



**HAL**  
open science

## Influence of the pore size and porosity of selective laser melted Ti6Al4V ELI porous scaffold on cell proliferation, osteogenesis and bone ingrowth

Ziyu Chen, Xingchen Yan, Shuo Yin, Liangliang Liu, Xin Liu, Guorui Zhao, Wenyu Ma, Weizhong Qi, Zhongming Ren, Hanlin Liao, et al.

### ► To cite this version:

Ziyu Chen, Xingchen Yan, Shuo Yin, Liangliang Liu, Xin Liu, et al.. Influence of the pore size and porosity of selective laser melted Ti6Al4V ELI porous scaffold on cell proliferation, osteogenesis and bone ingrowth. *Materials Sciences and Engineering: C*, 2020, 106, pp.110289 -. 10.1016/j.msec.2019.110289 . hal-03488879

**HAL Id: hal-03488879**

**<https://hal.science/hal-03488879v1>**

Submitted on 20 Jul 2022

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Distributed under a Creative Commons Attribution - NonCommercial 4.0 International License

# 1 **Influence of the pore size and porosity of selective laser melted Ti6Al4V ELI porous scaffold on** 2 **cell proliferation, osteogenesis and bone ingrowth**

3 Ziyu Chen <sup>1,3,4#</sup>, Xingchen Yan <sup>2,5#\*</sup>, Shuo Yin <sup>7</sup>, Liangliang Liu <sup>1,3,4#</sup>, Xin Liu <sup>1,3,4</sup>, Guorui Zhao <sup>2</sup>, Wenyu Ma <sup>2</sup>,

4 Weizhong Qi <sup>1,3,4</sup>, Zhongming Ren <sup>6</sup>, Hanlin Liao <sup>5</sup>, Min Liu <sup>2,\*</sup>, Daozhang Cai <sup>1,3,4\*</sup>, Hang Fang <sup>1,3,4\*</sup>

5 1. Department of Orthopedics, The Third Affiliated Hospital of Southern Medical University, No.183, Zhongshan  
6 West Avenue, Tianhe District, Guangzhou 510630, Guangdong, P.R. China

7 2. National Engineering Laboratory for Modern Materials Surface Engineering Technology; The Key Lab of  
8 Guangdong for Modern Surface Engineering Technology; Guangdong Institute of New Materials, Guangzhou  
9 510651, P.R. China

10 3. Academy of Orthopedics, Guangdong Province, P.R. China

11 4. Orthopedic Hospital of Guangdong Province, P.R. China

12 5. ICB UMR 6303, CNRS, Univ. Bourgogne Franche-Comté, UTBM, F-90010 Belfort, France

13 6. Shanghai University & State Key Laboratory of Advanced Special Steel, Shanghai 200072, P.R. China

14 7. Trinity College Dublin, The University of Dublin, Department of Mechanical and Manufacturing Engineering,  
15 Parsons Building, Dublin 2, Ireland

16 **Abstract:** This paper systematically investigates the biomedical performance of selective laser melted (SLM) porous  
17 Ti6Al4V ELI scaffolds for bone implantation through *in vitro* and *in vivo* experiments. Scaffolds with pore sizes of 500  
18  $\mu\text{m}$ , 600  $\mu\text{m}$  and 700  $\mu\text{m}$  and porosities of 60% and 70% were manufactured in order to explore the optimum pore size  
19 and porosity. Rat bone marrow mesenchymal stem cells (rBMMSCs) were used in the *in vitro* experiments. Cell  
20 Counting Kit-8, live/dead staining and scanning electron microscope were used to assess the cytotoxicity of the porous  
21 scaffolds. DNA content quantification was performed to investigate cell proliferation on the porous scaffolds. The  
22 osteogenic differentiation of cells was measured by alkaline phosphatase (ALP) activity and osteogenic gene expressions,  
23 including bone morphogenetic protein-2 (BMP-2), collagen type 1 $\alpha$ 1 (COL-1), osteocalcin (OCN), osteopontin (OPN)  
24 and runt-related transcription factor-2 (RUNX-2). The Sprague-Dawley (SD) rat models with distal femoral condyles  
25 defect were used in the *in vivo* experiments. Micro-CT analysis and histological analysis were performed after  
26 implantation surgery to reveal the bone ingrowth into the porous scaffolds. All *in vitro* data were analyzed by one-way  
27 ANOVA followed by Tukey post hoc tests, *in vivo* data were analyzed using Kruskal-Wallis ANOVA and  
28 Conover-Inman post-hoc test. Based on the *in vitro* and *in vivo* experiments, it is found that the porous scaffolds  
29 manufactured by SLM did not induce a cytotoxic effect. Among all the porous scaffolds, the scaffold with a pore size of  
30 500  $\mu\text{m}$  and porosity of 60% showed the best cell proliferation and osteogenic differentiation (*in vitro* experiments) and  
31 bone ingrowth (*in vivo* experiments).

---

# These authors contribute equally to this work: Ziyu Chen, Xingchen Yan, Liangliang Liu

\* Corresponding authors: Xingchen Yan (xingchen.yan@utbm.fr); Min Liu (liumin@gdas.gd.cn); Daozhang Cai (cdz@smu.edu.cn);  
Hang Fang (fanghang@smu.edu.cn)

32 **Keywords:** bone defect; pore size; porosity; Ti6Al4V ELI; osteogenesis; bone ingrowth

## 33 1 Introduction

34 Arthroplasty is an effective treatment of arthropathy as it can relieve pains, restore physical activities, and improve  
35 life quality of patients. Over the past 20 years, there was a considerable increase in the number of patients in the world  
36 who underwent arthroplasty. More than 800,000 patients receive primary arthroplasty every year with an annual growth  
37 rate of 20% [1]. However, the service life of an artificial joint prosthesis is normally limited due to the occurrence of  
38 aseptic loosening, joint instability and infection, and revision of previous arthroplasty is required. Many difficult issues  
39 may inevitably arise during the revision surgery, of which osseous defects are the most intractable situation [2]. Currently,  
40 the treatment of large or non-healing bone defects is generally performed with autografts or allografts. Despite regarded  
41 as the “golden standard” for repairing bone defects, autologous bone graft also encounters drawbacks. Donor site  
42 complications is a typical drawback of autologous bone graft. Allogeneic bone transplantation may cause immune  
43 rejection and disease transmission, which significantly harm the health of patients. Therefore, in recent years, synthetic  
44 alternatives are becoming a practicable and fascinating option [3].

45 Bio-ceramic bone implant is a bone graft substitute, consisting of calcium and phosphates, demonstrating good  
46 bioactivity and biodegradation properties. However, as degradation gradually occurs, the reduction of the mechanical  
47 properties of the implant may bring potential risks to the recovery. Alternatively, implant made by metals is another  
48 option for bone graft substitute. However, metal implants naturally have much higher elastic modulus (e.g. 100–140 GPa  
49 for Ti alloys [4], 210–253 GPa for Co alloys [5] and 190–210 GPa for stainless steel [6]) than bone tissues (0.5–20 GPa  
50 [7]). Such incompatible elastic modulus may lead to implant loosening or autogenous bone fracture. Due to the inferior  
51 biomechanical compatibility of the traditional metallic implants, the interfacial adhesion between the hard tissues and the  
52 implant is unstable. Porous structure has been recognized as an effective way to eliminate this mismatch of elastic  
53 modulus [8]. By adjusting pore size and porosity, an ideal metal implant with optimized density, strength and mechanical  
54 compatibility with the bone tissues can be achieved, which can effectively prevent osteonecrosis and osteogenesis  
55 deformity around the implant [9, 10]. In addition, the internal perforated porous structure is beneficial to the adhesion,  
56 proliferation and differentiation of mesenchymal stem cells. The porous structure also provides high interfacial bond area  
57 for vascularization and bone ingrowth [11], promoting the biological fixation of implants and bones.

58 Conventional manufacturing technologies for porous metals include powder sintering, deposition, and chemical  
59 reaction. However, due to the technological limitations, these methods generally bring undesirable properties to the  
60 implants. Powder sintering results in inferior mechanical properties of the implants due to the existence of residual  
61 defects. Deposition method suffers from a slow sedimentation rate and a high production cost. Chemical reaction cannot

62 accurately control pore size and porosity distribution, which is crucial to porous implants [12]. Therefore, considering the  
63 limitations of the aforementioned technologies, a promising manufacturing process with high controllability and  
64 repeatability for producing reliable mechanical and morphological properties of porous implants is urgently needed [13].

65 Selective laser melting (SLM) as a novel additive manufacturing technique has drawn increasing attention from both  
66 industrial and medical communities. With the assistance of computer-aided design (CAD), successive and selective  
67 powder bed fusion can be achieved through a high-energy laser beam [14, 15]. The SLM scaffold is then fabricated via  
68 the rapid solidification and the thin welding between each deposited layer. Due to the high freedom in complex geometry  
69 design, SLM can be used in the production of porous implants [16] by tailoring their pore size and porosity to satisfy  
70 specific requirements of different individuals [17, 18]. Recently, it has been reported that this technology can  
71 manufacture porous implants with profitable mechanical and biological properties [19-21]. Among all the relevant  
72 studies, there are few works concerning the effect of porosity and pore size on the mechanical and biological properties  
73 of SLM implants.

74 Fuduka et al. [19] studied the osteoinduction of SLM Ti implants with a channel structure. In these works,  
75 significant osteoinduction was observed when the pore sizes were 500 and 600  $\mu\text{m}$ . Wauthle et al. [12] investigated the  
76 SLM dodecahedron porous pure Ta implants with the average pore size about 500  $\mu\text{m}$  and porosity of 80 %. The *in vivo*  
77 test showed favorable biocompatibility of the SLM Ta implants and a yield strength of 12.7 MPa. Wally et al. [22]  
78 analyzed the role of the pore size of SLM Ti6Al4V porous structure in dental applications. However, no decisive  
79 conclusions were drawn due to the lack of regularity between the pore structure and osteointegration. Taniguchi et al. [2]  
80 reported that the SLM porous Ti6Al4V implant with a designated porosity of 65% and a pore size of 600  $\mu\text{m}$  had more  
81 comparable mechanical strength with the bone, higher fixation ability and more bone ingrowth than those with a pore  
82 size of 300 and 900  $\mu\text{m}$ . Moreover, based on a well-designed experiment, Wieding et al. [23] concluded that the SLM  
83 porous Ti6Al4V scaffold with a pore size of 700  $\mu\text{m}$  could stabilize segmental bone defects in the metatarsus of sheep. In  
84 addition to the aforementioned SLM porous Ti-based implants, the porosity and pore size of diffusion bonded porous Ti  
85 were also studied by Li et al. [24] and Chang et al. [25]. It was reported that the porous Ti with a porosity of 60-70%  
86 could greatly match the human trabecular bone in terms of mechanical properties. Furthermore, the porous Ti with a  
87 porosity of 70% and a pore size of 313  $\mu\text{m}$  and 390  $\mu\text{m}$  exhibited the best cell proliferation and bone ingrowth capability.  
88 However, it is worth noting that the surface of diffusion bonded porous meshes is much smoother than that of SLM  
89 porous structure. Hence, they may have different responses to cells.

90 Despite having a number of investigations, the optimum porosity and pore size of implants for bone ingrowth,

91 particularly the SLM porous implants, is still not well understood. A systematic investigation on the effect of the porosity  
 92 and pore size of SLM porous scaffolds on the mechanical and biological properties is urgently needed in order to  
 93 improve the reliability and safety of SLM porous scaffolds in medical applications. Therefore, the aim of this work is to  
 94 explore the optimum porous structure in terms of porosity and pore size of a SLM Ti6Al4V ELI scaffold for biomedical  
 95 implant. In order to achieve this objective, various scaffolds with pore sizes of 500, 600 and 700  $\mu\text{m}$  and porosities of 60%  
 96 and 70% were manufactured by SLM. Elaborate *in vitro* and *in vivo* experiments were then conducted to evaluate the  
 97 biological performance of the porous scaffolds.

## 98 2 Experimental details

### 99 2.1 Feedstock materials

100 Ti6Al4V ELI (Extra Low Interstitials, Grade 23) is known to have excellent mechanical and biological properties [8,  
 101 26] than other Ti alloys. As compared to Ti6Al4V (Grade 5), Ti6Al4V ELI contains lower levels of oxygen, nitrogen,  
 102 carbon and iron than, exhibiting better ductility and improved fracture toughness. Considering the superior biological  
 103 properties of Ti6Al4V ELI, gas atomized spherical Ti6Al4V ELI powder (EOS GmbH, Germany) was supplied as  
 104 feedstock in this work. The size range of the powder is measured to be 22-51  $\mu\text{m}$  by a laser particle sizer (Mastersizer  
 105 2000, Malvern Instruments Ltd., UK). The chemical composition of the Ti6Al4V ELI provided by supplier is listed in  
 106 Table. 1.

