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# Concentration and purification by crossflow microfiltration with diafiltration of carotenoids from a by-product of cashew apple

- 3 juice processing
- 4
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17 Declarations of interest: none

# 19 Abstract

- 20 This work aimed to further investigate microfiltration with diafiltration to obtain a rich
- 21 carotenoid extract from the solid by-product of cashew apple (*Anacardium occidentale* L.)
- 22 juice processing. This solid residue called cashew fibers is rich in bioactive compounds,
- especially carotenoids. After mixing with water and pressing, an aqueous suspension was
- obtained and processed by crossflow microfiltration  $(40^{\circ}C)$  using tubular ceramic membrane
- with 0.2  $\mu$ m pore diameter. Permeate flux, which increased with transmembrane pressure, could be maintained above 100 L·h<sup>-1</sup>·m<sup>-2</sup> at high volume reduction ratio by coupling
- could be maintained above  $100 \text{ L} \cdot \text{h}^{-1} \cdot \text{m}^{-2}$  at high volume reduction ratio by coupling mechanical extraction with enzyme liquefaction. The concentration step led to an increase of
- mechanical extraction with enzyme liquefaction. The concentration step led to an increase of
   the carotenoid content by up to 19-fold and the diafiltration step allowed the carotenoid purity
- to be multiplied by 5. The impact of the process on the retentate characteristics was assessed
- 30 using a model based on simple assumptions. This calculation tool can easily be implemented
- and is helpful for choosing the operating conditions, to minimize water consumption as well
- 32 as effluent production.
- 33

# 34 Industrial relevance text

- A driven pressure membrane operation is a mild and economic process which covers a broad
- variety of applications in the food industry. Most operations focus on permeate (clarification,
- 37 cold sterilization, etc.), however few attempts have been made to exploit the retentate which is
- 38 considered as waste in many cases. In this study, we devised an approach for an integrated
- 39 process of extraction and crossflow filtration combined with enzymatic liquefaction in order
- 40 to produce a carotenoid-rich extract from cashew apple fibers. This work also provided
- opportunities for cashew apple juice manufacturers to add value to their by-products at low
   cost, simultaneously producing a high value-added extract and a ready-to-drink clarified juice.
- 42 Cost, simultaneously producing a high value-added extract and a ready-to-drink clarified ju 43 Another originality of this work was to provide a simple equation set, accessible on an
- 45 Another originality of this work was to provide a simple equation set, accessible on an
   44 industrial scale, to forecast the effluent volume and the consumption of water during
- 44 diafiltration, by setting a target concentration factor and a target purification factor, correlated
- to the limit of the purification rate. This work can help industrials to plan production

- 47 providing them with the possibility of steering the process with a balance between final
- 48 product quality, process productivity, effluent generation and water consumption.

## 49 Highlights

- 50 Integrated extraction-filtration process of cashew fibers with enzyme liquefaction
- 51 Total carotenoid retention during concentration and purification by microfiltration
- 52 High permeate flux at a volume reduction ratio of up to 20
- 53 Carotenoid purity multiplied by 5 using diafiltration
- 54 Modelling to forecast purification rate minimizing effluent volume and water consumption
- 55 56
- Keywords: microfiltration efficiency, purification rate, diafiltration performance, carotenoid
   rejection, enzyme liquefaction
- 59

60 Abbreviations

- 61  $\alpha$ : purification rate (no unit)
- 62 CF: concentration factor (no unit)
- 63 C: carotenoid concentration (mg·kg<sup>-1</sup>)
- 64 DM: dry matter  $(g \cdot kg^{-1})$
- 65 DVR: diavolume ratio (no unit)
- 66 J<sub>p</sub>: permeate flux  $(L \cdot h^{-1} \cdot m^{-2})$
- 67 p: purity of carotenoids  $(mg \cdot kg^{-1})$
- 68 PF: purification factor (no unit)
- 69 R: retention rate (no unit)
- 70 SIS: suspended insoluble solids  $(g \cdot kg^{-1})$
- 71 TmP: transmembrane pressure (bar)
- 72 TSS: total soluble solids  $(g \cdot kg^{-1})$
- 73 VRR: volume reduction ratio (no unit)
- 74 V: volume (L)
- 75

77

76 Subscripts 0, r, p refer to initial, retentate and permeate respectively

78

#### 1. Introduction

79 Over the last decades, crossflow microfiltration, and more broadly pressure-driven membrane processes, have been further developed for the fruit juice industry for multiple operations 80 including clarification, sterilization, concentration or fractionation (Conidi et al., 2020; 81 Dornier et al., 2018; Lipnizki, 2010). Crossflow microfiltration involves suspensions and is 82 performed to separate insoluble compounds (particles, droplets, colloids) using 0.1 to 10 µm 83 pore diameter membranes while ultra- and nanofiltration are used for solute fractionation over 84 a large molecular weight range. Crossflow microfiltration under 0.2 µm pore diameter is 85 mainly carried out as a unit operation throughout the technology chain in the food industry. 86 87 This mild process is often used to decrease the particle content in a liquid (clarification), as a 88 pre-treatment to prevent any problems with subsequent operations (chromatographic separation, other membrane processes, etc.), and to lower the microbial load in the permeate 89 90 (Dornier et al., 2018). For industrial applications, multiple parameters should be considered including environmental, economic or technological ones. Regarding the process, key 91 92 parameters such as permeate flux, yields and rejections have to be evaluated and optimized to estimate the large-scale feasibility. Microfiltration is often associated with an enzymatic 93 treatment which aims to reduce viscosity and fouling, and in most cases, to improve the 94 95 system performance (De Oliveira et al., 2012; Laorko et al., 2010; Vaillant et al., 2005). Since the enzymes used are a mix of pectinases, cellulases and hemicellulases from mold cultures 96 which are commonly used in the fruit processing industry, the cost of such processing aids is 97 generally low, compared to the productivity gain. Most studies of membranes carried out in 98 various fields, have generally focused on enhancing the value of permeate while only a few 99 have highlighted retentate potential. For their part, they mainly describe the concentration and 100 the purification of bioactive compounds, associated with the comprehension of fouling 101 mechanisms in complex matrices (Cho et al., 2003; Cisse et al., 2011; Dahdouh et al., 2016). 102

