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Non-destructive evaluation of ceramic porosity using terahertz time-domain spectroscopy

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Abstract

Dielectric constants of Al_2O_3 (alumina) ceramic samples have been measured with non-destructive terahertz time-domain spectroscopy. Using an effective medium approximation, we demonstrated that the relative permittivity can be used to evaluate the porous alumina samples, with porosity fractions ranging from 0% to 20% per volume. This result makes it possible to control sample porosity, a key material parameter related to mechanical strength under compression load, hardness and wear resistance, or thermal stability. We also employed terahertz time-domain spectroscopy to differentiate alumina samples fabricated with different grain sizes, or reveal a small fraction of impurities, such as 5%_{vol} of ZrO_2 , embedded in non-porous alumina. These results demonstrated the potential of terahertz radiation for non-destructive characterization of low loss high dielectric constant ceramics.

Keywords: Porosity evaluation, aluminum oxide Al_2O_3 , ceramics, non-destructive evaluation, dielectric properties, terahertz time-domain spectroscopy.

1. Introduction

Bridging the boundary between the infrared and microwaves, terahertz (THz) radiation encompasses electromagnetic frequencies from 0.1 THz to roughly 10 THz. Its unique properties, such as good penetration through various non-conductive materials, low scattering, free-space propagation, low photon energy, and broad spectral bandwidth, encouraged the development of THz photonics [1]. To this end, one needs THz effective functional systems with improved quasi-optical components including mirrors and lenses, attenuators, isolators, modulators, directional couplers, etc. Ceramic dielectric materials, with high permittivity and low losses, could be selected for promising applications in the THz spectral region.

Main previous works concerning the study of ceramic materials with THz radiation were oriented towards the characterization of their dielectric properties within the relatively transparent

0 – 3 THz spectral window. In 2003, Bolivar *et al.* measured the dielectric constant and loss tangent of steatite, aluminium oxide (alumina), titania loaded polystyrene and zirconium–tin–titanate [2]. Among many other studies, one can mention broadband dielectric characterization of alumina [3, 4, 5, 6, 7, 8, 9], boron nitride [10], low temperature co-fired ceramics based on willemite [11], and fiber-reinforced oxide-oxide ceramic matrix composites [12].

The porosity of a material is defined as the fraction of the volume of voids – or empty spaces – over the total volume. A key parameter in ceramic material production concerns the control of this porosity, since it is related to several physical properties, such as mechanical strength under compression load, hardness and wear resistance, or thermal stability. The evaluation of ceramic porosity can be achieved by boiling method or mercury injection [13, 14]. Both techniques require sample destruction and sample contact. Several non-destructive approaches are reported in the literature using ultrasounds, X-rays, infrared waves or a split cylin-

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der [15]. Both split cylinder and ultrasonic techniques require sample contact. X-rays are harmful and additional resources are required to ensure the operator safety. Infrared-based techniques are sensitive to environment and, to obtain quantitative results, additional theoretical analysis are required. In contrast, THz radiation can propose an effective contact-less and non-destructive approach for the characterization and control of ceramic porosity. Recently, using zirconium dioxide ceramic, Ye and co-workers proposed an in-situ evaluation of porosity in thermal barrier coatings based on temporal broadening of THz pulses [16]. They demonstrated that, as the porosity increased, the refractive index decreased and the extinction coefficient increased. They also emphasized that the relative temporal broadening ratio could be obtained faster and in an easier manner compared to the dielectric parameters in both the transmission and reflection modes.

In this paper, we focused our attention on alumina since it is the most important, widely used and cost effective oxide ceramic material. After presenting the sample manufacturing procedure and characterization, we investigated the THz dielectric properties of alumina ceramic samples with porosity fractions equal to 0%_{vol}, 5%_{vol}, 10%_{vol}, 15%_{vol} and 20%_{vol}. Using an effective medium approximation, we found a simple relationship between the real part of the relative permittivity and the sample porosity. We also demonstrated that THz time-domain spectroscopy can be effective to reveal a small fraction of impurities, such as 5%_{vol} of ZrO_2 powder embedded in non-porous alumina.

2. Experimental procedures

2.1. Sample fabrication and characterization

Pure alumina samples were prepared by CTTC (Center for Technology Transfers in Ceramics) with two different Al_2O_3 powders with grain size distribution $d_{50} = 1 \mu m$ and $d_{50} = 9.3 \mu m$ (median diameters). The samples exhibit a porosity ranging from 0 (bulk material) to 20%_{vol} with an increment of 5%_{vol}. The powder mixtures were composed of Al_2O_3 granulated powder and a proper volume of spherical organic pore formers to control the final porosity of the material. The pore former sphere diameter was controlled by scanning electron microscopy (SEM) with a JEOL 6360 LA microscope with a $\times 5$ to $\times 60000$ magnification and

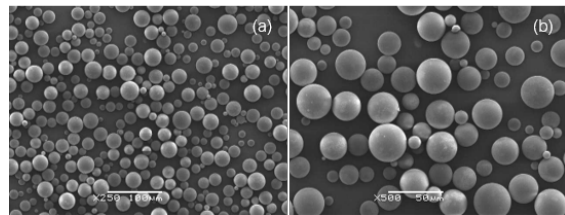


Figure 1: SEM pictures of spherical organic pore formers used to prepare Al_2O_3 porous samples. (a) Low magnification (white bar: 100 μm). (b) High magnification (white bar: 50 μm).

3 nm resolution. The sphere diameters range from 1 to 50 μm , as shown in Fig. 1. After debinding and sintering, the remaining pore geometry is therefore expected to be spherical.

To simulate a material phase inclusion or pollution in the sample, CTTC prepared an additional Al_2O_3 sample with ZrO_2 impurities. This sample is non-porous and thus contains 0%_{vol} theoretical volume porosity. The powder mixtures were composed of Al_2O_3 granulated powder ($d_{50} = 1 \mu m$ grain size) and 5%_{vol} of ZrO_2 powder. No pore former spheres were added in this case.

Due to isostatic pressing requirements, the ceramic powders (Al_2O_3 and Al_2O_3/ZrO_2) needed to be granulated to improve the mould filling and the microstructural homogeneity of the final samples. To do so, a freeze granulation process was performed, consisting in a pulverization of ceramic particle suspension droplets into liquid nitrogen followed by the sublimation of frozen solvent. All the powder mixtures were shaped by isostatic pressing with a 232 kN uniaxial press and a 30 mm in diameter stainless steel mould. The parts are then debinded and sintered under air from 1500°C to 1700°C in a muffle furnace. Final samples consist in pellets with 25 mm in diameter and 1 mm thickness after sintering. The porosity of each sample was characterized by the mercury porosimetry technique with a Micromeritics Autopore IV9510 allowing the detection of 0.003 to 360 μm pore size diameter. The microstructure and surface topography of the samples were controlled by SEM observations.

