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# A database of flow and near pressure field signals obtained for subsonic and nearly ideally expanded supersonic free jets using large-eddy simulations

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(Updated on March 31, 2022)

The time signals obtained in the flow and near pressure fields of subsonic and nearly ideally expanded supersonic free jets computed by highly-resolved compressible large-eddy simulations (LES) using cylindrical coordinates  $(r, \theta, z)$  have been stored in a database. **They can be shared with other researchers, upon request by email**, to investigate, for instance, the development of turbulent structures and noise generation mechanisms in high-speed jets. The jet conditions (Mach and Reynolds numbers, temperature) and nozzle-exit boundary-layer characteristics (thickness, velocity profile, fluctuation level), the LES grid parameters and the recorded signals (nature and location of the variables stored, time duration and sampling frequency) are briefly described in this short note.

## I. Nozzle-exit jet flow conditions

### A. Isothermal jets at a Mach number of 0.9 at low and high Reynolds numbers

At first, two isothermal jets at a Mach number  $M = u_j/c_0 = 0.9$  at diameter-based Reynolds numbers  $Re_D = u_j D/\nu = 3125$  and  $Re_D = 10^5$  [1], where  $u_j$ ,  $D = 2r_0$ ,  $c_0$  and  $\nu$  are the jet nozzle-exit velocity and diameter, the speed of sound in the ambient medium and the kinematic molecular viscosity, have been simulated using LES. They are represented by a red diamond and a red bullet in figure 1. Their initial conditions are given in table 1. The parameters of the simulations and flow and noise properties of the jets are detailed in recent papers [2–6]. More results can also be found in references [7–9]. The mesh grid used for the LES of the two jets are referred to as CGz75a and FGz40 and are described in section II. The sets of files recorded in the two cases, named D2 and D0, are presented in section III. The recording times  $T$  are equal to  $5,000r_0/u_j$  and  $3,625r_0/u_j$ . The simulation of the high Reynolds number jet M09Re1e5TaLd0150v9 is ongoing.

### B. Low-Reynolds-number isothermal jets

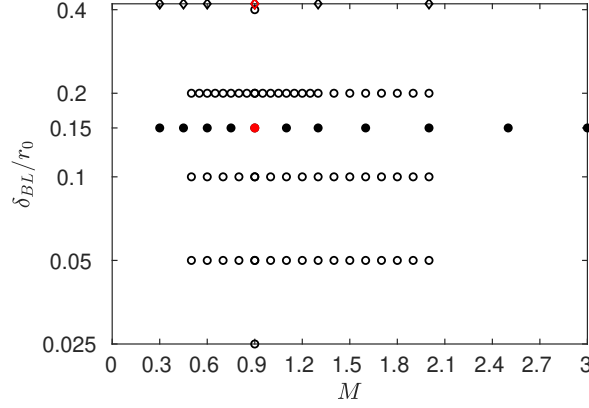
On the basis of the simulation of the low-Reynolds-number jet M09Re3125TaLd0420v1 at  $M = 0.9$  and  $Re_D = 3,125$ , isothermal jets also at  $Re_D = 3125$  but at  $M = 0.3, 0.45, 0.6, 1.3$  and  $2$ , with peak turbulence intensities at the nozzle exit of  $u'_e/u_j = 0.01$  for  $M \leq 1.3$  and  $0.025$  for  $M = 2$ , have been computed. They are collected in table 2, and represented by diamonds in figure 1. The simulations are ongoing for  $M = 0.3, 0.45$  and  $2$ .

### C. High-Reynolds-number isothermal jets with untripped boundary layers

Isothermal jets at a Reynolds number  $Re_D = 10^5$  with untripped boundary layers have been considered in order to investigate the flow and sound fields of initially fully laminar jets. They are represented by circles in figure 1. The simulations of such jets is cheaper than those of jets with tripped boundary layers, allowing us to perform parametric studies at a reasonable cost.

