# On the linearization of Antoine's law <br> Pascal Floquet 

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## On the linearization of Antoine's law

## Short Note

## Pascal Floquet


#### Abstract

A multivariate linearized Antoine's equation (MLAE) is presented in this short note. To our knowledge, it is the first time this multi-linear equation is proposed in the literature. Compared with initial null parameters or «Clapeyron» type initial parameters, that do not take into account the highly non-linear correlation between the parameters $B$ and $C$, our procedure gives a very good initial guess for the nonlinear regression of vapor pressure versus temperature. Fortunately, the multi-linear expression of linearized Antoine's law is obtained in a simple, non iterative manner. Examples relevant from thermodynamical literature are used to show the quality of our MLAE parameters in order to converge to nonlinear regression solution of Antoine's model and to compare our approach with the classical ones.


## Introduction

Historically, many different formulas and graphical representations have been suggested for the vapor pressure-temperature relationship for a pure component [Wisniak, 2001]. Clapeyron's formula proposed in 1834 and thermodynamically stated by Clausius in 1864 gave birth to the well-known ClausiusClapeyron differential relationship

$$
\begin{equation*}
\frac{d \ln P^{\circ}}{d\left(\frac{1}{T}\right)}=\frac{-\Delta H^{v}}{R \Delta z} \tag{1}
\end{equation*}
$$

Where $\Delta H^{\nu}$ is the latent heat of vaporization, $z=\frac{P^{\circ} v}{R T}$ the compressibility factor, $P^{\circ}, v$ and $T$ respectively the vapor pressure, the corresponding volume and the temperature. When $\frac{\Delta H^{v}}{\Delta z}$ is assumed to be constant, it leads to

$$
\begin{equation*}
\log P^{\circ}=A-\frac{B}{T} \tag{2}
\end{equation*}
$$

This assumption, or a stronger one of constant heat of vaporization, was soon found to be one of the main reasons why the Clausius-Clapeyron equation would only fit the experimental data in a limited temperature range. A common way to improve the fitting ability is to use the Antoine's equation for the vapor pressure of a saturated liquid which introduces a third parameter $C$ in the approximated ClausiusClapeyron equation

$$
\begin{equation*}
\log P^{\circ}=A-\frac{B}{T+C} \tag{3}
\end{equation*}
$$

Classically, the three coefficients $A, B$ and $C$ have to be determined thanks to experimental data.
From a numerical point of view, the equation (2) is clearly linear with the coefficients $A$ and $B$, in terms of $\log P^{\circ}$ and $1 / T$ variables; thus, if a substance behaves according to the Clausius-Clapeyron model, a plot of $\log P^{\circ}$ against $1 / T$ should yield a straight line with slope $-B$. On the contrary, Antoine's equation (3) is a non-linear equation with respect to parameters $A, B$ and $C$ and for the same variables $\log P^{\circ}$ and $1 / T$. This equation is a well-known non-linear model in the field of Chemical Engineering education and often used as an example for identification purpose of non-linear model [Corriou, 2004].
We propose, in this work, to promote a change of variables leading to a linearized Antoine's equation. It is easy, with this model, to compute the above coefficients $A, B$ and $C$ via a classical linear regression method. Thus, these values of coefficients are good candidates for initial points of a non-linear regression of complete non-linear Antoine's law. To prove the adequacy of a such initial guess, three examples have
been chosen with experimental value ( $T_{\text {exp }}, P_{\text {exp }}$ ) of temperature and vapor pressure: carbon tetrachloride $\mathrm{CCl}_{4}$ [Hildebrand and Mc Donald in Boublik et al., 1973], di-isobutyl hexahydrophtalate (DIBE) [Liu et al., 2005] and 2,6,10,14-tetramethylpentadecane (Pristane) [Bourasseau et al., 2004].