2.1.1. From 0 to 20%_{vol} Al_2O_3 porous samples with $d_{50} = 1 \mu m$ powder

The mercury porosimetry analysis were performed on the $d_{50} = 1 \mu m$ Al_2O_3 samples with porosities equals to 0, 5, 10, 15 and 20%_{vol} (Fig. 2).

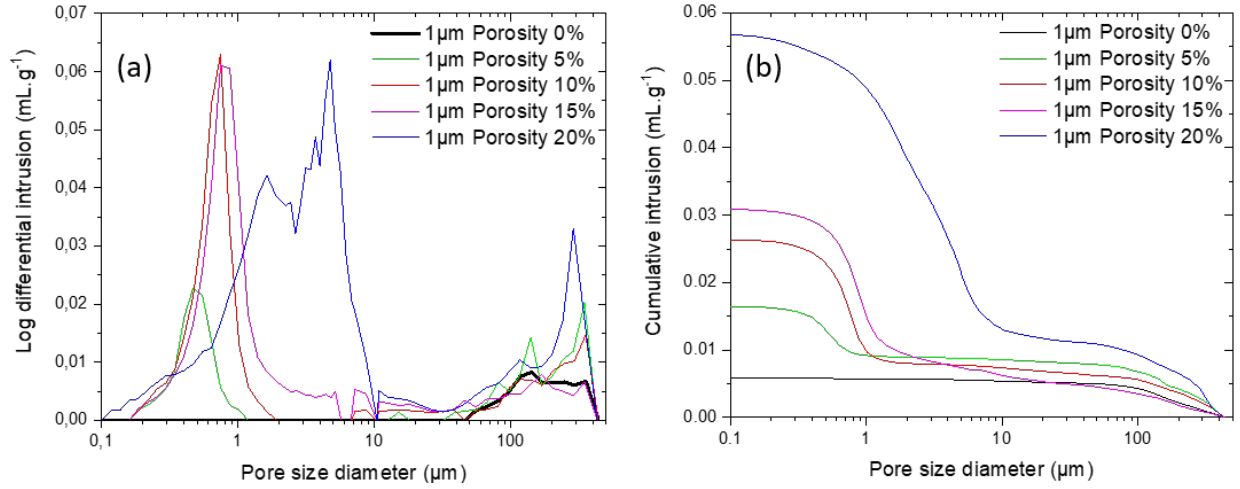


Figure 2: Mercury porosimetry analysis. Log of differential intrusion (a) and cumulative intrusion (b) as a function of pore size diameter for $d_{50} = 1 \mu\text{m}$ Al_2O_3 samples with 0 to 20% $_{vol}$ theoretical porosity.

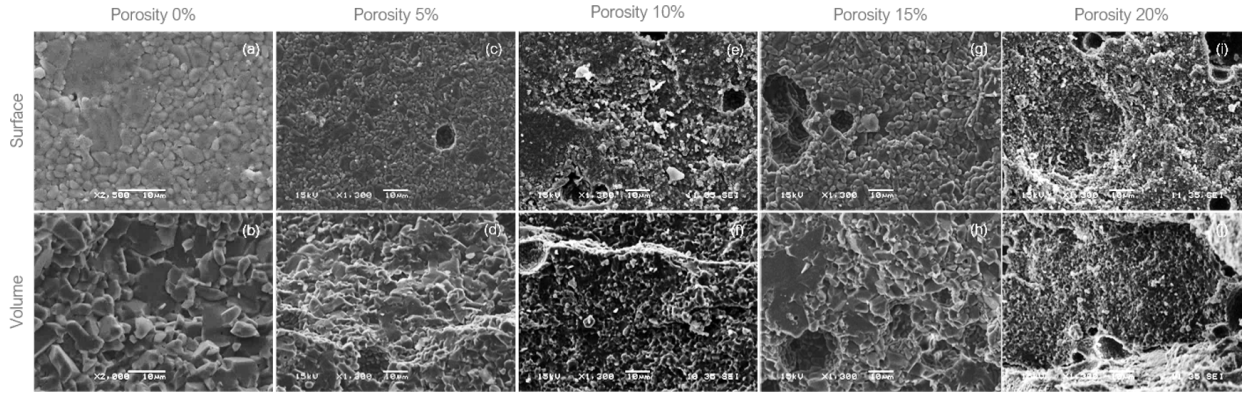


Figure 3: High magnification SEM pictures (surface and volume) for $d_{50} = 1 \mu\text{m}$ of Al_2O_3 samples with 0% $_{vol}$ (a,b), 5% $_{vol}$ (c,d), 10% $_{vol}$ (e,f), 15% $_{vol}$ (g, h) and 20% $_{vol}$ (i,j) porosity levels. White bar: 10 μm .

In this figure, and for all mercury porosimetry analysis performed in this paper, the minimum pore size diameter has been fixed to 0.1 μm since no porosity has been detected below this pore size. First, we notice that the 0% $_{vol}$ sample does not present any pore size diameter domain below 50 μm , visible on the log differential intrusion graphs (Fig. 2(a)). However, it appears a pore size diameter domain above 100 μm , indicating a remaining portion of voids in the sample. We can thus conclude that the 0% $_{vol}$ sample does not exactly correspond to bulk alumina material. Then, the profiles of the 5, 10 and 15% $_{vol}$ porosity curves look similar with three different pore size diameter domains from 0.1 to 2 μm , 2 to 100 μm and above 100 μm . We believe that the 0.1–2 μm pore size diameter domain could

be correlated to an inter/intra granular porosity or pore former spheres broken in smaller pieces during the shaping process. Nevertheless, the contribution of an inter/intra granular porosity could be more significant with the pore former content, as shown in Fig. 2(b). Indeed, to keep the spherical pore shape and to avoid material collapsing, the thermal treatment temperature has to be decreased with the increasing of pore former quantity. This modification could create lack of sintering in the ceramic pellets. The 2 – 100 μm domain is directly related to the size of pore former spheres introduced in the powder mixture. For the 15% $_{vol}$ and 20% $_{vol}$ Al_2O_3 porous samples, the contribution of 0.1 – 2 μm pore size diameter domain decreases to the benefit of the two other domains (2 – 10 μm and above 100 μm),