Cashew apple (Anacardium occidentale L.) is cultivated on a large scale, especially in Brazil 103 which ranked 1<sup>st</sup> in 2018 producing more than 1 500 000 tons according to FAO statistics. It 104 is associated with cashew nut production, which is the main reason why it is produced, 105 106 however it suffers from considerable post-harvest losses (Das & Arora, 2017). It is associated with cashew nut production, which is the main reason why it is produced. It has been reported 107 108 to be rich in organic acids, sugars, polysaccharides, mostly pectin, and in phytochemicals, 109 such as polyphenols, mainly flavonoids and tannins, carotenoids and vitamins, especially vitamin C. Like all fruits, it is highly perishable, and spoilage of the pulp occurs rapidly, only 110 a few hours after fruit injury or during the first step of juice processing. The type of spoilage 111 112 observed is usual, namely fermentation and oxidation leading mainly to browning and astringency development (Das & Arora, 2017). Cashew apple that is intended for human 113 consumption, is processed into multiple products such as sweet foods (candies, jam, etc.) or 114 115 beverages. This industrial production leads to the rejection of waste in significant quantities which is named cashew apple fibers (Damasceno et al., 2008; Talasila & Shaik, 2015). This 116 117 by-product, mainly destined for animal food production, is however rich in bioactive compounds, especially carotenoids. Carotenoids are liposoluble compounds that have been 118 studied for years because of their role as colorants and antioxidants. In addition to the pro-119 120 vitamin A status of some of them, they present known and significant beneficial effects on human health, for instance, reducing the risk of cancer, cardiovascular disease and cellular 121 degeneration (Rao & Rao, 2007). Pinto de Abreu et al. (2013), have characterized the 122 carotenoids and their relative contents in cashew apple fibers. The carotenoids identified were 123 mainly xanthophylls, such as auroxanthin, mutatoxanthin, lutein, zeaxanthin and β-124 cryptoxanthin at 31, 24.5, 10.4, 11 and 15% of total carotenoids respectively, but also 125 carotenes, mostly  $\beta$ -carotene, at 7.4%. In this work, the authors highlighted an approach using 126 pressing and enzyme treatment in order to optimize the extraction of carotenoids from cashew 127

fibers. A strategy based on a continuous helical-type press was suggested for optimal
carotenoid extraction, and a microfiltration trial was mentioned in order to obtain a
concentrated extract. Campos et al. (2002) and Castro et al. (2007) presented interesting
results using this strategy, demonstrating the feasibility of crossflow microfiltration applied to
cashew apple juice to decrease the microflora in the clarified permeate.

Crossflow microfiltration coupled with enzyme liquefaction, resulted in two promising 133 134 derived products with significant process performance. In the case of melon juice, Vaillant et al. (2005) obtained on one hand a retentate enriched 4-fold in  $\beta$ -carotene, and on the other a 135 clarified permeate which was organoleptically close to fresh melon juice. Introducing a 136 137 diafiltration step allows the purity of the obtained fractions to be increased. For watermelon, integrated processes combining crossflow microfiltration and enzyme liquefaction have been 138 developed for the production of a bioactive lycopene extract, concentrated between 8 and 11-139 fold and purified up to 25-fold by diafiltration (Chaparro et al., 2016) or between 12 and 18-140 fold, resulting in a higher antioxidant capacity of the extract (Oliveira et al., 2016). Using in 141 142 vitro human digestion models, Gence et al. (2018) highlighted the nutritional interest of a clementine juice concentrated 8-fold by crossflow microfiltration, taking into account 143 carotenoid bioaccessibility. This research also underlined the benefit of considering the 144 145 retentate as a high-value product, both economically and nutritionally.

Recently, a study was performed in order to assess the feasibility of coupling crossflow microfiltration and diafiltration for carotenoid concentration and purification from orange juice using an industrial approach (Polidori et al., 2018). In addition to the production of a concentrated carotenoid extract between 5 and 10-fold which was purified over a range of 8 to 20-fold by diafiltration with relevant process performances, the authors provided and validated a model based on simple assumptions in order to predict concentration and purification factors according to targeted conditions or *vice versa* on any filtration scale.

The present work aims to study the microfiltration process that includes a diafiltration step for 153 154 concentration and purification of carotenoids in an aqueous extract obtained from cashew apple fibers. It includes an evaluation of the interest of coupling the process with enzymatic 155 liquefaction. The study proposes to address the operation integrating product quality, process 156 productivity, and part of the environmental impact. A special focus is placed on developing a 157 simple simulation tool for helping the user to choose operating conditions that result in the 158 159 targeted concentration and purification levels minimizing effluent generation and processing duration. 160

161

#### 162 **2.** Experimental

163

#### 2.1 Cashew juice material

Raw material obtained from the by-product of cashew apple juice production as described by 164 Pinto de Abreu et al. (2013), was supplied by Sabor Tropical Ltda (Ceará, Brazil) and was 165 produced from the CCP-076 variety of cashew apple developed by Embrapa. This by-product, 166 called cashew apple fibers, was mixed with water using a mass ratio of 1:1. At this stage, 167 maceration for 60 min at 55°C with 500 mg·kg<sup>-1</sup> of pectinolytic enzyme Ultrazym AFP-L 168 (Novozymes, Bagsvaerd, Denmark) was, in certain cases, carried out. This aimed to improve 169 the release of carotenoids that are strongly entrapped within cell structures. The resulting 170 mixture was then pressed in a helical-type press with a nominal capacity of  $300 \text{ kg} \cdot \text{h}^{-1}$  using a 171 172 rotational speed of 30 rpm (Incomat 300, Fortaleza, Brazil). This operation was repeated 6 times after remixing the two phases obtained. The final extract was filtered through a 0.3 mm 173 sieve. For the study, one homogeneous batch of around 230 L of final extract was constituted, 174 distributed in sealed 3-10 L polyethylene bags and frozen at -20°C until use. 175