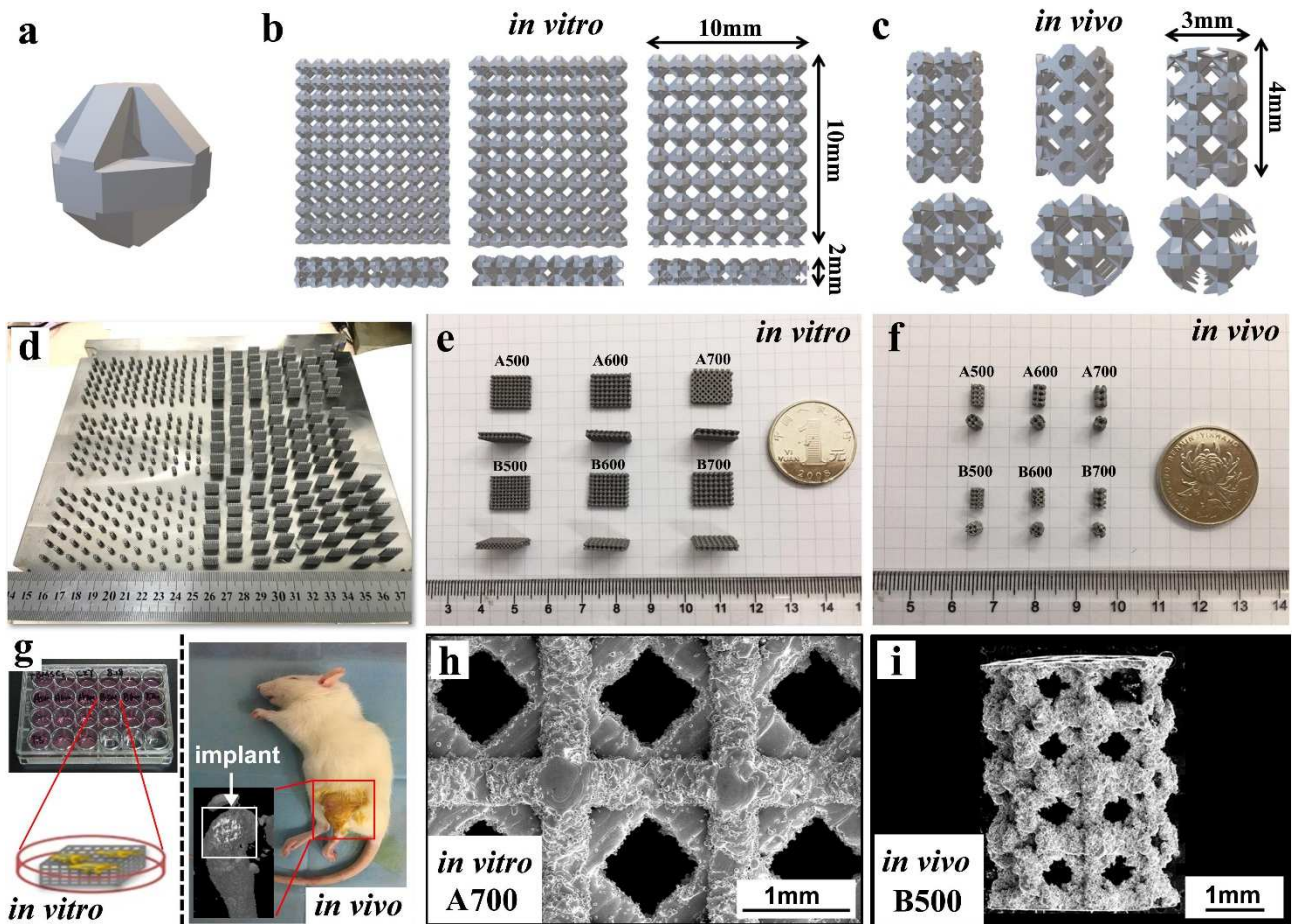
107 **Table. 1.** Chemical composition of the Ti6Al4V ELI powder used in this work

Element	Ti	Al	V	O	N	C	H	Fe
wt.%	Balance	5.5-6.5	3.5-4.5	<0.13	<0.03	<0.08	<0.012	<0.25

### 108 2.2 Design and manufacture of porous Ti6Al4V ELI scaffolds

109 Detailed information of the SLM Ti6Al4V ELI porous scaffolds used in this work is provided in Fig.1. Octahedron  
 110 crystal lattice with horizontal struts was adapted as the basic unit of the porous structure as shown in Fig. 1a. The  
 111 overhanging cuboid strut has an inclined angle of 45°. The octahedron lattice can improve the isotropic properties of the  
 112 structure under multidirectional compressive force and hence confers high safety as the bone substitute. The structure of  
 113 the scaffolds was designed using CAD software UG NX 10 (Siemens PLM Software, Germany). Fig. 1b and 1c show the  
 114 CAD-designed porous Ti6Al4V ELI scaffolds in flat shape (10 mm  $\times$  10 mm  $\times$  2 mm, layer thickness of 2 mm) for *in*  
 115 *vitro* experiments and in cylindrical shape (3 mm in diameter and 4 mm in length) for *in vitro* experiments, respectively.

116 By referring the previous works and considering the processing accuracy of the SLM machine used in this work, the  
 117 scaffolds were designed to have porosities of 60% and 70%, and pore sizes of 500, 600 and 700  $\mu\text{m}$ . For the convenience  
 118 of the following result demonstration and discussion, the scaffolds with a porosity of 60% and pore sizes of 500, 600 and  
 119 700  $\mu\text{m}$  were annotated as A500, A600 and A700, respectively. Similarly, the scaffolds with a porosity of 70% and pore  
 120 sizes of 500, 600 and 700  $\mu\text{m}$  were annotated as B500, B600 and B700, respectively. For emphasizing the advantages of  
 121 the porous scaffolds, a solid plate (10 mm  $\times$  10 mm  $\times$  2 mm) was also manufactured by SLM and compared with the  
 122 porous scaffolds in the *in vitro* experiments. As a reference, the solid plate was annotated as REF1.



123  
 124 **Fig. 1.** Design and manufacture of the Ti6Al4V ELI porous scaffolds (a) A single octahedral cell, (b) CAD-designed porous Ti6Al4V  
 125 ELI scaffolds in flat shape (10 mm  $\times$  10 mm  $\times$  2 mm, layer thickness of 2 mm) for *in vitro* experiments, (c) CAD-designed porous  
 126 Ti6Al4V ELI scaffolds in cylindrical shape (3 mm in diameter and length 4 mm in length) for *in vivo* experiments, (d) photo of the  
 127 as-fabricated Ti6Al4V ELI scaffolds on a Ti substrate, (e) high-magnification photo of the scaffolds for *in vitro* experiments, (f)  
 128 high-magnification photos of the scaffolds for *in vivo* experiments, (g) schematic of the *in vitro* and *in vivo* experiments, (h) SME  
 129 image of A700 scaffold used for *in vitro* experiments (i) SME image of B500 used for *in vivo* scaffold experiments.

130 EOS M290 system (EOS GmbH Germany) was used to produce Ti6Al4V ELI scaffolds. The system is equipped  
 131 with an Yb-Fiber laser (1064 nm) with a spot size of 100  $\mu\text{m}$ . Optimized manufacturing parameters were applied in the  
 132 experiments with a laser power of 240 W, a scanning speed of 240 mm/s, a layer thickness of 30  $\mu\text{m}$  and a hatch distance

133 of 50  $\mu\text{m}$  [27, 28]. Fig. 1d shows the photo of the as-fabricated SLM Ti6Al4V ELI scaffolds on a Ti substrate. The  
134 high-magnification photos of the scaffolds for *in vitro* and *in vivo* experiments are shown in Fig. 1e and f, respectively.

135 Fig. 1g shows the schematic of the *in vitro* and *in vivo* experiments. rBMSCs were used to investigate the  
136 cytotoxicity and proliferation and osteogenic differentiation of the cells on the porous scaffolds. The rat model with distal  
137 femoral condyles defect were used to investigate the effect of bone ingrowth into the porous scaffolds. Fig. 1h and i show  
138 the scanning electron microscope (SEM, FEI Nova NanoSEM 450) images of A700 scaffold used for *in vitro*  
139 experiments and B500 scaffold used for *in vivo* experiments, respectively. It can be seen that the waviness and staircase  
140 on the strut surfaces slightly reduce the dimensional accuracy of the SLM porous scaffolds as compared to the original  
141 CAD design (Fig. 1b and c), which has also been reported in previous work [8, 29].

### 142 **2.3 Porous scaffolds preparation, water contact angle, protein adsorption**

143 The porous Ti6Al4V ELI scaffolds were ultrasonically cleaned in ethanol and double distilled water for 15 minutes,  
144 dried in a furnace at 65 °C for 1 hour and sterilized in an autoclave (120 °C for 20 minutes) before they were used in *in*  
145 *vitro* and *in vivo* studies. Water contact angles of the scaffolds were measured by a contact angle goniometer (KRUSS,  
146 Germany). Liquid droplet was dropped vertically onto the surface in the central area of scaffolds and the shape of the  
147 liquid drop (diameter about 2.3 mm) was captured by a camera and analyzed using the corresponding software (n = 3).  
148 For protein adsorption study, the porous scaffolds (n = 3) were put into 500  $\mu\text{L}$  1 g/L bovine serum albumin (fraction V,  
149 Germany) solution prepared from phosphate buffer saline (PBS, pH 7.4) in a 24-well plate. After incubation for 1 hour  
150 and 24 hours at 37 °C, the scaffolds were carefully washed by PBS and 500  $\mu\text{L}$  2% sodium dodecyl sulfate solution  
151 prepared from PBS was used to elute the adsorbed proteins. BCA Protein Assay Kit (Beyotime, Haimen, China) was used  
152 to estimate the adsorbed protein concentration. The absorbance was measured using a microplate absorbance reader  
153 (synergy HTX multi-mode reader, USA) at 562 nm.

### 154 **2.4 Isolation and culture of rat bone marrow mesenchymal stem cells**

155 The Sprague-Dawley (SD) rats were purchased from the Animal Experimental Center of Southern Medical  
156 University. All procedures were performed in accordance with the guidelines of the University Research Ethics  
157 Committee of Southern Medical University. rBMSCs were obtained from the bone marrow of two-week-old rats, as  
158 reported previously [30]. Specifically, both femurs and tibias were aseptically dissected after the euthanasia of the rats.  
159 The bone marrow contents were flushed out from the diaphysis with minimal essential medium alpha basic ( $\alpha$ -MEM,



160 Gibco, USA), collected by centrifuging, resuspended in a growth medium containing  $\alpha$ -MEM, 10% (v/v) fetal bovine  
161 serum (FBS, Gibco, USA) and antibiotics (100 unit/mL penicillin, 100  $\mu$ g/mL streptomycin; Gibco, USA), and cultured  
162 in a humidified atmosphere with 5% CO<sub>2</sub> at 35 °C. The medium was refreshed every 3 days. When the adherent cells  
163 grew to about 80% confluence, the rBMSCs were passaged with 0.25% trypsin (Sigma, USA). The cells of passage 2  
164 were used in the experiments. The rBMSCs were seeded directly onto the scaffolds in the 24-well plates (Nest, USA)  
165 at a density of  $5 \times 10^4$  cells per well and cultured for 1 day. Then, the scaffolds were moved to new 24-well plates to  
166 discard cells that adhered to the plate rather than to the scaffolds.

## 167 **2.5 *In vitro* cytotoxicity and cell proliferation**

168 *In vitro* cell cytotoxicity effects of the porous scaffolds, in accordance with ISO 10993-5, were analyzed on the  
169 rBMSCs. Liquid extracts of the scaffolds (3 cm<sup>2</sup>/mL in  $\alpha$ -MEM with 10% FBS (v/v) at 37 °C) over 3 days were  
170 prepared and filter sterilized before utilized in cell cytotoxicity assays, which were assessed using Cell Counting Kit-8  
171 (CCK-8). The rBMSCs were seeded into 96-well plates (Nest, USA) at  $1 \times 10^4$  cells per well for 1 day, then the culture  
172 medium was replaced by liquid extracts of medical grade polyethylene (negative control, NC, non-cytotoxic),  $\alpha$ -MEM  
173 with 10% FBS (v/v) and 10% dimethyl sulfoxide (DMSO) (positive control, provide reproducible cytotoxic response),  
174 and the 100% liquid extracts of the Ti6Al4V ELI scaffolds from each group (100  $\mu$ L/well) for a further 1, 3 and 5 days (n  
175 = 6). Following this, 10  $\mu$ L of CCK-8 solution was added to each well of the plate and the plate was incubated without  
176 light for 2 hours. The absorbance at 450 nm was measured. The values of NC wells were averaged and taken as 100%  
177 cell survival. All other values were then averaged with respect to their groups and compared to the negative control.  
178 Moreover, after the cells were seeded onto the scaffolds and cultured for 1 and 7 days, live/dead staining was performed  
179 in accordance with the manufacturer's instruction. SEM was used to visualize the morphology of cells on the porous  
180 scaffolds after culture for 1 day.

181 Transfected with a lentiviral construct containing a green fluorescent protein (GFP) (cyagen, RASM-X-01101, USA)  
182 expression motif, the rBMSCs expressing GFP were used for cell proliferation assessment. The fluorescent images of  
183 cells on the scaffolds with different porosities and pore sizes were captured by an inverted fluorescence microscope  
184 (Olympus, Japan) after cultured for 1, 4, 7, 11, 14 and 21 days. DNA contents measurement were performed using  
185 Quant-iT PicoGreen dsDNA Assay Kit (Invitrogen, California, USA) to quantitatively assess the proliferation of the  
186 cells.