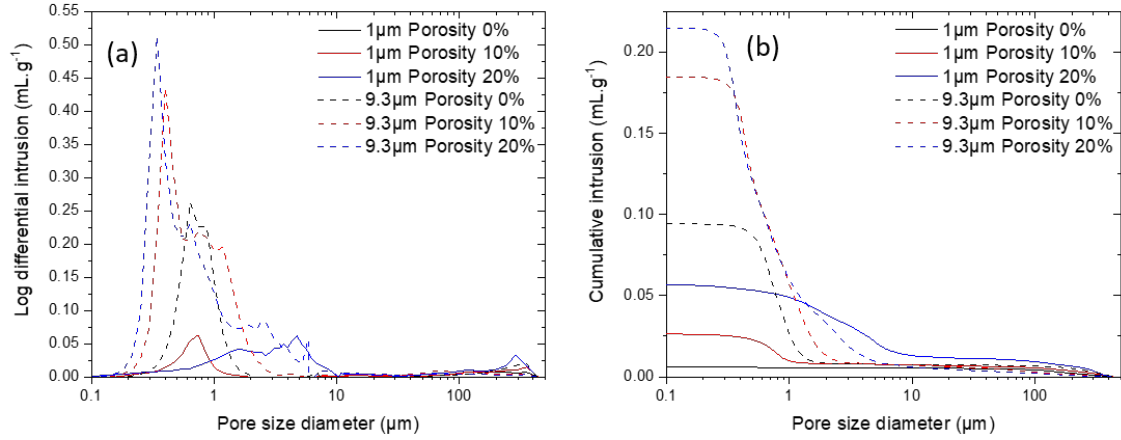


Figure 4: Mercury porosimetry analysis. Log of differential intrusion (a) and cumulative intrusion (b) as a function of pore size diameter. Comparison between Al_2O_3 samples with 0, 10 and 20% $_{vol}$ theoretical porosity, fabricated from $d_{50} = 1 \mu m$ and $d_{50} = 9.3 \mu m$ powders.

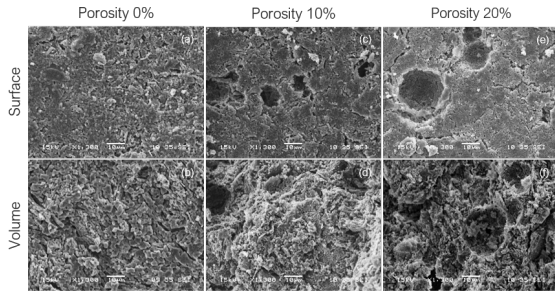


Figure 5: High magnification SEM pictures (surface and volume) for $d_{50} = 9.3 \mu m$ of Al_2O_3 samples with 0% $_{vol}$ (a,b), 10% $_{vol}$ (c,d), 20% $_{vol}$ (e,f) porosity levels. White bar: 10 μm .

as shown in Fig. 2(a) (purple and blue curves). This phenomenon is amplified for the 20% $_{vol}$ sample and maybe related to a decreasing rate of broken pore former spheres. Their integrity seems to be preserved by a lower amount of ceramic material contained in the 20% $_{vol}$ of porosity powder mixture.

The porosity modification is highlighted by the high magnification SEM observation of the surface and volume of the five samples (Fig. 3). The voids and pore concentration clearly increase with the amount of pore former volume. The remaining porosity in the sintered part is modified, as shown by the SEM analysis (Fig. 3). The only pore size diameter domain shared by all the samples is the one above 100 μm , which is not supposed to be present. This should indicate cracks or fractures in all the

samples which can appear during the shaping or the several thermal treatments. This hypothesis can be discarded by the SEM analysis carried on the samples (Fig. 3). Indeed, the high magnification SEM analysis, whatever the sample specification is, do not reveal the presence of any cracks on the surface or in the volume. To perform mercury porosimetry and SEM analysis, the pellets were broken and the mechanical stress may induce defect apparition above 100 μm .

It is important to note that SEM and mercury porosimetry represent destructive characterization techniques. The increase of the spherical pore concentration is the consequence of the introduction of larger spherical pore formers. Moreover, the very rugged profiles seen in the sample volumes (Fig. 3(f,j)) correspond to fracture faces which may cause porosity in the samples above 100 μm . Comparatively, we have to point out that the following analysis with THz radiation presented in this paper, will not undergo any sample stress or destruction.

2.1.2. From 0 to 20% $_{vol}$ porosity Al_2O_3 samples with $d_{50} = 9.3 \mu m$ powder

For each porosity, the $d_{50} = 9.3 \mu m$ sample pellets were shaped, debinded and sintered in the same conditions than the $d_{50} = 1 \mu m$ ones. The mercury porosimetry analysis were performed on the 0, 10 and 20% $_{vol}$ porosity Al_2O_3 samples and compared with those of the $d_{50} = 1 \mu m$ samples, as shown in Fig. 4. For the samples made with the

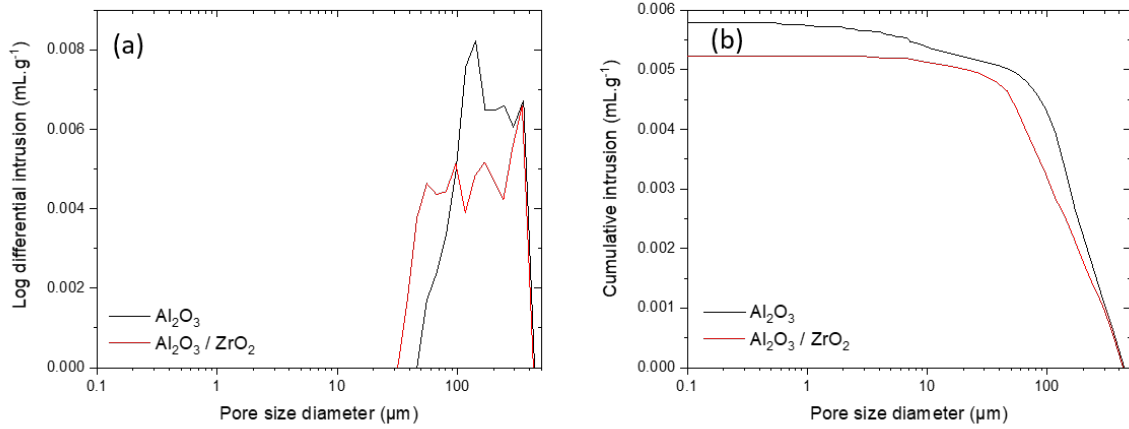


Figure 6: Mercury porosimetry analysis. Log of differential intrusion (a) and cumulative intrusion (b) as a function of pore size diameter for 0%_{vol} porosity $d_{50} = 1 \mu\text{m}$ Al_2O_3 and $\text{Al}_2\text{O}_3 - \text{ZrO}_2$ mixture.

