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# 1 Plasma properties conditioned by the magnetic throat location 2 in a Helicon plasma device

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6 (Dated: 21 September 2021)

Measurements are conducted in a Helicon plasma device to analyze the spatial distribution of plasma properties as the throat of the magnetic nozzle is axially shifted with respect to the antenna center. Krypton plasma is generated in the sub-kilowatt range and probed using a suite of diagnostics including a rf-compensated Langmuir probe, a planar probe and laser-induced fluorescence. It is found that larger ion currents and increased plasma confinement are achieved when the throat of the magnetic nozzle is located downstream the antenna center, at a distance that equals or exceeds two times the antenna length. The ions, although being accelerated, retain subsonic velocities even beyond the magnetic throat.

## 7 I. INTRODUCTION

8 A recent keen interest in electric space propulsion stems  
9 from an increasing number of small satellites being deployed  
10 for plural applications<sup>1–6</sup>. Simple and compact thrusters can  
11 allow for in-space maneuvering of such small spacecrafts<sup>7</sup>  
12 which usually do not boast large volume capacity to meet the  
13 needs of consolidated technologies, e.g. Gridded Ion thrusters  
14 and Hall thrusters. As a result, a portion of research and devel-  
15 opment efforts are being focused on electrodeless devices and  
16 magnetic nozzle (MN) acceleration<sup>8–13</sup>. This kind of technol-  
17 ogy can indeed offer a number of advantages compared to the  
18 aforementioned state-of-the-art devices. Issues linked to ero-  
19 sion of components are expected to be of little consequence  
20 due to the absence of direct interaction between plasma dis-  
21 charge and electrodes, resulting in a long lifetime. The plasma  
22 beam leaving the discharge chamber is quasineutral, thus no  
23 neutralizer is required. Furthermore, these plasma sources  
24 can more easily operate using condensable propellants with  
25 respect to those system that require a dedicated neutralizer,  
26 whose lifetime and reliable functioning can be considerably  
27 affected<sup>14</sup>.

28 The Helicon plasma (HP) thruster is one such a device. It  
29 mainly comprises three components: *i*) a dielectric tube as  
30 plasma discharge region, *ii*) a radiofrequency (rf) antenna for  
31 gas ionization and *iii*) an axially directed steady magnetic field  
32 for plasma confinement and expansion throughout its diverg-  
33 ing region, i.e. the magnetic nozzle. Power radiated by the an-  
34 tenna is deposited in the electron population as thermal energy  
35 by means of helicon wave modes<sup>15</sup> and Trivelpiece–Gould  
36 wave modes<sup>16</sup>. The energy is used for plasma production and  
37 transport phenomena, such as ambipolar electric field, result-  
38 ing in axial acceleration of the ions in the MN by conversion  
39 of the electron thermal energy.

40 The maturity of this technology is still relatively low<sup>5</sup>,  
41 whereby several undesired aspects come along with the con-  
42 sidered advantages. The most critical one perhaps regards the

43 thrust efficiency. Thus far, direct thrust measurements have  
44 revealed efficiencies typically below 10% in many different  
45 devices<sup>13,17–24</sup>, with the only recent exception of nearly 20%  
46 at several kW of input power<sup>12</sup>. In this scenario, improv-  
47 ing the attained performance is required in order to turn HP  
48 thrusters into a competitive technology in the near future. The  
49 better understanding of the physics governing such rf plasma  
50 sources by exploring the different working parameters is cur-  
51 rently the preferred approach to provide an exhaustive opti-  
52 mization pathway.

53 In an effort to model HP discharges, previous analy-  
54 ses have considered different magnetic topologies inside  
55 the source tube, e.g. uniform<sup>25,26</sup>, Helmholtz and Maxwell  
56 configurations<sup>27</sup>. The magnetic field inside the source is then  
57 matched with a divergent geometry through a magnetic throat  
58 localized in the proximity of the tube exit. This firm condi-  
59 tion is not necessarily the most convenient solution, as demon-  
60 strated in Ref. 28 where a stepped-diameter tube is employed  
61 and the magnetic throat is placed downstream the exit cross  
62 section of the small main tube. Besides, virtually every nu-  
63 merical and experimental work studying the influence of mag-  
64 netic nozzle on the plasma properties, limited the analysis to  
65 the exploitation of different magnitudes at the throat. A fruit-  
66 ful investigation is reported in Ref. 29, where the location of  
67 the magnetic throat is indirectly shifted with respect to the an-  
68 tenna – which is constantly located at the back plate – by  
69 changing the discharge tube length. Another relevant analy-  
70 sis is reported in Ref. 30, where the authors characterized the  
71 plasma and the rf power circuit when the magnetic throat lo-  
72 calized either within the source or at the exhaust. Bennet *et*  
73 *al.*<sup>31</sup> studied the generation of plasma as a function of the MN  
74 throat location. Yet, their setup did not include plasma expan-  
75 sion outside the discharge tube and many operating conditions  
76 relied on magnetized ions, which is not a typical scenario in  
77 propulsion. The shape of the magnetic nozzle and the location  
78 of the throat are presumably strongly linked to the amount  
79 of the input energy that can be usefully converted into axial  
80 thrust. Energetic electrons are mainly produced close to the  
81 region occupied by the antenna. Several phenomena occur  
82 in the nozzle, such as transport due to pressure gradient and  
83 electron cooling via convection and/or conduction, which de-  
84 termine the conversion efficiency of inlet thermal energy into