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**Fig. 1** Jets at  $\text{Re}_D = 10^5$  with  $\bullet$  tripped and  $\circ$  untripped boundary layers, and  $\diamond$  at  $\text{Re}_D = 3125$ : Mach number  $M$  and thickness  $\delta_{BL}$  of the Blasius profiles at the pipe-nozzle inlet;  $\diamond$  M09Re3125TaLd0420v1 and  $\bullet$  M09Re1e5TaLd0150v9.

### 1. Isothermal jets at a Mach number of 0.9 with different boundary-layers thicknesses

Isothermal jets at  $M = 0.9$  and  $\text{Re}_D = 10^5$  with untripped boundary layers of different thicknesses [10] between  $\delta_{BL} = 0.025r_0$  and  $\delta_{BL} = 0.4r_0$  have been computed by LES. They are defined in table 3. Results of the simulations are presented in several papers [2, 4–6].

### 2. Isothermal jets at Mach numbers between 0.5 and 2

Isothermal jets with untripped boundary-layers of thicknesses  $\delta_{BL} = 0.05r_0$ ,  $0.1r_0$  and  $0.2r_0$  at Mach numbers varying between 0.5 and 2 in increments of 0.05 or 0.1 have been computed. They are defined in table 4. Results of the simulations are presented in very recent papers [4, 5].

## D. High-Reynolds-number isothermal jets with tripped boundary-layers

Isothermal jets at  $\text{Re}_D = 10^5$  with tripped boundary-layers have been considered in order to investigate the flow and sound fields of initially highly disturbed jets. They are characterized by peak turbulence intensity  $u'_e/u_j$  typically of 9% at the nozzle exit.

### 1. Isothermal jets with nozzle-exit turbulence levels between 0 and 15%

Isothermal jets at  $M = 0.9$  and  $\text{Re}_D = 10^5$  with peak turbulence intensity at the nozzle exit of  $u'_e/u_j = 0, 3\%, 6\%, 9\%, 12\%$  and  $15\%$  have been computed to study the effects of the upstream turbulence levels [1, 11, 12]. They are defined in table 5.

### 2. Isothermal jets at Reynolds numbers between 12,500 and 400,000

Isothermal jets at  $M = 0.9$  with highly disturbed nozzle-exit boundary layers with  $u'_e/u_j \approx 9\%$  have been computed for Reynolds numbers  $\text{Re}_D$  varying between 12,500 and 400,000 [13] to examine the Reynolds number effects. They are presented in table 6.

### 3. Isothermal jets with different boundary-layer thicknesses

Isothermal jets at  $M = 0.9$  and  $\text{Re}_D \approx 50,000$  with highly disturbed boundary layers of different thicknesses between  $\delta_{BL} = 0.09r_0$  and  $0.42r_0$  have been computed [14]. They are reported in table 7. Results are available in a recent paper [15].

#### 4. Isothermal jets at Mach numbers between 0.3 and 3

On the basis of the simulation of the jet **M09Re1e5TaLd0150v9** at  $M = 0.9$  and  $Re_D = 100,000$  with  $u'_e/u_j = 9\%$ , isothermal jets also with  $Re_D = 100,000$  and  $u'_e/u_j = 9\%$  but at  $M = 0.3, 0.45, 0.6, 0.75, 1.1, 1.3, 1.6, 2, 2.5$  and  $3$  have been computed. They are collected in table 8, and are represented by bullets in figure 1. The parameters of the simulations and the flow and noise properties of the jets at  $M = 0.6, 0.75, 1.1, 1.3$  and  $2$  are presented in very recent papers [4–6]. The simulations are ongoing for all jets.

#### 5. Isothermal jets with non-laminar boundary-layer profiles

Isothermal jets at  $M = 0.9$  and  $Re_D = 50,000$  with highly disturbed boundary layers ( $u'_e/u_j = 6\%$  or  $9\%$ ) of different shapes (L: laminar Blasius profile; T1, T2 and T3: transitional and turbulent profiles) [16] have been computed. They are defined in table 9. The parameters of the simulations and the flow and noise properties of the jets are presented in references [15, 17].

