

Demonstrating the influence of sediment source in dredged sediment recovery for brick and tile production

Thomas Gillot, Isabelle Cojan, Haurine Frédéric, Poirier Catherine,

Marie-Anne Bruneaux

► To cite this version:

Thomas Gillot, Isabelle Cojan, Haurine Frédéric, Poirier Catherine, Marie-Anne Bruneaux. Demonstrating the influence of sediment source in dredged sediment recovery for brick and tile production. Resources, Conservation and Recycling, 2021, 10.1016/j.resconrec.2021.105653. hal-03595683

HAL Id: hal-03595683 https://hal.science/hal-03595683

Submitted on 24 May 2023 $\,$

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Distributed under a Creative Commons Attribution - NonCommercial 4.0 International License

Version of Record: https://www.sciencedirect.com/science/article/pii/S0921344921002627 Manuscript_d627c5765d97e5bcd2233b3ef15c22ee

1	Demonstrating	the influence of	f sediment	source in	dredged	sediment	recovery	for br	ick

- 2 and tile production
- 3 GILLOT Thomas^{1, 2}, COJAN Isabelle¹, HAURINE Frederic^{1, 3, 4}, POIRIER Catherine³,
- 4 BRUNEAUX Marie-Anne^{3, 5}
- ¹ MINES-ParisTech, PSL University, Geosciences, 35 rue Saint Honoré, 77300
- 6 Fontainebleau, France
- ² presently, MAGMA Caraibes, 309 Lotissement La Caraibe, Case-Pilote 97222, Martinique,
- 8 France
- 9 ³ CTMNC, 17, rue Letellier, 75786 Paris Cedex 15, France
- ⁴ presently, Université Paris-Saclay, CNRS, GEOPS, Orsay, 91405, France
- ⁵ presently, Andra, 1 rue Jean Monnet, 92290 Châtenay- Malabry, France
- 12
- 13 Corresponding author: isabelle.cojan@mines-paristech.fr

14 Abstract

- 15 The most important raw materials for the building industry are natural quarried rocks.
- 16 Preservation of this non-renewable resource needs valorizing products, the vast majority of
- 17 which is currently considered as waste. Among these, dredged sediments have gained much
- 18 attention and should play a key role in non-renewable natural resource preservation.
- 19 The aim of this paper is to achieve a resource-efficient evaluation for the re-use of fine-
- 20 grained dredged sediments in the heavy clay industry by investigating relationship between
- 21 sediment provenance and industrial properties. 86 spot samples from French dam reservoirs

22 and estuaries were studied, focusing on grain-size and mineralogy. Industrial technological 23 tests were performed on 53 samples representative of varied lithological sources. Following 24 PCA analysis, source fingerprinting in four categories is proposed, allowing for direct 25 evaluation of sediment for brick-tile making. Best technological scores, close to industrial values, were obtained for source category (3) mixture of sedimentary, plutonic and 26 27 metamorphic rocks and low scores for two source categories, (1) sedimentary rocks (high 28 carbonate content), (2) plutonic and metamorphic rocks (lack melting compound). Extrusion 29 failed for samples from category (4) plutonic or metamorphic rocks (lack clay minerals). Consistency between PCA fingerprinting categories, MIF (Mineralogical Industrial 30 31 Framework) and technological tests shows that even though the sediment source classification is simplified, it constitutes a reference to predict the recovery of dredged sediment for tile or 32 brick making. Insights from this study can be particularly useful to the heavy clay industry 33 34 managers when making decision regarding the fossil resource preservation by substitution 35 with dredged sediments.

<u>Keywords</u>: dredged sediment recovery; brick and tile production; provenance fingerprinting;
 technological properties; Principal Component Analysis.

38 *1 Introduction*

In a context of sustainable development, waste management has become an important target
in terms of natural resource preservation and environmental issues (Azapagic et al., 2004).
Among the multiple non-hazardous wastes, this paper focuses on fine-grained dredged
sediments that can be recovered by substitution of natural material in tile and brick building
materials (Hamer and Karius, 2002; Agostini et al., 2007; Mezencevova et al., 2012;

Cappuyns et al., 2015). Composition of raw mixtures for ceramic materials has an influence 44 45 on the sintering temperature and final properties of the produced material (Dondi, 2003; Cultrone et al., 2004). Mineralogical studies on fine-grained dredged harbor sediment (Hamer 46 47 and Karius, 2002; Mezencevova et al., 2012; Benyerou et al., 2015) or river material (Manap et al., 2016) have shown that silt carried in suspension can be valuable material for the 48 ceramic industry based on appropriate grain-size distribution and significant content in clay 49 50 minerals combined with quartz and some carbonates (Xu et al., 2014; Cappuyns et al., 2015; 51 Haurine, 2015, Haurine et al., 2016).

Fine-grained sediments silting in dam reservoirs or estuaries are regularly dredged for harbor, 52 53 water resource or maintenance management, and a vast majority is disposed at sea or inland 54 as a waste product. The re-use of dredged sediments in the heavy clay industry as an alternative to fossil sedimentary rocks requires further investigation to provide fingerprint of 55 56 these fine-grained sediment composition with respect to the geology of sediment source. 57 Provenance studies, traditionally focus on mineralogical composition of sand which is easier to analyze with standard petrography techniques (Zuffa, 2013 and references therein). 58 Mineralogy of silt and clay carried in suspension by rivers is determined by X-ray powder-59 diffraction analyses (XRD), composition is generally related to sediment provenance (Klages 60 61 and Hsieh, 1975; Benedetti et al., 2006; Garzanti et al, 2007; Garzanti et al., 2011), it may 62 change along the river course, influenced by sediment dilution or concentration from tributaries, chemical weathering during transport and seasonal input (Walling et al., 1999). 63

The aim of this study is to achieve a resource-efficient evaluation for the recovery of finegrained dredged sediments in the heavy clay industry by investigating relationship between
sediment provenance and industrial properties. Spot sampling of fine-grained sediment was

67	conducted in French dam reservoirs and estuaries, collecting sediments from a large diversity
68	of source rocks and geomorphic contexts. At first broad compositional pattern of surficial
69	sediments is described from two large dam reservoirs, Lake Serre Ponçon (Alps) and Lake
70	Grandval (Massif Central). Then, a resource-efficient evaluation using principal component
71	analysis (PCA) is conducted between provenance, geomorphic context, sediment composition
72	and scores during the technological tests of the heavy clay industry. Finally, consistency
73	between proposed fingerprint categories from PCA, Mineralogical Industrial Framework
74	domains (MIF, Haurine et al., 2016) and technological tests is discussed.

75 2 Setting

Among the numerous dams built along the course of the French rivers and estuaries, we
selected sites fed from great diversity of sediment sources (plutonic, volcanic, metamorphic
and sedimentary rocks) and geomorphic contexts (active mountain range, remains of ancient
volcanoes and chains, sedimentary basins) (Fig. 1).

