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Boundary Control of the Kuramoto-Sivashinsky Equation Under Intermittent Data Availability

M. Maghenem, C. Prieur, and E. Witrant

Abstract—In this paper, two boundary controllers are proposed to stabilize the origin of the nonlinear Kuramoto-Sivashinsky equation under intermittent measurements. More precisely, the spatial domain is divided into two sub-domains. The state of the system on the first sub-domain is measured along a given interval of time, and the state on the remaining sub-domain is measured along another interval of time. Under the proposed sensing scenario, we control the considered equation by designing the value of the state at three isolated spatial points, the two extremities of the spatial domain plus one inside point. Furthermore, we impose a null value for the spatial gradient of the state at these three locations. Under such a control loop, we propose two types of controllers and we analyze the stability of the resulting closed-loop system in each case. The paper is concluded with some discussions and future works.

I. INTRODUCTION

Partial differential equations (PDE)s have numerous applications in many engineering fields including fluid flows in conservation laws [1], flexible structures [2], electromagnetic waves, and quantum mechanics [3]. The control design for PDEs is a key step to guarantee that the related process achieves a desired behavior in closed loop, i.e., a state of interest converges (in an appropriate norm) to an invariant set [4], [5], or tracks the state of a driving process [6], [7]. Before designing the control input, it is important to know the control actions allowed by the physical process. Indeed, some processes allows to act on the dynamics at every spatial point and for all time [8]. However, in some other processes, we act intermittently in time or in space [9], [10]. Furthermore, in some scenarios, we can reset the state intermittently in time and at every spatial point [11], but in other scenarios, we reset the state only at some spatial points [6], the latter case corresponds to the well-studied boundary-control paradigm [12]. On the other hand, it is important to know the outputs available for input design. In some cases, we measure the state at every spatial point all the time [13]. However, in most realistic scenarios, we measure only intermittently in space and time [9], [14]. The feedback law, in consequence, must adapt to each of these control and sensing scenarios.

Some intermittent control strategies for PDEs are available in the literature. In [11], the Gray-Scott and the Kuramoto-

Sivashinsky equations are controlled via a periodic reset of the state using impulsive systems theory. Furthermore, in [9], the Kuramoto-Sivashinsky equation is controlled via a periodic update of the input affecting the right-hand side using sample-data control techniques. A common feature among the aforementioned works is that the PDEs are controlled at every spatial point. When controlling PDEs at isolated spatial points or intervals, the existing control literature considers only the particular case of boundary control. However, the physics community, since the late nineties, has shown an intensive interest in general spatially- and temporally-intermittent control of PDEs. For example, in [6], the Gray-Scott equation is controlled by resetting the state periodically in time and at periodically separated spatial points. In [10], [15], the Kuramoto-Sivashinsky equation is controlled by acting on the right-hand side at periodically separated spatial intervals. In [16], the Ginzburg-Landau equation is studied following the strategy in [10]. The results in the aforementioned physics literature are guaranteed via simulations, and experiments in some cases. To the best of our knowledge, a rigorous study of the aforementioned problems is not available in the literature.

The Kuramoto-Sivashinsky equation is one of the well-studied PDEs in control literature. In particular, different types of boundary controllers are proposed to stabilize the origin in a given norm. For example, in [17], the linear Kuramoto-Shavinsky equation is transformed into an equivalent finite-dimensional linear system using the Sturm-Liouville decomposition. As a consequence, a linear feedback law is assigned to one extremity of the spatial domain. Furthermore, the nonlinear equation is studied in [18], [19], [20], [21] under various boundary conditions. It is important to note that although the aforementioned results assume point-wise measurements, the equation is assumed to be either linear or intrinsically stable. To the best of our knowledge, boundary control of the nonlinear Kuramoto-Sivashinsky equation without restricting the destabilizing coefficient is studied only in [22], where the state, on the whole spacial domain, is assumed to be available all the time.

In this paper, we study boundary control of the nonlinear Kuramoto-Sivashinsky equation, without restricting the destabilizing coefficient, under intermittent measurements. Strictly speaking, we measure the state on a given spatial sub-domain along a given interval of time and, then, we measure the state on the remaining spatial sub-domain along another time interval. As a result, we do not measure the

M. Maghenem, C. Prieur, and E. Witrant are with Université Grenoble Alpes, CNRS, Grenoble-INP, GIPSA-lab, F-38000, Grenoble, France (e-mail: mohamed.maghenem,christophe.prieur,emmanuel.witrant@gipsa-lab.fr). This work has been partially supported by MIAI@Grenoble Alpes (ANR-19-P3IA-0003), the French program Investissement d'Avenir, and by ANR grant HANDY (ANR-18-CE40-0010).

state, on the whole spatial domain, at the same time. Under the proposed sensing scenario, we control the considered equation by designing the state at three isolated points, the two extremities of the spatial domain plus one inside point. Furthermore, we impose a null value for the spatial gradient of the state at these three locations. Two types of design approaches are proposed. In the first one, we design feedback laws at the two extremities and set the input to zero at the inside point. In the second case, we design a feedback law at one extremity and at the inside point, and set the input to zero at the remaining extremity. The stability properties of the resulting closed-loop system are analyzed in each case using Lyapunov methods.

The remainder of the paper is organized as follows. The problem formulation is in Section II. The proposed Lyapunov-based approach is described in Section III. The main results are in Sections IV and V, respectively. Finally, the paper is concluded by some discussions and future works.