#### 6. Hot jets at a Mach number of 0.9

Hot jets at a Mach number of  $M = 0.9$  and Reynolds numbers  $Re_D$  between 25,000 and 200,000 with highly disturbed boundary layers ( $u'_e/u_j = 9\%$ ) have been computed [18, 19]. Their nozzle-exit static temperatures are  $T_j = 1.5T_a$  or  $T_j = 2.25T_a$ , where  $T_a$  is the ambient temperature. They are defined in table 10. The simulations are ongoing for M09Re1e5Ta1\_5Ld0150v9 and M09Re1e5Ta2\_25Ld0150v9.

#### 7. Hot jets at Mach numbers between 0.45 and 1.3

Finally, hot jets at  $Re_D = 100,000$  and at  $M = 0.45, 0.6, 0.75, 1.1$  and  $1.3$  with highly disturbed boundary layers ( $u'_e/u_j = 9\%$ ) have been computed. As for the hot jets at  $M = 0.9$ , their nozzle-exit static temperatures are equal to  $T_j = 1.5T_a$  or  $T_j = 2.25T_a$ . They are defined in table 11. The simulations are all ongoing.

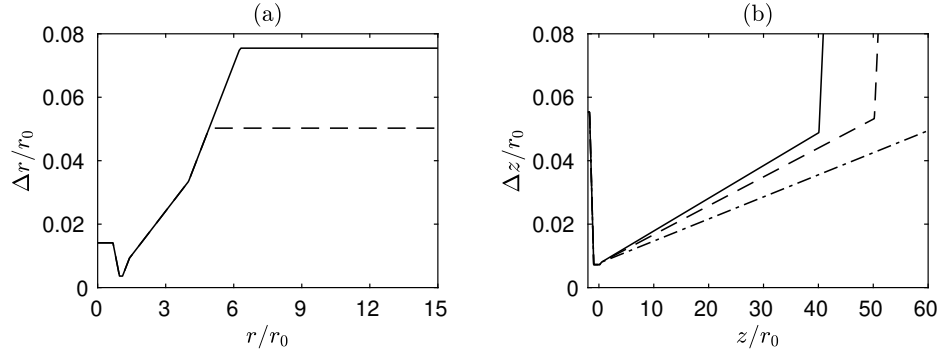
## II. Mesh grid parameters

Some characteristics of the mesh grids CGXX and FGXX used for the simulations in the radial and axial directions, namely the numbers of points, the grid physical extents and the mesh spacings at specific positions, are provided in table 12. The CG (coarse) and FG (fine) grids are employed for the jets at  $Re_D = 3,125$  and  $Re_D \geq 12,500$ , respectively, and *XX* indicates that the grid extends down to  $z = L_z = XXr_0$  in the axial direction, excluding the outflow sponge zone. The grids are detailed in recent papers [2–5]. In particular, a grid sensitivity study has been conducted in reference [2] to assess the quality of the FGz40 grid for the LES of the high Reynolds number tripped jet M09Re1e5TaLd0150v9. The numbers of points  $n_\theta$  in the azimuthal direction (256, 512 or 1024) in the different simulations, depending on the thickness and state of the nozzle-exit boundary layer, are given in tables 1-10. For illustration purposes, the variations of the radial and axial mesh spacings in FGz40, FGz50 and FGz60 are shown in figure 2.

## III. Recording files

The recording files (nature and location of the variables stored, time durations and sampling frequencies) are defined in table 13. Three-dimensional fields are stored in the 3Dxxx files, and two-dimensional fields at constant radial, azimuthal and axial positions are stored in the Rxx, Txx and Zxx files, respectively. The maximum Strouhal number  $St_D = fD/u_j$ , where  $f$  is the frequency, allowed by the sampling frequency is equal to 32 for  $T_{HF}$  and to 6.4 or 12.8 in the other cases.