## Several Non-linear Regressions on Antoine's Law

The non-linear Antoine's model (3) can be fitted with experimental data via a lot of distinct criteria to be minimized. Classical ones are the following:
Logarithmic Absolute criterion (LAC) $\sum_{i=1}^{n_{\text {exp }}}\left(\log P^{\circ}{ }_{\text {exp }}-\log P_{\text {calc }}^{\circ}\right)^{2}=\sum_{i=1}^{n_{\text {epp }}}\left(\log P_{\text {exp }}^{\circ}-\left(A-\frac{B}{T_{\exp }+C}\right)\right)^{2}$
Logarithmic Relative criterion (LRC) $\sum_{i=1}^{n_{\text {exp }}}\left(\frac{\log P^{\circ}{ }_{\text {exp }}-\log P_{\text {calc }}^{\circ}}{\log P_{\text {exp }}^{\circ}}\right)^{2}=\sum_{i=1}^{n_{\text {exp }}}\left(\frac{\log P_{\text {exp }}^{\circ}-\left(A-\frac{B}{T_{\text {exp }}+C}\right)}{\log P^{\circ}{ }_{\exp }}\right)^{2}$
Absolute criterion (AC) $\sum_{i=1}^{n_{\text {exp }}}\left(P_{\text {exp }}^{\circ}-P_{\text {calc }}^{\circ}\right)^{2}=\sum_{i=1}^{n_{\text {exp }}}\left(P^{\circ}{ }_{\text {exp }}-e^{A-\frac{B}{T_{\text {epp }}+C}}\right)^{2}$
Relative criterion (RC) $\sum_{i=1}^{n_{\text {exp }}}\left(\frac{P^{\circ}{ }_{\exp }-P^{\circ}{ }_{\text {calc }}}{P_{\text {exp }}^{\circ}}\right)^{2}=\sum_{i=1}^{n_{\text {exp }}}\left(\frac{P_{\text {exp }}^{\circ}-e^{A-\frac{B}{T_{\text {epp }}+C}}}{P_{\text {exp }}^{\circ}}\right)^{2}$
Boublik et al. criterion (BC) $\sum_{i=1}^{n_{\text {exp }}}\left(\left(\log P_{\text {exp }}^{\circ}-A\right)\left(T_{\text {exp }}+C\right)+B\right)^{2}$
All these criteria deal with least-square minimization problems that are not exactly equivalent in terms of parameter solutions or final criterion value. In this work, all the least-square fitting are performed with lsqnonlin program proceeding from Matlab ${ }^{\circledR}$ Optimization Toolbox, based on the Levenberg-Marquardt method with line search for medium-scale problem [Levenberg, 1944; Marquardt, 1963]. For comparison purpose, the tolerances associated with these problems (termination tolerance on the function value $\varepsilon_{F}$ and on variable change $\varepsilon_{X}^{1}$ ) are set to $10^{-7}$.

## Interaction between C and D coefficients

The difficulties of non-linear regression procedures (LAC, LRC, AC, RC, BC or other criteria) arise from the correlation between $B$ and $C$ coefficients and from the number of local minima of the optimization problem. As an example, it can be seen, for the carbon tetrachloride $\mathrm{CCl}_{4}$ [Boublik et al., 1973] example and for a fixed value of coefficient $A(A=15)$, the response surface (criterion AC) versus $B$ and $C$ values. It can be observed than the "minimum valley" is quite narrow and may explain the numerical difficulties encountered.

[^0]

Figure 1: Values of AC criterion versus coefficients $B$ and $C(A=15)$ for the $C C l_{4}$ example
A good initial point of the regression procedure provides us a less difficult path tracing to the solution and a clear advantage in terms of global minimum localization.

## Several Initial Points for the Non-linear Regression

All the non-linear regressions are performed with the following initial points:

- "Null" initial point: all the initial coefficient values $A$. $B$ and $C$ are set to zero;
- "Clapeyron" initial point: initial coefficient values $A$ and $B$ are set to the solution of the linear Clausius-Clapeyron equation (2); the initial value of $C$ is equal to zero;
- "Linearized Antoine" initial point: all the initial coefficient values $A, B$ and $C$ are set to the solution of the linearized Antoine equation below.
This new linear initial point we proposed is obtained by the following transformation of Antoine equation (3):

$$
\begin{gather*}
\log P^{\circ}=\frac{A T+A C-B}{T+C} \Rightarrow C \log P^{\circ}=A T-T \log P^{\circ}+(A C-B) \\
\Downarrow \\
\log P^{\circ}=\left(A-\frac{B}{C}\right)+\frac{A}{C} T-\frac{T \log P^{\circ}}{C} \tag{4}
\end{gather*}
$$

This equation (4) is linear with the coefficients $A / C,-1 / C$ and $(A-B / C)$, in terms of transformed variables $\log P^{\circ}, T$ and $T \log P^{\circ}$. It is then possible to linearly identify these coefficients and, thus, the original ones $A, B$ and $C$, by fitting $\log P^{\circ}{ }_{\text {exp }}$ with $T_{\text {exp }}$ and $T_{\text {exp }} \log P^{\circ}{ }^{\circ}$ exp.
If we note $X$ the following $\left(n_{\text {exp }} \times 3\right)$ matrix $X=\left(\begin{array}{ccc}1 & T_{\text {exp }}^{1} & T_{\text {exp }}^{1} \log P_{\text {exp }}^{\circ 1} \\ 1 & T_{\text {exp }}^{2} & T_{\text {exp }}^{2} \log P^{\circ}{ }_{\text {exp }}^{2} \\ \ldots & \ldots & \ldots \\ 1 & T_{\text {exp }}^{n_{\text {exp }}} & T_{\text {exp }}^{n_{\text {exp }}} \log P_{\text {exp }}^{\circ n_{\text {exp }}}\end{array}\right)$ and $Y$ the following array
$Y=\left(\begin{array}{c}\log P_{\text {exp }}^{\circ 1} \\ \log P_{\text {exp }}^{\circ{ }^{\circ}} \\ \ldots \\ \log P_{\text {exp }}^{\circ^{n_{\text {exp }}}}\end{array}\right)$, then the multi-linear least-square regression gives the coefficient array $\beta=\left(\begin{array}{c}A-\frac{B}{C} \\ \frac{A}{C} \\ \frac{-1}{C}\end{array}\right)$
by