Notation. For $x \in \mathbb{R}^n$, $(a, b) \in \mathbb{R} \times \mathbb{R}$ with $a < b$, and a function $z : [a, b] \rightarrow \mathbb{R}$, we let $|x| := \sqrt{x^\top x}$, $\|z\| := \sqrt{\int_a^b |z(x)|^2 dx}$, $z_x := \frac{\partial z}{\partial x}$, $z_{xx} := \frac{\partial^2 z}{\partial x^2}$, $z_{xxx} := \frac{\partial^3 z}{\partial x^3}$, and $z_{xxxx} := \frac{\partial^4 z}{\partial x^4}$. Furthermore, we say that $z \in \mathcal{L}^2(a, b)$ if $\|z\|$ is finite, $z \in H^1(a, b)$ if $\|z\| + \|z_x\|$ is finite and $z \in H^2(a, b)$ if $\|z\| + \|z_x\| + \|z_{xx}\|$ is finite. Moreover, we say that $z \in H_o^1(a, b)$ if $z \in H^1(a, b)$ and $z(a) = z(b) = 0$, and we say that $z \in H_o^2(a, b)$ if $z \in H^2(a, b)$ and $z(a) = z(b) = z_x(a) = z_x(b) = 0$. For a matrix $M \in \mathbb{R}^{n \times n}$, $\det M$ denotes the determinant of the matrix M . To avoid heavy notations, for a function $u : [a, b] \times \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}$, the time dependence is implicit when we write $u(x)$. In other words, we use $u(x)$, to express $u(x, t)$. Moreover, we use $\text{dom } u$ to denote the domain of definition of the map $t \mapsto u(x, t)$ for all $x \in [a, b]$. Finally, $\kappa : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}_{\geq 0}$ is a class \mathcal{K} function if it is continuous, increasing, and $\kappa(0) = 0$.

II. PROBLEM FORMULATION

Consider the nonlinear Kuramoto-Sivashinsky equation given by

$$\Sigma_1 : u_t = -uu_x - \lambda_1 u_{xx} - u_{xxxx} \quad x \in [0, L],$$

where $L > 0$ and $\lambda_1 \geq 0$ are constant coefficients assumed to be known. The boundary conditions of Σ_1 will be eventually specified.

A. Intermittent Sensing

For some $Y \in (0, L)$, we measure the state u on the spatial domain $[0, Y]$ for some interval of time and, then, we measure u on the domain $[Y, L]$ along another time interval. In particular, we do not measure u along the whole line $[0, L]$ simultaneously. The proposed sensing scenario has the following motivations.

In network control systems [23]. Assume that we dispose of two sensors, the first one measures $u([0, Y])$ and the second one measures $u([Y, L])$. The two sensors share the same channel when sending their data to the controller.

Hence, $u([0, Y])$ is available to the controller only for some interval of time and $u([Y, L])$ only for another interval of time. The same reasoning can be extended if a network of sensors share the same communication channel with the controller [24]. Also, when using mobile or scanning sensors; see [25] and [26], respectively. Assume that we dispose of one mobile sensor measuring the state $u([0, Y])$ for some interval of time, then, it changes location to measure $u([Y, L])$ for another interval of time. Note that, here, we are neglecting the dynamics of the mobile sensor compared to the dynamics of Σ_1 . This reasoning can be extended to a network of mobile sensors as in [27], [28], [29].

Strictly speaking, we assume the existence of a sequence of times $\{t_i\}_{i=1}^\infty$, with $t_1 = 0$ and $t_{i+1} > t_i$, such that

- $u([0, Y], t)$ is available for all $t \in \bigcup_{k=1}^\infty [t_{2k-1}, t_{2k})$.
- $u([Y, L], t)$ is available for all $t \in \bigcup_{k=1}^\infty [t_{2k}, t_{2k+1})$.

Next, we consider the following assumption:

Assumption 1: There exist $\bar{T}_1, \bar{T}_2 > 0$ such that, for each $k \in \{1, 2, \dots\}$, $t_{2k} - t_{2k-1} = \bar{T}_1$ and $t_{2k+1} - t_{2k} = \bar{T}_2$. •

Remark 1: The proposed sensing scenario can be generalized if we decompose the interval $[0, L]$ into many sub-intervals instead of only two. In this case, we define an increasing sequence $\{Y_i\}_{i=1}^N$, with $Y_1 = 0$ and $Y_N = L$ such that, for each $i \in \{1, 2, \dots, N\}$, $u([Y_i, Y_{i+1}], t)$ is available to the controller for all $t \in \bigcup_{k=1}^\infty [t_{(N-1)(k-1)+i}, t_{(N-1)(k-1)+i+1})$. •

Remark 2: Note that most of existing results on boundary stabilization of Σ_1 assume point-wise measurements; namely, the state u is measured at the isolated points where the control is effective; see for example [18], [19], [20], [21], [17]. However, in the aforementioned results either λ_1 is assumed to be sufficiently small or the linear version of Σ_1 is considered. To the best of our knowledge, boundary control of the nonlinear Kuramoto-Sivashinsky equation without restricting the size of λ_1 is studied only in [22], where the availability of u on the whole line $[0, L]$ and for all time is assumed. •

B. Boundary Control

We propose to control Σ_1 at three different locations; namely, at $x = 0$, $x = Y$, and $x = L$. As a result, we view Σ_1 as a system of two PDEs interconnected by a boundary constraint. That is, we consider the system

$$\Sigma_2 : \begin{cases} w_t = -w w_x - \lambda_1 w_{xx} - w_{xxxx} & x \in [0, Y] \\ v_t = -v v_x - \lambda_1 v_{xx} - v_{xxxx} & x \in [Y, L] \end{cases}$$

under the boundary constraints

$$w(Y) = v(Y) \text{ and } w_x(Y) = v_x(Y). \quad (1)$$

Condition (1) guarantees that w , defined on $[0, Y]$, is a continuously differentiable extension of v , defined on $[Y, L]$, and vice-versa.