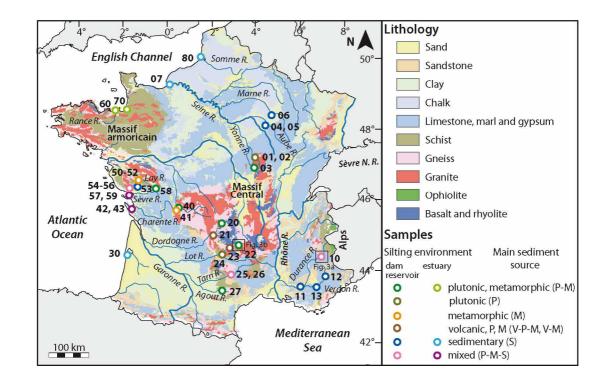
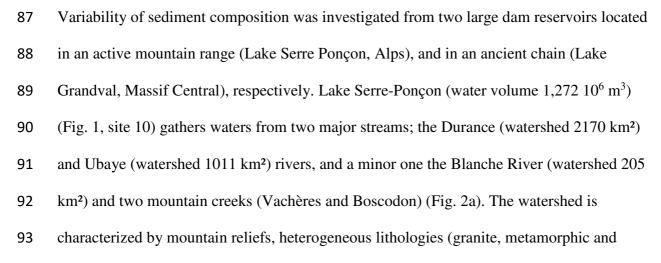


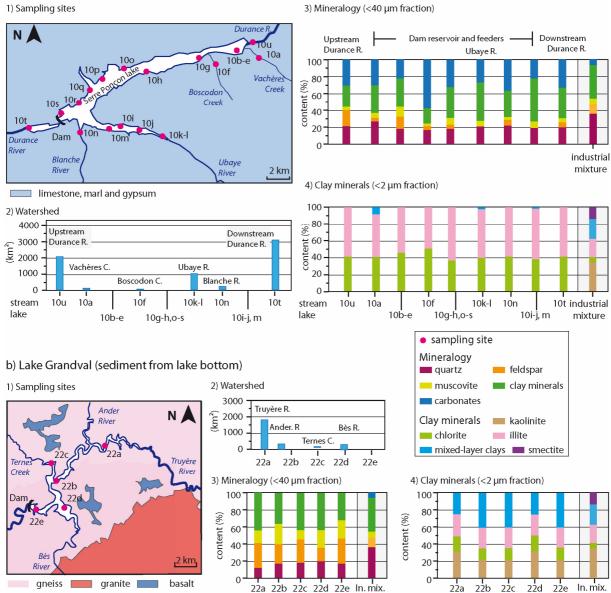
Fig. 1. Site location on the lithological map of France (BRGM, 2008). Sites labeled per river
system and color-coded according to the geology of the dominant source (see supplementary
material 1 for details).



94 sedimentary rocks) and a high erosion rate (Alary, 1998; Colmar et al., 2010). Lake Grandval is five times smaller (water volume 272 10^6 m³) (Fig. 1, site 22). It is fed by the Truyère River 95 (watershed 1782 km²) and minor creeks (L'Ander, watershed 310 km²; and Le Bès, watershed 96 97 283 km²) (Fig. 2b). The watershed corresponds to low mountain reliefs, heterogeneous 98 lithologies (granite, gneiss with some volcanic rocks), the erosion rate is moderate (Colmar et 99 al., 2010). Climate in both watersheds is mountainous with some Mediterranean influence 100 favoring seasonal high peak discharges during which sediment accumulates at the mouth of 101 the feeding rivers forming deltas that prograde into the dam reservoir. Fine-grained sediment 102 accumulates in distal depositional environments fed by suspension.



1) Sampling sites



104

105 Fig. 2. Sediment compositional pattern at the scale of large dam reservoirs: Lake Serre-Ponçon, sampling at intermediate water depth (a); and Lake Grandval, sampling on lake 106 107 bottom (b) (see Fig. 1 for lake location, supplementary materials 3 and 4 for mineralogical composition). 108

109

110 Furthermore, several dam reservoirs and estuaries were selected to sample sediments from varied provenances (Fig. 1). Dam reservoirs fed by sediment sources dominated by plutonic 111 112 rocks (sites 01, 02 and 24) or metamorphic ones (site 41) are located in the northern and 113 western parts of the ancient orogenic chain of the Massif Central and southern border of the relict chain of the Massif Armoricain (sites 50 to 52). Selected dams impounding sediment 114 115 transfer on rivers flowing over plutonic and metamorphic substrates rich in volcanic rocks are 116 located in the Cantal volcanic province of the Massif Central, (sites 21 and 23). Sediment 117 sources comprising metamorphic and plutonic rocks are located north (site 03) and west (sites 118 20, 22, 27 and 40) of the Massif Central, and in the southern part of the Massif Armoricain 119 (site 58). Dam reservoirs collecting sediment originating from the erosion of sedimentary 120 rocks are located in the south-western part of the alpine range (sites 12 and 13), in the Paris 121 basin (sites 04 to 06). Dam reservoir fed by a river flowing over substrates of varied 122 geological lithologies (metamorphic, plutonic, volcanic and sedimentary rocks) are situated on the Durance river in the outer Alpine chain (sites 10 and 11), the Tarn River in the Massif 123 Central (sites 25 and 26) and the Lay River along the southern border of the Massif 124 Armoricain (sites 50 to 52, 54 to 56). 125

Estuaries are located along the English Channel and the Atlantic coast (Fig. 1). To the north,
the Somme (site 80) and the Seine (sites 07) estuaries are fed by fluvial systems dominantly
flowing over sedimentary substrates (marl and limestone, clay and sand). Estuaries along the
north coast of the Massif Armoricain are fed by rivers flowing over mixed plutonic and
metamorphic rocks (sites 60 and 70). Those from the Atlantic coast are fed by rivers flowing
over mixed plutonic, metamorphic and sedimentary rocks (sites 42, 43, 57 and 59). Finally,

the Arcachon bay (site 30) is fed by a river flowing over sedimentary substrate composed ofsandy deposits.

Selected sites provide a variety of sediment sources in different physiographic settings: active
mountain range (Alps - sites 10 to 13), ancient chain (Massif Central - sites 01-03, 20 to 21,
40 to 41), remnant of a chain (Massif Armoricain - sites 50-55, 60 and 70) or sedimentary
basin (Paris basin - sites 04-07, 80; Aquitaine basin - sites 30, 42-43, 53, 56-59).

- 138 *3 Material and Methods*
- 139 *3.1 Material*

140 A total of 86 surficial spot samples were collected from 37 dam reservoirs and estuaries (Fig. 141 1; supplementary material 1). About two third of the samples come from dam reservoirs 142 (69%). Sediment sources are distributed as follow: sedimentary rocks (28%), plutonic and 143 metamorphic rocks (27%), plutonic, metamorphic and sedimentary rocks (28%), plutonic 144 rocks (7%), metamorphic rocks (4%) and dominant volcanic rocks (6%). In addition, 11 145 industrial mixtures from the French heavy clay industry were analyzed to enlarge the 146 industrial dataset built by Haurine (2015), now representative of 90% of the French 147 production over the last 15 years. For reasons of confidentiality, data from industrial mixtures 148 are not detailed in this paper.

Sampling (up to 20 kg per site) was conducted using a spade during low water levels to access the distal part of the reservoir sediment wedge where fine-grained sediment accumulate by silting. Lake Serre Ponçon sediment was sampled at the end of winter when lake level is at minimum, some 10 m below the high level. Lake Grandval and Lake Sarran were sampled

during the maintenance period; the nearly emptied reservoir gave access to lake-bottom
sediment. Similarly, estuaries were sampled at low tide, away from tidal channels. In addition,
four samples of dredged sediments were included, three from the Seine estuary (provided by
Le Havre seaport) and one from the Cadarache settling pond (Durance River - provided by
EDF). Samples were first oven dried at 40°C and stored in a dry room. Analyses were
conducted on samples dried in a forced-air drying oven at 40°C for 4 to 8 days.