#### 176 **2.2 Microfiltration process: clarification & purification**

Microfiltration trials were carried out at laboratory scale using a micro-pilot manufactured by 177 TIA (Bollène, France). This device is described in figure 1. It consisted of 4 single-channel 178 tubular  $\alpha$ -alumina membranes of 55 cm<sup>2</sup> each, with an average pore diameter of 0.2  $\mu$ m, 179 mounted in series (Pall Exekia, Bazet, France). This configuration allowed the simultaneous 180 testing of 4 transmembrane pressure (TmP) conditions ranging from 1.2 to 3.2 bar. For each 181 membrane TmP was evaluated from the input and output pressures in the retentate loop 182 considering head losses as linear. Crossflow velocity was set at around 6 m  $\cdot$  s<sup>-1</sup> independently 183 of TmP using a volumetric feed pump. This high value ensured that the system acted as a 184 perfectly stirred reactor. The temperature of the whole system was maintained at  $40 \pm 2^{\circ}C$ 185 186 using a heat exchanger connected to a running water cryostat. This pilot was equipped with a feeding tank of 3 L. Membrane cleaning operations were based on manufacturer 187 recommendations, including classical alkaline (NaOH 2 %, 80°C, 20 min without pressure, 20 188 min with pressure) and acidic phases (HNO<sub>3</sub> 1 %, 50°C, 20 min), and was controlled by the 189 verification of pure water permeability  $(374 \pm 103 \text{ L} \cdot \text{h}^{-1} \cdot \text{m}^{-2} \cdot \text{bar}^{-1} \text{ at } 25^{\circ}\text{C} \text{ and } 6 \text{ m} \cdot \text{s}^{-1})$ . 190

As usual, the concentration level of the extract was characterized by the volume reduction
ratio (VRR) defined according to the volumes of permeate V<sub>p</sub> and retentate V<sub>r</sub> (Equation 1).

193 
$$VRR = \frac{V_r + V_p}{V_r} = 1 + \frac{V_p}{V_r}$$
 (1)

Each filtration was carried out in concentration mode extracting the permeate continuously.
Starting with 2.5-3 L of the product, the system was continuously fed with fresh raw extract,
maintaining the retentate volume constant (concentration at constant volume) up to VRR
between 5 and 8. Then, in order to reach a higher VRR more quickly, feeding was stopped,
allowing the volume of the retentate to decrease (concentration at variable volume). At the
end of the concentration step, the V<sub>r</sub> was still 1.5 L. During filtration, the retention rate (R) is

200 defined using Equation 2 comparing the concentrations in the permeate  $(C_p)$  and in the 201 retentate  $(C_r)$  as usual.

$$R = 1 - \frac{c_p}{c} \qquad (2)$$

203 A diafiltration step could then be added at the end of the concentration step when the targeted VRR was reached. In this case, diafiltration was carried out at constant  $V_r$  value (1.5 L) by 204 feeding the system with distilled water instead of fresh raw extract in order to compensate the 205 volume of permeate recovered. Therefore, the diafiltration was continuous, without 206 207 interruption between the concentration and the diafiltration steps. This diafiltration mode allowed water consumption to be minimized because it was carried out at the end of the 208 concentration step when V<sub>r</sub> was the lowest (Polidori et al. 2018). Diafiltration ended when 209 permeate reached a content of total soluble solids below 5  $g \cdot kg^{-1}$ . The diavolume ratio (DVR) 210 was defined as the ratio between the volume of added water  $V_w$  and  $V_r$  (Equation 3). It can 211 also be considered as a water consumption indicator. 212

213 
$$DVR = \frac{V_W}{V_r}$$
(3)

214 **2.3 Extract analysis** 

Total soluble solids (TSS) were measured with a PAL-α refractometer (Atago, Tokyo, Japan) 215 with  $\pm 0.5 \text{ g} \cdot \text{kg}^{-1}$  of bias. To assess the suspended soluble solids (SIS), a sample of precisely 216 20 g was homogenized and centrifuged at 14 000 x g for 20 min (Allegra 21 centrifuge, 217 Beckman Coulter, USA). The supernatant was discarded and replaced by 20 g of deionized 218 water and then the sample was homogenized and centrifuged again. After 3 repetitions, the 219 residue was dried at 70°C under vacuum (100 mPa) and weighted. The term dry matter (DM) 220 221 refers to the residues remaining after the total evaporation of water. DM includes both TSS and SIS. Therefore, it was calculated as the sum of these two fractions. 222

To quantify the total carotenoid content, 10 mL of the sample to be analyzed were 223 224 homogenized with 35 mL of a mixture made of ethanol/hexane (4:3 v/v) (Sigma-Aldrich, Santa-Clara, USA). After dephasing in a separating funnel, the organic phase was recovered, 225 dried with anhydrous sodium sulfate (Sigma-Aldrich, Santa Clara, USA) and its absorbance 226 was then measured at 450 nm with a Variant 50 Bio spectrophotometer (Variant Inc, 227 California, USA). Results were expressed in mg  $\beta$ -carotene equivalent using the molar 228 229 extinction coefficient of  $\beta$ -carotene at 450 nm. Carotenoid purity p was calculated as carotenoid content expressed in DM. 230

All analyses were carried out in triplicates.

