given in the text.

5

## 6 **References**

7 Andersson, R., Fridh, K., Stripple, H., Häglund, M., 2013. Calculating CO<sub>2</sub> uptake for  
8 existing concrete structures during and after service life. *Environ. Sci. Technol.* 47, 11625–  
9 11633. <https://doi.org/10.1021/es401775w>.

10 Andersson, R., Stripple, H., Gustafsson, T., Ljungkrantz, C., 2019. Carbonation as a method  
11 to improve climate performance for cement-based material. *Cem. Concr. Res.* 124, 105819.  
12 <https://doi.org/10.1016/j.cemconres.2019.105819>.

13 Andrade, C., Sanjuán, M., 2018. Updating Carbon Storage Capacity of Spanish Cements.  
14 *Sustainability* 10. <https://doi.org/10.3390/su10124806>.

15 Andrade, C., 2020. Evaluation of the degree of carbonation of concretes in three  
16 environments. *Constr. Build. Mater.* 230. [https://doi-org.gutenberg.univ-](https://doi-org.gutenberg.univ-lr.fr/10.1016/j.conbuildmat.2019.116804)  
17 [lr.fr/10.1016/j.conbuildmat.2019.116804](https://doi-org.gutenberg.univ-lr.fr/10.1016/j.conbuildmat.2019.116804).

18 Andrew, R.M., 2019. Global CO<sub>2</sub> emissions from cement production, 1928–2018. *Earth Syst.*  
19 *Sci. Data.* 11, 1675–1710. <https://doi.org/10.5194/essd-11-1675-2019>.

1 Ashraf, W., 2016. Carbonation of cement-based materials: challenges and opportunities.  
2 *Constr. Build. Mater.* 120, 558–570. <https://doi.org/10.1016/j.conbuildmat.2016.05.080>.

3 Bordy, A., Younsi, A., Aggoun, S., Fiorio, B., 2017. Cement substitution by a recycled cement  
4 paste fine: role of the residual anhydrous clinker. *Constr. Build. Mater.* 132, 1–8.  
5 <https://doi.org/10.1016/j.conbuildmat.2016.11.080>.

6 Boumaaza, M., Turcry, Ph., Huet, B., Aït-Mokhtar, A., 2020. Influence of carbonation on the  
7 microstructure and the gas diffusivity of hardened cement pastes. *Constr. Build. Mater.* 253,  
8 119-227. <https://doi.org/10.1016/j.conbuildmat.2020.119227>.

9 Boumaaza, M., Huet, B., Turcry, Ph., Aït-Mokhtar, A., 2020. The CO<sub>2</sub>-binding capacity of  
10 synthetic anhydrous and hydrates: Validation of a test method based on the instantaneous  
11 reaction rate. *Cem. Concr. Res.* 135. <https://doi.org/10.1016/j.cemconres.2020.106113>.

12 Costa, F.N., Ribeiro, D.V., 2020. Reduction in CO<sub>2</sub> emissions during production of cement,  
13 with partial replacement of traditional raw materials by civil construction waste (CCW). *J.*  
14 *Clean. Prod.* 276, 123302. <https://doi.org/10.1016/j.jclepro.2020.123302>.

15 Drouet, E., Poyet, S., Le Bescop, P., Torrenti, J.M., Bourbon, X., 2019. Carbonation of  
16 hardened cement pastes: influence of temperature. *Cem. Concr. Res.*, 115, 445-459.

17 Ekolu, S.O., 2016. A review on effects of curing, sheltering, and CO<sub>2</sub> concentration upon  
18 natural carbonation of concrete. *Constr. Build. Mater.* 127, 306–320.

19 Elchalakani, M., Basarir, H., Karrech, A., 2017. Green concrete with high-volume fly ash and  
20 slag with recycled aggregate and recycled water to build future sustainable cities. *J. Mater.*  
21 *Civ. Eng.* 29. [https://doi.org/10.1061/\(asce\)mt.1943-5533.0001748](https://doi.org/10.1061/(asce)mt.1943-5533.0001748).

22 Esfahani, S.M.R.A., Zareei, S.A., Madhkhan, M., Ameri, F., Rashidiani, J., Taheri, R.A.,  
23 2021. Mechanical and gamma-ray shielding properties and environmental benefits of concrete  
24 incorporating GGBFS and copper slag. *J. Build. Eng.* 33, 101615.  
25 <https://doi.org/10.1016/j.job.2020.101615>.

1 Feiz, R., Ammenberg, J., Baas, L., Eklund, M., Helgstrand, A., Marshall R., 2015. Improving  
2 the CO<sub>2</sub> performance of cement, part I: utilizing life-cycle assessment and key performance  
3 indicators to assess development within the cement industry. *J. Clean. Prod.* 98, 272–281.  
4 <http://dx.doi.org/10.1016/j.jclepro.2014.01.083>.