159 3.2 Analytical methods

160

3.2.1 Particle size analysis

Dried samples were suspended in an excess of water, mixed to separate particles, and 161 162 separation at 40 µm was obtained by wet sieving. Particle size distribution was determined by 163 dry sieving (fraction > 40 μ m) and by sedimentation with SediGraph 5100 Particle Size Analyser (Micrometrics) (fraction $< 40 \ \mu$ m). A dispersing and deflocculating agent (sodium 164 165 polymetaphosphate, 1%, pH 6.5-7.2) was added to the aqueous suspension. Error is \pm 10%. Results are presented for the particle-size classes used in the heavy clay industry: 0.5, 2.5, 40, 166 200, 500 and >500 µm (supplementary material 2). Particle-size analysis was conducted on 53 167 168 sediment samples, representative of the varied sediment sources and geomorphological contexts (supplementary material 2). Results are plotted on the Winkler diagram (Winkler, 169 170 1954), a ternary plot of three particle size fractions (< 2.5 μ m, 2.5-25 μ m and > 25 μ m) 171 (Supplementary material 2). Domains from the French tile and brick raw materials are also indicated on the ternary plot. 172

173

174

3.2.2 Mineralogical analyses

Mineralogical analyses were conducted on the silt fraction ($< 40 \,\mu$ m). They were carried out 175 via X-ray diffraction (XRD) using PANalytical's X-ray diffractometer (Phillips), CuKa 176 177 radiation. Quantitative mineral analysis of the bulk sample was performed using random 178 powder mounts. EVA software (Bruker DIFFRACPlus 2007) was used for identification and 179 quantitative phase analysis based on scan wavelength (lambda) and the normalized intensity 180 ratio (RIR) method (Chung, 1974), (supplementary material 3). Relative Error is \pm 5%. Following the removal of carbonate by weak acid, particles smaller than 2 μ m were 181 182 separated by sampling the upper 2 cm of the clay suspension after 100 min. Identification of the clay minerals was performed according to the position of the (001) series of basal 183 reflections on three XRD diagrams (air-drying, ethylene-glycol salvation and heating at 184 490 °C for 2 h, Moore and Reynolds, 1997). Identification and relative proportion of clay 185 minerals was performed using recommended protocol by Kahle et al. (2002) (supplementary 186 187 material 4). Error estimate is $\pm 5\%$.

Mineralogical analyses were performed on the 86 samples (supplementary materials 3 and 4)
to investigate the compositional pattern within dam reservoirs (Lake Serre Ponçon, 21
samples, Fig. 2a, Lake Grandval, 5 samples, Fig. 2b); and to compare silting sites fed by
different lithological sources (Fig. 3a, b).

192 *3.2.3 Extrusion*

A representative subsample of 8 kg of dried sediment was gently crushed to eliminate the
aggregates that formed during the drying. The loose sediment was then weighted, mixed with
the suitable quantity of water to obtain a plastic paste with extrusion shaping capacity (for
shaping water content see supplementary material 6). For each sample, several specimen bars
were extruded to conduct tests at the laboratory scale (10 x 2 x 2 cm³ for shrinkage and water

198	absorption measurement, and $13 \times 2.5 \times 1 \text{ cm}^3$ for bending strength test) (supplementary
199	material 5). The plastic paste was weighted to evaluate the proportion of water in the paste
200	(water shaping). Raw specimen bar plasticity was appraised in a semi-quantitative way using
201	an index ranging from poor, fair, good, very good (plasticity raw) (supplementary material 6).

202

203

3.2.4 Technological tests

Technological tests were performed on the 24 successfully extruded samples (i.e. with a
suitable plasticity) (Fig. 4, 3c, supplementary material 5, 6 and 7). Extruded specimen bars
dedicated to the determination of the drying behavior were dried at room temperature for
24 h. During this period, the drying behavior was measured with a barrelatograph (Adamel),
which traces the Bigot's curve, representing the humidity in percentage of the dry weight (and
thus the moisture loss) as a function of the longitudinal shrinkage in percentage of the dry

211 Specimen bars dedicated to the study of the characteristics of the material after firing (water 212 absorption, aspect changes, and mechanical resistance, i.e. flexural strength) were dried at room temperature for one week. Then, they were placed for 48 h at 105 °C in ovens to 213 214 complete drying, before being fired. The firing cycle consisted in a slow heating gradient of 100° C/h followed by a 2 h steady stage at maximum temperature (50 °C steps from 850 to 215 216 1150 °C), before cooling. Tests were only conducted on specimen bars fired at 950 °C, 217 average temperature of industrial kiln between that of bricks (Johari et al., 2010) and tiles (Cultrone et al., 2004). For each sample, a visual inspection of the fired specimen bar at 950 218 219 °C evaluated the bar alteration during the firing process by comparison with the crude

specimen bar: occurrences of cracks, scum, lime blowing, shape deformation (shape 950)
(supplementary material 5). Finally, flexural strength was investigated through 3-points
flexural bending tests (press LFPlus– Lloyd Instruments LTD- 1KN) on unfired (F. strength
dry) and fired at 950 °C (F. strength 950) specimen bars.

224

3.3 PCA analysis

225 Identification of indicator minerals from sampled sediments can help trace related sediment 226 source; identify sediment with the most appropriate properties for a use by the heavy clay 227 industry. With this scope, we carried out Principal Component Analysis (PCA) with XLStat 228 software, three dataset including sediment and industrial mixtures were considered: 229 mineralogy, clay minerals, and technical properties. Loading plot, scree plot and projection of 230 observations on the first two components (F1 vs. F2) are given in Fig. 3. Eigenvectors, factor 231 loadings for each component are given in supplementary material 8. Plot of the samples on F1 232 vs. F2 was coded according to the geology of the dominant sediment source and the results of 233 the extrusion process (Fig. 3, observations).

234 4 Results

235

4.1 Particle-size distribution

Particle-size analysis of the 53 samples representative of the varied sediment sources
showed that they correspond to silt (supplementary material 2). Half of the samples are
medium to fine silt with less than 5% of particles larger than 200 µm. Sediments showing a
poor sorting (30 to 50% of particles larger than 200 µm) correspond to 25% of the samples.
Plot of the particle size distribution on the Winkler diagram (Winkler, 1954) shows that most

of the samples fall within or close to the tile hollow brick or solid brick domains
(supplementary material 2). Samples with more than 70% of large particles (>25 µm) are
from dam reservoirs (plutonic and metamorphic sources); and those with less than 10% are
from dam reservoirs and estuaries (mainly mixed sources). Some contain a high percentage (>
60%) of particles between 2.5-25 µm, they were collected in dam reservoirs.

Particle-size distributions of industrial materials – i.e. crushed sedimentary rocks extracted
from quarries - are distributed between the three industrial domains (supplementary material
2). Those of industrial mixtures cluster within the respective industrial domains, industrial
mixtures for brick production contain slightly more coarse-grained particles than those
dedicated to tiles.