#### 232 **2.4 Modelling**

Assuming that there were no losses of matter during the operation, that the system behaved 233 like a perfectly stirred reactor and that the retentions were constant, the retentate composition 234 could be predicted using a simple equation set tested in previous studies (Acosta et al., 2014; 235 Polidori et al., 2018). Indeed, since the insoluble compounds (SIS and carotenoids) were 236 completely retained by the membrane, unlike the TSS, which were not retained at all 237 (Chaparro et al., 2016; Oliveira et al., 2016; Polidori et al., 2018), carotenoid concentration 238 (C), SIS and TSS could be calculated in the final retentate from volume reduction ratio 239 (VRR), diavolume ratio (DVR) and initial values (subscript 0) using Equations 4 to 6. 240

$$C = C_0 VRR \tag{4}$$

$$SIS = SIS_0 VRR \tag{5}$$

$$TSS = TSS_0 e^{-DVR}$$
(6)

244 Therefore, for carotenoids the concentration factor in the retentate (CF) is equal to the VRR.

Since DM is the sum of SIS and TSS, the purity of carotenoids in the retentate p and thepurification factor (PF) could be assessed through Equations 7 and 8.

$$p = \frac{C_0 VRR}{SIS_0 VRR + TSS_0 e^{-DVR}}$$
(7)

248 
$$PF = \frac{(SIS_0 + TSS_0) VRR}{SIS_0 VRR + TSS_0 e^{-DVR}}$$
(8)

In this case, the purity of carotenoids cannot exceed the ratio  $C_0/SIS_0$  when DVR increases. Thus, whatever the VRR, it is not possible to exceed a maximum purification factor  $PF_{lim}$ . In order to quantify the progress of the purification, we defined the ratio between the obtained PF and  $PF_{lim}$  (Equation 9). It ranges from 0 to 1 and was called the purification rate  $\alpha$ (Equation 10).

254 
$$PF = \alpha PF_{lim} = \alpha (TSS_0/SIS_0 + 1)$$
(9)

$$\alpha = \frac{VRR}{VRR + (TSS_0/SIS_0) e^{-DVR}}$$
(10)

256

#### 257 **3. Results and discussions**

258 **3.1. Effect of transmembrane pressure** 

In order to find an optimal transmembrane pressure, preliminary trials were carried out using 259 260 the extract obtained without enzymes (Table 1) up to a VRR of around 10. In figure 2, the permeate flux (J<sub>p</sub>) during microfiltration of cashew apple extract without enzyme liquefaction 261 using 5 growing TmP (from 2.2 to 3.2 bar) were plotted versus VRR. As presented, permeate 262 263 flux abruptly decreased at the beginning as soon as concentration occurred. This initial phase is usual in crossflow microfiltration and corresponds to a rapid membrane fouling mainly due 264 to accumulation of insoluble solids on the membrane surface (external fouling) and/or into the 265 membrane pores (internal fouling). This fouling leads to an increase in the total hydraulic 266

resistance of the system and so causes the drop in transmembrane flux. Shortly afterwards, 267 268 from a VRR of around 1.2, the flux decrease slowed down, what could be linked to backtransport phenomena due to crossflow velocity that counterbalanced the input of fouling 269 270 material to the membrane. From a VRR = 3,  $J_p$  stabilized up to the final VRR. This behavior was observed irrespective of the transmembrane pressure. By comparison with many 271 references in literature that dealt with crossflow microfiltration of various fruit juices, these 272 273 last results were different (Emani et al., 2013; Fukumoto et al., 1998; Qin et al., 2015; Ushikubo et al., 2007; Wang et al., 2005). Even if the flux range was in accordance with the 274 values generally mentioned for fruit juice microfiltration (Dornier et al., 2018; Rai & De, 275 276 2009), stabilization at such a high VRR is uncommon. Generally transmembrane transfers are continuously slowed down by the increase in viscosity and fouling power of the retentate 277 during concentration (Tarabara et al., 2002). This original behavior was probably linked to the 278 279 extract composition that was quite different from classical fruit juices in terms of soluble/colloidal/insoluble fractions and led to a more moderate fouling of the membrane 280 during concentration. Indeed, it is well established that fouling not only depends on the 281 hydrodynamic conditions in the vicinity of the membrane but also on suspension 282 characteristics (Dahdouh et al., 2016). Nevertheless, because the phenomena involved in 283 284 membrane fouling are multiple and complex, further investigations should be carried out for a better understanding. This configuration is particularly favorable for an industrial application 285 as it makes it possible to reconcile high concentration factors and high treatment processing 286 rates, close to  $100 \text{ L}\cdot\text{h}^{-1}\cdot\text{m}^{-2}$ , considered very interesting from an economic point of view for 287 microfiltration of food liquids (Daufin et al., 2001). This promising performance underlined 288 the fact that the fouling property of the product was limited. 289

The figure 3 represented the stabilized permeate flux J<sub>p</sub> depending on the used TmP (from 2.2
to 3.2 bar) for a range of VRR between 1 to 9. Comparing the permeate flux for the same

VRR, it linearly increased with pressure both at low and high VRR. These results showed that 292 293 permeate fluxes were mainly impacted by the driving force of the mass transfer through the porous medium (i.e. the transmembrane pressure gradient) with a total hydraulic resistance of 294 295 the system, defined according to the generalized Darcy's law, that increased with the volumetric reduction level at low VRR and then tended to a constant value for higher VRR. 296 297 Therefore, in the chosen operating conditions, high TmP at about 3 bar has to be selected in 298 order to maximize permeate flux whatever the desired targeted concentration factor for carotenoids. These experimental results were significantly different from those obtained by 299 Polidori et al. (2018) with orange juice which showed that the effect of pressure on permeate 300 301 flux depended on VRR. The much weaker fouling power of cashew apple fiber extract could be linked, as mentioned by Dahdouh et al., (2016); Vaillant et al., (2008) and Tarabara et al., 302 (2002), to multiple factors such as its composition, particle size distribution and rheological 303 304 characteristics, related to the specific extraction press-processing, but further studies are needed to confirm this. 305