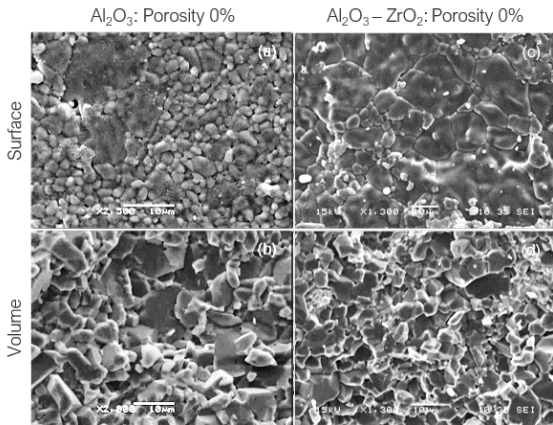


Figure 7: High magnification SEM pictures (surface and volume) for $d_{50} = 1 \mu\text{m}$ of Al_2O_3 samples with 0%_{vol} (a,b) and $\text{Al}_2\text{O}_3 - \text{ZrO}_2$ (c,d) mixture samples. White bar: 10 μm .

9.3 μm powder, the introduced mercury volume is clearly higher for all porosities. The samples show a 30% porous volume increase compared to the 1 μm powder. The very low porosity at high pore size diameter above 100 μm is again due to the preparation procedure for sample characterization). A 0.3 to 2 μm pore size diameter domain, which is not supposed to be present, appears on the profile of the $d_{50} = 9.3 \mu\text{m}$ 0%_{vol} porosity (Fig. 4(a), black dash curve) and is absent on the $d_{50} = 1 \mu\text{m}$ 0%_{vol} porosity profile (Fig. 4(a), black curve). This phenomenon is not due to an addition of pore formers since no spheres were introduced in this case, but

related to an inter/intra granular porosity caused by a lack of sintering. The $d_{50} = 9.3 \mu\text{m}$ 10%_{vol} and 20%_{vol} porosity samples (Fig. 4(a), red dash and blue dash curves, respectively) show a shift towards smaller and bigger pore size diameters, respectively due to inter/intragranular porosity and pore formers spheres introduction. The pore size diameters and porous volume evolutions of these two samples are similar those of $d_{50} = 1 \mu\text{m}$ 10%_{vol} and 20%_{vol} porosity samples (Fig. 4(a), red and blue curves, respectively) down to the final porosity (Fig. 4(b)).

We also used high magnification SEM images to analyze the porosity modification of the surface and volume of the three samples (Fig. 5). Again, the voids and pore concentration increase with the amount of introduced pore formers. Indeed, the spherical pore concentration increase is the sign of a larger pore former sphere introduction. The lack of sintering and consolidation is still present and observed whatever the pore former sphere amount introduced. The comparison of SEM images in Figs. 3(a,b) and 5(a,b) exhibits the remaining porosity and the different microstructures between $d_{50} = 9.3 \mu\text{m}$ 0%_{vol} porosity and $d_{50} = 1 \mu\text{m}$ 0%_{vol} porosity. Indeed, full sintering of larger Al_2O_3 grain size can be harder to achieve inducing a high residual porosity and a lack of consolidation.

2.1.3. 0%_{vol} Al₂O₃ and Al₂O₃-5%_{vol} ZrO₂ mixture samples with $d_{50} = 1 \mu\text{m}$ powder

The mercury porosimetry analysis of Al₂O₃ and Al₂O₃ – ZrO₂ mixture samples are very similar (Fig. 6). The very low porosity at high pore size diameter is again due to the preparation procedure for sample characterization. The presence of a secondary phase cannot be detected by mercury porosimetry but some inclusions are revealed by SEM images, as shown in Fig. 7. Indeed, the whiter and clearer grains or areas correspond to dispersed ZrO₂ material in the Al₂O₃ matrix. No cracks are detected on the surface or in the volume of the pellets.

2.2. THz time-domain spectroscopy

To measure the dielectric properties of the samples, we used THz time-domain spectroscopy. This technique can provide both amplitude and phase information of THz radiation transmitted by a sample in a single measurement and does not require the use of Kramers-Krönig relations to extract both real and imaginary parts of the dielectric permittivity [17]. Moreover, THz time-domain spectrometers are now commercially available with high detection sensitivity and large spectral range, contributing to the development of a valuable material THz database.

For our study, we used a commercially available THz time-domain spectrometer (TeraFlash, Topica Photonics). The THz beam is sent onto a sample with a beam diameter of 2.5 mm to ensure a large and homogenized illumination. The system measures a signal proportional to the temporal evolution of the THz electric field transmitted by the sample with a dynamic range of 100 dB and a spectral bandwidth up to 6 THz. Owing to a highly precise mechanical delay stage, the system acquires up to 60 temporal waveforms per second along a 50 ps scan range. The entire setup was enclosed inside a dry air injected chamber to eliminate the absorption of THz radiation by ambient water vapor.

Using fast Fourier transform, temporal data are transformed into the frequency domain. The ratio between sample and reference signals provides the complex function, from which one can extract the complex relative permittivity $\tilde{\epsilon}_r = \epsilon_r - i\epsilon_r'$ as a function of the THz frequency [17]. From this procedure, one can obtain the THz dielectric properties of the sample, represented for instance by the relative permittivity ϵ_r and the dielectric loss tangent

defined as:

$$\tan \delta = \frac{\epsilon_r'}{\epsilon_r}. \quad (1)$$

The measurement procedure is as follows. For a given sample family (same porosity fraction, same grain size, same composition), three different alumina samples have been studied to reduce uncertainty coming from both sample fabrication and experimental measurement. For each sample, we precisely measured the pellet thickness, by means of a micrometer caliper with an accuracy of up to 5 μm and with a ratchet stop, before extracting the average relative permittivity and loss tangent. Simultaneously, we also recorded a reference signal obtained without sample. The three consecutive sample measurements make it possible to calculate the average and standard deviation of both relative permittivity and loss tangent. It should be also mentioned that mercury porosimetry only captures open pores whereas THz spectroscopy is more accurate providing a measurement that reflects both open and closed pores.