## 187 2.6 Alkaline phosphatase (ALP) activity and relative gene expression

188 The osteogenic differentiation was measured by ALP activity and osteogenic related genes expression. At day 7, 14  
189 and 21, the ALP levels of the cells on the scaffolds were assessed using an alkaline phosphatase colorimetric assay kit  
190 (Beyotime, China) (n = 3) and normalized by the total protein contents which were measured by a BCA protein assay kit.  
191 The expression levels of osteogenic genes including bone morphogenetic protein-2 (BMP-2), collagen type 1 $\alpha$ 1 (COL-1),  
192 osteocalcin (OCN), osteopontin (OPN) and runt-related transcription factor-2 (RUNX-2) were evaluated by quantitative  
193 real-time PCR at day 7, 14 and 21. Specifically, the total RNA was extracted using Trizol reagent (Invitrogen, USA) and  
194 converted to cDNA using a HiScript II Q RT SuperMix (Vazyme, Nanjing, China). Then, the analysis was performed  
195 with ChamQ SYBR qPCR Master Mix (Vazyme, China) using the Roche Applied Science Light Cycler 96 system  
196 (Roche Applied Science, Penzberg, Germany) (n = 3). The relative expression levels of the osteogenic genes were  
197 standardized to the housekeeping gene glyceraldehyde-3-phosphate dehydrogenase (GAPDH). The synthesized primers  
198 employed in this study are listed in Table. 2.

199 **Table. 2.** Primers used in real-time PCR

Gene		Primer sequence (5'-3')	
		Forward	Reverse
GAPDH	Housekeeping	GGCACAGTCAAGGCTGAGAATG	ATGGTGGTGAAGACGCCAGTA
BMP-2	Osteogenic	CAACACCGTGCTCAGCTTCC	TTCCCACTCATTTCTGAAAGTTCC
COL-1	Osteogenic	GCCTCCCAGAACATCACCTA	GCAGGGACTTCTTGAGGTTG
OCN	Osteogenic	ATGAGAGCCCTCACACTCCTC	GCCGTAGAAGCGCCGATAGGC
OPN	Osteogenic	ACAAGCAGACGTTTTGACTC	CTTTGACCTCAGTCCGTAAG
RUNX-2	Osteogenic	CCATAACGGTCTTCACAAATCCT	TCTGTCTGTGCCTTCTTGTTTC

200 Abbreviations: GAPDH, glyceraldehyde-3-phosphate dehydrogenase; BMP-2, bone morphogenetic protein-2; COL-1, collagen type  
201 1 $\alpha$ 1; OCN, osteocalcin; OPN, osteopontin; RUNX-2, runt-related transcription factor-2.

## 202 2.7 Surgical procedures

203 According to international standards, the *in vivo* experiment was approved by the Laboratory Animal Care &  
204 Welfare Committee of Southern Medical University. 10-week-old SD rats (n = 84) with body weight in the range of 350–  
205 400 g were used in this study. All rats were fed with a standard diet separately in polypropylene cages in the laboratory  
206 animal house at 20–25 °C under 50–55% humidity. All rats were randomly allocated to two time points (4 and 12 weeks).  
207 At each time point, the rats were randomly divided into seven groups (n = 6). General anesthesia was implemented with  
208 intraperitoneal injection of 1% pentobarbital sodium (6 mL/kg). Local anesthesia was implemented with a solution of 0.5%

209 lidocaine (0.2 mL/rat). The drilling of bone defects was conducted using a drill with a diameter of 3 mm, under the  
210 irrigation of physiological saline. The cylindrical porous implants (Fig. 1i) were inserted into the drilled holes at the  
211 distal lateral femoral condyle of the left hind leg. Then, the incisions were closed in a layered fashion with 6-0 absorbable  
212 catgut suture for muscles and 4-0 non-absorbable suture for the skin. Subcutaneous implantation was also made under the  
213 back skin of the rats to observe soft tissues ingrowth. For comparison, in the reference group (annotated as REF2), the  
214 bone defects were not repaired, and incisions were closed without any implantations. Cephazolin (10 mg/kg) was  
215 administered intramuscularly immediately after the suture and once a day for 3 days after the surgery. After 4 and 12  
216 weeks of implantation, the rats were euthanized by injecting an overdose of pentobarbital sodium, and specimens  
217 containing the scaffolds were retrieved and fixed in 4% paraformaldehyde for 24 hours for further studies.

## 218 **2.8 Micro-CT assay**

219 In order to evaluate the effectiveness of new bone ingrowth formation, the rats with porous scaffold implantation  
220 were scanned using X-ray micro computed tomography ( $\mu$ -CT, X5000, North Star Imaging, USA). The scanning  
221 resolution was approximately 4  $\mu$ m/voxel. Three-dimensional (3D) volume of the scaffolds and bones were reconstructed  
222 by Amira-Avizo software. VGStudio MAX (Volume Graphics, Germany) was used for data analysis. The scaffolds and  
223 the bone tissues growing into the inner space of the scaffolds were defined as the volume of interest for detailed data  
224 analysis. Bone volume (BV) and total pore volume (TV) were measured using the  $\mu$ -CT. The ratio of BV to TV (BV/TV)  
225 was then calculated to quantitatively evaluate the bone ingrowth performance. A higher value of BV/TV indicates better  
226 bone growth into the pore space. Note that TV in the reference group (REF2) equals to the volume of the entire bone  
227 defect.

## 228 **2.9 Histological evaluation**

229 After fixation for 1 day, the dehydration process of the specimens was done by a graded ethanol series. Then the  
230 specimens were embedded in methyl methacrylate solution at 37 °C for 1 week. Polymerized blocks were cut into thin  
231 sections (approximately 100  $\mu$ m in thickness) along the perpendicular direction towards the long axis of the scaffolds,  
232 using an interlocked diamond saw (Leica Microtome, Germany). To investigate bone ingrowth into the porous scaffolds,  
233 Van-Gieson staining (1.2% trinitrophenol and 1% acid fuchsin) was performed on the sections.

## 234 **2.10 Statistical analysis**

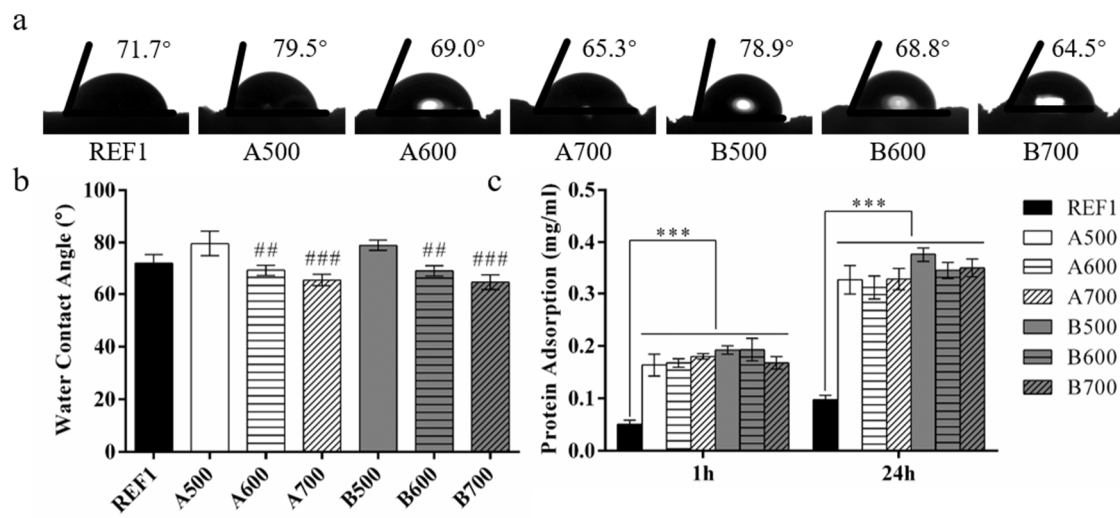
235 All results in this study were retrieved from at least 3 independent experiments on at least three different samples,  
236 and expressed as the means  $\pm$  standard deviations (SDs). Error bars in the charts represent SDs. Statistical analyses for *in*

237 *vitro* studies were done using one-way ANOVA and Tukey post hoc tests, and that for *in vivo* studies were done using  
 238 Kruskal-Wallis ANOVA and Conover-Inman post-hoc test, while  $p < 0.05$  indicates statistically significant.

### 239 3 Results

#### 240 3.1 Water contact angle and protein adsorption

241 The image of water droplets and measured contact angle of the scaffolds are shown in Fig. 2a and b. As can be seen,  
 242 all scaffolds exhibited a water contact angle of smaller than  $90^\circ$ . The water contact angle gradually decreased as the pore  
 243 size increased. Porosity seemed to have no significant influence on the water contact angle; increasing porosity only  
 244 slightly reduced water contact angle. As compared with REF1, A500 and B500 scaffolds had higher water contact angle,  
 245 and the other porous scaffolds showed lower values, but the differences between the porous scaffolds and REF1 were not  
 246 statistically significant. In order to investigate the influence of water contact angle on the protein adsorption ability of the  
 247 porous scaffolds, Fig. 2c shows the results of the protein adsorption study. The protein adsorbed by the scaffolds after  
 248 incubation for 24 hours was significantly higher than incubation for 1 hour. All the porous scaffolds had higher protein  
 249 adsorption ability than REF1 ( $p < 0.001$ ). However, no obvious regularity was observed as the porosity or pore size  
 250 varied.

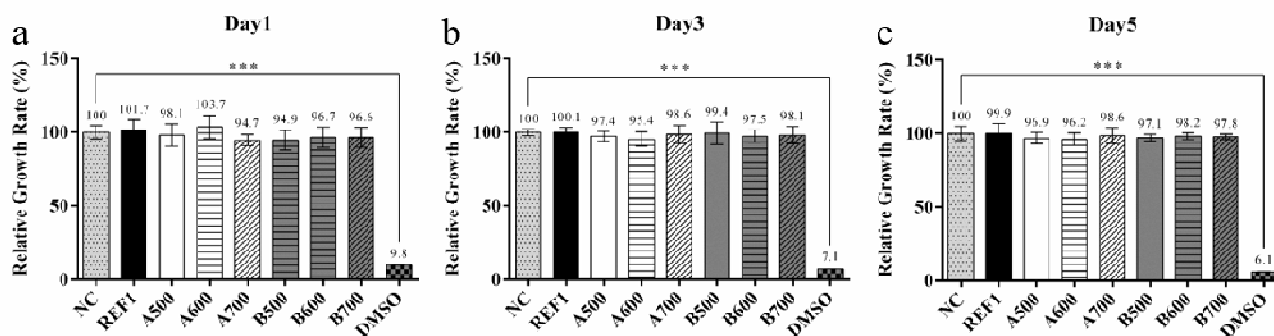


251  
 252 **Fig. 2.** Water contact angle and protein adsorption test of the SLM scaffolds. (a) image of water droplets showing measured water  
 253 contact angle; (b) average water contact angle of the scaffolds; (c) adsorbed protein contents of the scaffolds. Water contact angle and  
 254 adsorbed protein were analyzed by one-way ANOVA and Tukey post hoc tests. \* $p < 0.05$ , \*\* $p < 0.01$  and \*\*\* $p < 0.001$  compared with  
 255 REF1; # $p < 0.05$ , ## $p < 0.01$  and ### $p < 0.001$  compared with A500. For each group,  $n = 3$ .