The sets of files recorded in the different simulations, referred to as D0, D1, D2 and D3 in tables 1-10, are defined in table 14. For storage issues, all the files are saved (case D0) only for the isothermal tripped jet at Mach 0.9 and Reynolds 100,000 (**M09Re1e5TaLd0150v9**). For most other jets at high Reynolds numbers, the 3-D fields and the 2-D fields at  $\theta = \pi/4 \rightarrow 13\pi/4$  every  $\pi/2$  are not stored (case D1). For the jets at Reynolds 3,125, in addition, the Fourier coefficients for  $n_{\theta=5-8}$  are not recorded (case D2). Finally, case D3 applies to the untripped jets at  $M \neq 0.9$ .



**Fig. 2** Variations (a) of radial mesh spacing  $\Delta r$  for ——— FGz40 and - - - FGz50 and FGz60 and (b) of axial mesh spacing  $\Delta z$  for ——— FGz40, - - - FGz50 and - · - · FGz60.

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**Table 1 Mach and Reynolds numbers  $M$  and  $Re_D$ , jet temperature  $T_j$ , shape (L: laminar Blasius profile, T: transitional or turbulent profile) and thickness  $\delta_{BL}$  of the boundary-layer profile imposed at the pipe nozzle inlet, peak turbulence intensity  $u'_e/u_j$  at the nozzle exit, grid used, number of points  $n_\theta$  in the azimuthal direction, simulation time  $T$  after the transient period and recording files.**

jet	M	$Re_D$	$T_j/T_a$	BL	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
M09Re3125TaLd0420v1	0.9	3,125	1	L	0.42	1%	CGz75	512	5,000	D2
M09Re1e5TaLd0150v9	0.9	100,000	1	L	0.15	9%	FGz40	1,024	3,625	D0

**Table 2 LES of low-Reynolds-number isothermal jets; see caption of table 1 for the different parameters.**

jet	M	$Re_D$	$T_j/T_a$	BL	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
M03Re3125TaLd0420v1	0.3	3,125	1	L	0.42	1%	CGz75a	512	1,000	D2
M045Re3125TaLd0420v1	0.45	3,125	1	L	0.42	1%	CGz75a	512	1,500	D2
M06Re3125TaLd0420v1	0.6	3,125	1	L	0.42	1%	CGz75a	512	4,000	D2
M09Re3125TaLd0420v1	0.9	3,125	1	L	0.42	1%	CGz75a	512	5,000	D2
M13Re3125TaLd0420v1	1.3	3,125	1	L	0.42	1%	CGz75b	512	4,000	D2
M2Re3125TaLd0420v2_5	2	3,125	1	L	0.42	2.5%	CGz90	512	3,000	D2

**Table 3** LES of untripped isothermal jets at a Mach number of 0.9; see caption of table 1 for the different parameters.

jet	M	$Re_D$	$T_j/T_a$	L	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
M09Re1e5TaLd0400v0	0.9	100,000	1	L	0.4	0%	FGz40	256	500	D1
M09Re1e5TaLd0200v0	0.9	100,000	1	L	0.2	0%	FGz40	256	3,000	D1
M09Re1e5TaLd0100v0	0.9	100,000	1	L	0.1	0%	FGz40	512	1,000	D1
M09Re1e5TaLd0050v0	0.9	100,000	1	L	0.05	0%	FGz40	512	1,000	D1
M09Re1e5TaLd0025v0	0.9	100,000	1	L	0.025	0%	FGz40	512	2,000	D1

**Table 4** LES of untripped isothermal jets at Mach numbers between 0.5 and 2; see caption of table 1 for the different parameters.