Furthermore, each equation in Σ_2 allows for four boundary conditions, counting the two conditions in (1), we conclude

that we are allowed to control Σ_2 by imposing six other boundary conditions, which are given by

$$\begin{aligned} v_x(L) = 0, \quad w_x(Y) = 0, \quad w_x(0) = 0, \\ w(0) = u_1, \quad w(Y) = u_2, \quad v(L) = u_3, \end{aligned} \quad (2)$$

where (u_1, u_2, u_3) are control inputs to be designed.

Next, we specify the set of solutions to Σ_2 .

Definition 1: A pair $((w, v), \{u_i\}_{i=1}^3)$, with $w : [0, Y] \times \text{dom } w \rightarrow \mathbb{R}$, $v : [Y, L] \times \text{dom } v \rightarrow \mathbb{R}$, and $u_i : \text{dom } u_i \rightarrow \mathbb{R}$, is a solution pair to Σ_2 if $\text{dom } w = \text{dom } v = \text{dom } u_1 = \text{dom } u_2 = \text{dom } u_3$, $(w(\cdot, t), v(\cdot, t)) \in H^4(0, Y) \times H^4(Y, L)$, $(w(x, \cdot), v(x, \cdot))$ is locally absolutely continuous, (1)-(2) hold, and

$$\begin{aligned} \frac{\partial w}{\partial t}(x, t) &= -w(x, t)w_x(x, t) - \lambda_1 w_{xx}(x, t) - w_{xxx}(x, t) \\ &\quad \text{for almost all } (x, t) \in [0, Y] \times \text{dom } w, \\ \frac{\partial v}{\partial t}(x, t) &= -v(x, t)v_x(x, t) - \lambda_1 v_{xx}(x, t) - v_{xxx}(x, t) \\ &\quad \text{for almost all } (x, t) \in [Y, L] \times \text{dom } v. \end{aligned}$$

As a consequence, we study Σ_1 under

$$\begin{aligned} (u_x(L), u_x(Y), u_x(0)) &= (0, 0, 0), \\ (u(0), u(Y), u(L)) &= (u_1, u_2, u_3) \end{aligned} \quad (3)$$

by studying Σ_2 under (1)-(2). Hence, we specify the set of solutions to Σ_1 as follows:

Definition 2: A pair $(u, \{u_i\}_{i=1}^3)$, with $u : [0, L] \times \text{dom } u \rightarrow \mathbb{R}$ and $u_i : \text{dom } u_i \rightarrow \mathbb{R}$, is a solution pair to Σ_1 if there exists (w, v) such that $((w, v), \{u_i\}_{i=1}^3)$ is a solution pair to Σ_2 , $\text{dom } u = \text{dom } w = \text{dom } v$, $u(x, t) = w(x, t)$ for all $(x, t) \in [0, Y] \times \text{dom } u$, and $u(x, t) = v(x, t)$ for all $(x, t) \in [Y, L] \times \text{dom } u$.

Remark 3: In [18], Σ_1 is considered under the boundary conditions $u_x(L) = u_x(0) = 0$, $u_{xxx}(0) = u_1$, and $u_{xxx}(L) = u_2$. Furthermore, in [22], the boundary conditions $u(L) = u(0) = 0$, $u_{xx}(0) = 0$, $u_{xx}(L) = u_2$ are considered. Compared to the latter two references, in our work, we use an additional control action at $x = Y$ to handle the intermittent availability of the measurements.

In the sequel, we design (u_1, u_2, u_3) for Σ_1 , by following two scenarios. First, we set $u_2 = 0$ and we design u_1 and u_3 . Second, we set $u_3 = 0$ and we design u_1 and u_2 .

III. GENERAL APPROACH

Before designing the control inputs, we consider the following two Lyapunov function candidates:

$$V_1(w) := \frac{1}{2} \int_0^Y w(x)^2 dx, \quad V_2(v) := \frac{1}{2} \int_Y^L v(x)^2 dx. \quad (4)$$

Lemma 1: Along the solutions to Σ_2 and under (1) and (2), we have

$$\begin{aligned} \dot{V}_1 &= - \int_0^Y w_{xx}(x)^2 dx + \lambda_1 \int_0^Y w_x(x)^2 dx \\ &\quad - \frac{u_2^3 - u_1^3}{3} - u_2 w_{xxx}(Y) + u_1 w_{xxx}(0), \\ \dot{V}_2 &= - \int_Y^L v_{xx}(x)^2 dx + \lambda_1 \int_Y^L v_x(x)^2 dx \\ &\quad - \frac{u_3^3 - u_2^3}{3} - u_3 v_{xxx}(L) + u_2 v_{xxx}(Y). \end{aligned} \quad (5)$$

□

Next, we introduce a key result that allows us to upper bound the terms $[- \int_0^Y w_{xx}(x)^2 dx + \lambda_1 \int_0^Y w_x(x)^2 dx]$ and $[- \int_Y^L v_{xx}(x)^2 dx + \lambda_1 \int_Y^L v_x(x)^2 dx]$ in (5) using V_1 , V_2 , and the inputs (u_1, u_2, u_3) . To this end, we introduce the following eigenvalue problem.

Problem 1: Given $\lambda \geq 0$, find the smallest $\delta \in \mathbb{R}$, denoted δ_o , such that

$$z_{xxxx} + \lambda z_{xx} = \delta z \quad x \in [a, b] \quad (6)$$

• admits a nontrivial solution $z : [a, b] \rightarrow \mathbb{R}$ in $H^2(a, b)$ satisfying

$$z(a) = z(b) = z_x(a) = z_x(b) = 0. \quad (7)$$

•

The following result can be found in [19, Lemma 2.1, Theorem 2.1, and Remark 1].