#### 256 3.2 *In vitro* cytotoxicity and cell morphology

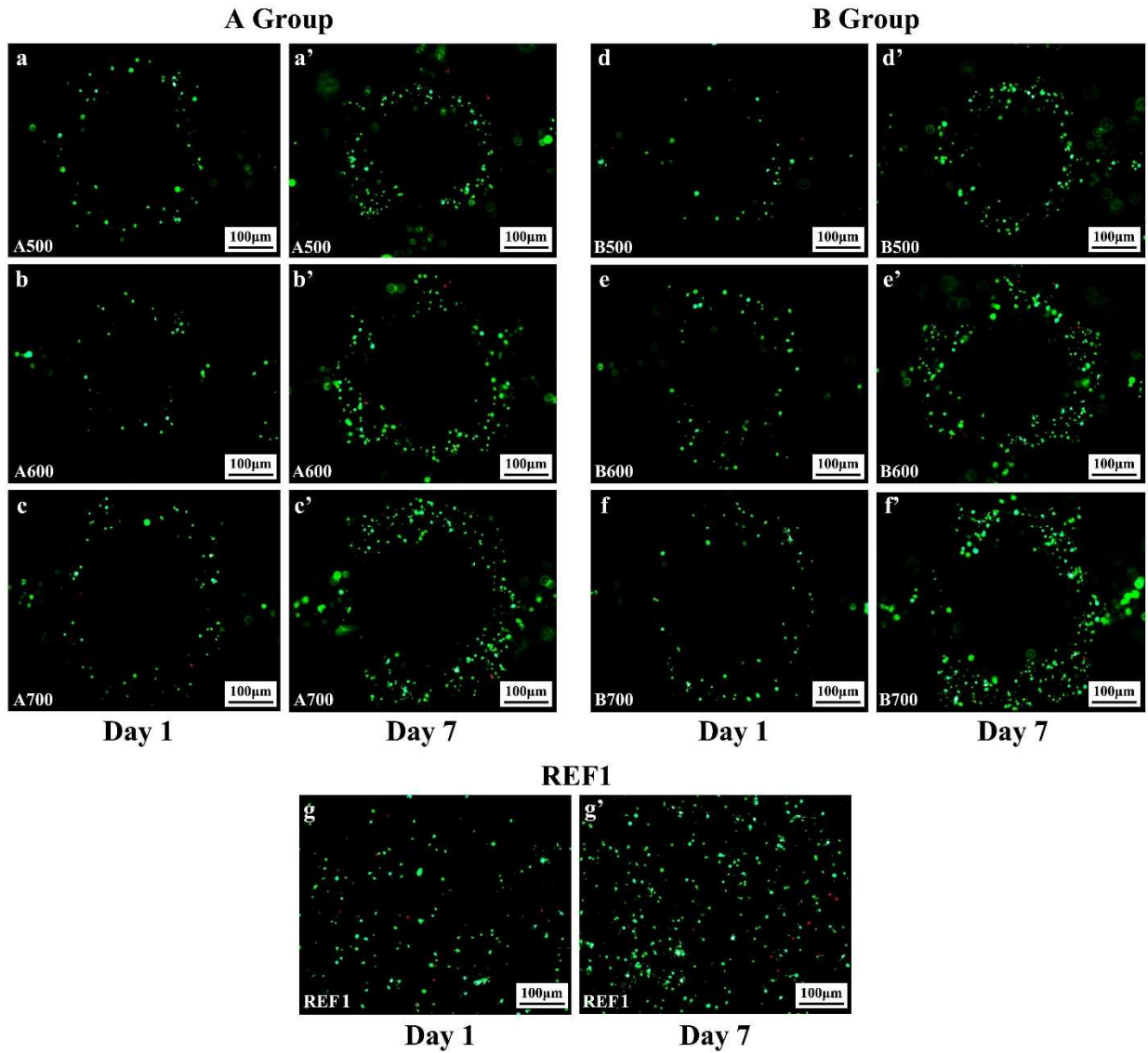
257 In order to evaluate the cytocompatibility of the scaffolds, rBMMSCs were cultured. For comparison, the

258 cytocompatibility of REF1 was also evaluated. CCK-8 assays were conducted to evaluate the cell viability after the cells  
 259 were cultured in the 100% liquid extracts for 1, 3 and 5 days. The relative cell growth rates on the porous scaffolds and  
 260 solid plate are shown in Fig. 3. Clearly, the relative growth rates were higher than 94% in all cases at different time points.  
 261 However, the viability of cells cultured in 10% (v/v) DMSO was significantly lower than that of the control group.



262  
 263 **Fig. 3.** Cytotoxicity test of the Ti6Al4V ELI scaffolds by CCK-8 assays. Relative growth rates were analyzed by one-way ANOVA and  
 264 Tukey post hoc tests. \* $p < 0.05$ , \*\* $p < 0.01$  and \*\*\* $p < 0.001$ . For each group,  $n = 6$ .

265 The fluorescence images of live/dead staining of rBMSCs seeded on the SLM porous scaffolds and REF1 were  
 266 displayed in Fig. 4. In the images, the green color indicates live cells, and red color indicates dead cells. The prevalence  
 267 of live cells could be seen on the scaffold surfaces with only few dead cells detected. For the porous scaffolds as shown  
 268 in Fig. 4a-c (Group A) and Fig. 4 d-f (Group B), after the cells were seeded onto the scaffolds for 1 day, the cells have  
 269 adhered to the struts of the scaffolds. After culture for 7 days, the number of live cells increased as shown in Fig. 4a'-c'  
 270 (Group A) and Fig. 4 d'-f' (Group B). It should be noted that the cells on the struts also migrated to the back of the struts,  
 271 which cannot be directly observed due to their 3D spatial characteristic. In contrast, the number of cells on the REF1  
 272 showed random distribution after culture for 1 day and 7 days (Fig. 4g and g').



273  
274 **Fig. 4.** Fluorescence images showing live and dead staining. Green color indicates living cells and red color indicates dead cells.

275 Fig. 5 shows the cell morphologies observed by SEM. Black arrows point to healthy cells which are uniformly  
276 distributed on the surface of all samples. It is seen from the low-magnification images (Fig. 5a-g) that, the adherent  
277 Ti6Al4V ELI powder particles on the struct and plate surfaces seemed to have influence on the preferential adsorption of  
278 the cells. From the high-magnification view (Fig. 5a'-g'), it is found that the cells preferentially grew within the waviness  
279 of the surfaces and particularly between small particles. This fact may indicate that larger adherent particles on the SLM  
280 Ti6Al4V ELI surface could hinder the attachment of cells.

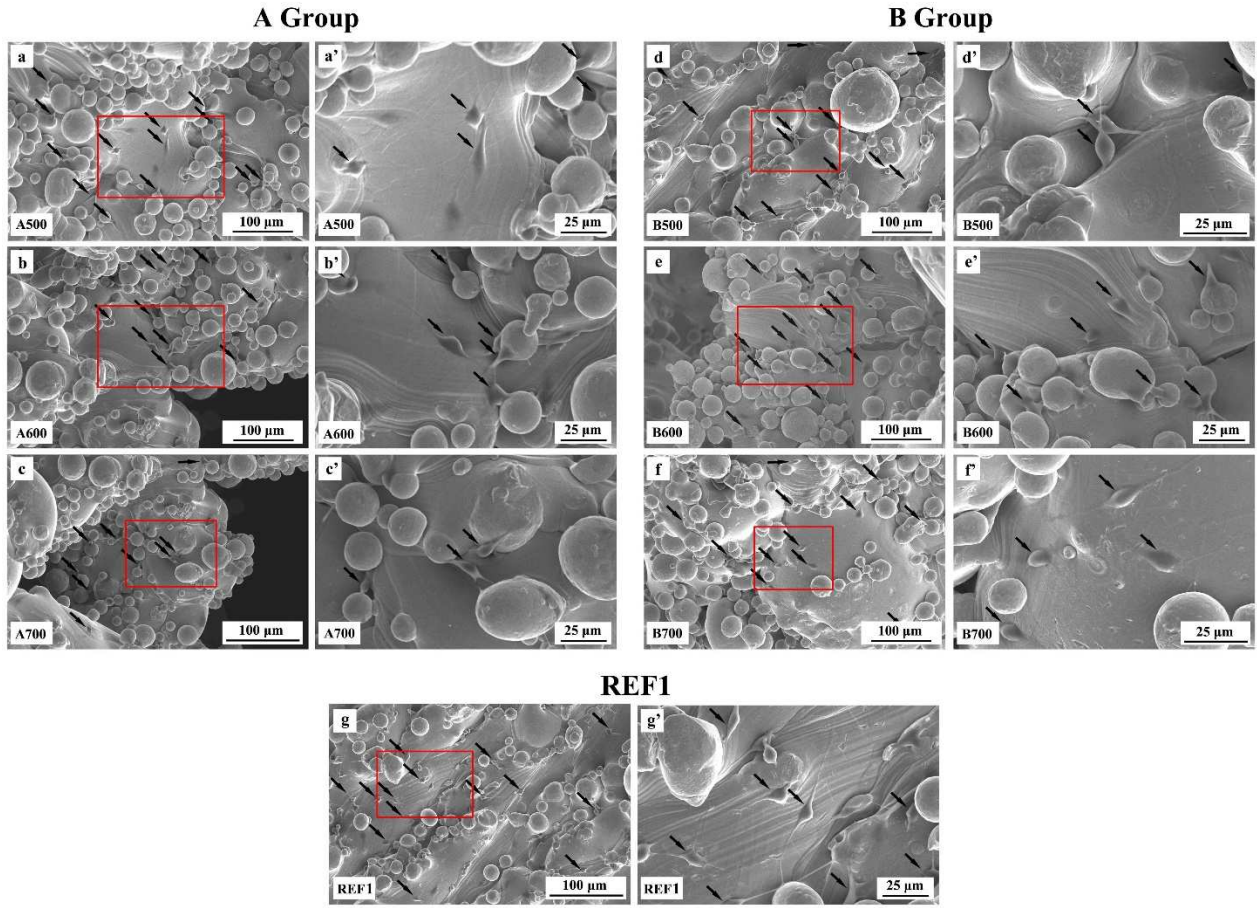
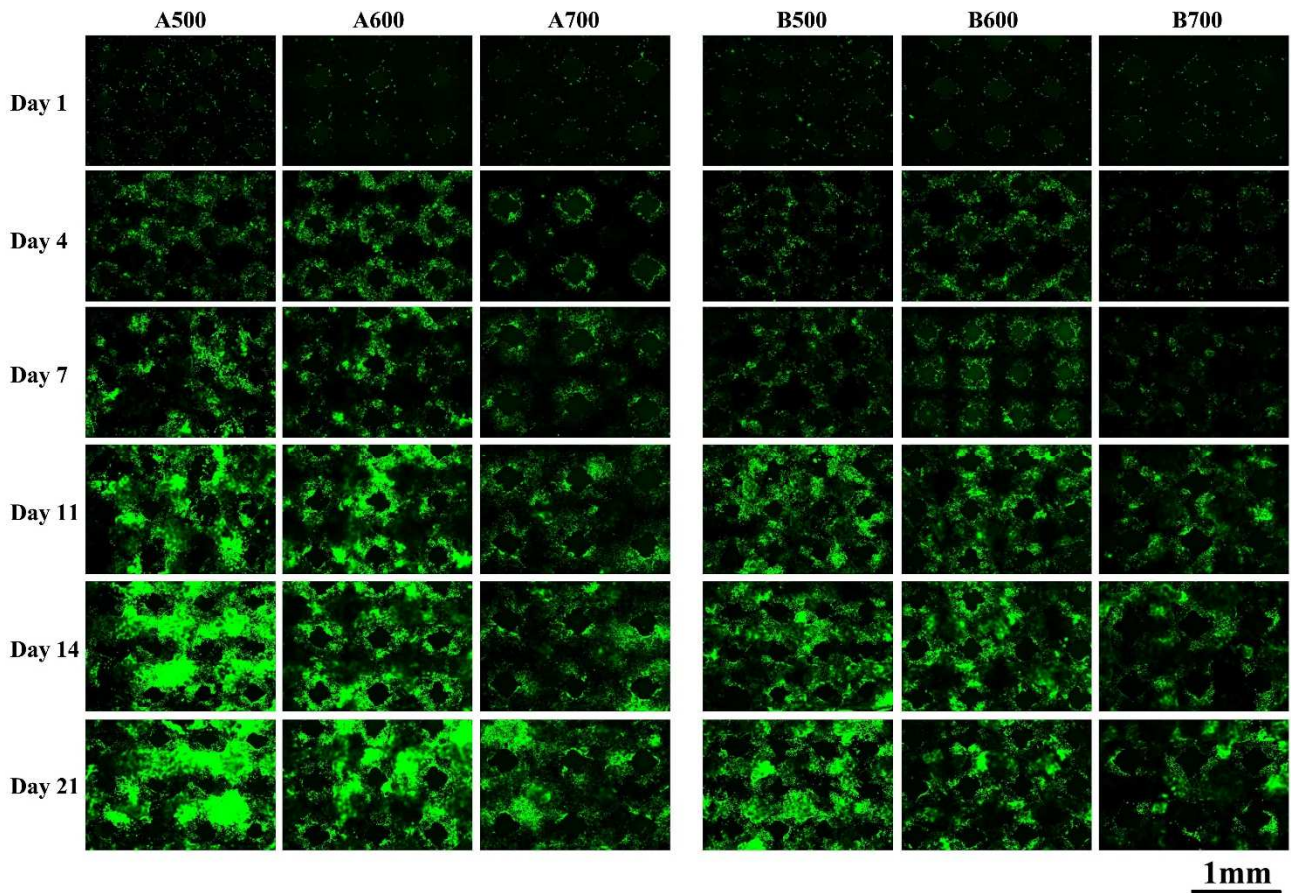


Fig. 5. SEM observation of rBMMSCs. Black arrows point to cells.

### 3.3 Cell proliferation

Cells expressing GFP will emit green fluorescence and can be observed using a fluorescence microscope. In order to study the effect of pores size and porosity on cell proliferation, Fig. 6 shows the fluorescent images of the cells growing on the porous scaffolds. It is seen that the number of the cells growing on the porous scaffolds increased gradually with the culture time. The difference in the fluorescent images between each scaffold became gradually significant after the cells being cultured for 3 days. After cultured for 21 days, the cells growing on the surfaces of A500 and B500 scaffolds showed the brightest green fluorescence within each group. This result suggests that cells proliferated faster on the scaffolds with a pore size of 500  $\mu\text{m}$  than those with larger pore sizes. In addition, by comparing Group A (porosity of 60%) to Group B (porosity of 70%), it is seen that the cells growing on the surfaces of Group A scaffolds showed brighter green fluorescence those on the surfaces of Group B scaffolds. This fact implies that cells proliferated faster on the scaffolds with lower porosity. The fluorescent images clearly revealed that A500 scaffold was much better than the other scaffolds in facilitating cell growth.