jet	M	$Re_D$	$T_j/T_a$	L	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
MxxxRe1e5TaLd0200v0	0.5 → 2	100,000	1	L	0.2	0%	FGz40	256	500	D3
MxxxRe1e5TaLd0100v0	0.5 → 2	100,000	1	L	0.1	0%	FGz40	256	500	D3
MxxxRe1e5TaLd0050v0	0.5 → 2	100,000	1	L	0.05	0%	FGz40	256	500	D3

**Table 5** LES of tripped isothermal jets at M = 0.9; see caption of table 1 for the different parameters.

jet	M	$Re_D$	$T_j/T_a$	BL	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
M09Re1e5TaLd0150v0	0.9	100,000	1	L	0.15	0%	FGz40	512	500	D1
M09Re1e5TaLd0150v3	0.9	100,000	1	L	0.15	3%	FGz40	1,024	500	D1
M09Re1e5TaLd0150v6	0.9	100,000	1	L	0.15	6%	FGz40	1,024	500	D1
<b>M09Re1e5TaLd0150v9</b>	0.9	100,000	1	L	0.15	9%	FGz40	1,024	3,625	D0
M09Re1e5TaLd0150v12	0.9	100,000	1	L	0.15	12%	FGz40	1,024	500	D1
M09Re1e5TaLd0150v15	0.9	100,000	1	L	0.15	15%	FGz40	1,024	500	D1

**Table 6** LES of tripped isothermal jets at Reynolds numbers between 12,500 and 400,000; see caption of table 1 for the different parameters.

jet	M	$Re_D$	$T_j/T_a$	BL	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
M09Re1_25e4TaLd0150v7_5	0.9	12,500	1	L	0.15	7.5%	FGz40	1,024	500	D1
M09Re2_5e4TaLd0150v9	0.9	25,000	1	L	0.15	9%	FGz40	1,024	500	D1
M09Re5e4TaLd0150v9	0.9	50,000	1	L	0.15	9%	FGz40	1,024	500	D1
<b>M09Re1e5TaLd0150v9</b>	0.9	100,000	1	L	0.15	9%	FGz40	1,024	3,000	D0
M09Re2e5TaLd0150v9	0.9	200,000	1	L	0.15	9%	FGz40	1,024	500	D1
M09Re4e5TaLd0150v9	0.9	400,000	1	L	0.15	9%	FGz40	1,024	500	D1

**Table 7** LES of isothermal tripped jets with different boundary-layer thicknesses; see caption of table 1 for the different parameters.

jet	M	Re <sub>D</sub>	T <sub>j</sub> /T <sub>a</sub>	L	δ <sub>BL</sub> /r <sub>0</sub>	u' <sub>e</sub> /u <sub>j</sub>	grid	n <sub>θ</sub>	Tu <sub>j</sub> /r <sub>0</sub>	data
M09Re5e4TaLd0150v9	0.9	50,000	1	L	0.15	9%	FGz40	1,024	500	D1
M09Re5e4TaLd0090v9	0.9	50,000	1	L	0.09	9%	FGz40	1,024	500	D1
M09Re5e4TaLd0250v9	0.9	50,000	1	L	0.25	9%	FGz40	1,024	500	D1
M09Re5e4TaLd0420v9	0.9	50,000	1	L	0.42	9%	FGz40	1,024	500	D1
M09Re8_3e4TaLd0250v9	0.9	83,333	1	L	0.09	9%	FGz40	1,024	500	D1
M09Re3e4TaLd0250v9	0.9	30,000	1	L	0.25	9%	FGz40	1,024	500	D1
M09Re1_8e4TaLd0250v9	0.9	18,000	1	L	0.42	9%	FGz40	1,024	500	D1

**Table 8** LES of isothermal tripped jets at Mach numbers between 0.3 and 3; see caption of table 1 for the different parameters.