251

4.2 Mineralogical composition

252

253

4.2.1 Compositional pattern at the scale of a dam reservoir – Lake Serre Ponçon and Lake Grandval

254 In Lake Serre Ponçon, the average mineralogical composition of the silt fraction (Fig. 2a) comprises carbonate (29%), quartz (19%), and clay minerals (36%). Carbonate content 255 (dominantly calcite) shows the highest variability ($\sigma = 13$). Carbonates in the upstream reach 256 257 (30%) and lacustrine delta of the Durance (22%) are present in fairly similar proportion than 258 in the Ubaye River sediments (28%). The largest carbonate content is observed in the 259 Boscodon (58%) and Blanche (36%) delta sediments and close by beaches (36%). 260 Downstream of the Serre-Ponçon dam, the carbonate content (30%) of the Durance sediment 261 is very similar to that of the upstream Durance or Ubaye sediments, reflecting the major 262 contribution from these two streams draining large basins. Clay minerals and non-expandable

clay mineral chlorite, muscovite, quartz and feldspar contents are less variable, fluctuations ($\sigma < 6\%$) are within the error range. The average clay mineral assemblages are composed of illite (60%) and chlorite (40%) (Fig. 2a). Kaolinite is present in the upstream Durance delta samples (20%) resulting in lower illite (50%) and chlorite (30%) contents. Mixed layers (I/S) were identified in the Vachère creek sediment (10%).

268 In Lake Grandval, the average composition of lake-bottom sediment is dominated by clay minerals (40%), feldspars (24%), muscovite (19%), quartz (17%) (Fig. 2b). Fluctuations are 269 270 within the error range ($\sigma \le 7$). Clay mineral content shows the highest variability: from 38% in the proximal sediments of the Truvères River and Ternes Creek, to 20% in the distal lake 271 272 deposits. The average clay mineral association comprises illite and mixed-layer clays 273 (illite/smectite and chlorite/smectite) in equal proportions (30%), then kaolinite (20%) and chlorite (20%) (Fig. 2b). No smectite was identified. Mixed-layer clays are present in lower 274 275 proportion in the proximal delta sediment (25%) than in the distal ones (40%).

276

4.2.2 Sediments

Sediments are composed of a limited number of minerals, but with contrasted proportions. Sediments comprise quartz (~ 30%) in association with K-feldpars (10 to 40%), clay minerals (25 to 55%), muscovite (<10%) and calcite (0 to 35%) (supplementary material 3). Clay mineral assemblages are composed of kaolinite (25 to 45%), illite (15 to 40%), chlorite (0 to 20%), and mixed-layer clays (0 to 40%); smectite (5 to 35%) is present in less than 25% of the samples (supplementary material 4). Other minerals - albite, microcline and dolomite – are generally present in very low proportion (\leq 5%). In the following, albite and microcline are

included in the feldspar group with K-feldspars; and dolomite in the carbonate group withcalcite.

286

4.2.3 Industrial mixtures

Mean composition of industrial mixtures is dominated by clay minerals (39%) and quartz
(35%) associated to feldspar (10%), muscovite (7%) and calcite (6%). Clay mineral
assemblages comprise kaolinite (34%), mixed-layer clays (24%), illite (22%), smectite (14%)
and chlorite (6%).

291 4.3 Minerals as provenance indicators of sediments

292 The PCA results of the mineralogical associations of the sediments and industrial mixtures are

293 presented in Figure 3a, b. In this study we only considered the first two eigenvalues,

accounting for 61% of the total variance of the mineralogy dataset (Fig. 3a); and 74% of the

clay mineral dataset (Fig. 3b).

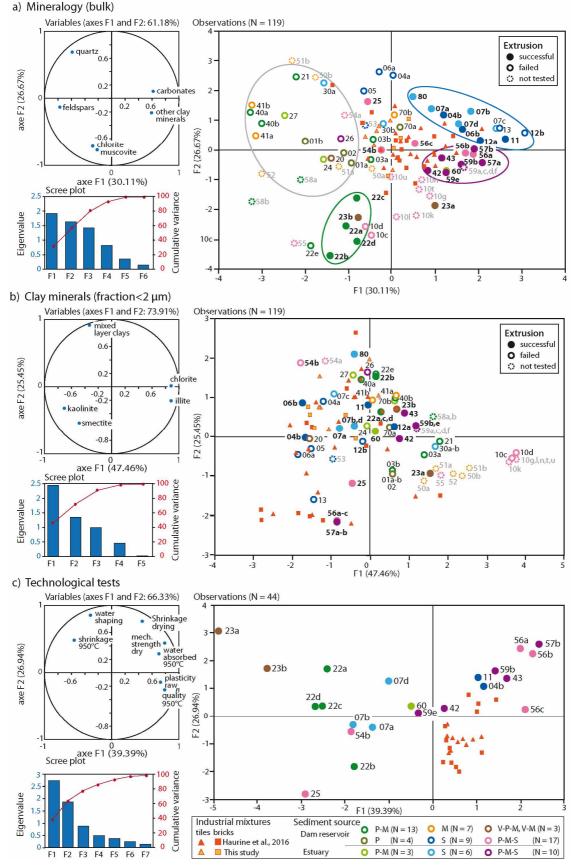




Fig. 3. PCA results from sediments and industrial mixtures (detailed results in supplementarymaterial 8).

299

300 In the mineralogical analysis, 32% of the total variance is captured by the first principal 301 component (F1) whereas the second component (F2) captures 29% (Fig. 3a). Variable plot 302 and associated factor loadings on F1 vs. F2 axes show that the first axis (F1) mostly exhibits 303 the opposition between the clay mineral and carbonate variables, and the feldspar and quartz 304 variables. The second component (F2) shows that the chlorite and muscovite variables are 305 coupled and negatively correlated to the quartz variable. Plot of the samples (observations) on 306 F1 vs. F2 shows that F1 allows a separation between the sediment sources dominated by 307 sedimentary (S sources), a mixture of plutonic, metamorphic and sedimentary rocks (P-M-S 308 sources), mixed plutonic-metamorphic-(volcanic) rocks (P-M-(V) sources) and plutonic (P 309 source) or metamorphic (M source) rocks. The second component F2 allows a fairly good 310 separation between the S and M sources, and those dominated by P, P-M-(V) and P-M-S 311 rocks. Four main sample clusters are identified in relation to the sediment provenance: 1) S 312 sources (F1, F2 positive values), 2) P-M-S sources (F1 positive and F2 negative values), 3) P-313 M-(V) sources (F1 and F2 negative values), and 4) M sources and some samples from P-M sources (F1 negative and F2 positive values). Industrial mixtures are mainly clustered in the 314 315 middle of the score plot with a slight distribution towards the right side of F1 and upper side 316 of F2.

In the clay mineral analysis, 39% of the total variance is captured by the first principal
component (F1) and 31% by the second one (F2) (Fig. 3b). Variable plot and associated factor

loadings on F1 vs. F2 axes show that the chlorite and illite variables are coupled, and 319 320 negatively correlated to the kaolinite and smectite variables (component F1). The second 321 component (F2) shows that the mixed-layer clay variable is negatively correlated to the 322 smectite variable. Plot of the samples (observations) on F1 vs. F2 shows that F1 allows a 323 slight separation between the sediment sources dominated by sedimentary rocks (S sources) 324 and the other sources (P, M, P-M-(V) and P-M-S sources). The second component F2 also 325 allows a slight separation between the sediment sources dominated by S sources or P source 326 or P-M-(V) sources, and those corresponding to M source, and P-M-S sources, in fluvial dam 327 reservoirs. Samples from coastal sites fed by P-M-S sources are scattered over the plot. 328 Despite some overlapping, it is possible to identify three main sample groups for the fluvial 329 samples: 1) S sources (F1 negative values); 2) P, P-M-(V) sources (F1, F2 positive or slightly 330 negative values); 3) M sources and P-M-S sources (F1 positive and F2 negative values). 331 Industrial mixtures are scattered on the left side of the score plot.