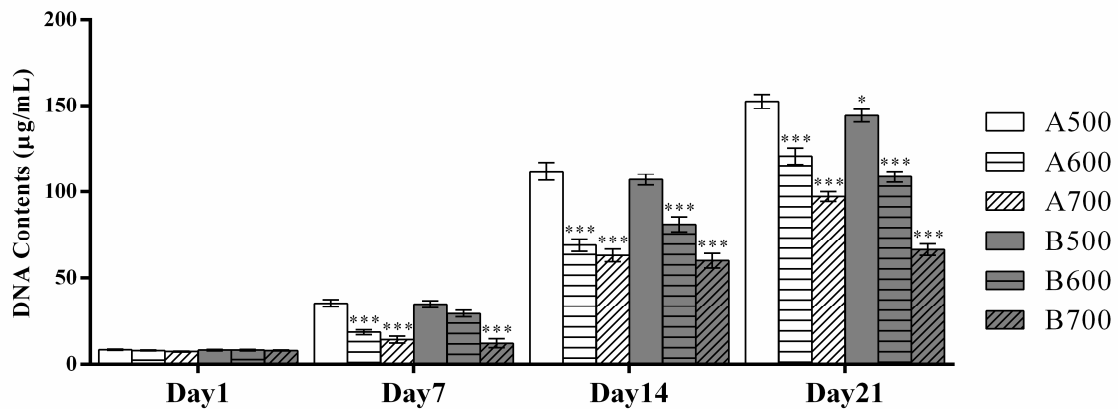


**Fig. 6.** Fluorescent images showing cell proliferation on the porous scaffolds.

295  
296

297 It is known that DNA content is directly related to cell population and can help quantitatively evaluating the number  
 298 of cells on the porous scaffolds. Therefore, DNA content in each scaffold was measured and the results are shown in Fig.  
 299 7. Note that the test was conducted on cell lysates which were extracted after specific time intervals. It is seen that the  
 300 DNA content increased gradually with the increase in cell culture time for all the porous scaffolds. In addition, no  
 301 significant difference in DNA content was observed among different porous scaffolds after culture for 1 day. However,  
 302 after culture for 7 days, A500 scaffold revealed more DNA content than the other scaffolds. As the culture time further  
 303 increased, the difference between A500 scaffold and the other scaffolds in DNA content became increasingly larger. DNA  
 304 content study indicates that A500 scaffold is the best scaffold for cell proliferation, which is consistent with the  
 305 fluorescent images shown in Fig. 6.



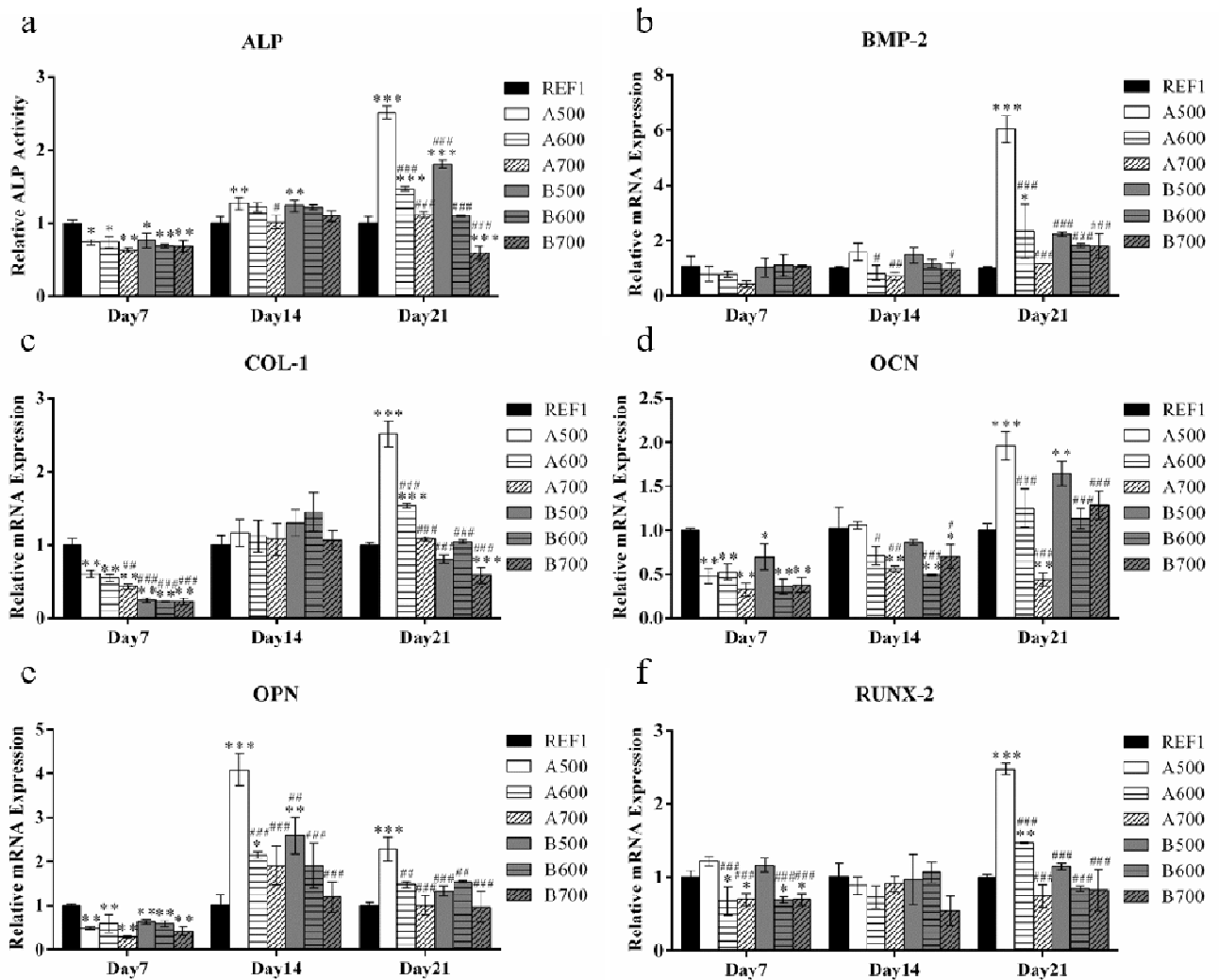


306

307 **Fig. 7.** DNA contents assessed by one-way ANOVA and Tukey post hoc tests. \* $p < 0.05$ , \*\* $p < 0.01$  and \*\*\* $p < 0.001$  compared with  
 308 A500. For each group,  $n = 3$ .

309 **3.4 Osteogenic differentiation**

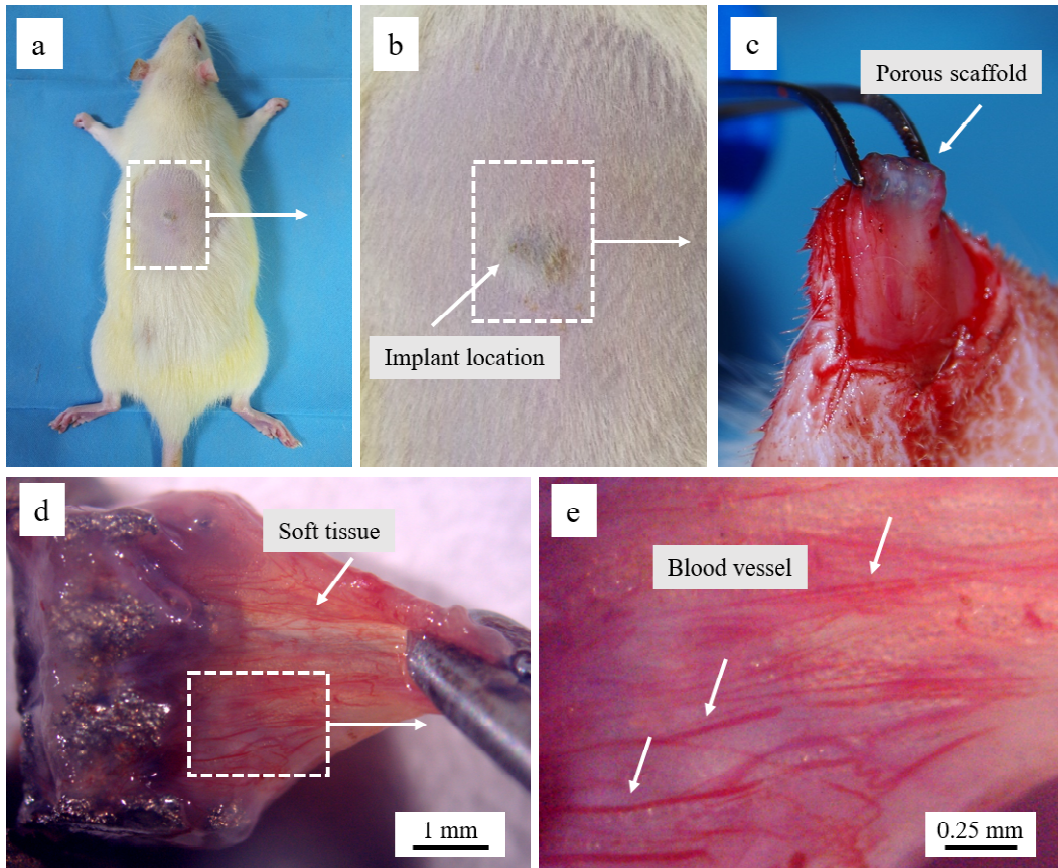
310 The results of osteogenic differentiation evaluation are shown in Fig. 8. For ALP activity assessment as shown in  
 311 Fig. 8a, after 7 days' culture, the ALP activity of cells on the porous scaffolds was lower than that on REF1. However, at  
 312 day 14, the ALP activity on the porous scaffolds started to exceed that on REF1. Furthermore, the ALP activity on A500  
 313 and B500 scaffolds was 2.52 and 1.81 times higher than on REF1 ( $p < 0.001$ , Fig. 8a) after culture for 21 days. The  
 314 results of osteogenic related gene expression were, to some extent, similar to the results of ALP activity. Briefly, the  
 315 expression of most osteogenic genes of cells on the porous scaffolds were lower than that on REF1 at day 7 and enhanced  
 316 as the culture time increased. It is worth noting that the relative expression of BMP-2 of A500 scaffold was 6 times  
 317 higher than that of REF1 and significantly higher than the other porous scaffolds (Fig. 8b). For COL-1, OCN and  
 318 RUNX-2, higher expression could also be observed on A500 scaffolds at day 21 (Fig. 8c, d, f). However, the result of  
 319 OPN was different (Fig. 8e). The highest expression on A500 scaffold (4.08 times) occurred on day 14 and then declined  
 320 to 2.28 times on day 21, and the difference between A500 scaffold and REF1 was statistically significant at these two  
 321 time points. More importantly, it can be seen that all tested osteogenic gene expression levels decreased from A500 to  
 322 A700 at day 21.



323  
 324 **Fig. 8.** Osteogenic differentiation assessed by ALP activity and express of osteogenic related genes. (a) ALP activity of the cells on  
 325 different porous scaffolds; (b–f) relative mRNA expression of BMP-2, COL-1, OCN, OPN and RUNX-2 at day 7, 14 and 21. \* $p < 0.05$ ,  
 326 \*\* $p < 0.01$  and \*\*\* $p < 0.001$  compared with REF1; # $p < 0.05$ , ## $p < 0.01$  and ### $p < 0.001$  compared with A500. For each group,  $n =$   
 327 3.

### 328 3.5 Subcutaneous implant

329 In order to assess the interaction between the porous scaffolds and soft tissues, *in vivo* study was conducted. The  
 330 scaffolds were implanted under the back skin of the rats, and Fig. 9 shows the general results of the *in vivo* study. No  
 331 obvious subcutaneous effusion, redness and infection were observed after implantation (Fig. 9a and b). As shown in Fig.  
 332 9c, d and e, after implantation for 4 weeks, soft tissues grew tightly on the surface of the scaffolds and some blood  
 333 vessels could also be found.



334

335

336

337

**Fig. 9.** General results of the *in vivo* study. (a) overview of the implant location for subcutaneous implantation; (b) magnified view of the implant location; (c) porous scaffold under the skin; (d) soft tissues on the porous scaffold; (e) magnified view of the soft tissues attached on scaffold, white arrows point to blood vessels.