jet	M	Re <sub>D</sub>	T <sub>j</sub> /T <sub>a</sub>	BL	δ <sub>BL</sub> /r <sub>0</sub>	u' <sub>e</sub> /u <sub>j</sub>	grid	n <sub>θ</sub>	Tu <sub>j</sub> /r <sub>0</sub>	data
M03Re1e5TaLd0150v9	0.3	100,000	1	L	0.15	9%	FGz40	1,024	500	D1
M045Re1e5TaLd0150v9	0.45	100,000	1	L	0.15	9%	FGz40	1,024	800	D1
M06Re1e5TaLd0150v9	0.6	100,000	1	L	0.15	9%	FGz40	1,024	2,000	D1
M075Re1e5TaLd0150v9	0.75	100,000	1	L	0.15	9%	FGz40	1,024	2,000	D1
M09Re1e5TaLd0150v9	0.9	100,000	1	L	0.15	9%	FGz40	1,024	3,625	D0
M11Re1e5TaLd0150v9	1.1	100,000	1	L	0.15	9%	FGz40	1,024	2,000	D1
M13Re1e5TaLd0150v9	1.3	100,000	1	L	0.15	9%	FGz50	1,024	2,000	D1
M16Re1e5TaLd0150v9	1.6	100,000	1	L	0.15	9%	FGz50	1,024	600	D1
M2Re1e5TaLd0150v9	2	100,000	1	L	0.15	9%	FGz60	1,024	2,000	D1
M25Re1e5TaLd0150v9	2.5	100,000	1	L	0.15	9%	FGz60	1,024	400	D1
M3Re1e5TaLd0150v9	3	100,000	1	L	0.15	9%	FGz70	1,024	600	D1

**Table 9** LES of isothermal tripped jets with non-laminar boundary-layer profiles; see caption of table 1 for the different parameters.

jet	M	Re <sub>D</sub>	T <sub>j</sub> /T <sub>a</sub>	BL	δ <sub>BL</sub> /r <sub>0</sub>	u' <sub>e</sub> /u <sub>j</sub>	grid	n <sub>θ</sub>	Tu <sub>j</sub> /r <sub>0</sub>	data
M09Re5e4TaLd0250v0	0.9	50,000	1	L	0.25	0%	FGz40	1,024	500	D1
M09Re5e4TaT1d0250v0	0.9	50,000	1	T1	0.25	0%	FGz40	1,024	500	D1
M09Re5e4TaT2d0250v0	0.9	50,000	1	T2	0.25	0%	FGz40	1,024	500	D1
M09Re5e4TaT3d0250v0	0.9	50,000	1	T3	0.25	0%	FGz40	1,024	500	D1
M09Re5e4TaLd0250v6	0.9	50,000	1	L	0.25	6%	FGz40	1,024	500	D1
M09Re5e4TaT1d0250v6	0.9	50,000	1	T1	0.25	6%	FGz40	1,024	500	D1
M09Re5e4TaT2d0250v6	0.9	50,000	1	T2	0.25	6%	FGz40	1,024	500	D1



**Table 10** LES of hot tripped jets at a Mach number of 0.9; see caption of table 1 for the different parameters.

jet	M	Re <sub>D</sub>	$T_j/T_a$	BL	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
<b>M09Re1e5TaLd0150v9</b>	0.9	100,000	<b>1</b>	L	0.15	9%	FGz40	1,024	3,625	D0
M09Re5e4Ta1_5Ld0150v9	0.9	50,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	500	D1
M09Re1e5Ta1_5Ld0150v9	0.9	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	1,800	D1
M09Re2e5Ta1_5Ld0150v9	0.9	200,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	500	D1
M09Re2_5e4Ta2_25Ld0150v9	0.9	25,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	500	D1
M09Re1e5Ta2_25Ld0150v9	0.9	100,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	1,800	D1

**Table 11** LES of hot tripped jets at Mach numbers between 0.3 and 1.3; see caption of table 1 for the different parameters.