3. Results and discussion

3.1. THz dielectric properties of Al₂O₃ porous samples with $d_{50} = 1 \mu\text{m}$ powder

In this first experiment, we studied the dielectric properties of Al₂O₃ samples composed of $d_{50} = 1 \mu\text{m}$ grain size with porosity fractions equal to 5, 10, 15 and 20%_{vol}.

For these porosity fractions, Fig. 8 shows the evolution of both the relative permittivity (a) and the loss tangent (b) as a function of frequency from 0.3 to 2 THz. Above this latter frequency, the signal-to-noise ratio is too small owing to important absorption of THz radiation by the samples. In the figure, the markers indicate the average values over three samples fabricated under same conditions. The color shade backgrounds are the standard deviations over the three samples.

First, as shown in Fig. 8(a), the relative permittivities of the different samples are all distributed between 7.5 and 9.3, in agreement with previous studies [2, 3, 4, 5, 7, 8], even if it is difficult to compare separate studies since the fabrication protocol and porosity fraction can strongly differ. Then, for all porosity fractions, we observe that the relative permittivity increases as a function of THz frequency. This is especially remarkable considering

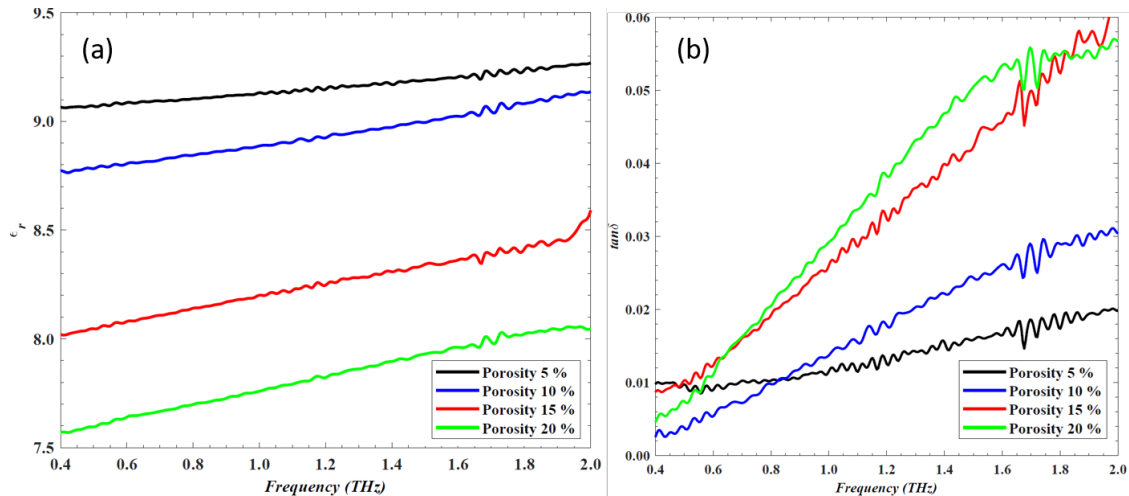


Figure 8: Dielectric properties of $d_{50} = 1 \mu\text{m}$ grain size alumina samples with porosity fractions equal to 5%, 10%, 15% and 20%. (a) Relative permittivity. (b) Loss tangent. Markers correspond to the average values measured over three different samples.

samples with higher porosity. We observe a similar behavior for the dielectric loss tangent (Fig. 8(b)). It is around 0.005 below 0.5 THz, confirming that alumina ceramic can be considered as a low loss high dielectric constant material, in agreement with previous studies [2, 3, 4, 5, 7, 8]. The loss tangent also gradually increases as a function of THz frequency. Similarly, this trend is more remarkable considering samples with higher porosity. For example, the dielectric loss tangent of alumina sample with 20% porosity is around 0.003 at 0.3 THz but nearly 20 times larger at 2 THz. Since higher frequencies are related to shorter wavelengths (1 THz corresponds to a wavelength of 0.3 mm), this trend may be attributed to higher scattering of THz radiation by the samples at high frequencies. THz scattering can also explain the increase of loss tangent as a function of sample porosity due to the presence of larger voids or empty spaces between alumina grains.

Regarding differences of dielectric properties between samples with different porosity fractions, we observe a decrease of the relative permittivity for samples with higher porosity, as shown in Fig. 8(a). Globally, we observe a 15% decrease of the sample permittivity as the porosity fraction changes from 5% to 20%. We note a qualitatively similar behavior for the dielectric loss tangent above 0.5 THz. It strongly increases for the samples with higher porosity fractions (Fig. 8(b)). However, this trend is not properly preserved for lower frequencies than

0.5 THz.

3.2. Effective medium approximation description

The effective medium theory (EMT) has been used for over a century to study the optical, electric, magnetic and mechanical properties of materials [18, 19]. With THz radiation, EMT has been used to characterize pellets composed of polyethylene powder and specific molecules such as explosives, drugs, etc. We can also cite the THz detection of porosity in pharmaceutical tablets [20]. The mathematical equations describing different transport phenomena (dielectric permittivity, electrical conductivity, etc.) in each of these fields are interchangeable. At the macroscopic scale, the effective properties of a multi-phase composite material can be accurately computed using the properties and the relative fractions of its components. The complex effective permittivity of a heterogeneous medium in the THz range can be estimated from effective medium models (EMMs). The most well-known one is the Maxwell-Garnett model, which is limited to spherical inclusion embedded in a host material with a low volume fraction [21]. Many studies have been performed to extend the effective model to higher volume fractions and handling more complicated shapes of inclusions [22, 23, 24, 25].

In this section, we evaluate the applicability of different EMMs on our experimental data. Each model gives the relationship between the complex