$$
\beta=\left(X^{T} X\right)^{-1} X^{T} Y
$$

Then

$$
\left\{\begin{array}{l}
A=-\frac{\beta_{2}}{\beta_{3}} \\
B=\frac{\beta_{2}}{\beta_{3}{ }^{2}}+\frac{\beta_{1}}{\beta_{3}} \\
C=-\frac{1}{\beta_{3}}
\end{array}\right.
$$

The adequation of the linearized model can be seen in the following figure that gives the response $\log P^{\circ}$ with $T$ and $T \log P^{\circ}$ for the Pristane example. Scatter points are experimental points and surface corresponds to the multi-linear model.


Figure 2: Values of response $\log P^{\circ}$ with $T$ and $T \log P^{\circ}$ for the Pristane example
The table 1 shows the complete non-linear regression results for all the criteria and examples, in terms of coefficient initialization.
It is easy to see that our MLAE initialization procedure gives in all cases better results compared with other initialization methods. The convergence of the non-linear regression to optimal solution with the different initializations is shown, for the DIBE example and the LAC criterion, in the following figure.


Figure 3: Convergence versus Initialization for the DIBE example and the RC criterion (Null Initialization: left Y axis, Clapeyron and MLAE Initializations: right Y axis)

As foreseen, the proposed MLAE procedure is quite good for quickly converge to optimal solution. The table 2 shows the literature results and the criterion chosen. In all the case, the initialization proposed and the non-linear regression end to the same or better solution.

## Conclusion and Significance

A new linearized Antoine equation is proposed to initialize the well-known Antoine's regression problem. This equation is easy to compute and allows to obtain quickly good results to the non-linear regression of vapor pressure versus temperature of pure component.

## Notations

| $P^{\circ}$ | Vapor pressure |
| :--- | :--- |
| $A$ | First Antoine's coefficient |
| $B$ | Second Antoine's coefficient |
| $C$ | Third Antoine's coefficient |
| $T$ | Temperature (K) |
| $X$ | Experiment matrix $\left(n_{\text {exp }} \times 3\right)$ |
| $Y$ | Response array $\left(n_{\text {exp }} \mathrm{X} 1\right)$ |
| $\underline{\text { Acronym }}$ |  |
| AC | Absolute Criterion |
| BC | Boublik’s Criterion |
| $M L A E$ | Multivariate Linearized Antoine's Equation |
| DIBE | Di-IsoButyl hExahydrophtalate |
| LAC | Logarithmic Absolute Criterion |
| LRC | Logarithmic Relative Criterion |
| RC | Relative Criterion |
| Greek Letters |  |
| $\beta$ | Parameter array $(3 \times 1)$ |
| $\Delta V$ | Volume change |

Subscript
exp
calc

Heat of vaporization
termination tolerance on the variable change (least-square procedure)
termination tolerance on the function value
(least-square procedure)
experimental
calculated