#### 306

#### 3.2. Effect of enzymatic liquefaction during extraction

Extracts obtained with and without enzyme treatment exhibited very similar TSS and SIS 307 contents (Table 1). Thus, liquefaction did not drastically modify the soluble/insoluble solid 308 309 distribution in the final product. On the contrary, carotenoid content was 30% higher in the enzyme-treated product, which confirmed the enzyme liquefaction enhanced extractable 310 fraction of carotenoids. This observation is probably due to cell wall weakening leading to the 311 depolymerization of pectin chains through polygalacturonase and pectin-lyase activities 312 (Çinar, 2005). It favored cell breakdown during the pressing and so allowed a better release of 313 314 carotenoids. This higher recovery of phytochemicals using enzymes is consistent with various other studies (Acosta et al., 2014; Carneiro et al., 2002; Çinar, 2005; Puri et al., 2012). 315

Both these extracts then underwent microfiltration up to a VRR of about 20 using high 316 317 transmembrane pressure (Figure 4). First, repetitions showed that the process was repeatable with a difference of permeate flux for the same operating conditions of around 10%, which is 318 319 similar to the repeatability usually achieved using a crossflow microfiltration pilot unit at laboratory scale. Second, the interest of the liquefaction as a pre-treatment is clearly 320 demonstrated from the point of view of process performance. Indeed, combining enzyme 321 liquefaction with physical treatment resulted in the permeate flux being multiplied by 1.5. For 322 the extract with enzyme liquefaction, after a first drop of up to VRR=3, the permeate flux 323 stopped decreasing and remained at around 140 L·h<sup>-1</sup>·m<sup>-2</sup> up to VRR=19. Therefore, the 324 325 extraction procedure resulted in a multiphasic solution being obtained, in which high fouling compounds were removed. This positive effect of enzyme liquefaction on the filterability has 326 already been well illustrated in many cases with fruit juices (Domingues et al., 2014; 327 328 Machado et al., 2012; Pinelo et al., 2010; Rai et al., 2007). It is not only related to the viscosity decrease of the product due to depolymerization and demethylation of the soluble 329 330 pectic compounds, but probably also to changes of the fouling power of the insoluble fraction (Dahdouh et al., 2016; Vaillant et al., 2008). These insoluble solids mainly consist of tissue 331 and cell fragments that can be greatly modified by pectinolytic and cellulolytic enzymes 332 through the deconstruction of cell walls. Therefore, the interest of the enzymatic treatment 333 was twofold: it led not only to an increase in the carotenoid extraction yield but also to a 334 significant improvement in the performance of the subsequent operation of separation. 335 Because the chosen enzymes were classical adjuvants commonly used in fruit juice industry, 336 they were not purified and consequently were not very expensive. So as often in fruit juice 337 processing, the additional cost of using enzymes would probably be justified by the reduction 338 in investment (membrane area needed) and operating costs (time, energy). 339

These first trials also confirmed that in all the cases, with or without enzyme liquefaction, carotenoids and SIS were completely retained by the membrane (neither carotenoid nor SIS were found in the permeate, R = 1) and that there was no solute retention (same TSS content in permeate and retentate, R = 0).

344

#### 3.3. Purification by diafiltration

To improve the purity of the carotenoids, a diafiltration step was added to the concentration 345 346 process. Diafiltration is simple to carry out, but for industrial application a compromise between permeate flux and water consumption has to be found (Fikar et al., 2010). Indeed, for 347 a targeted purification rate, if the diafiltration is implemented at the beginning of the 348 349 concentration step, i.e. at low VRR, the permeate flux will be at a very good level but the volume of water needed will be substantial. On the contrary, the higher the VRR chosen for 350 diafiltration, the worse the flux might be, but at the same time, the amount of water needed 351 will be lower. In the case of cashew apple extract, because permeate fluxes were maintained 352 at a high value at high VRR, it was clear that priority had to be given to water savings. For 353 354 that reason, we chose to conduct diafiltration at the end of the concentration phase. When the 355 retentate volume reached the minimal operational volume in the system, and therefore targeted VRR was achieved, cashew apple extract was replaced by water to feed the device 356 357 and diafiltration began.

Figure 5 represents the evolution of DVR, VRR, TSS and  $J_p$  as a function of time during the process that included diafiltration. The first part of the filtration referred to a regular VRR increase of up to 6-7. During this phase, the volume of retentate was maintained constant by compensating the volume of permeate removed through feeding the system with the same volume of cashew apple extract. Afterwards, a rapid increase of VRR was observed as the feed was stopped in a second phase and thus the volume of the retentate circulating in the concentration loop rapidly decreased. Once the VRR setpoint was reached, diafiltration was

initiated compensating the volume of extracted permeate by the same volume of water and so 365 366 DVR increased. It is worth noting that after the initial drop, permeate fluxes remained almost constant throughout the concentration and diafiltration steps. Only a slight increase was 367 observed during the diafiltration step, due to the diminution of viscosity caused by dilution 368 with water. In addition, the values obtained were very similar to those obtained previously. 369 From around 230 L·h<sup>-1</sup>·m<sup>-2</sup> at the beginning, they stabilized at VRR=19 at about 130 L·h<sup>-1</sup>·m<sup>-</sup> 370 <sup>2</sup> and 75  $L \cdot h^{-1} \cdot m^{-2}$  for enzyme liquefied and untreated extracts respectively. By using 371 enzymes, the time needed to reach VRR=19 was 30% shorter and the time needed to reach a 372 DVR of 3.5, was reduced by 40%. As expected, TSS decreased exponentially in the system as 373 374 soon as the diafiltration step started. This also implied that the system could be considered as being very similar to a perfectly stirred reactor. Obviously, the time needed to reach a TSS 375 below 5  $g \cdot kg^{-1}$  was much shorter for the enzyme treated extract because of the greater 376 377 permeate flux.