332

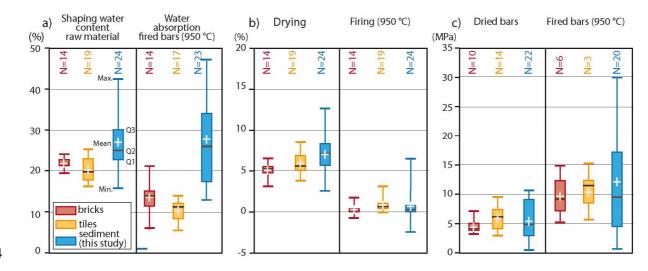
4.4 Technological tests

333 Extrusion success rate (24 samples out of 53) is very high for samples that plot within the tile 334 domain or show a lower content in particles larger than 25 µm. It is lower for samples that 335 plot within the brick domain (50%). Finally samples plotted within the solid brick domain or 336 with more than 50% of particles between 2.5 - 25 μ m or >25 μ m could not be extruded (supplementary material 2). Half of the specimen bars (12 samples) had excellent plasticity, 337 338 an even shape, sharp edges and a smooth surface (sample 22a presents some cracks). More than half of the specimen bars with a medium plasticity (7 samples) presents irregular shapes 339 340 (samples 23a, 23b) or cracks along the edges (samples 22a, 22d). Specimen bars with low

plasticity show either a rough surface (samples 07b, 07d), an irregular shape (sample, 80), or

342 cracks along the edges (sample 25).

343



344

Fig. 4. Box plot of technological tests of sediments and industrial mixtures: affinity with
water (a), shrinkage (b) and mechanical strength (bending test) (c) (see supplementary
materials 6, 7 for detailed results).

Results of the technological tests conducted on the specimen bars from sediment and 348 industrial mixtures are presented together on Figure 4. The amount of water needed for 349 350 shaping the raw material from the sediment samples shows a large dispersion (15 to 42%), far larger than that observed from the industrial mixtures (16 to 26%) (Fig. 4a), resulting in 351 352 median (25%) and mean (27%) values higher than those of the industrial mixtures (21%) 353 bricks, 20% tiles). Shrinkage during drying shows similar trends (Fig. 4b), minimum values 354 (around 2%) are comparable to the industrial ones (bricks 4%, tiles 2%), maximum ones 355 (13%) are nearly two times larger (bricks 6.5%, tiles 7%). Mean values of sediment bars (15%) are also higher than those from the brick (5%) or tile (7%). Data from the bending 356

mechanical strength test on dried bars indicate a larger dispersion for the sediment values than
the industrial mixture ones, mean and median values are quite comparable for all materials
(sediment 5MPa, bricks 4 MPa, and tiles 6 MPa) (Fig. 4c).

360 Examination of the fired bars showed that more than half of the sediment bars of excellent to 361 good quality kept their original shape (supplementary material 5 and 6). Several fired bars of good quality present some defects developed during firing such as deformation (samples 57a, 362 363 59b), cracks (samples 12a, 23a, 54b), lime blowing (samples 04b, 42), and deformation in association to some lime blowing (samples 06b, 07a, 07b). Lime blowing can be easily 364 eliminated by immersion in slightly acidic water after firing, a process that is used in the 365 366 firing industry (Kornmann, 2005). One sample is of medium quality with soluble salts 367 efflorescence (80).

368 Data from water absorption of sediment specimen bars after firing at 950 °C show a large 369 dispersion (12 to 47%), mean values (around 37%), higher than those of the industrial 370 mixtures (bricks 13%, tiles 11%) (Fig. 4a). Mean values of shrinkage associated to firing 371 (0.9%) are very close of those obtained from the industrial mixtures (bricks 0.5%, tiles 0.7%) 372 with a good overlap (80% of the sediment data fall within the industrial values) (Fig. 4b). 373 Results from mechanical strength tests on fired bars are in the range of the industrial values with a larger dispersion (Fig. 4c). Mean values from fired sediment bars (around 13 MPa) are 374 375 slightly higher than those from the industrial mixtures (around 10 MPa).

PCA results of the technological tests of the sediment samples and industrial mixtures are
presented in Figure 3c. The first principal component (F1) captures 39% of the total variance
whereas the second component (F2) captures 27% Variable plot and associated factor

loadings on F1 vs. F2 axes show that the first axis (F1) mostly exhibits that plasticity of 379 380 extruded material (plasticity raw), fired specimen bar quality (quality 950 °C) and water 381 absorption after firing at 950 °C (water absorbed 950 °C) variables are coupled. The second 382 component (F2) shows a high loading factor for the water shaping variable. Plot of the 383 samples (Fig. 3c, observations) on F1 vs. F2 shows that F1 allows a separation between the 384 sediment sources dominated by P-M-S rocks (fluvial and coastal sites) and those by P-M-(V) rocks. Samples from S sources are scattered along F1. No specific distribution is observed 385 386 along the second component F2. It is possible to identify two main sample clusters: the first 387 one contains samples from P-M-S sources (F1, F2 positive values), the second one corresponds to samples from P-M-(V) sources (F1 negative and F2 positive values). Industrial 388 389 mixtures are mainly clustered in the lower right-hand of the score plot (F1 positive values, F2 390 negative to slightly positive values).

391 *5 Discussion*

392

5.1 *Representativeness of spot sediment samples*

Particle-size distribution of spot samples in environment dominated by silting processes
shows some variability partly controlled by external parameters (erosion process, hydrological
regime) and internal ones (geometry of the water body and the sediment wedge) (Lane et al.,
2019; Loizeau et al., 2012; Valero-Garcés et al., 1999). Low variability at the scale of a dam
reservoir or estuary is attributed to efficient particle sorting such as series of dam along the
river or tidal currents in estuaries (Bertin et al., 2005).

399 Sediment composition - mineralogy and clay minerals does not vary significantly at the scale

400 of a dam reservoir or estuary. Changes in proportion are larger for minerals than clay
 22

401 minerals; this is likely to be attributed to the lower dependence of the clay minerals to the
402 sampling site during silting. Sediment composition may be locally influenced by the input
403 from tributaries draining areas with distinct substrates and by calcite precipitation that may
404 occur in the lakes during summer (Filippi et al., 1998).

Despite their limitations, results of the spot sediment samples serve to demonstrate the
potential of the fingerprinting approach in establishing composition patterns - mineralogy and
clay minerals - from silted sediment in water bodies fed from a diversity of sediment sources.

408

5.2 Sediment source fingerprinting

In this study, attention focused on the <40 μm sediment fraction with the objective of the
recovery of dredged sediments, as full or partial substitution of fossil resource in the heavy
clay industry. Although particle-size distribution and proportion of plastic clays play a
significant role in the extrusion process, sediment composition is also crucial. Thus, extrusion
process failed on 52% of the sediments with particle-size distribution similar to those of the
industrial domains on the Winkler diagram (supplementary material 2).