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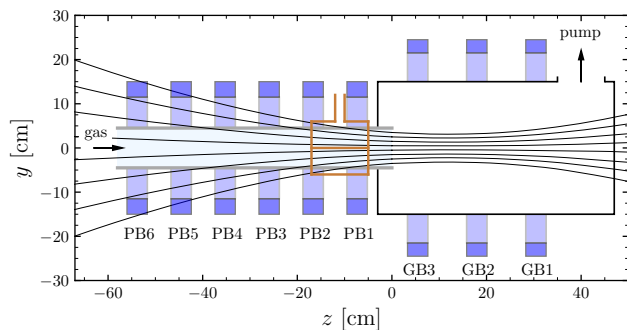


FIG. 1. Helicon source schematics. The  $z = 0$  position refers to the discharge tube outlet,  $y = 0$  refers to the reactor axis.

ion acceleration. Furthermore, as the throat is shifted along the thruster axis with respect to the antenna location, the expansion ratio of the plasma beam changes, thus resulting in possibly different thrust levels.

This paper reports on experimental results obtained in a HP source operating with krypton under several configurations of the external magnetic field. Numerous plasma properties are spatially resolved as the throat of the magnetic field is moved with respect to the antenna axial position. A detailed description of the experimental setup is provided in Section II, including the HP source and the magnetic configurations. In Section III, the diagnostics are extensively described. They include: a rf-compensated Langmuir probe to spatially characterize plasma density, electron temperature, and plasma potential; a planar probe to measure the ion current density; laser-induced fluorescence to explore the axial ions and atoms velocity distribution function. Measurements are presented and discussed in Section IV. Eventually, conclusions are drawn in Section V.

## II. EXPERIMENTAL SETUP

A schematics of the HP source employed in this study is shown in Figure 1 along with an example of computed magnetic field lines. The entire experimental setup is oriented in a vertical position.

The discharge chamber consists in a borosilicate glass tube with  $\phi = 9$  cm inner diameter and  $L = 58$  cm length, whose open exit arbitrarily identifies the origin of the axial coordinate  $z$ . Krypton gas is introduced off-axis in the tube through its top aperture at a nominal flow rate of  $1 \pm 0.004$   $\text{mg s}^{-1}$ . The bottom part is connected to a 30 cm in inner diameter and 50 cm in length expansion chamber made in aluminum which is equipped with a turbomolecular/primary pumping system. The ultimate base pressure is in the order of  $10^{-5}$  mbar, whereas the typical pressure during operation reads  $\sim 5 \times 10^{-3}$  mbar.

The rf antenna in use is a double-saddle type with  $d_A = 12$  cm length centered at  $z \cong -11$  cm. It is made of pure copper and features two feeding arms which are long enough to be directly connected to the matching network so

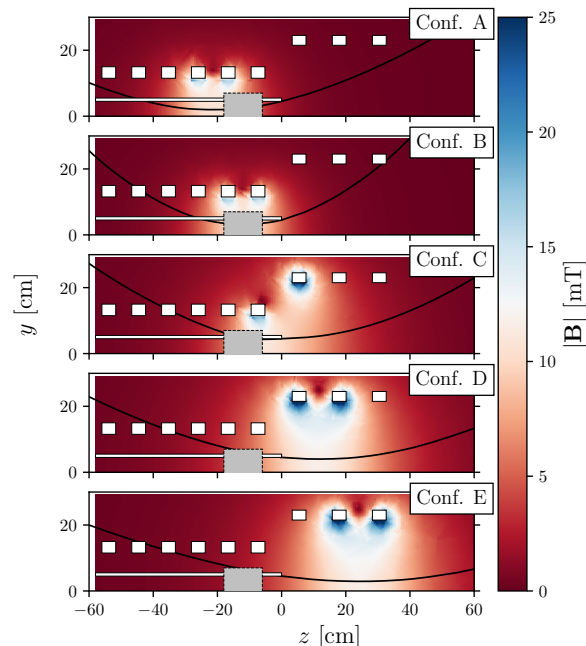


FIG. 2. 2D profiles of the externally applied magnetic fields. White line indicates the discharge tube walls, white rectangles represent the magnetic coils, the gray rectangle indicates the antenna region and the black solid line exemplifies the magnetic streamline crossing the tube edge at  $z = 0$ .