Lemma 2: Given $\lambda \geq 0$, we let $\delta_o \in \mathbb{R}$ be the corresponding solution to Problem 1. Then, if $\lambda < 4\pi^2$ then $\delta_o > 0$. Furthermore, if $\lambda > 4\pi^2$ then $\delta_o < 0$. Finally, if $\lambda = 4\pi^2$ then $\delta_o = 0$. □

The following lemma can be found in [19, Lemma 3.1].

Lemma 3: Given $\lambda \geq 0$ and $z \in H_o^2(a, b)$. Let $\delta_o \in \mathbb{R}$ be the solution to Problem 1. Then,

$$- \int_a^b z_{xx}(x)^2 dx + \lambda \int_a^b z_x(x)^2 dx \leq -\delta_o \int_a^b z(x)^2 dx. \quad (8)$$

□

Now, we propose a generalization of Lemma 3.

Lemma 4: Given $\lambda_1 > 0$ and $z \in H^2(a, b)$ with $z_x(a) = z_x(b) = 0$. Let δ_o be the solution to Problem 1 with $\lambda := 3\lambda_1$. Then, for each $\delta \leq \delta_o$, we have

$$\begin{aligned} - \int_a^b z_{xx}(x)^2 dx + \lambda_1 \int_a^b z_x(x)^2 dx &\leq \delta_1 \int_a^b z(x)^2 dx \\ &+ C_{z1}(z(a), z(b)) + \delta_2 C_{z2}(z(a), z(b)) + \lambda_1 C_{z3}(z(a), z(b)), \end{aligned} \quad (9)$$

where $\delta_1 := (|\delta| - 2\delta)/3$, $\delta_2 := (4|\delta| - 2\delta)/3$,

$$\begin{aligned} C_{z1}(\cdot) &:= 2 \int_a^b \kappa_{xx}(x)^2 dx, \\ C_{z2}(\cdot) &:= \int_a^b \kappa(x)^2 dx, \quad C_{z3}(\cdot) := 2 \int_a^b \kappa_x(x)^2 dx, \end{aligned} \quad (10)$$

$$\begin{aligned} \kappa(x) := & z(a) - 2[z(b) - z(a)] \left(\frac{x-a}{b} \right)^3 \\ & + 3[z(b) - z(a)] \left(\frac{x-a}{b} \right)^2. \end{aligned} \quad (11)$$

□

Remark 4: We can explicitly compute δ , a lower bound of δ_o , and numerically approach δ_o . This is omitted due to space limitation. •

Remark 5: According to (10) and (11), we conclude that, for each $i \in \{1, 2, 3\}$, $C_{zi}(z(a), z(b)) := a_{zi}z(a)^2 + b_{zi}z(b)^2 + c_{zi}z(a)z(b)$, where (a_{zi}, b_{zi}, c_{zi}) are constants obtained by integrating the polynomials κ^2 , κ_x^2 , and κ_{xx}^2 on the interval $[a, b]$. It is also important to note that the parameters (a_{zi}, b_{zi}, c_{zi}) depend only on the domain of z , which is the interval $[a, b]$. •

At this point, using Lemma 4, we translate the analysis of Σ_2 , which is an infinite-dimensional system, into the analysis of a finite-dimensional system of differential inequalities.

Lemma 5: Along the solutions to Σ_2 and under (1) and (2), we have

$$\begin{aligned} \dot{V}_1 &\leq 2\delta_1 V_1 + C_{w1}(u_1, u_2) + \delta_2 C_{w2}(u_1, u_2) \\ &\quad + \lambda_1 C_{w3}(u_1, u_2) - \frac{u_3^3 - u_1^3}{3} - u_2 w_{xxx}(Y) + u_1 w_{xxx}(0), \\ \dot{V}_2 &\leq 2\delta_1 V_2 + C_{v1}(u_2, u_3) + \delta_2 C_{v2}(u_2, u_3) \\ &\quad + \lambda_1 C_{v3}(u_2, u_3) - \frac{u_3^3 - u_2^3}{3} - u_3 v_{xxx}(L) + u_2 v_{xxx}(Y), \end{aligned} \quad (12)$$

where (δ_1, δ_2) are given in Lemma 4, and $\{C_{wi}\}_{i=1}^3$ and $\{C_{vi}\}_{i=1}^3$ are obtained as in Lemma 4 while substituting (a, b, z) therein by $(0, Y, w)$ and (Y, L, v) , respectively. □

Remark 6: The control action $u_2 = w(Y) = v(Y)$ will be helpful to handle the boundary terms at $x = Y$ that appear in (12). Without this additional control action, the problem is hard to solve when $\lambda_1 \geq 4\pi^2$. •

IV. MAIN RESULT 1:

ACTIVE CONTROL AT $x = 0$ AND $x = L$

In this section, we let $u_2 = 0$; hence, (12) becomes

$$\begin{aligned} \dot{V}_1 &\leq 2\delta_1 V_1 + C_{w1}(u_1, 0) + \delta_2 C_{w2}(u_1, 0) \\ &\quad + \lambda_1 C_{w3}(u_1, 0) + u_1 w_{xxx}(0) + u_1^3/3, \\ \dot{V}_2 &\leq 2\delta_1 V_2 + C_{v1}(0, u_3) + \delta_2 C_{v2}(0, u_3) \\ &\quad + \lambda_1 C_{v3}(0, u_3) - u_3 v_{xxx}(L) - u_3^3/3. \end{aligned}$$