jet	M	Re <sub>D</sub>	$T_j/T_a$	BL	$\delta_{BL}/r_0$	$u'_e/u_j$	grid	$n_\theta$	$Tu_j/r_0$	data
M045Re1e5Ta1_5Ld0150v9	0.45	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	400	D1
M06Re1e5Ta1_5Ld0150v9	0.6	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	400	D1
M075Re1e5Ta1_5Ld0150v9	0.75	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	400	D1
M09Re1e5Ta1_5Ld0150v9	0.9	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	1,800	D1
M11Re1e5Ta1_5Ld0150v9	1.1	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	400	D1
M13Re1e5Ta1_5Ld0150v9	1.3	100,000	<b>1.5</b>	L	0.15	9%	FGz40	1,024	300	D1
M06Re1e5Ta2_25Ld0150v9	0.6	100,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	50	D1
M075Re1e5Ta2_25Ld0150v9	0.75	100,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	400	D1
M09Re1e5Ta2_25Ld0150v9	0.9	100,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	1,800	D1
M11Re1e5Ta2_25Ld0150v9	1.1	100,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	400	D1
M13Re1e5Ta2_25Ld0150v9	1.3	100,000	<b>2.25</b>	L	0.15	9%	FGz40	1,024	200	D1

**Table 12** Numbers of points  $n_r$  and  $n_z$  and extents of the physical domain  $L_r$  and  $L_z$  in the radial and axial directions, and mesh spacings  $\Delta r$  and  $\Delta z$  at different positions.

grid	$n_r$	$n_z$	$L_r$	$L_z$	$\Delta r/r_0$ (%) at			$\Delta z/r_0$ (%) at		
					$r = 0$	$r = r_0$	$r = L_r$	$z = 0$	$z = 15r_0$	$z = L_z$
CGz75a	427	2458	$25r_0$	$75r_0$	2.48	0.72	14.94	1.45	2.49	6.25
CGz75b	479	2458	$25r_0$	$75r_0$	2.48	0.72	10.03	1.45	2.49	6.25
CGz90	479	3058	$25r_0$	$90r_0$	2.48	0.72	10.03	1.45	2.49	6.25
FGz40	504	2085	$15r_0$	$40r_0$	1.41	0.36	7.55	0.72	2.30	4.88
FGz50	572	2412	$15r_0$	$50r_0$	1.41	0.36	5.03	0.72	2.12	5.31
FGz60	572	2947	$15r_0$	$60r_0$	1.41	0.36	5.03	0.72	1.82	4.95
FGz70	626	3822	$15r_0$	$70r_0$	1.41	0.36	4.02	0.72	1.47	4

**Table 13 Recording files: Strouhal number given by the sampling frequency, recording positions, and variables recorded (density  $\rho$ , velocity components  $u_i = (u_r, u_t, u_z)$ , pressure  $p$ , vorticity norm  $|\omega|$ , dilatation  $\Theta$ ).**