5 Fitzpatrick, D., Richardson, M., Nolan, E., 2015. Sequestration of carbon dioxide by concrete  
6 infrastructure: a preliminary investigation in Ireland. *J. Sustain. Archit. Civ. Eng.* 1, 66–77.  
7 <https://doi.org/10.5755/j01.sace.10.1.8037>.

8 Flower, D.J.M., Sanjayan, J.G., 2007. Greenhouse gas emissions due to concrete manufacture.  
9 *Int. J. Life Cycle Assess.* 12, 282–288. <http://dx.doi.org/10.1007/s11367-007-0327-3>.

10 Galan, I., Andrade, C., Mora, P., Sanjuan, M.A., 2010. Sequestration of CO<sub>2</sub> by concrete  
11 carbonation. *Environ. Sci. Technol.* 44, 3181–3186. <https://doi.org/10.1021/es903581d>.

12 Gartner, E., Hirao, H., 2015. A review of alternative approaches to the reduction of CO<sub>2</sub>  
13 emissions associated with the manufacture of the binder phase in concrete. *Cem. Concr. Res.*  
14 78, 126–142. <http://dx.doi.org/10.1016/j.cemconres.2015.04.012>.

15 Houst, Y.F., Wittmann, F.H., 2002. Depth profiles of carbonates formed during natural  
16 carbonation. *Cem. Concr. Res.* 32, 1923–1930.

17 Huy Vu, Q., Pham, G., Chonier, A., Brouard, E., Rathnarajan, S., Pillai, R., Gettu, R.,  
18 Santhanam, M., Aguayo, F., Folliard, K.J., Thomas, M.D., Moffat, T., Shi, C., Sarnot, A.,  
19 2019. Impact of different climates on the resistance of concrete to natural carbonation. *Constr.*  
20 *Build. Mater.* 216, 450–467. <https://doi.org/10.1016/j.conbuildmat.2019.04.263>.

21 Jang, J.G., Kim, G.M., Kim, H.J., Lee, H.K., 2016. Review on recent advances in CO<sub>2</sub>  
22 utilization and sequestration technologies in cement-based materials. *Constr. Build. Mater.*  
23 127, 762–773. <https://doi-org.gutenberg.univ-lr.fr/10.1016/j.conbuildmat.2016.10.017>.

24 Kangni-Foli, E., Poyet, S., Le Bescop, P., Charpentier, T., Bernachy-Barbe, F., Dauzeres, A.,  
25 L'Hopital, E., d'Espinose de Lacaillerie, J.-B., 2021. Carbonation of model cement pastes:

1 The mineralogical origin of microstructural changes and shrinkage. *Cem. Concr. Res.* 144,  
2 106446. <https://doi.org/10.1016/j.cemconres.2021.106446>.

3 Khokhar, M.I., Roziere, E., Turcry, Ph., Grondin, F., Loukili, A., 2010. Mix design of concrete  
4 with high content of mineral additions: optimisation to improve early age strength. *Cem.*  
5 *Concr. Compos.* 32, 377–385. <http://dx.doi.org/10.1016/j.cemconcomp.2010.01.006>.

6 Kreijger, P.C., 1984. The skin of concrete composition and properties. *Mat. Constr.* 17, 275–  
7 283. <https://doi.org/10.1007/BF02479083>.

8 Kwon, S.-J., Wang, X.-Y., 2021. CO<sub>2</sub> uptake model of limestone-powder-blended concrete  
9 due to carbonation. *J. Build. Eng.* 38, 102176. <https://doi.org/10.1016/j.jobe.2021.102176>.

10 Lagerblad, B., 2005. Carbon dioxide uptake during concrete life cycle – State of the art.  
11 Swedish Cem. Concr. Res. Inst.

12 Lee, H., Wang, X., 2016. Evaluation of the carbon dioxide uptake of slag-blended concrete  
13 structures, considering the effect of carbonation. *Sustainability.* 8, 312–329.  
14 <https://doi.org/10.3390/su8040312>.

15 Leemann, A., Nygaard, P., Kaufmann, J., Loser, R., 2015. Relation between carbonation  
16 resistance, mix design and exposure of mortar and concrete. *Cem. Concr. Compos.* 62, 33–43.  
17 <https://doi.org/10.1016/j.cemconcomp.2015.04.020>.