Next, using Remark 5, we obtain

$$\begin{aligned} \dot{V}_1 &\leq 2\delta_1 V_1 + a_{w1}u_1^2 + \delta_2 a_{w2}u_1^2 \\ &\quad + \lambda_1 a_{w3}u_1^2 + u_1 w_{xxx}(0) + u_1^3/3, \\ \dot{V}_2 &\leq 2\delta_1 V_2 + b_{v1}u_3^2 + \delta_2 b_{v2}u_3^2 \\ &\quad + \lambda_1 b_{v3}u_3^2 - u_3 v_{xxx}(L) - u_3^3/3. \end{aligned}$$

A. Control Design

- When $t \in I_1$, we measure $w([0, Y], t)$ and we choose (u_1, u_3) so that $u_3 = 0$ and

$$\begin{aligned} &\frac{u_1^3}{3} + (a_{w1} + \delta_2 a_{w2} + \lambda_1 a_{w3})u_1^2 + u_1 w_{xxx}(0) \\ &\leq -(\alpha_1 + 2\delta_1)V_1, \end{aligned} \quad (13)$$

for some $\alpha_1 > 0$. Hence, we have

$$\dot{V}_1 \leq -\alpha_1 V_1 \quad \text{and} \quad \dot{V}_2 \leq 2\delta_1 V_2. \quad (14)$$

- When $t \in I_2$, we measure $u([Y, L], t)$ and we choose (u_2, u_3) so that $u_1 = 0$ and

$$\begin{aligned} &-\frac{u_3^3}{3} + (b_{v1} + \delta_2 b_{v2} + \lambda_1 b_{v3})u_3^2 - u_3 v_{xxx}(L) \\ &\leq -(\alpha_2 + 2\delta_1)V_2, \end{aligned} \quad (15)$$

for some $\alpha_2 > 0$. Hence, we obtain

$$\dot{V}_1 \leq 2\delta_1 V_1 \quad \text{and} \quad \dot{V}_2 \leq -\alpha_2 V_2. \quad (16)$$

In the following lemma, we show how to design u_1 and u_3 to satisfy (13) and (15), respectively.

Remark 7: Note that (13) involves $w_{xxx}(0)$, which is not guaranteed to remain bounded. Hence, it is important to design $u_1 := \kappa_1(V_1, w_{xxx}(0))$ with $w_{xxx}(0) \mapsto \kappa_1(V_1, w_{xxx}(0))$ globally bounded. Similarly, (15) involves $v_{xxx}(L)$. Hence, it is important to design $u_3 := \kappa_3(V_2, v_{xxx}(L))$ with $v_{xxx}(L) \mapsto \kappa_3(V_2, v_{xxx}(L))$ globally bounded. •

Lemma 6: To satisfy (13), we take

$$u_1 := \kappa_1(\cdot) := \begin{cases} -\text{sign}(w_{xxx}(0))V_1 & \text{if } |w_{xxx}(0)| \geq l_1(V_1) \\ k_1(V_1) & \text{otherwise,} \end{cases}$$

where k_1 is such that

$$\begin{aligned} &k_1^3 + 3(a_{w1} + \delta_2 a_{w2} + \lambda_1 a_{w3} + 1)k_1^2 + 3l_1(V_1)^2 \\ &\leq -3(\alpha_1 + 2\delta_1)V_1, \end{aligned} \quad (17)$$

and $l_1(V_1) := V_1^2/3 + (a_{w1} + \delta_2 a_{w2})V_1 + (\alpha_1 + 2\delta_1)$.

Similarly, to satisfy (15), we take

$$u_3 := \kappa_3(\cdot) := \begin{cases} -\text{sign}(v_{xxx}(L))V_2 & \text{if } |v_{xxx}(L)| \geq l_3(V_2) \\ k_3(V_2) & \text{otherwise,} \end{cases}$$

where k_3 is such that

$$\begin{aligned} &k_3^3 + 3(b_{v1} + \delta_2 b_{v2} + \lambda_1 b_{v3} + 1)k_3^2 + 3l_3(V_2)^2 \\ &\leq -3(\alpha_2 + 2\delta_1)V_2, \end{aligned} \quad (18)$$

and $l_3(V_2) := V_2^2/3 + (b_{v1} + \delta_2 b_{v2})V_2 + (\alpha_2 + 2\delta_1)$. □

Remark 8: Note that (17) and (18) always admit a solution k_1 and k_3 function of V_1 and V_2 , respectively. For example, one can take k_1 as a second-order polynomial of V_1 with strictly negative coefficients that are sufficiently large. •

B. \mathcal{L}^2 Exponential Stability

Let Σ_1^{cl} be the system obtained from Σ_1 when (3) holds, $u_2 = 0$, $(u_1, u_3) = (\kappa_1, 0)$ on I_1 , and $(u_1, u_3) = (0, \kappa_3)$ on I_2 . In this section, we show how to find positive constants α_1 and α_2 such that the trivial solution to Σ_1^{cl} is \mathcal{L}^2 globally exponentially stable.

Definition 3: The trivial solution to Σ_1^{cl} is \mathcal{L}^2 -GES if there exist $\gamma, \kappa > 0$ such that, for each solution u to Σ_1^{cl} , we have $\|u(t_o + t)\| \leq \kappa e^{-\gamma t} \|u(t_o)\|$ for all $(t_o, t) \in \mathbb{R}_{\geq 0} \times \mathbb{R}_{\geq 0}$. • According to the proposed approach, we establish the \mathcal{L}^2 -GES for Σ_1^{cl} by showing, for an appropriate choice of (α_1, α_2) , GES of the origin for the switched system

$$\Sigma_3 : \begin{cases} \dot{V}_1 = -\alpha_1 V_1 \\ \dot{V}_2 = 2\delta_1 V_2 \end{cases} \quad t \in I_1, \\ \begin{cases} \dot{V}_1 = 2\delta_1 V_1 \\ \dot{V}_2 = -\alpha_2 V_2 \end{cases} \quad t \in I_2, \quad (V_1, V_2) \in \mathbb{R}_{\geq 0} \times \mathbb{R}_{\geq 0}.$$