338

### 3.6 Micro-CT scanning for bone ingrowth

339

340

341

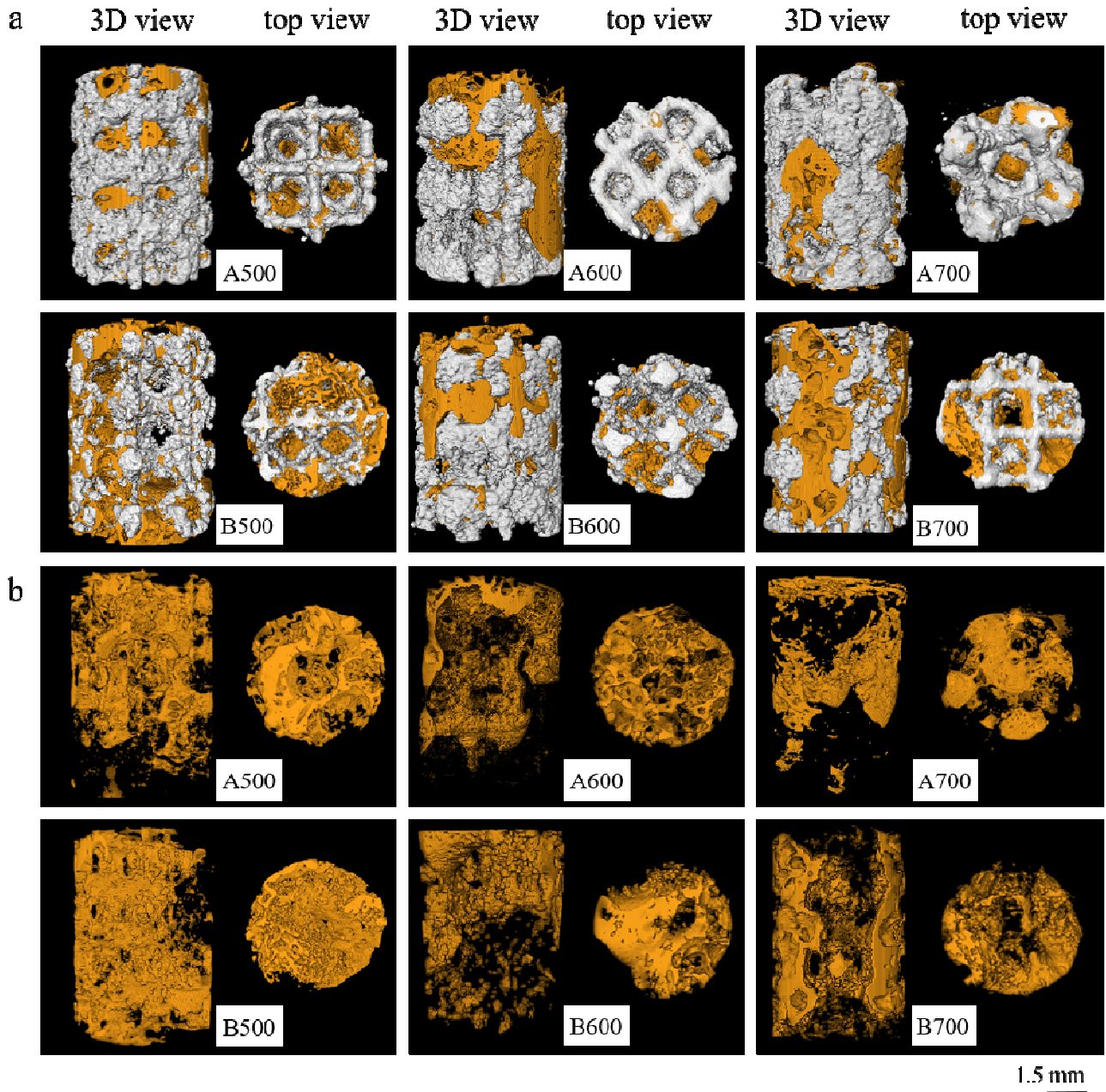
342

343

344

345

New bone formation in the porous scaffolds was studied through  $\mu$ -CT scanning. Fig. 10 shows the 3D reconstruction of the porous scaffold and surrounding bone tissues, respectively. The 3D reconstruction images of the porous implant shown in Fig. 10a provide clear evidence that new bone had grown into the porous scaffolds after healing for 12 weeks. The reconstructed spatial distribution of the new bone formation shown in Fig. 10b qualitatively illustrates the difference of bone ingrowth ability between each scaffold. As can be seen, the volume of the bone ingrowth decreased in each group as the pore size increased. Therefore, A500 and B500 scaffolds showed better new bone formation ability than the other scaffolds.



**Fig. 10.**  $\mu$ -CT analysis of new bone formation. (a) reconstruction images of porous implants; (b) reconstruction images of bone formation. Orange area: new bone formation.

346

347

348

349

350

351

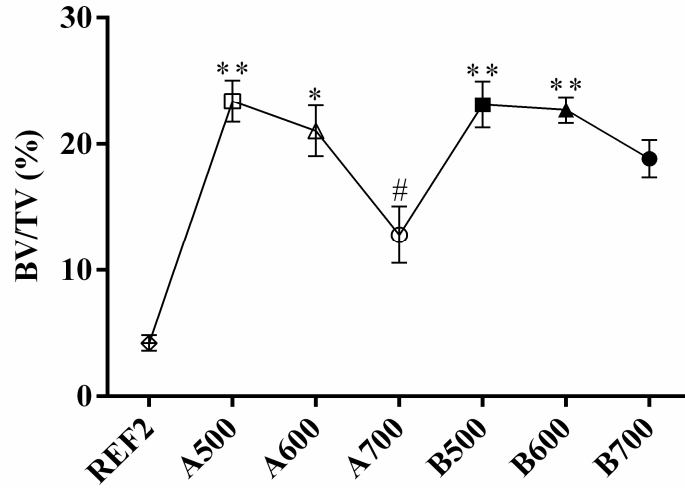
352

353

354

The ratio of BV to TV has been widely used to quantitatively evaluate the bone ingrowth [25, 31, 32]. Therefore, BV/TV was also used in this work to evaluate the effect of pore size and porosity on the bone ingrowth. Fig. 11 shows the values of BV/TV of different samples (porous scaffolds and REF2) after bond healing for 12 weeks. Clearly, the porous scaffolds showed better bone ingrowth than REF2, indicating the superiority of the porous scaffolds over REF2. In addition, as the pore size increased, BV/TV reduced for each group, which suggests that lower pore size benefit the bone growth. By comparing Group A to Group B, no obvious regularity could be found. However, among all the samples,

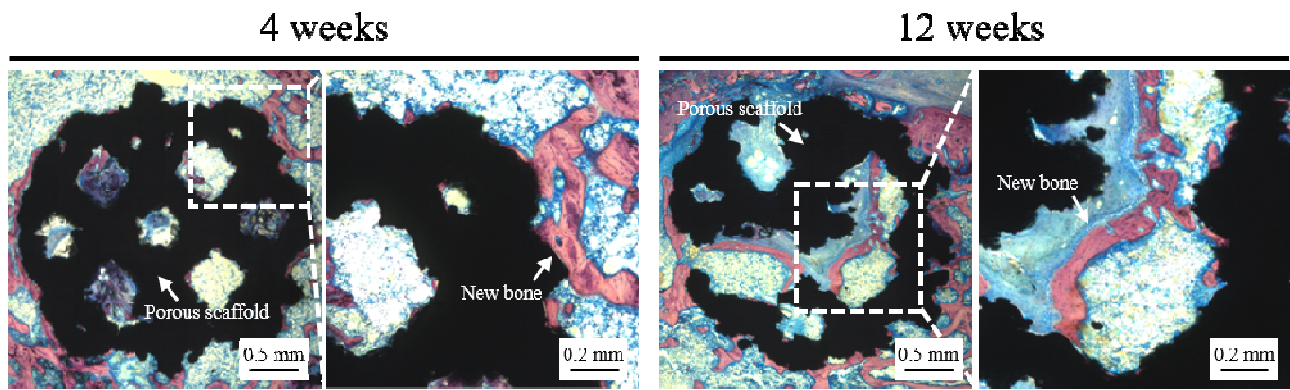
355 A500 scaffold had the highest BV/TV and hence the best bone ingrowth, which is in good agreement with the *in vitro*  
356 study.



357  
358 **Fig. 11.** The ratio of BV/TV of the porous scaffolds and reference sample (REF2). \* $p < 0.05$ , \*\* $p < 0.01$  compared with REF2; # $p <$   
359 0.05 with A500.

### 360 3.7 Histological evaluation

361 The above *in vitro* and *in vivo* studies above have shown that A500 scaffold has the best bone ingrowth. Therefore,  
362 the osteointegration of the bone and A500 scaffold was further assessed by Van-Gieson staining. The results after  
363 implantation for 4 weeks and 12 weeks were showed in Fig. 12. Note that the red area represents new bone tissues and  
364 blue area represents fibrous tissues. As can be seen, after implantation for 4 weeks, newly generated bone started to grow  
365 into the pore space of A500 scaffold from the surrounding bone tissues. In addition, it is also found that the bone tissues  
366 adhered tightly to the surfaces of the scaffold, which indicates a good osteointegration. In addition, the newly regenerated  
367 bone tissues increased as healing progressed. After implantation for 12 weeks, it is obvious that new bone can be detected  
368 in the central area of the scaffold, which is consistent with the results of  $\mu$ -CT.



**Fig. 12.** Histological assessment of A500 scaffold by VG staining after implantation for 4 and 12 weeks. The scaffold implant is black, new bone is stained red, fibrous tissues is stained blue.

#### 4 Discussion

Large bone defect is still a challenge for orthopedists, as even the “gold standard” treatment, autologous bone graft, would face some drawbacks [33, 34]. In the past few years, Ti and its alloys have been widely studied for orthopedic applications [35-37]. The results of these studies reveal the promising prospects of Ti alloys. Porous Ti and Ti alloys have many advantages over traditional solid metal materials. Porous scaffolds significantly reduce stress shielding effects and prevent mechanical failure. Furthermore, the interconnected pore structure is proven to be beneficial to vascularization, nutrient-waste exchange, osteoconduction and bone ingrowth, which leads to good osseointegration and long-term stability [13]. In this study, SLM technology was used to manufacture porous Ti6Al4V ELI scaffolds with pore sizes of 500, 600 and 700  $\mu\text{m}$  and porosities of 60% and 70%. The microstructure evolution and mechanical performance of these SLM porous scaffolds have already been investigated and published elsewhere [18, 38]. The results have suggested that the porous Ti6Al4V ELI scaffolds had sufficiently high mechanical strength and comparable elastic module to the real bone, which is the fundamental of the current research. Further to the mechanical properties, in this study, the biomedical properties of these scaffolds were systematically investigated through well-designed *in vitro* and *in vivo* experiments. Special attention was paid on the determination of optimum scaffold porosity and pore size for bone substitute.

The SLM porous scaffolds with different surface roughness can lead to different wettability and thus influence the permeability of the scaffolds. The contact angles of all the scaffolds were smaller than  $80^\circ$ , indicating a hydrophobic surface. The values of the contact angles of A500 and B500 scaffolds were higher than those of REF1, which could contribute to the side effect on the water drop molding into the scaffolds [25]. In each group, with the increase of pore size or porosity, the contact angle gradually decreased (see Fig. 2b). It can be speculated that the porous scaffolds with higher porosity show more hydrophilic surfaces due to their relatively higher surface roughness [39]. Cytoactivity of the

392 cells on the material surface could be greatly affected by the adsorption ability of proteins, which was beneficial to cell  
393 accommodation and proliferation [40]. Moreover, the adsorption capacity of proteins was directly related to surface  
394 wettability, which was greatly influenced by the surface roughness. Consequently, the cell viability on the tested samples  
395 could be attributed to the different scaffold surface properties caused by different porosities and pore sizes. Although the  
396 ratio of surface to volume (BS/TV) of each scaffold were different, the difference in proteins that were adsorbed by the  
397 scaffolds was not statistically significant after culture for 1 hour. As the soaking time increased to 24 hours, the scaffolds  
398 with higher porosity displayed slightly higher protein adsorption, which is similar to the result of a previous study [41].  
399 Furthermore, all the scaffolds showed obvious higher protein adsorption ability than REF1 at the prescribed time of 1  
400 hour and 24 hours ( $p < 0.001$ ) (see Fig. 2c), because BS/TV of porous scaffolds are much higher than that of Ti6Al4V  
401 plate. Proper wettability and protein adsorptive ability of the porous scaffolds could provide a suitable environment for  
402 cell adhesion and proliferation.

403 The cytocompatibility of the porous scaffolds was qualitatively assessed by CCK-8 assay, live/dead staining, and  
404 SEM observation. According to ISO 10993, for a biocompatible material, the viability of cells cultured in its 100% liquid  
405 extracts should not fall below 70% compared to a blank and negative (nontoxic) control. In this assessment, the viability  
406 of the cells in 100% liquid extracts of all the porous scaffolds was above 90% compared to the negative control after  
407 being cultured for 1, 3 and 5 days (see Fig. 3). Live/dead staining showed that there were few dead cells on the scaffolds  
408 after the rBMSCs were seeded directly onto the scaffolds. Then, after culture for 7 days, the green fluorescence (live  
409 cells) increased, while the red fluorescence (dead cells) remained at a low level, which indicates that cells proliferated  
410 normally on the surface of the scaffolds. From the SEM images, the cells on the porous scaffolds exhibited a well-spread  
411 shape and drifted to the inner space of the interconnected porous scaffolds, which can promote nutrient-waste exchange  
412 and hence benefit to cell culture. In previous reports [42, 43], it was found that a porous structure with a high surface area  
413 and average curvature conduce to induce tissue amplification *in vitro*. Moreover, the rough surface could increase the  
414 anchorage possibility of bone cells in addition to the surface energy of the materials, which benefited the adsorption of  
415 macromolecules and the attachment of cells. Furthermore, the rough interface had a similar curvature to bone cells,  
416 which helped the physical/chemical combination of the cells or macromolecules [3, 44]. However, it is found that the  
417 cells preferentially grew within the waviness of the surfaces and particularly between small particles. Larger powder  
418 particles adhered to the strut surfaces could hinder the attachment of cells and may bring risks to human health due to the  
419 high possibility of flaking from the strut surface after implantation. The findings in this work clearly showed the good  
420 cytocompatibility of the porous Ti6Al4V ELI scaffolds.