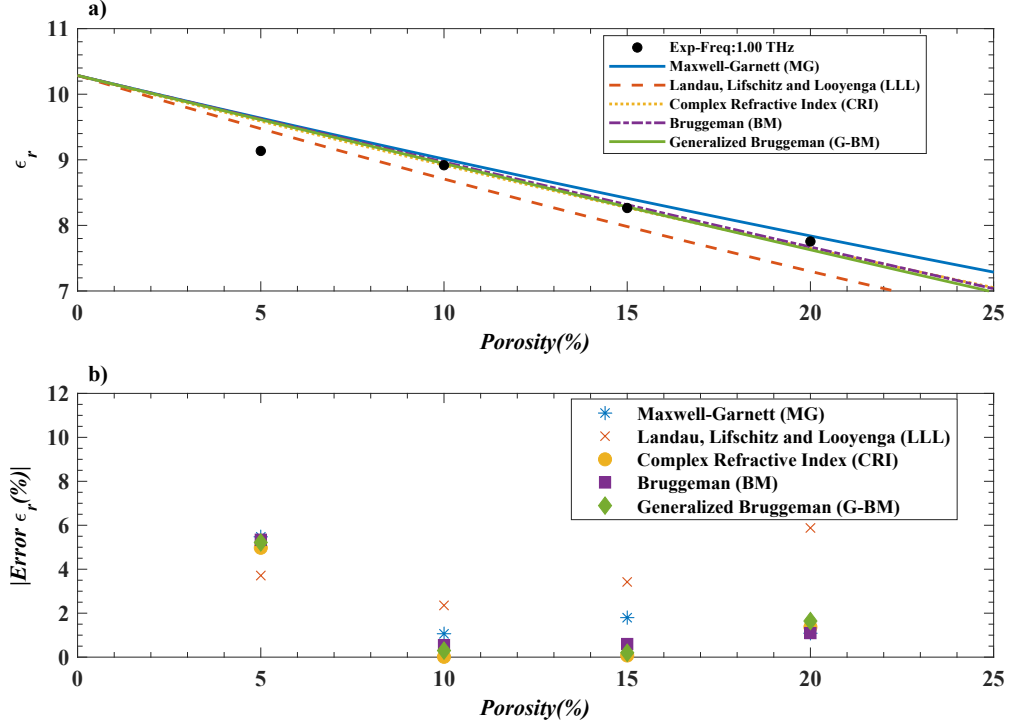


Figure 9: (a) Comparison between experimental relative permittivity of the samples (black dots) and the one predicted from EMMs (solid lines), at 1 THz and as a function of the sample porosity fraction. To estimate the 0%_{vol} relative permittivity we applied the ZPA calculation. (b) Absolute error between experimental data and the EMM simulations as a function of the sample porosity fraction.

relative permittivity of the effective medium $\tilde{\epsilon}_r$ and those of the Al_2O_3 host material and the embedded spherical inclusions (air or pores). These equations are as follows.

- Maxwell-Garnett model (MG) [21]:

$$\left(\frac{\tilde{\epsilon}_r - \tilde{\epsilon}_0}{\tilde{\epsilon}_r + 2\tilde{\epsilon}_0} \right) = \phi_1 \left(\frac{\tilde{\epsilon}_1 - \tilde{\epsilon}_0}{\tilde{\epsilon}_1 + 2\tilde{\epsilon}_0} \right), \quad (2)$$

where $\tilde{\epsilon}_0$ and $\tilde{\epsilon}_1$ are the complex relative permittivities, respectively, of the Al_2O_3 host material and pore guest material, and ϕ_1 is the volume fraction of the pore guest. In this model, the host and guest materials are not exchangeable. As a consequence, the value of $\tilde{\epsilon}_r$ is very sensitive to the difference between $\tilde{\epsilon}_0$ and $\tilde{\epsilon}_1$, and also to a high volume fraction of pore inclusions [26].

- Bruggeman model (BM) [27]:

$$\phi_1 \left(\frac{\tilde{\epsilon}_1 - \tilde{\epsilon}_r}{\tilde{\epsilon}_1 + 2\tilde{\epsilon}_r} \right) + \phi_2 \left(\frac{\tilde{\epsilon}_2 - \tilde{\epsilon}_r}{\tilde{\epsilon}_2 + 2\tilde{\epsilon}_r} \right) = 0, \quad (3)$$

where $\tilde{\epsilon}_1$ and $\tilde{\epsilon}_2$ are the complex relative permittivities of the material 1 (Al_2O_3 host) and material

2 (pore guest), ϕ_1 and ϕ_2 their volume fractions, respectively, with the relation $\phi_1 + \phi_2 = 1$.

For ellipsoidal voids, the equation is modified as follows (generalized BM model, noted G-BM):

$$\phi_1 \left(\frac{\tilde{\epsilon}_1 - \tilde{\epsilon}_r}{\tilde{\epsilon}_1 + L(\tilde{\epsilon}_1 - \tilde{\epsilon}_r)} \right) + \phi_2 \left(\frac{\tilde{\epsilon}_2 - \tilde{\epsilon}_r}{\tilde{\epsilon}_2 + L(\tilde{\epsilon}_2 - \tilde{\epsilon}_r)} \right) = 0, \quad (4)$$

where L is a depolarization factor, with $L = 1/3$ for spherical voids [27, 28, 29]. This model can be applied with contrasted values of $\tilde{\epsilon}_1$ and $\tilde{\epsilon}_2$ and any volume fractions [26].

- Landau, Lifschitz and Looyenga model (LLL) [22]:

$$\sqrt[3]{\tilde{\epsilon}_r} = \phi_1 \sqrt[3]{\tilde{\epsilon}_1} + \phi_2 \sqrt[3]{\tilde{\epsilon}_2}, \quad (5)$$

where $\tilde{\epsilon}_1$ and $\tilde{\epsilon}_2$ are again the complex relative permittivities of the material 1 (Al_2O_3 host) and material 2 (pore guest), ϕ_1 and ϕ_2 their volume fractions, respectively, with the relation $\phi_1 + \phi_2 = 1$. This model is well-suited for arbitrarily shaped particles.

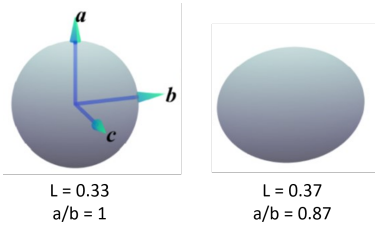


Figure 10: Dependency of the inclusion shape on the depolarization factor L and the aspect ratio a/b . Left: spherical intrusion. Right: ellipsoidal inclusion with L and a/b calculated from Eqs. 4 and 7, respectively.

- Complex Refractive Index model (CRI) [22, 30].

$$\sqrt{\tilde{\epsilon}_r} = \phi_1 \sqrt{\tilde{\epsilon}_1} + \phi_2 \sqrt{\tilde{\epsilon}_2}, \quad (6)$$

where $\tilde{\epsilon}_1$ and $\tilde{\epsilon}_2$ are the complex relative permittivities of the material 1 (Al_2O_3 host) and material 2 (pore guest), ϕ_1 and ϕ_2 their volume fractions, respectively, with the relation $\phi_1 + \phi_2 = 1$. This empirical model is well-suited for porous material.