Provenance fingerprinting method is based on sediment mineralogical composition. The multivariate statistical analysis (PCA) is supportive in predicting the potential of sediment for the heavy clay industry based on five broad provenances (S, P, M, P-M-(V), P-M-S). Four groups of sediment sources have been categorized according to the sample clustering in the principal component F1-F2 plot (Fig. 3).

420 The first category shows the fingerprint of particles produced by the erosion of sedimentary

421 rocks (S source). Composition varies widely between carbonate and siliciclastic sources, but

422 is dominated by quartz (20 to 70%), carbonates (20 to 60%) and clay minerals (5 to 40%).

423 Clay mineral assemblages comprise mixed-layer clays and kaolinite, with around 10% of 424 smectite. This group (despite being projected in the hollow brick domain on the Winkler 425 diagram) had poor technological results such as high water absorption and low shrinkage after 426 firing certainly because of carbonate decomposition between 700-900 °C observed on the 427 DTA/GTA diagrams, the loss of weight and the endothermic specific peaks of magnesium or 428 calcium carbonates decomposition (Haurine; 2015), or high quartz content associated to a low 429 clay mineral one (siliciclastic source).

430 The second category shows the fingerprint of detritus produced by the weathering of plutonic, 431 metamorphic and/or volcanic rocks of ancient orogen (P, M, P-M-(V) sources). Composition 432 consists of silicates (60 to 80% - quartz, feldspars, mica and chlorite) and clay minerals (20 433 and 40%). They include a large content of mixed-layer clays associated to chlorite and illite. This group had also poor technological results despite particle-size distribution falling within 434 435 the brick and solid brick domains. The need of high quantity of water to be extruded without a 436 high drying shrinkage, high water absorption et low mechanical strength at 950°C are put in 437 relation to a lack of melting compounds like soda or potassic feldspars.

438 The third category corresponds to the fingerprint of the erosion of basement and sedimentary 439 cover of active or ancient orogen (P-M-S source). Composition comprises relatively high percentages of clay minerals (40 to 60%) associated to quartz (20 to 50%) and low amount of 440 441 carbonates (10-20%) and feldspars and mica (10 to 30%). Clay mineral assemblages are quite 442 dispersed, mainly consisting of mixed-layer clay and smectite in association with some 443 chlorite and illite. High smectite content (35%) is observed in some samples. Best results for the technological tests were obtained for this group of particle-size distribution mainly 444 445 characterized by a low content in particles > $25 \,\mu$ m. High mechanical strength on dried and

fired samples, poor firing shrinkage but high drying shrinkage (that could be problematic for
drying) are attributed to the smectite content and the presence of diatoms in the estuary
sediments (Paulmier, 1994), these are mechanically resistant, with a high porosity and without
transformation or decomposition during firing (Escalera et al., 2015).

The fourth one is composed of sediments from P, M and P-M-(V) sources that could not be extruded. Composition is dominated by quartz and feldspars (60 to 100%), no specific pattern is observed for the clay mineral association. Extrusion results may have also been influenced by the particle-size distribution, mostly with a large amount of medium (2.5 to 25 μ m) or coarse grained particles (> 25 μ m), certainly because of a lack of clay minerals that permits sliding and cohesion between particles.

456 Mineral association reflects the sediment provenance from the rocks of the watershed. Clay 457 minerals are more complex to relate to a specific sediment source because they depend on 458 dominant weathering processes, i.e. physical in active mountain ranges (illite and chlorite) vs 459 chemical in ancient orogen (mixed-layer clays and smectite) or sedimentary basins (mixed-460 layer clays and kaolinite). In addition to the fluvial input, a contribution from marine origin 461 may be observed in macrotidal estuaries as for example in the Seine estuary, where sediments from the erosion of the Cotentin peninsula are brought in by the longshore drift (Walter-462 463 Simmonet, 2008).

Although simplified, the proposed categories of sediment provenance help defining the
dredged sediment properties for substitution of fossil material in the heavy clay industry. Best
technological results are obtained from P-M-S sources either in fluvial or estuaries.
Dispersion suggests that refined classifications might capture specific sediment composition

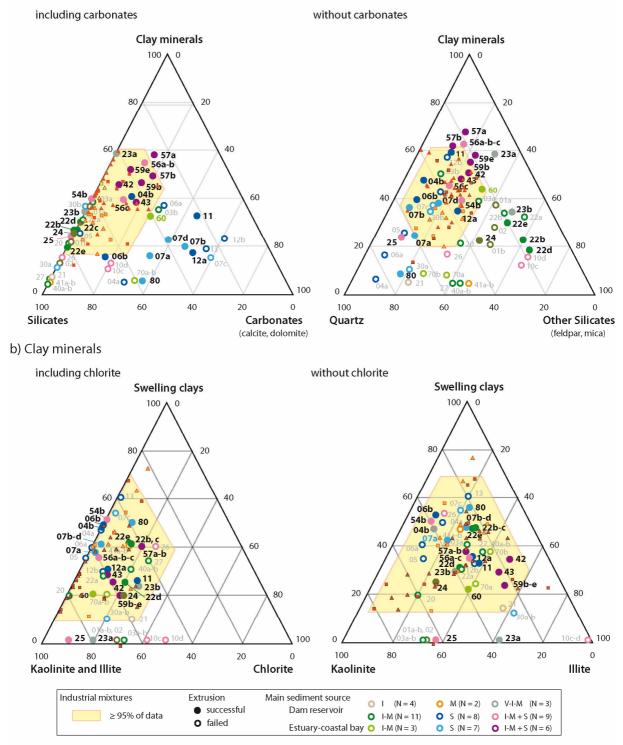
468 in relation to provenance (e.g. siliciclastic vs carbonate-rich sedimentary rocks, types of469 metamorphic or volcanic rocks).

470 5.3 Consistency between PCA results and the Mineralogical Industrial

471 *Framework*

The Mineralogical Industrial Framework (MIF, Haurine et al., 2016) is a decision tool based mineralogy and clay mineral assemblages of industrial mixtures clustering in domains on each of four ternary diagrams (Fig. 5). Plot of the composition of the industrial mixtures analyzed in this study falls within the originally defined industrial domains, complementing areas with few data. As for the original data set, no specific pattern is observed between the tile or brick industrial mixtures.

a) Mineralogy



480 Fig. 5. Projection of sediment samples on the Mineralogical industrial framework (MIF), a
481 decision tool developed from the composition of industrial mixtures (Haurine et al., 2016).

Provenance categories defined during PCA, cluster also on the MIF (dominant geology and 482 483 extrusion result) (Fig. 5). Samples from P-M-S sources which obtained the best technological 484 scores mostly plot within the industrial domains in each of the ternary diagrams. They show quite high content in clay minerals, which is put in relation to their particle size distribution 485 486 dominated by particles smaller than 25 μ m (90%). Samples from S sources largely plot 487 outside of the first diagram due to their high carbonate content; which explains the low results 488 of the technological tests because these high amounts of inert particles decrease the structure 489 cohesion by lack of clay minerals that act as a binder. Samples from P-M sources plot outside 490 of the second ternary diagram due to their high silicate content (feldspar and chlorite) that also 491 explains the low technological results for similar reasons as the high carbonate content. 492 Samples that could not be extruded (all samples from P, M sources and some samples from P-493 M and S sources) plot outside of the ternary diagrams because of low clay content associated to very high silicate content (quartz, or feldspar and mica) (P, M, P-M sources), or a very high 494 495 carbonate content (S source) (Fig. 5a). Nearly all samples fall within the industrial domains on the clay ternary diagrams (Fig. 5b). These results indicate that the further the sediment 496 497 samples plot outside the industrial domains, the lesser is the possibility to extrude the wet 498 paste, or the lower are the scores of the technological tests.