Theorem 1: Consider system Σ_1 under the sensing scenario in Section II-A and the boundary conditions in (3). Assume that, for some $\bar{T}_1, \bar{T}_2 > 0$, Assumption 1 holds. Furthermore, we let $u_2 = 0$, $(u_1, u_3) = (\kappa_1, 0)$ on I_1 , and $(u_1, u_3) = (0, \kappa_3)$ on I_2 , where κ_1, κ_3 come from Lemma 6. Then, for (α_1, α_2) satisfying

$$\alpha_1 > \frac{2\delta_2 \bar{T}_2}{\bar{T}_1} \quad \text{and} \quad \alpha_2 > \frac{2\delta_2 \bar{T}_1}{\bar{T}_2}, \quad (19)$$

the trivial solution to the closed-loop system is \mathcal{L}^2 -GES. \square

V. MAIN RESULT 2 :

ACTIVE CONTROL AT $x = 0$ AND $x = Y$

In this section, we let $u_3 = 0$. As a result, (12) reduces to

$$\begin{aligned} \dot{V}_1 &\leq 2\delta_1 V_1 - \frac{u_2^3}{3} - u_2 w_{xxx}(Y) + \frac{u_1^3}{3} + u_1 w_{xxx}(0) \\ &\quad + C_{w1}(u_1, u_2) + C_{w2}(u_1, u_2)\delta_2 + C_{w3}(u_1, u_2)\lambda_1, \\ \dot{V}_2 &\leq 2\delta_1 V_2 + \frac{u_2^3}{3} + u_2 v_{xxx}(Y) \\ &\quad + C_{v1}(u_2, 0) + C_{v2}(u_2, 0)\delta_2 + C_{v3}(u_2, 0)\lambda_1. \end{aligned} \quad (20)$$

A. Control Design

When $t \in I_1$, we set $u_2 = 0$ and choose u_1 such that (13) holds. To obtain

$$\dot{V}_1 \leq -\alpha_1 V_1 \quad \text{and} \quad \dot{V}_2 \leq 2\delta_1 V_2. \quad (21)$$

When $t \in I_2$, we note that the first inequality in (20) involves the term $[u_1 w_{xxx}(0)]$. Note that $w_{xxx}(0)$ is unknown on the interval I_2 . Hence, before designing (u_1, u_2) , we introduce the following lemma.

Lemma 7: Consider Σ_2 under (1) and (2). Then

$$w_{xxx}(0) = w_{xxx}(Y) + \frac{u_2^2 - u_1^2}{2} + \dot{\gamma},$$

where $\gamma := \left(\int_0^Y w(x) dx\right)$. \square

Using Lemma 7, (20) becomes

$$\begin{aligned} \dot{V}_1 &\leq -\frac{u_2^3}{3} + (u_1 - u_2)w_{xxx}(Y) - \frac{u_1^3}{6} \\ &\quad + C_{w1}(u_1, u_2) + \frac{u_1 u_2^2}{2} + 2\delta_1 V_1 + \delta_2 C_{w2}(u_1, u_2) \\ &\quad + \lambda_1 C_{w3}(u_1, u_2) + u_1 \dot{\gamma}, \\ \dot{V}_2 &\leq \frac{u_2^3}{3} + C_{v2}(u_2, 0)\delta_2 + C_{v3}(u_2, 0)\lambda_1 \\ &\quad + C_{v1}(u_2, 0) + u_2 v_{xxx}(Y) + 2\delta_1 V_2. \end{aligned} \quad (22)$$

Now, we introduce constants $B > 0$ and $C > 0$ such that

$$\begin{aligned} B u_2^2 &:= C_{v3}(u_2, 0)\lambda_1 + C_{v2}(u_2, 0)\delta_2 + C_{v2}(u_2, 0), \\ C u_2^2 &:= C_{w1}(u_2, u_2) + \delta_2 C_{w2}(u_2, u_2) + \lambda_1 C_{w3}(u_2, u_2). \end{aligned}$$

Hence, on the interval I_2 , we propose to choose (u_1, u_2) such that $u_1 = u_2$ and

$$\frac{u_2^3}{3} + B u_2^2 + u_2 v_{xxx}(Y) \leq -\alpha_2 V_2^3. \quad (23)$$

As a consequence, we obtain, for almost all $t \in I_2$,

$$\begin{aligned} \dot{V}_1 &\leq 2\delta_1 V_1 + u_2 \dot{\gamma} + C u_2^2 \\ \dot{V}_2 &\leq -\alpha_2 V_2^3 + 2\delta_1 V_2. \end{aligned} \quad (24)$$

Now, we propose to find $\kappa_2 \left(\alpha_2^{\frac{1}{3}} V_2, v_{xxx}(Y)\right)$ such that, when $u_2 = \kappa_2 \left(\alpha_2^{\frac{1}{3}} V_2, v_{xxx}(Y)\right)$, both (23) and the following property hold.