421 The proliferation of the cells on the scaffolds using rBMMSCs expressing GFP were investigated, which can emit  
422 green fluorescence, due to the good adhesion environment provided by the scaffolds. The fluorescent images of the cells  
423 on the scaffolds were captured at different time points during 21-day culture period (Fig. 6). It is worth noting that after  
424 the same amounts of cells were seeded, more cells could be observed in A500 and B500 scaffolds than in the other  
425 porous scaffolds within each group after culture for 7 days. In the designed model, as can be seen in Fig. 2, the shape of  
426 the struts is rectangle, while after the laser processing the rectangle struts could be transformed into approximately  
427 cylindrical struts. As the culture time increased, significant difference in the cell proliferation was gradually observed.  
428 Rumpler et al. [45] quantitatively studied the growth kinetics of collagenous tissues in an osteoblast culture for different  
429 3D channel geometries. They concluded that the mechanism of curvature-driven tissue growth, that is, the amount of  
430 tissues deposited in the geometries was proportional to the local curvature. This means that the local curvature of the  
431 scaffolds could affect the tissue formation kinetics, which could further influence the cell deposition result. Having the  
432 highest curvature, A500 scaffold exhibited the brightest green fluorescence (Fig. 6), which could be explained by this  
433 curvature-driven mechanism [45].

434 In previous research, Chang et al. [25] investigated the influence of the pore size of porous Ti on cell penetration  
435 and bone ingrowth. The results illustrated that the porous scaffolds with a pore size of 188  $\mu\text{m}$  were covered by cells;  
436 however, the oxygen and nutrient exchange were affected, which led to cell death inside the scaffold. Furthermore, Xue  
437 et al. [42] suggested that an optimum pore size of larger than 200  $\mu\text{m}$  could be favorable to cell ingrowth into the pore  
438 structures. Knychala et al. [46] qualitatively studied the forces exerted by cells which could drive proliferation and  
439 increase with curvature. They also assumed that as the curvature increased, the net force exerted on the underlying tissues  
440 would increase. Moreover, to investigate the influence of pore size, Hollander et al. [47] cultured human osteoblasts on  
441 porous Ti6Al4V ELI discs with the nominal pore diameters of 500, 700 and 1000  $\mu\text{m}$ . The specimens of 500  $\mu\text{m}$  showed  
442 predominant overgrown with cells, which is similar to our results. In our study, although the pores of the porous scaffolds  
443 were not completely covered by cells, a predominant trend of cells attached on A500 scaffold after seeding for 21 days  
444 could be observed. This means that the transport of nutrients and the emission of metabolites could be ensured by A500  
445 scaffold. The DNA content assay confirms this observation and suggests that A500 scaffold was more appropriate for cell  
446 penetration and proliferation than the other scaffolds. This could be explained by the following two aspects. First, the  
447 scaffolds with a small pore size of 500  $\mu\text{m}$  had higher seeding efficiency. It was reported that porous scaffolds with a  
448 lower pore size may lead to inferior permeability [48, 49], which could result in lower fluid velocity and higher cell  
449 seeding efficiency [25]. Higher permeability led to higher fluid velocities, allowing cells to attach on the surface of the



450 scaffold with less time. The contact angle measurements supported this fact. Second, A500 scaffold had the largest  
451 surface area, which could provide larger surface area for cell adsorption and proliferation. For the scaffolds with the same  
452 pore size, the number of cells on the scaffolds with a porosity of 60% was higher than those with a porosity of 70%,  
453 which suggests that the porosity of 60% was better for vascularization and more beneficial to nutrient and oxygen  
454 exchange and cell penetration [50].

455 The expression of ALP and COL-1 during the formation and maturation of extracellular bone matrix, and the  
456 expression of OCN and OPN during the process of bone matrix mineralization, are main indications of osteogenic  
457 differentiation. All the cells on the scaffolds were supplemented with osteogenic medium to evaluate the influence of  
458 pore size and porosity on osteogenic differentiation. At day 7, RT-PCR profiling exhibited relatively lower expression of  
459 osteogenic genes (BMP-2, OCN, OPN and RUNX-2) for the porous scaffolds than for REF1. Previous studies suggested  
460 that the excessive space of porous scaffolds may delay the differentiation process in the initial stage [25, 51]. ALP and  
461 COL-1 are markers of osteoblast differentiation and maturation which can promote cell differentiation and reflect the  
462 phenotypic characteristics of osteogenic differentiation, respectively. At day 14, no significant differences in ALP and  
463 COL-1 could be found. Moreover, higher expression of ALP and COL-1 for A500 scaffold could be seen at day 21,  
464 indicating that the cells on A500 scaffold had better differentiation performance. BMP-2 and OPN facilitate the  
465 development of bone and cartilage and are beneficial to the mineralization of bone, respectively. The expression of the  
466 osteogenic genes (BMP-2 and OPN) for the porous scaffolds was higher than that for REF1 at day 14. Specifically, the  
467 expression of OPN for A500 scaffold was 4 times higher than that for REF1 (Fig. 8). At day 21, all the osteogenic genes  
468 for A500 were significantly higher than REF1 (6 times for BMP-2, 2.5 times for COL-1, 1.7 times for OCN, 2.2 times for  
469 OPN, 2.5 times for RUNX-2). It should be noted that the osteogenic gene for A500 scaffold was also significantly higher  
470 than that for the other porous scaffolds. These results may be explained by the mechano-transduction mechanism, which  
471 is a hypothesis with regard to stimuli and cell differentiation [25, 52]. It is suggested that cells on implants with relatively  
472 small pores were more inclined to differentiate as they had more chance to feel stimuli from different struts [53-55]. In  
473 this study, A500 had more struts within the same volume, which was beneficial to cell differentiation. Furthermore, based  
474 on the results of cell proliferation, the number of cells on A500 was greater than on the other scaffolds. This could be due  
475 to the direct cell-cell contacts which significantly enhanced the osteogenic differentiation of rBMSCs owing to the  
476 rapid transduction of cell signaling molecules through their gap junctions [56].

477 Evident adhesion of soft tissues on the porous scaffolds could be observed after subcutaneous implantation for 4  
478 weeks (Fig. 9), which shows good biocompatibility and ability for tissues ingrowth [40]. Moreover, the formation of

479 blood vessels is a favorable sign for tissue penetration, since productive exchange of oxygen and nutrients are beneficial  
480 to bone regeneration.

481  $\mu$ -CT scanning can evaluate bone formation qualitatively through radiography and quantitatively through 3D  
482 ingrowth in a non-destructive way. Different bone ingrowth can be observed in the reconstruction images after 12 weeks  
483 of healing (Fig. 10). Bone ingrowth towards the interior of the porous scaffolds can be seen, which led to the density of  
484 the bone decreasing gradually from outside to inside. Moreover, bone ingrowth could be found in all locations of the  
485 porous scaffolds. The detailed results of bone ingrowth are displayed in Fig. 11. As can be seen, in each group, the porous  
486 scaffolds with 500  $\mu$ m pore size showed the highest BV/TV ratios, which were 23.41% for A500 scaffold and 23.15% for  
487 B500 scaffold. For the scaffolds in group A, the BV/TV ratio decreased to 21.04% when the pore size increased from 500  
488  $\mu$ m to 600  $\mu$ m, and further decreased to 12.81% when the pore size increased to 700  $\mu$ m. The same trend can also be  
489 observed in group B. It has been reported that when a scaffold was implanted into a host, cell adhesion was the first  
490 cellular event, which greatly affected subsequent cellular biological functions, including proliferation, differentiation, and  
491 tissues formation [57-59]. The results of the *in vivo* study in this work are consistent with the conclusions of *in vitro*  
492 studies where A500 and B500 scaffolds provided a better condition for cell penetration and differentiation than the other  
493 scaffolds. Moreover, the BV/TV ratio of all the porous scaffolds were significantly higher than that of REF2 (4.27%), and  
494 no new bone formation could be detected in the middle of the defects of REF2. The histological staining results also  
495 confirm that newly generated bone tissues were found in the pore space of the scaffolds and good integration of bone  
496 tissues and scaffolds were achieved. These results clearly indicate that the porous scaffolds are suitable for cell  
497 penetration and bone ingrowth into the center of the bone defects and accelerates the restoration of bone defects. Based  
498 on the results obtained in this work, A500 scaffold with the lowest pore size and porosity had the most promising cell  
499 penetration and bone ingrowth. Therefore, A500 is suggested the optimum scaffold for bone implant. While, it should be  
500 noticed that the optimum pore size and porosity identified in this paper is only applicable to octahedral cell structure but  
501 not a universal conclusion.

502 SLM products typically have complex structures (e.g., lattice structures produced in this work), and hence it is very  
503 difficult to quantify the geometrical comparability between the CAD design and as-built structure using traditional  
504 metrology techniques [60, 61]. Due to the staircase and balling effect, powder adhesion is an inevitable phenomenon in  
505 the SLM fabricating process [62, 63]. The adhered powders on the sample surface have high risks of detaching from the  
506 base structure and will be harmful to human bodies, which have to be removed before implantation. In some studies,  
507 traditional grinding or sandblasting method have been adapted to remove the residual powders on the sample surface [64,

508 65]. However, it is difficult to process samples with complex internal structures through the traditional surface treatment  
509 methods. Dual acid etching process is the most popular chemical method [66] to polish SLM porous structures. Wysocki  
510 et.al. [67, 68] proved that chemical polishing with hydrofluoric (HF) acid or HF acid + nitric acid (HNO<sub>3</sub>) is an effective  
511 way for the removal of partially molten powder particles on the porous scaffolds as the acid-based solutions can penetrate  
512 into the porous structures through the interconnected pores. The pore sizes after HF/HNO<sub>3</sub> treatment were almost equal  
513 to those designed in the CAD models. The HF/HNO<sub>3</sub> treated structures even showed a decrease in water contact angle  
514 and had no negative effect on neither cell proliferation and differentiation, which demonstrates the potentials of chemical  
515 polishing method for removing the partially molten powder particles. Although the current work did not include the  
516 surface post-treatment procedure, considering its importance, it is encouraged that future *in-vitro* or *in-vivo* studies shall  
517 take the HF/HNO<sub>3</sub> surface treatment into account before any biological tests.

518 Compared to autologous bone graft and other synthetic bone graft substitutes, the SLM porous Ti6Al4V ELI  
519 scaffolds produced in this work provide better biocompatibility and long-term stability due to their superior bone  
520 ingrowth. Therefore, they are conducive to fulfilling biological fixation. Lower stress shielding led to earlier defect  
521 bridging, increased bone formation, and advanced bony regeneration of the critical size defect.

## 522 **Conclusions**

523 This paper conducts a systematic investigation on the SLM porous Ti6Al4V ELI scaffolds for bone implantation  
524 based on well-designed *in vitro* and *in vivo* experiments. Scaffolds with pore sizes of 500 μm, 600 μm and 700 μm and  
525 porosities of 60% and 70% were studied and compared with each other. The *in vitro* experimental results indicate that  
526 cell proliferation and differentiation were significantly dependent on the pore size and porosity of the porous scaffolds.  
527 On the basis of the porous scaffolds used in this work, it is found that lower pore size and porosity resulted in better cell  
528 adhesion, proliferation and osteogenic differentiation of rBMMSCs. Particularly, the scaffold with a pore size of 500 μm  
529 and porosity of 60% showed the best results. In the *in vivo* study, the μ-CT analysis revealed that the scaffold with a pore  
530 size of 500 μm and porosity of 60% also had the highest BV/TV value and hence the best bone ingrowth among all the  
531 scaffolds. Therefore, based on the findings in this work, it is plausible to suggest that the SLM porous Ti6Al4V ELI  
532 scaffold with a pore size of 500 μm and porosity of 60% is a promising for the fabrication of porous load-bearing  
533 implants for cementless fixation (e.g., acetabular cup and hip prosthesis).