Characterization results highlighted that both concentrates exhibited close values considering 378 379 biochemical analyses (Table 2). TSS decreased considerably following diafiltration. Between 92-96% of solutes were removed from the retentate. While for the insoluble fraction (SIS), it 380 was concentrated 18 to19-fold in accordance with the final VRR. Total carotenoid content 381 382 was logically higher for enzyme-treated retentate because of the difference between initial contents and of the higher VRR reached. The ratio between the concentration factor CF and 383 VRR was about 1.04 and 1.01 with and without enzymes respectively. Therefore, 384 concentration factors for carotenoids were almost equal to the VRR with and without enzyme 385 liquefaction after diafiltration, as expected. This result showed that there was no loss in 386 carotenoids during processing. It is concomitant with Polidori et al. (2018) who demonstrated 387 similar carotenoid behavior during orange juice microfiltration, using a 0.2 µm membrane 388 389 with a CF/VRR ratio of 1.06 with or without diafiltration. Chaparro et al. (2016) and Oliveira et al. (2016), who studied lycopene concentration from watermelon juice, found a ratio of
between 1.00 and 1.06, confirming complete retention of carotenoids. For cashew apple fiber
extracts, with or without enzyme liquefaction, the process resulted in a significant
improvement of the purity of carotenoids with respect to the total dry matter reaching a
purification factor of around 5.

**395 3.4. Modelling** 

396 From the initial characteristics of the extract (TSS<sub>0</sub>, SIS<sub>0</sub>, C<sub>0</sub>) and assuming that SIS/carotenoid (insoluble fraction) and the TSS (soluble fraction) retentions were respectively 397 equal to 1 and zero, theoretical final values for all characteristics could be evaluated 398 399 combining equations 4 to 8 for the targeted VRR and DVR values. In all the cases, the predicted compositions of the final retentate were very close to the experimental values (Table 400 2). A slight deviation can be noticed for TSS, probably because the hypothesis of a perfectly 401 stirred reactor was not entirely true. Nevertheless, these results validated the model with its 402 assumptions. Thanks to a simple set of calculations, it is thus possible to predict the quality of 403 404 the extract or to simulate situations without carrying out extensive experiments. Therefore, the 405 question of purification rate can be put forward in order to better optimize the diafiltration step. At VRR of 18-19 with DVR of 3-4, the reached purification rates  $\alpha$  were close to the 406 maximum, over 0.99. Obviously, the maximum purity that can be achieved with the process is 407 indeed reached. However, through calculation, we showed that a DVR of 1.5 (that 408 corresponds to a final TSS of 11-12 g·kg<sup>-1</sup>) would be sufficient to reach a  $\alpha$  of 0.95, which is 409 already a very interesting value. Therefore, the maximum purity that is achievable can be 410 reasonably attained at lower DVR (1.5 instead of 4), allowing water consumption to be more 411 than halved, to reduce processing time by around 20% and to decrease the production of 412 permeate, considered here as an effluent to be treated, by 10%. 413

This model can be easily generalized for all the VRR/DVR combinations. For example, it can 414 415 be used to generate charts that link DVR and  $\alpha$  as a function of the chosen concentration factor (Figures 6 and 7). These couples of figures are presented for two different TSS<sub>0</sub>/SIS<sub>0</sub> 416 417 ratios. The first one corresponds to cashew apple fiber extract with a ratio of 4, and the second one corresponds to a classical fruit juice with a ratio of 33. These charts could be useful to 418 quickly determine the DVR to be used for given concentration level and purification rate. We 419 420 can notice in the equation set how important the TSS<sub>0</sub>/SIS<sub>0</sub> rate is. The higher this quotient and the lower the concentration factor to be reached, the higher the DVR needed to obtain a 421 targeted purification level. Applied to our extract that had a TSS<sub>0</sub>/SIS<sub>0</sub> value of 4 plotted in 422 423 figure 6 or to a citrus fruit juice with a TSS<sub>0</sub>/SIS<sub>0</sub> ratio of 33 for instance illustrated in figure 7 (Polidori et al., 2018), the obtained curve pattern is completely different. 424

For industrial applications a compromise should often be found between permeate flux,
concentration factor, purification rate and water consumption. In this respect, the tested model
is an interesting tool that should help for the guidance of the process considering the
functional potential of the carotenoid concentrate and, the economic cost of the operation.

#### 429 **4.** Conclusion

The aim of this work was to evaluate crossflow microfiltration in order to produce a 430 431 concentrate that is enriched and purified in carotenoids from the extract of a cashew apple byproduct. The process coupled with enzyme liquefaction and using a transmembrane pressure 432 around 3 bar, allowed the carotenoid content to be multiplied by up to 19 while keeping the 433 permeate flux above  $100 \text{ L} \cdot \text{h}^{-1} \cdot \text{m}^{-2}$ . In the case of cashew apple fiber extract, this step 434 complies with the reduction of the energy costs which might render the expense of purchasing 435 the enzyme negligible when compared to the increase in volume production. Adding a 436 diafiltration step led to a 5-fold purification of the carotenoids. The final concentrate 437 contained between 0.2 and 0.3  $g kg^{-1}$  of carotenoids in dry matter. A simple model was 438

validated that predicted carotenoid concentration and purity according to the filtration 439 440 conditions, that is to say the VRR and DVR. This model can be used as a decision aid tool for piloting the process in relation to quality, economic and environmental considerations. This 441 study also showed that cashew apples fibers, that are a low-cost and abundant by-product 442 from the fruit juice industry, especially in Brazil, could be easily treated in order to obtain 443 interesting carotenoid concentrates through the described process. The final extract can be 444 directly used as a natural food coloring and provides an important added value. So, crossflow 445 microfiltration can find its place in sustainable development for the cashew apple processing 446 chain. However, to consider any industrial application, further studies must be conducted on a 447 448 larger scale, with higher membrane area in order to validate the robustness of the process. Moreover, other aspects such as environmental impact and economic criteria (investment and 449 operation costs) have to be considered in order to demonstrate the interest of an industrial line 450 establishment and scale up, according to the targeted production capacity, equipment 451 availability and local constraints. Eventually, the compositional characterization of the extract 452 has to be completed in order to better evaluate its potential but also to better understand the 453 impact of the process on its composition. The stability of the extract during storage should be 454 investigated in order to determine its shelf life as well. 455

456

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### 590 **TABLES**

591

Table 1: Composition of the initial cashew apple extracts obtained by pressing, coupled with
or without enzyme liquefaction, and used as raw materials for crossflow microfiltration
experiments (average value and standard deviation evaluated with 3 repetitions). TSS: total
soluble solids; SIS: suspended insoluble solids; DM: dry matter; C: carotenoid content; p:
carotenoid purity.