499 Consistent results between the PCA categories for sediment source fingerprinting and the MIF
500 domains based on mineralogy and scores of technological tests indicate that sediments
501 originating from P-M-S sources show the closest properties to those of industrial mixtures.

502 Properties of other sediments could be easily enhanced by mixing with materials having

complementary properties (in-between sites or with fossil material), or by addition of
correcting agents (quartz sand, grinded calcined clay wastes...), a conventional practice in the
heavy clay industry (Haurine et al., 2016).

Environmental studies (emission, carbon, metals) are needed to further characterize the silted
sediments. Estuary sediments are rich in chlorine and sulphur, seawater containing more
dissolved ions than most rivers (supplementary material 9). Some compounds could be
transformed during firing between 850 and 1100 °C on gaseous pollutants and be emitted on
atmosphere; which environmental impact should be evaluated.

511 6 Conclusions

Sediment provenance was identified as the main parameter controlling the recovery of dredged sediment in the characterization of silted in the heavy clay industry, thus contributing to reduce the proportion of quarried fossil materials by substituting part of a non renewable resource by material from dredging in dams, canals and harbors, by material presented considered as waste. Mineralogy plays an important role as indicated by the contrasted results during technological tests of samples having similar particle-size distributions.

In this context, PCA analyses (mineralogical composition) showed four categories of samples
based on their provenance, confirming the fingerprinting approach from spot sampling of fine
grained sediments in dam reservoirs and estuaries. Mineralogy proved to be more
discriminating than clay-mineral associations, the later being controlled by weathering
processes in geomorphic contexts. Samples from sites fed from the erosion of P-M-S rocks
obtained the best scores during the technological tests, close to the industrial values.

525 Composition is dominated by clay minerals and quartz with some carbonates, chlorite and 526 muscovite. Sediments from S and P-M sources obtained less effective scores attributed to the 527 high content in carbonates (S source) or silicates (P-M sources, chlorite, muscovite and 528 feldspars). Sediment from P or M sources could not be extruded partly due to the low clay 529 mineral content and coarser particle-size.

Consistent results between the PCA fingerprinting method, MIF industrial domains, and
technological tests show that even though the sediment source categories are simplified, they
constitute a reference to predict the potential of sediment as raw material for the heavy clay
industry. The MIF decision tool proved to be an efficient reliable tool as it only necessitates
sediment composition.

In an industrial scale perspective, environmental chemical analyses (such as S, F, Cl compounds and CO2) should be conducted to further characterize the silted sediments. Costs associated to sediment transport and treatments should also be taken into account keeping in mind that environmental standards of the industry are evolving due to the awareness of the benefits of a sustainable environment policy. This classification should be useful to the heavy clay industry managers when making decision regarding the fossil resource preservation by substitution with dredged sediments.

542 7 Acknowledgements

543 This work benefited from an ANRT support (convention N°2012-093) and is associated to the
544 SEDIBRIC project financed by ADEME and Région Normandie, AMI funding CPIER VDS.

545	Authors wish to thank the heavy clay producers for providing industrial mixtures. We also
546	wish to acknowledge F. Théry, W. Pesle and G. Vuarand (EDF); F. Bourdin and S. Brasselet
547	(Le Havre harbor); and E. Philippe and B. Benatier (Vendée Eau) for giving us access to dam
548	reservoirs and providing dredged sediment. Finally, we would like to warmly thank L.
549	Vincent and V. Tchemoun (CTMNC), N. Martineau and L. Marlot (Mines-Paristech) for their
550	precious help in the field and during laboratory analyses.

551 8 *References*

- 552 Agostini, F., Skoczylas, F., Lafhaj, Z., 2007. About a possible valorisation in cementitious
- materials of polluted sediment after treatment. Cement and Concrete Composites, 29(4),

554 270-278. https://doi.org/10.1016/j.cemconcomp.2006.11.012

- Alary, C., 1998. Mécanismes et bilans de l'érosion dans le bassin versant méditerranéen
 aménagé : le cas de la Durance (S-E France)., Doctoral dissertation, Université AixMarseille III, France.
- Azapagic, A., Perdan, S., Clift, R. (Eds.), 2004. Sustainable development in practice: case
 studies for engineers and scientists. John Wiley Sons.
- 560 Benedetti, M. M., Raber, M. J., Smith, M. S., Leonard, L. A., 2006. Mineralogical indicators
- of alluvial sediment sources in the Cape Fear River Basin, North Carolina. Physical
- 562 Geography, 27(3), 258-281. https://doi.org/10.2747/0272-3646.27.3.258
- 563 Benyerou, D., Boudjenane, N., Belhadri, M., 2015. Physicochemical characteristics of port
- dredging sediment and of the brick slip used in the manufacture of bricks: a comparative

- study. Coastal Cities and their Sustainable Future, 148, 289-296.
- 566 DOI:10.2495/CC150241Bertin, X., Chaumillon, E., Sottolichio, A., Pedreros, R., 2005.
- 567 Tidal inlet response to sediment infilling of the associated bay and possible implications of
- human activities: the Marennes-Oléron Bay and the Maumusson Inlet, France. Continental
- 569 Shelf Research, 25(9), 1115-1131. https://doi:10.1016/j.csr.2004.12.004
- 570 BRGM, 2008. Carte lithologique simplifiée de la France au 1/1 000 000, Bureau de
- 571 recherches géologiques et minières, Orléans, France
- 572 Cappuyns, V., Deweirt, V., Rousseau, S., 2015. Dredged sediments as a resource for brick
- 573 production: Possibilities and barriers from a consumers' perspective. Waste management,
- 574 38, 372-380. https://doi.org/10.1016/j.wasman.2014.12.025
- 575 Chung, F.H., 1974. Quantitative interpretation of X-ray diffraction patterns. I. Matrix
- flushing method of quantitative multicomponent analysis. Journal of Applied
- 577 Crystallography 7, 519–525.
- 578 Colmar, A., Walter, C., Le Bissonnais, Y., Daroussin, J., 2010. Démarche de validation
- régionale par avis d'experts du modèle MESALES d'estimation de l'aléa érosif. Etude et
- 580 Gestion des Sols, Association Française pour l'Etude des Sols, 2010, 17 (1), 19-32.
- 581 Cultrone, G., Sebastián, E., Elert, K., De la Torre, M. J., Cazalla, O., Rodriguez–Navarro, C.
- 582 (2004). Influence of mineralogy and firing temperature on the porosity of bricks. Journal of
- the European Ceramic Society, 24(3), 547-564. https://doi.org/10.1016/S0955-
- 584 2219(03)00249-8.