## 534 **Acknowledgements**

535 The authors would like to acknowledge financial supports provided by the founds of Guangdong Academy of

536 Science Projects 2019GDASYL-0502006, Science and Technology Planning Project of Guangdong province  
537 (2016B090916003), Science and Technology Planning Project of Guangzhou (201704030111), 201807010030,  
538 2017A070701027, 2016A030312015, 2017G1FC0008, 2018GDASCX-0402. Sanming Project of Medicine in Shenzhen  
539 (SZSM201612023)

#### 540 **Conflicts of interest statement**

541 The authors report no conflicts of interest in this work.

#### 542 **References**

- 543 [1] D.A. Belatti, A.J. Pugely, P. Phisitkul, A. Amendola, J.J. Callaghan, *The Journal of Arthroplasty*, 29 (2014)  
544 1539-1544.
- 545 [2] N. Taniguchi, S. Fujibayashi, M. Takemoto, K. Sasaki, B. Otsuki, T. Nakamura, T. Matsushita, T. Kokubo, S. Matsuda,  
546 *Materials science & engineering. C, Materials for biological applications*, 59 (2016) 690-701.
- 547 [3] M. Fousova, D. Vojtech, J. Kubasek, E. Jablonska, J. Fojt, *J Mech Behav Biomed Mater*, 69 (2017) 368-376.
- 548 [4] B. Dutta, F.H. Froes, *Metal Powder Report*, 72 (2017) 96-106.
- 549 [5] L.H.M. Antunes, C.R.P. de Lima, *Cobalt-Chromium Alloys – Properties and Applications*☆, Reference Module in  
550 *Materials Science and Materials Engineering*, Elsevier, 2017.
- 551 [6] A. Goharian, M. Abdullah, *Trauma Plating System*. Amsterdam: Elsevier, (2017) 115-142.
- 552 [7] P.K. Zysset, X.E. Guo, C.E. Hoffler, K.E. Moore, S.A. Goldstein, *Journal of biomechanics*, 32 (1999) 1005-1012.
- 553 [8] D.K. Pattanayak, A. Fukuda, T. Matsushita, M. Takemoto, S. Fujibayashi, K. Sasaki, N. Nishida, T. Nakamura, T.  
554 Kokubo, *Acta Biomater*, 7 (2011) 1398-1406.
- 555 [9] Y. Kosashvili, D. Backstein, O. Safir, D. Lakstein, A.E. Gross, *The Journal of Bone and Joint Surgery. British volume*,  
556 91-B (2009) 870-876.
- 557 [10] P. Derome, A. Sternheim, D. Backstein, M. Malo, *The Journal of Arthroplasty*, 29 (2014) 122-126.
- 558 [11] Y. Li, C. Yang, H. Zhao, S. Qu, X. Li, Y. Li, *Materials (Basel)*, 7 (2014) 1709-1800.
- 559 [12] R. Wauthle, J. van der Stok, S. Amin Yavari, J. Van Humbeeck, J.P. Kruth, A.A. Zadpoor, H. Weinans, M. Mulier, J.  
560 Schrooten, *Acta Biomater*, 14 (2015) 217-225.
- 561 [13] G. Li, L. Wang, W. Pan, F. Yang, W. Jiang, X. Wu, X. Kong, K. Dai, Y. Hao, *Scientific reports*, 6 (2016) 34072.
- 562 [14] B. Vandenbroucke, J.P. Kruth, *Rapid Prototyping Journal*, 13 (2007) 196-203.
- 563 [15] X. Yan, C. Huang, C. Chen, R. Bolot, L. Dembinski, R. Huang, W. Ma, H. Liao, M. Liu, *Surface and Coatings*  
564 *Technology*, 371 (2019) 161-171.
- 565 [16] B. Vandenbroucke, J.-P. Kruth, *RAPID PROTOTYPING J*, 13 (2007) 196-203.
- 566 [17] L. Thijs, F. Verhaeghe, T. Craeghs, J.V. Humbeeck, J.-P. Kruth, *Acta Materialia*, 58 (2010) 3303-3312.
- 567 [18] X. Yan, S. Yin, C. Chen, C. Huang, R. Bolot, R. Lupoi, M. Kuang, W. Ma, C. Coddet, H. Liao, M. Liu, *Journal of*  
568 *Alloys and Compounds*, 764 (2018) 1056-1071.
- 569 [19] A. Fukuda, M. Takemoto, T. Saito, S. Fujibayashi, M. Neo, D.K. Pattanayak, T. Matsushita, K. Sasaki, N. Nishida, T.  
570 Kokubo, T. Nakamura, *Acta Biomater*, 7 (2011) 2327-2336.
- 571 [20] B. Wysocki, J. Idaszek, J. Zdunek, K. Roźniatowski, M. Pisarek, A. Yamamoto, W. Świążkowski, *International*  
572 *journal of molecular sciences*, 19 (2018) 1619.
- 573 [21] L. Rony, R. Lancigu, L. Hubert, *Morphologie*, 102 (2018) 231-242.
- 574 [22] Z.J. Wally, A.M. Haque, A. Feteira, F. Claeysens, R. Goodall, G.C. Reilly, *J Mech Behav Biomed Mater*, 90 (2019)

575 20-29.

576 [23] J. Wieding, T. Lindner, P. Bergschmidt, R. Bader, *Biomaterials*, 46 (2015) 35-47.

577 [24] F. Li, J. Li, G. Xu, G. Liu, H. Kou, L. Zhou, *Journal of the Mechanical Behavior of Biomedical Materials*, 46 (2015)

578 104-114.

579 [25] B. Chang, W. Song, T. Han, J. Yan, F. Li, L. Zhao, H. Kou, Y. Zhang, *Acta Biomater*, 33 (2016) 311-321.

580 [26] M. Kruyt, J.D. de Bruijn, C. Wilson, F. Oner, C. Van Blitterswijk, A. Verbout, W. Dhert, *Tissue engineering*, 9 (2003)

581 327-336.

582 [27] S. Yin, X. Yan, C. Chen, R. Jenkins, M. Liu, R. Lupoi, *Journal of Materials Processing Technology*, 255 (2018)

583 650-655.

584 [28] X. Yan, C. Chen, C. Huang, R. Bolot, M. Kuang, W. Ma, C. Coddet, H. Liao, M. Liu, *Journal of Alloys and*

585 *Compounds*.

586 [29] T.B. Kim, S. Yue, Z. Zhang, E. Jones, J.R. Jones, P.D. Lee, *Journal of Materials Processing Technology*, 214 (2014)

587 2706-2715.

588 [30] L. Zhao, L. Liu, Z. Wu, Y. Zhang, P. Chu, *Biomaterials*, 33 (2012) 2629-2641.

589 [31] D. Agius, K.I. Kourousis, C. Wallbrink, T. Song, *Materials Science and Engineering: A*, 701 (2017) 85-100.

590 [32] K. Kapat, P.K. Srivas, A.P. Rameshbabu, P.P. Maity, S. Jana, J. Dutta, P. Majumdar, D. Chakrabarti, S. Dhara, *ACS*

591 *applied materials & interfaces*, 9 (2017) 39235-39248.

592 [33] S. Green, *Clin. Orthop. Relat. Res.*, (1994) 111-117.

593 [34] R. Capanna, D.A. Campanacci, N. Belot, G. Beltrami, M. Manfrini, M. Innocenti, M. Ceruso, *Orthopedic Clinics of*

594 *North America*, 38 (2007) 51-60.

595 [35] A.-M. Pobloth, S. Checa, H. Razi, A. Petersen, J.C. Weaver, K. Schmidt-Bleek, M. Windolf, A.Á. Tatai, C.P. Roth,

596 K.-D. Schaser, G.N. Duda, P. Schwabe, *Science Translational Medicine*, 10 (2018) eaam8828.

597 [36] R. Yan, D. Luo, H. Huang, R. Li, N. Yu, C. Liu, M. Hu, Q. Rong, *Sci Rep*, 8 (2018) 750.

598 [37] B. Yin, B. Xue, Z. Wu, J. Ma, K. Wang, *Am J Transl Res*, 10 (2018) 474-482.

599 [38] X. Yan, Q. Li, S. Yin, Z. Chen, R. Jenkins, C. Chen, J. Wang, W. Ma, R. Bolot, R. Lupoi, Z. Ren, H. Liao, M. Liu,

600 *Journal of Alloys and Compounds*, 782 (2019) 209-223.

601 [39] R.N. Wenzel, *Industrial & Engineering Chemistry*, 28 (1936) 988-994.

602 [40] K. Kapat, P.K. Srivas, A.P. Rameshbabu, P.P. Maity, S. Jana, J. Dutta, P. Majumdar, D. Chakrabarti, S. Dhara, *ACS*

603 *applied materials & interfaces*, 9 (2017) 39235-39248.

604 [41] F. Fang, J. Satulovsky, I. Szeifer, *Biophysical journal*, 89 (2005) 1516-1533.

605 [42] W. Xue, B.V. Krishna, A. Bandyopadhyay, S. Bose, *Acta Biomater*, 3 (2007) 1007-1018.

606 [43] R. Stangl, B. Rinne, S. Kastl, C. Hendrich, *European Cells and Material*, 2 (2001) 1-9.

607 [44] P. Heintl, L. Muller, C. Korner, R.F. Singer, F.A. Muller, *Acta Biomater*, 4 (2008) 1536-1544.

608 [45] M. Rumpler, A. Woesz, J.W. Dunlop, J.T. van Dongen, P. Fratzl, *Journal of the Royal Society, Interface*, 5 (2008)

609 1173-1180.

610 [46] J. Knychala, N. Bouropoulos, C.J. Catt, O.L. Katsamenis, C.P. Please, B.G. Sengers, *Annals of biomedical*

611 *engineering*, 41 (2013) 917-930.

612 [47] D.A. Hollander, M. von Walter, T. Wirtz, R. Sellei, B. Schmidt-Rohlfing, O. Paar, H.J. Erli, *Biomaterials*, 27 (2006)

613 955-963.

614 [48] S. Impens, Y. Chen, S. Mullens, F. Luyten, J. Schrooten, *Tissue Eng Part C Methods*, 16 (2010) 1575-1583.

615 [49] S. Van Bael, Y. Chai, S. Truscello, M. Moesen, G. Kerckhofs, H. Van Oosterwyck, J. Kruth, J. Schrooten, *Acta*

616 *Biomater*, 8 (2012) 2824-2834.

617 [50] V. Karageorgiou, D. Kaplan, *Biomaterials*, 26 (2005) 5474-5491.

618 [51] J. Yan, C. Zhang, Y. Zhao, C. Cao, K. Wu, L. Zhao, Y. Zhang, *Biomaterials*, 35 (2014) 7734-7749.

619 [52] A. Ataee, Y. Li, M. Brandt, C. Wen, *Acta Materialia*, 158 (2018) 354-368.  
620 [53] G. Stein, J. Lian, T. Owen, *FASEB J.*, 4 (1990) 3111-3123.  
621 [54] E. Tsuruga, H. Takita, H. Itoh, Y. Wakisaka, Y. Kuboki, *J. Biochem.*, 121 (1997) 317-324.  
622 [55] G. Reilly, A. Engler, *J Biomech*, 43 (2010) 55-62.  
623 [56] P.-Y. Wang, D.T. Bennetsen, M. Foss, T. Ameringer, H. Thissen, P. Kingshott, *ACS applied materials & interfaces*, 7  
624 (2015) 4979-4989.  
625 [57] L. Bacakova, E. Filova, M. Parizek, T. Ruml, V. Svorcik, *Biotechnol. Adv.*, 29 (2011) 739-767.  
626 [58] Y. Estrin, E. Ivanova, A. Michalska, V. Truong, R. Lapovok, R. Boyd, *Acta Biomater*, 7 (2011) 900-906.  
627 [59] Y.R. Yun, J.E. Won, E. Jeon, S. Lee, W. Kang, H. Jo, J.H. Jang, U.S. Shin, H.W. Kim, *Journal of tissue engineering*,  
628 2010 (2010) 218142.  
629 [60] A. Hadi, F. Vignat, F. Villeneuve, 2015.  
630 [61] M. Suard, P. Lhuissier, R. Dendievel, J.-J. Blandin, F. Vignat, F. Villeneuve, *Powder Metallurgy*, 57 (2014) 190-195.  
631 [62] C. Yan, L. Hao, A. Hussein, P. Young, D. Raymont, *Materials & Design*, 55 (2014) 533-541.  
632 [63] G. Thomann, C. Magnier, F. Villeneuve, R. Palluel-Germain, *Disability and Rehabilitation: Assistive Technology*, 11  
633 (2016) 695-700.  
634 [64] W. Peng, L. Xu, J. You, L. Fang, Q. Zhang, *Biomedical engineering online*, 15 (2016) 85.  
635 [65] J.R. Strub, E.D. Rekow, S. Witkowski, *The Journal of the American Dental Association*, 137 (2006) 1289-1296.  
636 [66] P.R. Klokkevold, P. Johnson, S. Dadgostari, J.E. Davies, A. Caputo, R.D. Nishimura, *Clinical oral implants research*,  
637 12 (2001) 350-357.  
638 [67] B. Wysocki, J. Idaszek, K. Szlżak, K. Strzelczyk, T. Brynk, K.J. Kurzydłowski, W. Świeszkowski, *Materials*  
639 (Basel), 9 (2016).  
640 [68] B. Wysocki, J. Idaszek, J. Buhagiar, K. Szlżak, T. Brynk, K.J. Kurzydłowski, W. Świeszkowski, *Materials Science*  
641 *and Engineering: C*, 95 (2019) 428-439.  
642