With these five EMMs, we can calculate the theoretical relative permittivities of the effective medium ϵ_r as a function of the porosity fraction and compare the results to the experimental data already shown in Fig. 8(a). Moreover, EMMs assume that scattering of THz radiation is negligible [20]. Since we did not observe any significant broadening of the THz temporal waveforms for all the samples, we can conclude that scattering effects are not dominant in our work. This is also consistent with the $d_{50} = 1 \mu\text{m}$ grain size of pure alumina which is negligible compared to the wavelength of THz radiation. For different sample porosity fractions, Fig. 9(a) shows the experimental relative permittivity of the samples (black points) at 1 THz, extracted from the data presented in Fig. 8(a), together with the values predicted from the previous EMMs (lines). First, all models are in good agreement with the experimental data, even if the LLL one underestimates the value of the relative permittivity for porosity levels higher than 5% $_{vol}$. Then, it is important to note, in the range from 0 to 25% $_{vol}$, the linear dependency between the relative permittivity and the porosity, well reproduced by the EMM simulations. According to the fitting parameters, the linear dependency can be written as $\epsilon_r = -0.13P + 10.25$, where P is the sample porosity fraction (in % $_{vol}$).

Figure 9(b) shows that the absolute calculated error between experimental data and the EMMs sim-

Porosity [%]	$[\epsilon_0]$		
	ZPA	BM	MG
10	10.28	10.23	10.17
15	10.28	10.22	10.1
20	10.44	10.41	10.17
Average	10.33	10.29	10.15

Table 1: Relative permittivity ϵ_0 of pure Al_2O_3 host material estimated by the ZPA, BM and MG models at porosity levels equal to 10% $_{vol}$, 15% $_{vol}$ and 20% $_{vol}$ at 1 THz. Last line: mean value for each model.

ulations stands in the 0 to 6% range. Again, we can observe that the predicted permittivities, except for the LLL model, are in good agreement with the experimental values. Considering the spherical aspect of pore formers, as previously shown in Fig. 1, we logically expect spherical inclusions. The LLL model, which does not consider any inclusion shape, cannot perform the accuracy of the other models. We suspect the minor discrepancy to the experimental data of the MG model is due to a slight deformation of the predicted spherical shaped inclusions. Logically, we can expect ellipsoidal inclusions with aspect ratio a/b , linked to the depolarization factor L , of the principle axis (a) and the two common axes (b,c) of a spheroid (Fig. 10) [31]. Using an iterative least-square fitting to the G-BM model (see Eq. 4) and the THz effective permittivities, the depolarization factor L has been estimated to 0.37. Then, the aspect ratio a/b can be estimated with the equation [31]:

$$L = \frac{1}{1 + 1.6(a/b) + 0.4(a/b)^2}, \quad (7)$$

which provides the result $a/b = 0.87$, illustrated in Fig. 10 to better show the ellipsoid shape of the inclusions.

For a 5% $_{vol}$ porosity fraction, the significant discrepancy of all EMMs to the experimentally data can be explained by the large volume of the pore size between 10 μm and 100 μm (Fig. 2(b), green curve), leading to more scattering effects which are not considered in the currently used EMMs. We shall point out the absence of any pore size diameter domains in the log differential intrusion profiles (Fig. 2(a), black curve related to 1 μm grain size and 0% $_{vol}$ porosity), at least, regarding to the resolution limit of the used mercury porosimetry system.

Obviously, the good agreement of the experimental effective permittivity of the sample to theoretical curves confirms our assumption about the origin of the low accuracy of the EMMs at 5%_{vol} of porosity.

It is important to recall that the permittivities of the different components of the samples (host Al_2O_3 and pore guest materials) used in the EMM equations corresponds to pure bulk form. This bulk Al_2O_3 permittivity, corresponding to the real part of ε_0 in our EMMs, was calculated by considering the effective permittivities of the samples with known porosity fractions (10%_{vol}, 15%_{vol} and 20%_{vol}), the MG and BM models and the additional zero porosity approximation (ZPA) [32]. At porosity levels equal to 10%_{vol}, 15%_{vol} and 20%_{vol}, Table 1 shows the relative permittivity ε_0 of pure Al_2O_3 host material, at 1 THz, estimated by ZPA, BM and MG models. The mean value of the relative permittivity across all models is close to the value for bulk alumina reported elsewhere, between 9.45 and 11.72 [33].

3.3. Impact of the alumina powder grain size on THz dielectric properties

In this second experiment, for porosity fractions equal to 0%, 10% and 20%, we compared the dielectric properties of Al_2O_3 samples composed of $d_{50} = 1 \mu\text{m}$ grain size with those of Al_2O_3 samples composed of $d_{50} = 9.3 \mu\text{m}$ grain size. For all samples, the experimental procedure is similar to that described in the previous section, with again an averaging of the data provided by three different samples for a given grain size and porosity. For the different porosity fractions, Fig. 11 shows the evolution of the relative permittivity (a) and the loss tangent (b) as a function of frequency from 0.3 to 2 THz. Markers indicate the average values over three samples fabricated under same conditions and color shade backgrounds are the standard deviations. Experimental points corresponding to $d_{50} = 1 \mu\text{m}$ grain size, already plotted in Fig. 11, have been plotted again for comparison with those corresponding to $d_{50} = 9.3 \mu\text{m}$ grain size. First, the permittivity of 9.3 μm grain size samples increases slower than that of 1 μm grain size samples over the observed THz spectral range. Then, the permittivity of 9.3 μm grain size samples is about 30 to 40% lower than that of 1 μm grain size samples. This can be explained by the lower density of 9.3 μm grain size sample with respect to that of 1 μm grain size one.

For the $d_{50} = 9.3 \mu\text{m}$ grain size samples, the loss tangents exhibit large standard deviations due to larger THz absorption. Again, the dielectric loss tangent rapidly increases as a function of THz frequency, even if we note a more complex behavior for 9.3 μm grain size samples. For example, we observe an oscillation of the loss tangent for the 9.3 μm grain size sample with 10% porosity fraction, which was not observed for the 1 μm grain size sample. Since standard deviations for 9.3 μm grain size samples are also very large, it is difficult to go further with this observation. Moreover, the loss tangent of 1 μm grain size samples is smaller than that of 9.3 μm grain size samples over the considered THz frequency range, except the presence of some overlapping for the 20% porous samples above 1.5 THz. We attribute this behavior to the remaining porosity and the different microstructures between the two samples with a more difficult full sintering of larger Al_2O_3 grain size inducing higher residual porosity.

3.4. Impact of impurity inclusions on THz dielectric properties

The last experiment is slightly different since it does not concern the influence of sample porosity on THz dielectric constants, but rather the potential of THz time-resolved spectroscopy to detect an impurity in a sample. As explained before, the sample is non-porous and composed of $d_{50} = 1 \mu\text{m}$ grain size with 5%_{vol} ZrO_2 impurities.