files	$St_D$	$z$	$r$	$\theta$	variables
<i>3Daero</i>	6.4	$0 \rightarrow 30r_0$ every $2\Delta z$	$0 \rightarrow 6r_0$ every $2\Delta r$	$0 \rightarrow 2\pi - 2\pi/512$ every $2\pi/512$	$\rho, u_i, p$
<i>3Dac</i>	6.4	$0 \rightarrow L_z$ every $2\Delta z$	$L_r$	$0 \rightarrow 2\pi - 2\pi/512$ every $2\pi/512$	$p$
	6.4	$0 \rightarrow L_z$ every $2\Delta z$	$0 \rightarrow L_r$ every $\Delta r$	$0 \rightarrow 3\pi/2$ every $\pi/2$	$p$
	6.4	$0 \rightarrow L_z$ every $10r_0$	$0 \rightarrow L_r$ every $\Delta r$	$0 \rightarrow 2\pi - 2\pi/512$ every $2\pi/512$	$p$
$R_0$	12.8	$-1.25r_0 \rightarrow L_z$ every $2\Delta z$	0	$0 \rightarrow 2\pi - 2\pi/256$ every $2\pi/256$	$\rho, u_i, p,  \omega , \Theta$
$R_1$	12.8	$-1.25r_0 \rightarrow L_z$ every $2\Delta z$	$r_0$	$0 \rightarrow 2\pi - 2\pi/256$ every $2\pi/256$	$\rho, u_i, p,  \omega , \Theta$
$R_{WP}$	12.8	$-1.25r_0 \rightarrow L_z$ every $2\Delta z$	$1.4r_0$ at $z = 0$ $8^\circ$ cone angle	$0 \rightarrow 2\pi - 2\pi/256$ every $2\pi/256$	$\rho, u_i, p,  \omega , \Theta$
$R_{NF}$	12.8	$-1.25r_0 \rightarrow L_z$ every $2\Delta z$	$L_r$	$0 \rightarrow 2\pi - 2\pi/256$ every $2\pi/256$	$\rho, u_i, p$
$T_{axi}$	6.4	$-1.25r_0 \rightarrow L_z$ every $\Delta z$	$0 \rightarrow L_r$ every $\Delta r$		Fourier coef $n_{\theta=0}$ for $\rho, u_i, p$
$T_{0-270}$	6.4	$-1.25r_0 \rightarrow L_z$ every $\Delta z$	$0 \rightarrow L_r$ every $\Delta r$	$0 \rightarrow 3\pi/2$ every $\pi/2$	$\rho, u_i, p, \partial u_i / \partial \theta$
$T_{45-315}$	6.4	$-1.25r_0 \rightarrow L_z$ every $\Delta z$	$0 \rightarrow L_r$ every $\Delta r$	$\pi/4 \rightarrow 13\pi/4$ every $\pi/2$	$\rho, u_i, p, \partial u_i / \partial \theta$
$T_{n_{\theta}=0-4}$	6.4	$0 \rightarrow L_z$ every $2\Delta z$	$0 \rightarrow L_r$ every $2\Delta r$		Fourier coef $n_{\theta=0-4}$ for $\rho, u_i, p,  \omega , \Theta$
$T_{n_{\theta}=5-8}$	6.4	$0 \rightarrow L_z$ every $2\Delta z$	$0 \rightarrow L_r$ every $2\Delta r$		Fourier coef $n_{\theta=5-8}$ for $\rho, u_i, p,  \omega , \Theta$
$T_{HF}$	32	$0 \rightarrow 20r_0$ every $2\Delta z$	$0 \rightarrow 3.5r_0$ every $2\Delta r$	0	$\rho, u_i, p$
$Z_{0/start/end}$	12.8	$-1.25r_0, 0, L_z$	$0 \rightarrow L_r$ every $\Delta r$	$0 \rightarrow 2\pi - 2\pi/256$ every $2\pi/256$	$\rho, u_i, p$
$Z_{5-35}$	6.4	$5r_0 \rightarrow 35r_0$ every $5r_0$	$0 \rightarrow L_r$ every $2\Delta r$	$0 \rightarrow 2\pi - 2\pi/256$ every $2\pi/256$	$\rho, u_i, p$

**Table 14 Set of files recorded in the simulations.**

jets	case	files recorded
<b>M09Re1e5TaLd0150v9</b>	D0	all files
most jets at $Re_D \geq 12,500$	D1	all files except for <i>3Daero</i> , <i>3Dac</i> and $T_{45-315}$
jets at $Re_D = 3,125$	D2	all files except for <i>3Daero</i> , <i>3Dac</i> , $T_{45-315}$ , $T_{n_{\theta}=5-8}$ and $T_{HF}$
untripped jets at $M \neq 0.9$	D3	all files except for <i>3Daero</i> , <i>3Dac</i> , $T_{45-315}$ , $T_{n_{\theta}=2-8}$ , $T_{HF}$ and $Z_{5-35}$