TSS  $(g \cdot kg^{-1})$ SIS  $(g \cdot kg^{-1})$  $DM (g \cdot kg^{-1})$  $C(mg\cdot kg^{-1})$  $p (mg \cdot kg^{-1})$ Without 52 12.7 64.7 2.9 45 enzyme (1) (0.1)(1.1)(0.1) (2)With 52 13.0 65.0 3.8 58 (1) (0.2)(1.2)(0.1)(3) enzyme

597

598 Table 2: Experimental (Exp.) and calculated (Calc.) composition of the concentrates obtained

599 by microfiltration with and without enzyme liquefaction (average value and standard

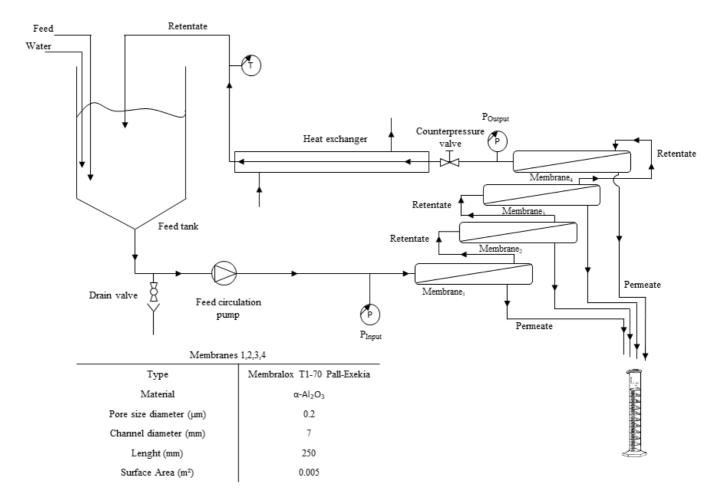
600 deviation evaluated with 3 repetitions). VRR: volume reduction ratio; DVR: diavolume ratio;

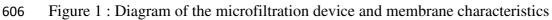
TSS: total soluble solids; SIS: suspended insoluble solids; DM: dry matter; C: carotenoid

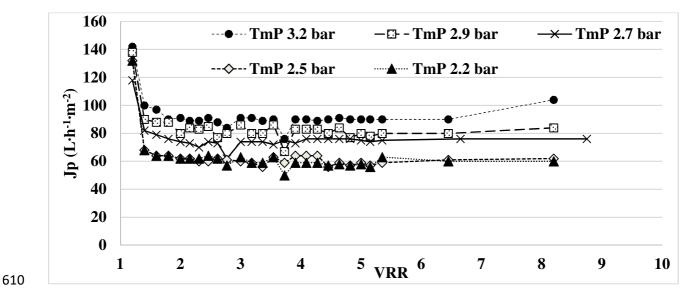
Initial extract	VRR	DVR		TSS (g·kg <sup>-1</sup> )	SIS (g·kg <sup>-1</sup> )	DM (g·kg <sup>-1</sup> )	C (mg·kg <sup>-1</sup> )	p (mg·kg <sup>-1</sup> )	PF
Without enzyme	17.8	3.81	Exp.	4	227.0	231.0	54	234	5.2
				(1)	(0.6)	(1.6)	(2)	(10)	(0.5)
			Calc.	1	226.1	227.1	52	228	5.1
With enzyme	19.1	3.13	Exp.	2	248.4	250.4	73	292	5.0
				(1)	(1.5)	(2.5)	(3)	(15)	(0.5)
			Calc.	1	248.3	249.3	73	290	5.0

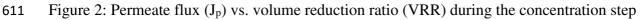
602 content; p: carotenoid purity.

# 604 FIGURES

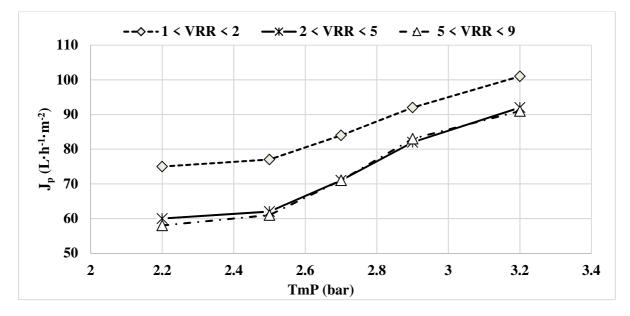








by crossflow microfiltration of the cashew apple fiber extract without enzyme liquefaction at
5 transmembrane pressures (TmP).

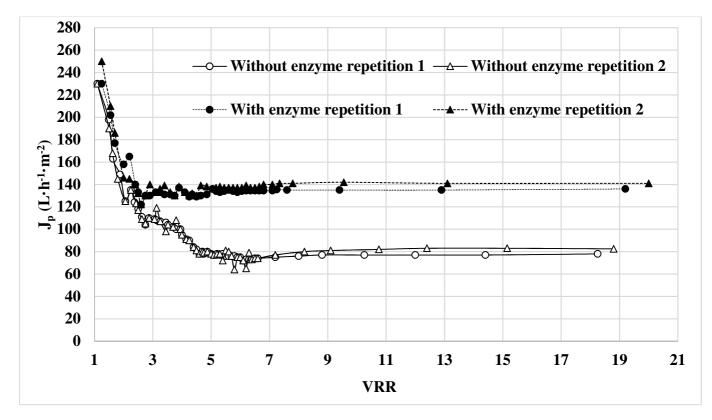


 $\label{eq:Figure 3: Average permeate flux (J_p) vs. transmembrane pressure (TmP) for different intervals$ 

623 of volume reduction ratio (VRR) during the concentration step by microfiltration of the

624 cashew apple fiber extract without enzyme liquefaction.