THz dielectric constants were extracted with the similar approach as before. Figure 8 shows the evolution of the relative permittivity (a) and the loss tangent (b) as a function of frequency from 0.3 to 2 THz. Markers indicate again the average values over three samples fabricated under same conditions and color shade backgrounds are the standard deviations over the three samples. Experimental points corresponding to the Al_2O_3 sample composed of $d_{50} = 1 \mu\text{m}$ grain size and 0% porosity (in blue), already plotted in Fig. 8, have been plotted again for comparison with those corresponding to the above-described alumina sample with the zirconium dioxide impurity. For the sample with zirconium, the permittivity slightly increases as a function of THz frequency, as shown in Fig. 12(a). We also note that the standard deviation is larger, specially for frequencies lower than 0.7 THz. Again, the dielectric loss tangent increases as a function of THz frequency (Fig. 12(b)).

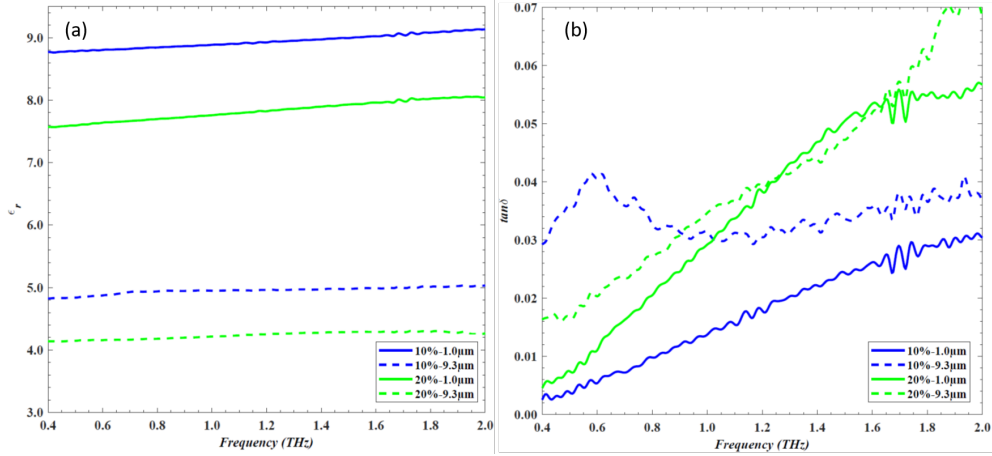


Figure 11: Dielectric properties of Al_2O_3 samples composed of $1 \mu m$ d_{50} grain size and $9.3 \mu m$ d_{50} grain size, with porosity fractions equal to 0% (yellow markers), 10% (blue markers) and 20% (red markers). (a) Permittivity. (b) Loss tangent. Markers correspond to the average values measured over three different samples.

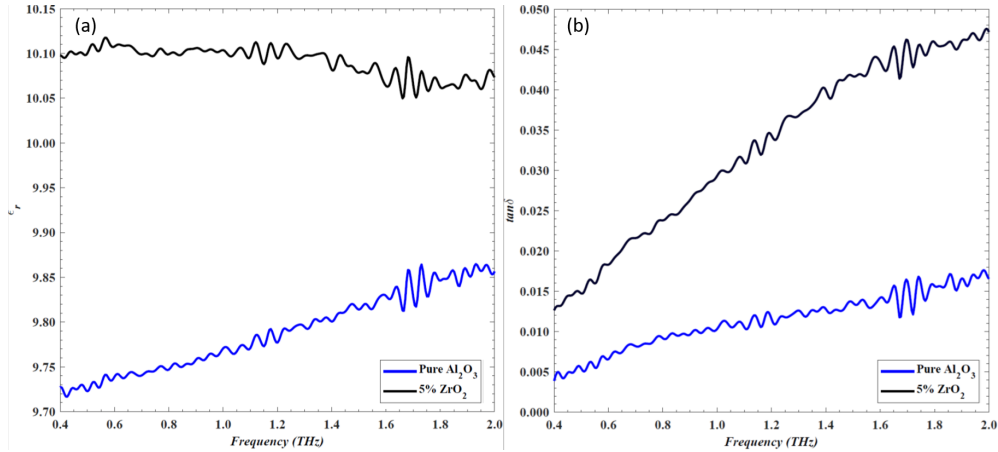


Figure 12: Dielectric properties of: (blue) Al_2O_3 sample composed of $1 \mu m$ d_{50} grain size and 0% porosity ; (red) Al_2O_3 sample composed of $1 \mu m$ d_{50} grain size with 5% $_{vol}$ ZrO_2 impurities. (a) Relative permittivity. (b) Loss tangent. Markers correspond to the average values measured over three different samples.

We also compare these results with the dielectric properties of the Al_2O_3 sample composed of $d_{50} = 1 \mu m$ grain size and 0% porosity. Clearly, for all considered THz frequencies, the permittivity is higher for the sample with impurities. This may be attributed to the larger density of the sample with zirconium inclusions compared to the pure Al_2O_3 sample. We observe a similar behavior for the dielectric loss tangent, which is larger for the sample with the zirconium impurity. This additional experiment shows that THz time-domain spectroscopy is also a convenient and powerful method to detect impurities embedded in ceramic materials. Considering that the uncertainty of relative permittivity

measurement is around 0.1 at 1 THz, we can estimate that the lowest ZrO_2 impurities concentration that can be detected is around 1%.

4. Conclusion

We reported on the non-destructive and contactless evaluation of Al_2O_3 ceramic porosity using terahertz time-domain spectroscopy. Up to 2 THz, the extraction of the relative permittivity and dielectric loss tangent of different porous samples and the help of an effective medium approximation make it possible to reveal a simple linear relationship between the permittivity and the sample porosity

within the 0% to the 20% fraction range. From a given set of samples with a calibrated fabrication process, this can be applied to non-destructively determine the porosity of an unknown sample. In addition, we tested our approach by introducing changes in the fabrication parameters of the alumina ceramic, stimulating both structural and material modifications. Our results indicated that THz time-domain spectroscopy can easily differentiate alumina samples fabricated with different grain sizes or with impurity inclusions. More generally, these results demonstrate the potential of THz radiation for the non-destructive analysis of ceramic materials, providing an alternative evaluation technique for the fabrication and quality maintenance of ceramic products. Besides, we also pointed out that, owing to their high THz permittivity and low losses, ceramic materials could provide a new class of optical components and encourage the development of THz photonics.

Declaration of Competing Interest

The authors declare no known competing financial interests or personal relationships influencing the presented work.

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