- 585 Dondi, M., 2003. Technological and compositional requirements of clay materials for
- 586 ceramic tiles. In: Domínguez, E.A., Mas, G.R., Cravero, F. (Eds.), Proc. 12th Int. Clay
- 587 Conference Elsevier, Bahía Blanca, Argentina, pp. 23–30.
- 588 Escalera, E., Garcia, G., Terán, R., Tegman, R., Antti, M. L., & Odén, M., 2015. The
- 589 production of porous brick material from diatomaceous earth and Brazil nut shell ash.
- 590 Construction and Building Materials, 98, 257-264.
- 591 https://doi.org/10.1016/j.conbuildmat.2015.08.003
- 592 Filippi, M. L., Lambert, P., Hunziker, J. C., Kübler, B., 1998. Monitoring detrital input and
- resuspension effects on sediment trap material using mineralogy and stable isotopes (δ 180
- and $\delta 13C$): The case of Lake Neuchâtel (Switzerland). Palaeogeography, Palaeoclimatology,
- 595 Palaeoecology, 140(1-4), 33-50.https://doi.org/10.1016/S0031-0182(98)00040-6.
- 596 Garzanti, E., Vezzoli, G., Andò, S., Lavé, J., Attal, M., France-Lanord, C., DeCelles, P.,
- 597 2007. Quantifying sand provenance and erosion (Marsyandi River, Nepal Himalaya). Earth
- and Planetary Science Letters, 258(3-4), 500-515.
- 599 https://doi.org/10.1016/j.epsl.2007.04.010.
- 600 Garzanti, E., Andó, S., France-Lanord, C., Censi, P., Vignola, P., Galy, V., Lupker, M.,
- 601 2011. Mineralogical and chemical variability of fluvial sediments 2. Suspended-load silt
- 602 (Ganga–Brahmaputra, Bangladesh). Earth and Planetary Science Letters, 302(1-2), 107-120.
- 603 https://doi.org/10.1016/j.epsl.2010.11.043.

- Hamer, K., Karius, V., 2002. Brick production with dredged harbour sediment. An
- 605 industrial-scale experiment. Waste Management, 22(5), 521-530.

606 https://doi.org/10.1016/S0956-053X(01)00048-4.

- Haurine, F., 2015. Caractérisation d'atterrissements d'argiles récents sur le territoire français,
- 608 en vue de leur valorisation dans l'industrie des matériaux de construction en terre cuite,
- 609 Doctoral dissertation, Paris, ENMP, France.
- Haurine, F., Cojan, I., Bruneaux, M. A., 2016. Development of an industrial mineralogical
- framework to evaluate mixtures from reservoir sediment for recovery by the heavy clay
- 612 industry: Application of the Durance system (France). Applied Clay Science, 132, 508-517.
- 613 https://doi.org/10.1016/j.clay.2016.07.022
- Johari, I., Said, S., Hisham, B., Bakar, A., Ahmad, Z. A., 2010. Effect of the change of firing
- temperature on microstructure and physical properties of clay bricks from Beruas
- 616 (Malaysia). Science of Sintering, 42(2), 245-254. https://doi.org/10.2298/SOS1002245J
- 617 Kahle, M., Kleber, M., Jahn, R., 2002. Review of XRD-based quantitative analyses of clay
- 618 minerals in soils: the suitability of mineral intensity factors. Geoderma, 109(3-4), 191-205.
- 619 https://doi.org/10.1016/S0016-7061(02)00175-1
- 620 Klages, M. G., Hsieh, Y. P., 1975. Suspended solids carried by the Gallatin River of
- 621 southwestern Montana: II. Using mineralogy for inferring sources. Journal of Environmental
- 622 Quality, 4(1), 68-73. https://doi.org/10.2134/jeq1975.00472425000400010016x
- 623 Kornmann, M., 2005. Matériaux de construction en terre cuite fabrication et propriétés,
- 624 Septima, Paris, 119-120.
 - 34

- 625 Lane, S. N., Bakker, M., Costa, A., Girardclos, S., Loizeau, J. L., Molnar, P., Silva, T.,
- 626 Stutenbecker, L. Schlunegger, F., 2019. Making stratigraphy in the Anthropocene: climate
- 627 change impacts and economic conditions controlling the supply of sediment to Lake
- 628 Geneva. Scientific reports, 9(1), 1-11. https://doi.org/10.1038/s41598-019-44914-9
- 629 Loizeau, J. L., Girardclos, S., Dominik, J., 2012. Taux d'accumulation de sédiments récents
- et bilan de la matière particulaire dans le Léman (Suisse-France). Arch. Sci, 65, 81-92.
- 631 Mezencevova, A., Yeboah, N. N., Burns, S. E., Kahn, L. F., Kurtis, K. E., 2012. Utilization
- of Savannah Harbor river sediment as the primary raw material in production of fired brick.
- 533 Journal of environmental management, 113, 128-136.
- 634 https://doi.org/10.1016/j.jenvman.2012.08.030.
- Moore, D.M., Reynolds, R.C., 1997. X-Ray Diffraction and the Identification and Analysis
 of Clay Minerals. Oxford University Press, New York.
- 637 Paulmier, G., 1997. Atlas des diatomophycées des côtes françaises et des aires océaniques
- adjacentes. Direction des ressources vivantes, IFREMER, Concarneau.
- 639 Pereira, C. G., Castro-Gomes, J., de Oliveira, L. P., 2009. Influence of natural coarse
- 640 aggregate size, mineralogy and water content on the permeability of structural concrete.
- 641 Construction and Building Materials, 23(2), 602-608.
- 642 https://doi.org/10.1016/j.conbuildmat.2008.04.009.
- 643 Valero-Garcés, B. L., Navas, A., Machín, J., Walling, D., 1999. Sediment sources and
- siltation in mountain reservoirs: a case study from the Central Spanish Pyrenees.
- 645 Geomorphology, 28(1-2), 23-41. https://doi.org/10.1016/S0169-555X(98)00096-8.
 - 35

646	Walter-Simonnet, A. V., 2008. Impacts sédimentaires de la présence humaine et des
647	variations climatiques. Exemples d'enregistrements lacustres, fluviatiles et estuariens
648	(Doctoral dissertation).
649	Walling, D. E., 1999. Linking land use, erosion and sediment yields in river basins. In Man
650	and iver Systems, Garnier J. and Mouchel JM. (Eds), Hydrobiologia, 223-240.
651	Warr, L.N., 2020. Recommended abbreviations for the names of clay minerals and
652	associated phases. Clay minerals, 55, 261-264. doi:10.1180/clm.2020.30
653	Winkler, H.G.F., 1954. Bedeutung der Korngrössenverteilung und des mineral-bestandes
654	von Tonen für die Herstellung grobkeramischer erzeugnisse. Ber. DKG 31, 337–343.
655	Whitney, D. A. and Evans, B.W., 2010, Abbreviations for names of rock-forming minerals,
656	American mineralogist, 95, 185-187. DOI: 10.2138/am.2010.3371
657	Xu, Y., Yan, C., Xu, B., Ruan, X., Wei, Z., 2014. The use of urban river sediment as a
658	primary raw material in the production of highly insulating brick. Ceramics International,
659	40(6), 8833-8840. https://doi.org/10.1016/j.ceramint.2014.01.105.
660	Zuffa, G. G. (Ed.)., 2013. Provenance of arenites (Vol. 148). NATO ASI Series C, 148,
661	Springer Science + Business Media, B.V. DOI 10.1007/978-94-017-2809-6