18 Lim, T.H., Ellis, B.L., Skerlos, S.J., 2019. Mitigating CO<sub>2</sub> emissions of concrete  
19 manufacturing through CO<sub>2</sub>-enabled binder reduction. *Environ. Res. Lett.* 14, 114014.  
20 <https://doi.org/10.1088/1748-9326/ab466e>

21 Miller, S.A., Horvath, A., Monteiro, P.J.M., 2016. Readily implementable techniques can cut  
22 annual CO<sub>2</sub> emissions from the production of concrete by over 20%. *Environ. Res. Lett.* 11,  
23 074029. <https://doi.org/10.1088/1748-9326/11/7/074029>

24 fib, 2006. Model Code for Service Life Design, Bulletin No. 34.

25 Olivier, J.G.J., Janssens-Maenhout, G., Muntean, M., Peters, J.A.H.W., 2016. Trends in global

1 CO<sub>2</sub> emissions: 2016 report, PBL Netherlands Environmental Assessment Agency, European  
2 Commission, Joint Research Centre, <https://www.pbl.nl/en/publications/trends-in-global->  
3 [CO2-emissions-2016-report](https://www.pbl.nl/en/publications/trends-in-global-co2-emissions-2016-report).

4 Omikrine-Metalssi, O., Aït-Mokhtar, A., 2009. A proposed methodology for a quantitative  
5 investigation of carbonation in polymer-modified mortars. *Experimental Techniques*, 33, 59-  
6 65.

7 Otieno, M., Ikotun, J., Ballim, Y., 2020. Experimental investigations on the effect of concrete  
8 quality, exposure conditions and duration of initial moist curing on carbonation rate in  
9 concretes exposed to urban, inland environment. *Constr. Build. Mater.* 246, 118443.

10 Pade, C., Guimaraes, M., 2007. The CO<sub>2</sub> uptake of concrete in a 100-year perspective. *Cem.*  
11 *Concr. Res.* 37, 1348–1356. <https://doi.org/10.1016/j.cemconres.2007.06.009>.

12 Papadakis, V.G., Vayenas, C.G., Fardis, M.N., 1991. Fundamental modeling and experimental  
13 investigation of concrete carbonation. *ACI Materials Journal* 88, 363-373.

14 Possan, E., Felix, E., Thomaz, W., 2016. CO<sub>2</sub> uptake by carbonation of concrete during life  
15 cycle of building structures. *J. Build. Rehabil.* 1 -7. <https://doi.org/10.1007/s41024-016-0010->  
16 9.

17 Ren, C., Wang, W., Yao, Y., Wu, S., Qamar, Yao, X., 2020. Complementary use of industrial  
18 solid wastes to produce green materials and their role in CO<sub>2</sub> reduction. *J. Clean. Prod.* 252,  
19 119840. <https://doi.org/10.1016/j.jclepro.2019.119840>.

20 Saillio, M, Baroghel-Bouny, V, Pradelle, S., Bertin, M., Vincent, J., d’Espinose de Lacaillerie,  
21 J.B. Effect of supplementary cementitious materials on carbonation of cement pastes. *Cem.*  
22 *Concr. Res.* 142 (2021) 106358

23 Sanjuán, M., Estevez, E., Argiz, C., 2019. Carbon dioxide absorption by blast-furnace slag  
24 mortars in function of the curing intensity. *Energies* 2346.  
25 <https://doi.org/10.3390/en12122346>.

1 Sanjuán, M.A., Andrade, C., Mora, P., Zaragoza A., 2020. Carbon dioxide uptake by cement-  
2 based materials: A Spanish case study. *Appl. Sci.* 10, 339.  
3 <https://doi.org/10.3390/app10010339>.

4 EN 16757 Standard, 2017. Sustainability of construction works – Environmental product  
5 declaration – Product Category Rules for concrete and concrete elements.

6 EN 197-1 Standard, 2011. Cement – Part 01:00 Composition, specifications and conformity  
7 criteria for common cements.

8 EN 450-1 Standard 2012. Fly ash for concrete – Part 01:00 Definition, specifications and  
9 conformity criteria.

10 EN 15167-1 Standard, 2006. Ground granulated blast furnace slag for use in concrete, mortar  
11 and grout – Part 01:00 Definitions, specifications and conformity criteria.

12 EN 13139 Standard, 2003. Aggregates for mortar.

13 EN 934-2+A1 Standard, 2012. Admixtures for concrete, mortar and grout – Part 02:00  
14 Concrete admixtures – Definitions, requirements, conformity, marking and labelling.

15 EN 206/CN Standard, 2014. Concrete, specification, performance, production and conformity.

16 EN 12390-12 Standard, 2020. Testing hardened concrete – Part 12:00 Determination of the  
17 carbonation resistance of concrete – Accelerated carbonation method.

18 Steiner, S., Lothenbach, B., Proske, T., Borgschulte, A., Winnefeld, F., 2020. Effect of relative  
19 humidity on the carbonation rate of portlandite, calcium silicate hydrates and ettringite. *Cem.*  
20 *Concr. Res.* 135. <https://doi.org/10.1016/j.cemconres.2020.106116>.