Property 1: There exists $P > 0$ such that

$$\left| \kappa_2 \left(\alpha_2^{\frac{1}{3}} V_2, v_{xxx}(Y)\right) \right| \leq P \alpha_2^{\frac{1}{3}} V_2 \quad \forall v_{xxx}(Y) \in \mathbb{R}, \quad (25)$$

and, for almost all $t \geq t_o \geq 0$, we have

$$\frac{d}{dt} \kappa_2 \left(\alpha_2^{\frac{1}{3}} V_2(t_o), v_{xxx}(Y, t)\right) = 0. \quad (26)$$

Lemma 8: Property 1 and (23) hold for

$$\kappa_2(\cdot) := \begin{cases} -\text{sign}(v_{xxx}(Y)) \alpha_2^{\frac{1}{3}} V_2 & \text{if } |v_{xxx}(Y)| \geq 2\alpha_2^{\frac{2}{3}} V_2^2 \\ -\beta \alpha_2^{\frac{1}{3}} V_2 & \text{otherwise,} \end{cases}$$

where $\beta > 0$ is chosen so that $-\beta^3 + 6\beta + 3 \leq 0$. \square

B. \mathcal{L}^2 -Stability Analysis

Let Σ_1^{cl} be the system obtained from Σ_1 when (3) holds, $u_3 = u_2 = 0$, $u_1 = \kappa_1$ on I_1 , and $u_3 = 0$ and $u_1 = u_2 = \kappa_2 \left(\alpha_2^{\frac{1}{3}} V_2(t_{2k}), v_{xxx}(Y)\right)$ on each interval $[t_{2k}, t_{2k+1}] \subset I_2$. Recall that, by definition of κ_1 and κ_2 , Σ_1^{cl} includes (α_1, α_2) as free design parameters. Next, inspired by [30], we introduce some useful \mathcal{L}^2 -semi-global and \mathcal{L}^2 -practical-stability notions.

The trivial solution to Σ_1^{cl} is \mathcal{L}^2 practically semi-globally attractive (\mathcal{L}^2 -PSGA) if, for each $\beta > \epsilon > 0$, there exists $\alpha_2^* > 0$ such that, for each $\alpha_2 \geq \alpha_2^*$, there exists α_1^* such that, for each $\alpha_1 \geq \alpha_1^*$, every solution u to Σ_1^{cl} with $\|u(t_o)\| \leq \beta$, there exists $T > 0$ such that $\|u(t_o + T)\| \leq \epsilon$.

Σ_1^{cl} is \mathcal{L}^2 semi-globally bounded (\mathcal{L}^2 -SGB) if, for each $\beta > 0$, there exists $\gamma > 0$ and $\alpha_2^* > 0$ such that, for each $\alpha_2 \geq \alpha_2^*$, there exists α_1^* such that, for each $\alpha_1 \geq \alpha_1^*$, we have, for every solution u to Σ_1^{cl} with $\|u(t_o)\| \leq \beta$, $\|u(t_o + t)\| \leq \gamma$ for all $t \geq 0$. Furthermore, Σ_1^{cl} is \mathcal{L}^2 semi-globally ultimately bounded (\mathcal{L}^2 -SGUB) if there exists $\gamma > 0$ such that, for each $\beta > 0$, there exists $\alpha_2^* > 0$ such that, for each $\alpha_2 \geq \alpha_2^*$, there exists α_1^* such that, for each $\alpha_1 \geq \alpha_1^*$, for every solution u to Σ_1^{cl} with $\|u(t_o)\| \leq \beta$, there exists $T > 0$ such that $\|u(t_o + t)\| \leq \gamma$ for all $t \geq T$.

The trivial solution to Σ_1^{cl} is \mathcal{L}^2 practically stable (\mathcal{L}^2 -PS) if there exists $\kappa \in \mathcal{K}$ such that, for each $\epsilon > 0$, there exists $\alpha_2^* > 0$ such that, for each $\alpha_2 \geq \alpha_2^*$, there exists α_1^* such that, for each $\alpha_1 \geq \alpha_1^*$, we have $\|u(t)\| \leq \kappa(\|u(t_o)\|) + \epsilon$ for $t \geq t_o$.

Remark 9: Note that to guarantee \mathcal{L}_2 -practical semi-global asymptotic stability, we need to guarantee \mathcal{L}_2 -PSGA, \mathcal{L}_2 -SGB, and \mathcal{L}_2 -PS. However, in our case, we will be able to show only \mathcal{L}_2 -PSGA, \mathcal{L}_2 -SGB, and \mathcal{L}_2 -SGUB. •

Theorem 2: Consider system Σ_1 under the sensing scenario in Section II-A and the boundary conditions in (3). Assume that, for some $\bar{T}_1, \bar{T}_2 > 0$, Assumption 1 holds. Furthermore, we let $u_3 = u_2 = 0$, $u_1 = \kappa_1$ on I_1 , and $u_1 = u_2 = \kappa_2 \left(\alpha_2^{\frac{1}{2}} V_2(t_{2k}), v_{xxx}(Y) \right)$ on each interval $[t_{2k}, t_{2k+1}] \subset I_2$ and $u_3 = 0$ on I_2 , where κ_1, κ_2 come from Lemmas 6 and 8, respectively. Then, the trivial solution to Σ_1^{cl} is \mathcal{L}_2 -PSGA and Σ_1^{cl} is \mathcal{L}^2 -SGB and \mathcal{L}^2 -SGUB. □

VI. CONCLUSIONS

This paper proposed two boundary controllers to stabilize the origin of the nonlinear Kuramoto-Sivashinsky equation, under intermittent measurements. Using the first controller, we are able to provide stronger stability properties compared to the second one. In future work, we would like to improve the stability properties of the second controller and consider the case where the coefficient λ_1 is unknown.

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REFERENCES

- [1] Y. Kuramoto, "Instability and turbulence of wavefronts in reaction-diffusion systems," *Progress of Theoretical Physics*, vol. 63, no. 6, pp. 1885–1903, 1980.
- [2] A. Hać and L. Liu, "Sensor and actuator location in motion control of flexible structures," *Journal of sound and vibration*, vol. 167, no. 2, pp. 239–261, 1993.
- [3] P. Rouchon, "Quantum systems and control 1," *Revue Africaine de la Recherche en Informatique et Mathématiques Appliquées*, vol. 9, 2008.
- [4] G. Schneider and H. Uecker, *Nonlinear PDEs*, vol. 182. American Mathematical Soc., 2017.
- [5] I. Karafyllis and M. Krstic, *Input-to-state stability for PDEs*. Springer, 2019.
- [6] L. Kocarev, Z. Tasev, and U. Parlitz, "Synchronizing spatiotemporal chaos of partial differential equations," *Physical Review Letters*, vol. 79, no. 1, p. 51, 1997.