625



626

Figure 4: Permeate flux  $(J_p)$  vs. volume reduction ratio (VRR) during the concentration by microfiltration of cashew apple extracts with and without enzyme liquefaction (TmP = 3.2 bar).

630

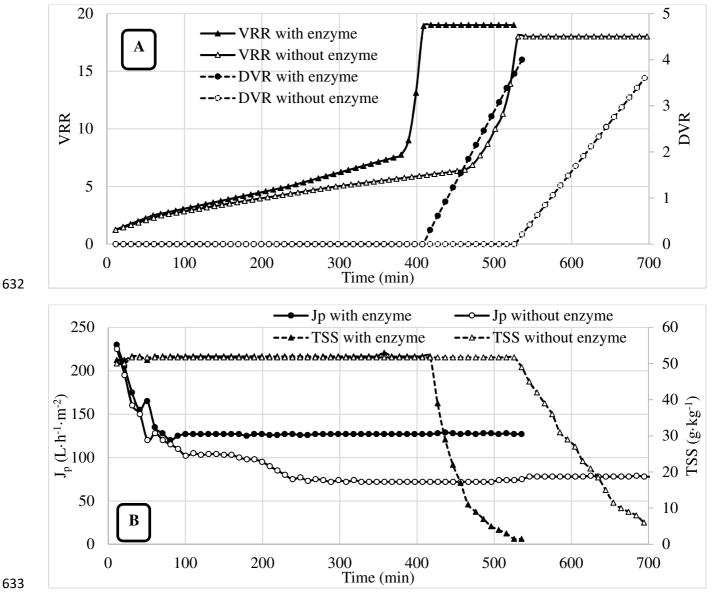


Figure 5: Evolution of A- volume reduction ratio (VRR) and diavolume ratio (DVR), and Bpermeate flux  $(J_p)$  and total soluble solids in the concentrate (TSS) versus time during the

636 concentration and the purification by microfiltration and diafiltration of the cashew apple

637 extracts with and without enzyme liquefaction (TmP = 3.2 bar).

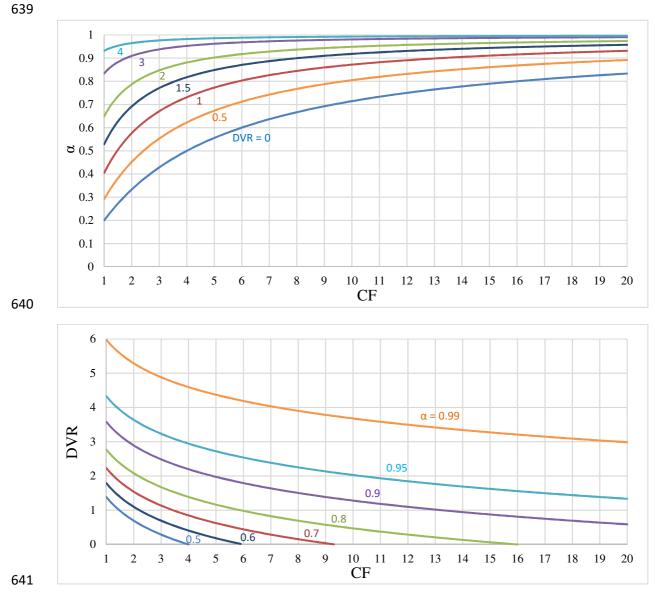
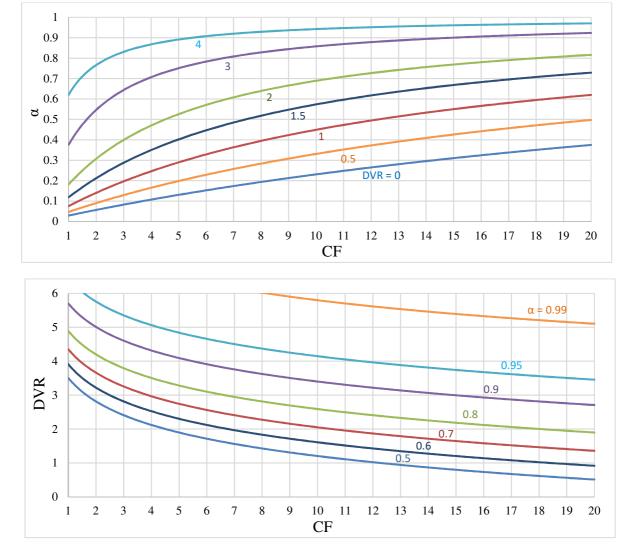


Figure 6: Predicted charts from the model, plotting the purification rate of carotenoids ( $\alpha$ ) that is

achievable for different diavolume ratios (DVR) and the DVR that is requiered to reach different  $\alpha$ , as a function of the concentration factor (CF), for a cashew apple fiber extract with an initial total soluble and suspended insoluble solids ratio **TSS<sub>0</sub>/SIS<sub>0</sub> of 4**.

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Figure 7: Predicted charts from the model, plotting the purification rate of carotenoids ( $\alpha$ ) that is

achievable for different diavolume ratios (DVR) and the DVR that is requiered to reach different  $\alpha$ , as a function of the concentration factor (CF), for a citrus juice with an initial total soluble and suspended insoluble solids ratio **TSS<sub>0</sub>/SIS<sub>0</sub> of 33**.

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