21 Steinour, H.H., 1959. Some effects of carbon dioxide on mortars and concrete discussion. *J.*  
22 *Am. Concr. Inst.* 30, 905–907.

23 Thiery, M., Villain, G., Dangla, P., Platret, G., 2007. Investigation of the carbonation front  
24 shape on cementitious materials: effects of the chemical kinetics. *Cem. Concr. Res.* 37, 1047–  
25 1058. <https://doi.org/10.1016/j.cemconres.2007.04.002>.

1 Thiery, M., 2005. Modélisation de la carbonatation atmosphérique des matériaux cimentaires.  
2 Prise en compte des effets cinétiques et des modifications microstructurelles et hydriques,  
3 Ph.D. Thesis, LCPC Paris (in French).

4 Turcry, Ph., Oskri-Nelfia, L., Younsi, A., Aït-Mokhtar, A., 2014. Analysis of an accelerated  
5 carbonation test with severe preconditioning. *Cem. Concr. Res.* 57, 70–78.  
6 <https://doi.org/10.1016/j.cemconres.2014.01.003>.

7 Villain, G., Thiery, M., Platret, G., 2007. Measurement methods of carbonation profiles in  
8 concrete: thermogravimetry, chemical analysis and gammadensimetry. *Cem. Concr. Res.* 37,  
9 1182–1192. <https://doi.org/10.1016/j.cemconres.2007.04.015>.

10 Witkowski, H., Koniorczyk, M., 2020. The influence of pozzolanic additives on the  
11 carbonation rate and Life Cycle Inventory of concrete. *Constr. Build. Mater.* 254, 119301.  
12 <https://doi.org/10.1016/j.conbuildmat.2020.119301>.

13 Xi, F., Davis, S.J., Ciais, P., Crawford-Brown, D., Guan, D., Pade, C., Shi, T., Syddall, M., Lv,  
14 J., Ji, L., Bing, L., Wang, J., Wei, W., Yang, K.-H., Lagerblad, B., Galan, I., Andrade, C.,  
15 Zhang, Y., Liu, Z., 2016. Substantial global carbon uptake by cement carbonation. *Nat.*  
16 *Geosci.* 9, 880–883. <https://doi.org/10.1038/ngeo2840>.

17 Yang, K.-H., Seo, E.-A., Tae, S.-H., 2014. Carbonation and CO<sub>2</sub> uptake of concrete. *Environ.*  
18 *Impact Assess. Rev.* 46, 43–52. <https://doi.org/10.1016/j.eiar.2014.01.004>.

19 Yoon, I.-S., Çopuroglu, O., Park, K.-B., 2007. Effect of global climatic change on carbonation  
20 progress of concrete. *Atmos. Environ.* 41, 7274–7285.  
21 <https://doi.org/10.1016/j.atmosenv.2007.05.028>.

22 Younsi, A., Turcry, Ph., Rozière, E., Aït-Mokhtar, A., Loukili, A., 2011. Performance-based  
23 design and carbonation of concrete with high fly ash content. *Cem. Concr. Compos.* 33, 993–  
24 1000. <http://dx.doi.org/10.1016/j.cemconcomp.2011.07.005>.

25 Younsi, A., Turcry, Ph., Aït-Mokhtar, A., Staquet, S., 2013. Accelerated carbonation of

1 concrete with high content of mineral additions: effect of interactions between hydration and  
2 drying. *Cem. Concr. Res.* 43, 25–33. <https://doi.org/10.1016/j.cemconres.2012.10.008>.

3 Younsi, A., Turcry, Ph., Aït-Mokhtar, A., Staquet, S., 2019. Numerical study of the influence  
4 of drying on properties governing the carbonation mechanism of concretes with low clinker  
5 content. *Eur. J. Environ. Civ. Eng.* 23, 172–192.  
6 <https://doi.org/10.1080/19648189.2016.1271364>.

7 Younsi, A., Cherif, R., Trabelsi, A., Hamami, A.E.A., Belarbi, R., Aït-Mokhtar, A., 2021.  
8 Hydration-drying interactions in a high-volume ground granulated blast-furnace slag mortar.  
9 *Constr. Build. Mater.* 279, 122427. <https://doi.org/10.1016/j.conbuildmat.2021.122427>.

10 Younsi, A., Bordy, A., Aggoun, S., Fiorio, B., 2018. Hydration-drying interactions in OPC  
11 pastes blended with recycled OPC paste fine powder: critical curing relative humidity  
12 hampering hydration. *Constr. Build. Mater.* 90, 403–413.  
13 <https://doi.org/10.1016/j.conbuildmat.2018.09.132>