- [7] B.-Z. Guo and T. Meng, "Robust error based non-collocated output tracking control for a heat equation," *Automatica*, vol. 114, p. 108818, 2020.
- [8] A. Armaou and P. Christofides, "Nonlinear feedback control of parabolic partial differential equation systems with time-dependent spatial domains," *Journal of mathematical analysis and applications*, vol. 239, no. 1, pp. 124–157, 1999.
- [9] W. Kang and E. Fridman, "Distributed sampled-data control of Kuramoto-Sivashinsky equation," *Automatica*, vol. 95, pp. 514–524, 2018.
- [10] Z. Tasev, L. Kocarev, L. Junge, and U. Parlitz, "Synchronization of Kuramoto-Sivashinsky equations using spatially local coupling," *International Journal of Bifurcation and Chaos*, vol. 10, no. 04, pp. 869–873, 2000.
- [11] A. Khadra, X. Liu, and X. Shen, "Impulsive control and synchronization of spatiotemporal chaos," *Chaos, Solitons & Fractals*, vol. 26, no. 2, pp. 615–636, 2005.
- [12] M. Krstic and A. Smyshlyaev, *Boundary control of PDEs: A course on backstepping designs*. SIAM, 2008.
- [13] M. Krstic and A. Smyshlyaev, "Adaptive boundary control for unstable parabolic PDEs—Part I: Lyapunov design," *IEEE Transactions on Automatic Control*, vol. 53, no. 7, pp. 1575–1591, 2008.
- [14] R. Curtain, "Finite-dimensional compensator design for parabolic distributed systems with point sensors and boundary input," *IEEE Transactions on Automatic Control*, vol. 27, no. 1, pp. 98–104, 1982.
- [15] P. Parmananda, "Generalized synchronization of spatiotemporal chemical chaos," *Physical Review E*, vol. 56, no. 2, p. 1595, 1997.
- [16] L. Junge and U. Parlitz, "Synchronization and control of coupled ginzburg-landau equations using local coupling," *Physical Review E*, vol. 61, no. 4, p. 3736, 2000.
- [17] R. Katz and E. Fridman, "Finite-dimensional control of the Kuramoto-Sivashinsky equation under point measurement and actuation," in *2020 59th IEEE Conference on Decision and Control (CDC)*, pp. 4423–4428, IEEE, 2020.
- [18] K. Toshihiro, "Adaptive stabilization of the Kuramoto-Sivashinsky equation," *International Journal of Systems Science*, vol. 33, no. 3, pp. 175–180, 2002.
- [19] W.-J. Liu and M. Krstić, "Stability enhancement by boundary control in the Kuramoto-Sivashinsky equation," *Nonlinear Analysis: Theory, Methods & Applications*, vol. 43, no. 4, pp. 485–507, 2001.
- [20] R. Sakthivel and H. Ito, "Non-linear robust boundary control of the Kuramoto-Sivashinsky equation," *IMA Journal of Mathematical Control and Information*, vol. 24, no. 1, pp. 47–55, 2007.
- [21] P. Guzmán, S. Marx, and E. Cerpa, "Stabilization of the linear Kuramoto-Sivashinsky equation with a delayed boundary control," *IFAC-PapersOnLine*, vol. 52, no. 2, pp. 70–75, 2019.
- [22] J.-M. Coron and Q. Lü, "Fredholm transform and local rapid stabilization for a Kuramoto-Sivashinsky equation," *Journal of Differential Equations*, vol. 259, no. 8, pp. 3683–3729, 2015.
- [23] W. Zhang, M. S. Branicky, and S. M. Phillips, "Stability of networked control systems," *IEEE control systems magazine*, vol. 21, no. 1, pp. 84–99, 2001.
- [24] Y. Sun, S. Ghantasala, and N. H. El-Farra, "Networked control of spatially distributed processes with sensor-controller communication constraints," in *2009 American Control Conference*, pp. 2489–2494, IEEE, 2009.
- [25] X.-W. Zhang and H.-N. Wu, "Fuzzy stabilization design for semilinear parabolic PDE systems with mobile actuators and sensors," *IEEE Transactions on Fuzzy Systems*, vol. 28, no. 3, pp. 474–486, 2019.
- [26] A. Y. Khapalov, "Observability of parabolic systems with scanning sensors," in *[1992] Proceedings of the 31st IEEE Conference on Decision and Control*, pp. 1311–1312, IEEE, 1992.
- [27] W. Mu, B. Cui, W. Li, and Z. Jiang, "Improving control and estimation for distributed parameter systems utilizing mobile actuator-sensor network," *ISA transactions*, vol. 53, no. 4, pp. 1087–1095, 2014.
- [28] M. A. Demetriou, "Guidance of mobile actuator-plus-sensor networks for improved control and estimation of distributed parameter systems," *IEEE Transactions on Automatic Control*, vol. 55, no. 7, pp. 1570–1584, 2010.
- [29] X.-W. Zhang and H.-N. Wu, "Switching state observer design for semilinear parabolic PDE systems with mobile sensors," *Journal of the Franklin Institute*, vol. 357, no. 2, pp. 1299–1317, 2020.
- [30] A. A. R. Teel, J. Peuteman, and D. Aeyels, "Semi-global practical asymptotic stability and averaging," *Systems & control letters*, vol. 37, no. 5, pp. 329–334, 1999.