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| Criterion | Initialization | CCl4 |  |  |  |  | DIBE |  |  |  |  | Pristane |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | C | Norm | Iterations (Function evaluations) | A | B | C | Norm | Iterations (Function evaluations) | A | B | C | Norm | Iterations (Function evaluations) |
| MLAE |  | 15.8502 | 2794.9 | -46.64 |  |  | 11.4945 | 2658.0 | -209.45 |  |  | 20.4388 | 4274.8 | -116.09 |  |  |
| LAC | Zero | 15.872 | 2807.1 | -46.041 | $6.0610^{-6}$ | 39 (298) | 13.394 | 3817.6 | -154.95 | $1.0910^{-2}$ | 88 (684) | 20.479 | 4296.8 | -115.42 | $1.1210^{-3}$ | 57 (440) |
|  | Clapeyron | 17.567 | 3824.4 | -0.026 | $2.5010^{-4}$ | 2 (12) | 13.394 | 3817.6 | -154.95 | $1.0910^{-2}$ | 122 (943) | 20.479 | 4296.8 | -115.42 | $1.1210^{-3}$ | 58 (445) |
|  | Antoine Linear | 15.850 | 2794.9 | -46.638 | $6.1210^{-6}$ | 2 (12) | 13.394 | 3817.6 | -154.95 | $1.0910^{-2}$ | 49 (377) | 20.438 | 4274.8 | -116.07 | $1.1410^{-3}$ | 3 (19) |
| LRC | Zero | 13.393 | 1606.8 | -112.460 | $4.1410^{-5}$ | 85 (664) | 9.606 | 1768.1 | -256.00 | $1.3210^{-2}$ | 88 (671) | 20.360 | 4242.1 | -116.79 | $1.8010^{-4}$ | 578 (4304) |
|  | Clapeyron | 17.346 | 3678.2 | -6.436 | $6.9410^{-6}$ | 9 (65) | 9.606 | 1768.1 | -256.00 | $1.3210^{-2}$ | 176 (1348) | 20.360 | 4242.1 | -116.79 | $1.8010^{-4}$ | 418 (3147) |
|  | Antoine Linear | 15.850 | 2794.9 | -46.638 | $1.8310^{-7}$ | 2 (12) | 9.606 | 1768.1 | -256.00 | $1.3210^{-2}$ | 49 (371) | 20.360 | 4242.1 | -116.79 | $1.8010^{-4}$ | 21 (154) |
| AC | Zero | 16.020 | 2890.5 | -41.925 | 0.939 | 234 (1770) | 13.254 | 3681.1 | -163.13 | 0.236 | 188 (1433) | NON CONVERGENCE |  |  |  |  |
|  | Clapeyron | 16.020 | 2890.5 | -41.925 | 0.939 | 108 (816) | 13.254 | 3681.1 | -163.13 | 0.236 | 248 (1897) | 26.276 | 8647.3 | 13.91 | 28.424 | 1524 (6100) |
|  | Antoine Linear | 16.020 | 2890.5 | -41.925 | 0.939 | 24 (197) | 13.254 | 3681.1 | -163.13 | 0.236 | 70 (522) | 23.998 | 6726.6 | -38.82 | 28.820 | 2466 (9868) |
| RC | Zero | 16.000 | 2879.2 | -42.488 | 0.024 | 220 (1681) | 14.024 | 4251.5 | -136.51 | 0.109 | 134 (1038) | NON CONVERGENCE |  |  |  |  |
|  | Clapeyron | 16.000 | 2879.2 | -42.488 | 0.024 | 95 (730) | 14.024 | 4251.5 | -136.51 | 0.109 | 131 (1004) | 21.603 | 4938.5 | -96.33 | 5.198 | 25000 (100004)* |
|  | Antoine Linear | 16.000 | 2879.2 | -42.488 | 0.024 | 25 (202) | 14.024 | 4251.5 | -136.51 | 0.109 | 59 (446) | 21.123 | 4657.6 | -104.59 | 4.912 | 16534 (66140) |
| BC | Zero | 15.883 | 2813.3 | -45.739 | 0.472 | 224 (1699) | 12.869 | 3475.2 | -170.10 | 31.550 | 7949 (31800) | 20.459 | 4285.5 | -115.76 | 9.807 | 7295 (29184) |
|  | Clapeyron | 15.883 | 2813.3 | -45.739 | 0.472 | 57 (441) | 12.901 | 3495.4 | -169.19 | 31.551 | 20878 (83512) | 20.460 | 4286.3 | -115.74 | 9.807 | 17647 (70592) |
|  | Antoine Linear | 15.883 | 2813.3 | -45.739 | 0.472 | 11 (80) | 12.878 | 3481.4 | -169.82 | 31.550 | 16641 (66568) | 20.458 | 4285.5 | -115.76 | 9.807 | 393 (1576) |

Table 1: Comparison of initialization techniques on Antoine regression problem with several criteria
(* maximal number of function calls)

|  | CCl 4 |  |  | DIBE |  |  | Pristane |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Criterion | A | B | C | A | B | C | A | B | C |
|  | 15.938 | 2844.1 | -44.213 | 12,866 | 3471,6 | -170,35 | 20,489 | 4301,7 | -115,26 |
| LAC | $2.5810^{-3}$ |  |  | $1.0610^{-1}$ |  |  | $3.3710^{-2}$ |  |  |
| LRC | $4.7910^{-4}$ |  |  | $1.8010^{-1}$ |  |  | $2.9710^{-1}$ |  |  |
| AC | 0.9974 |  |  | 0.69629 |  |  | 41.129 |  |  |
| RC | 0.1596 |  |  | 0.37515 |  |  | 5.5148 |  |  |
| BC | 0.7093 |  |  | 31.56 |  |  | 9.8759 |  |  |

Table2: Literature results (norm of the criterion) on Antoine regression problem with several criteria (in grey, the criterion chosen by the authors, if known)


[^0]:    ${ }^{1}$ Three termination criteria have been applied: non evolution on variables (evolution less than $\varepsilon_{X}$ ), non evolution of leastsquare function (evolution less than $\varepsilon_{F}$ ) and first-order optimality conditions less than $\varepsilon_{F}$.