that power losses due to intermediate links are prevented. Input rf power is generated by a 1 kW-class power supply at 13.56 MHz and kept constant to 750 W throughout the reported measurements. The power carried by higher order harmonics is certified to be lower than  $-40$  dBc. Matching of the rf power is attained via a custom  $\pi$ -type network. During operation, values of the reflected power are below  $\sim 2\%$ .

A set of nine electromagnets surrounds both the discharge tube and the expansion chamber. Their denomination is reported in Figure 1. Each electromagnet is made up of a 2 mm diameter copper wire, constituting 510 loops for PB1-6 and 430 loops for GB1-3. The presence of multiple electromagnets enables the investigation of profoundly different magnetic field topologies. For the purpose of this study, five magnetic configurations are examined by powering two electromagnets at once. In doing so, the location of the magnetic throat is intentionally relocated along the  $z$  axis. The tested magnetic configurations are progressively labeled as Conf. A to Conf. E. When involved, PB coils are powered with 3 A and GB coils with 6 A of direct current. Figure 2 shows the computed 2D magnetic field maps, highlighting the streamline that crosses the discharge tube edge at  $z = 0$ , thus defining the ideal shape of the plasma plume (whether it is assumed fully magnetized). With reference to Figure 2, it is noteworthy to emphasize on the magnetic throat location. It moves from upstream the antenna in Conf. A to far downstream the an-

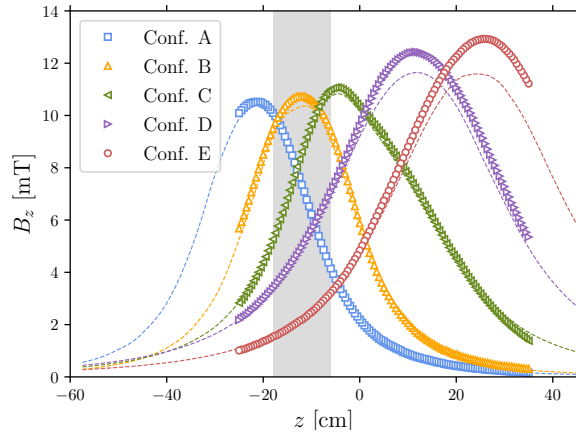


FIG. 3. Externally applied magnetic field on-axis profiles. Shaded area indicates the antenna location. Dashed lines represent simulation profiles, scatter points indicate probe measurements.

150 tenna in Conf. E. The first axial mode the antenna can generate  
 151 translates in an axial wavelength as  $\lambda_z = 24$  cm, see Section  
 152 IV C. Notice that the magnetic throat in Conf. D is approxi-  
 153 mately one wavelength downstream of the antenna center. The  
 154 magnitude of the on-axis magnetic field is reported in Figure  
 155 3 by comparing computed values and measured values. All  
 156 magnetic configurations feature a peak value of  $10 \div 13$  mT  
 157 with a similar qualitative profile but shifted along  $z$ .

### 158 III. DIAGNOSTICS

#### 159 A. RF-compensated Langmuir probe

160 Plasma density  $n_p$ , electron temperature  $T_e$  and plasma po-  
 161 tential  $V_p$  are measured using a rf-compensated Langmuir  
 162 probe (LP), see Figure 4. A detailed description of the probe  
 163 has been previously reported in<sup>11</sup>. It is designed in accord-  
 164 ance with the results reported in<sup>32-34</sup>. A tungsten wire of  
 165 0.38 mm in diameter and 5 mm in length constitutes the probe  
 166 tip. An additional electrode made of stainless steel contributes  
 167 to rf compensation and provides mechanical support to the as-  
 168 sembly. The electrode is electrically insulated from the probe  
 169 tip using a 1 mm in outer diameter alumina tube. A 1 nF axi-  
 170 al capacitor is soldered to the compensation electrode and  
 171 connected in parallel with the probe tip and a series of three  
 172 axial chokes, each of which self-resonates at one of the first  
 173 three harmonics. The whole assembly is encapsulated inside  
 174 a borosilicate glass tube of 6 mm outer diameter, which also  
 175 accommodates the coaxial cable for probe biasing and current



FIG. 4. RF-compensated Langmuir probe.

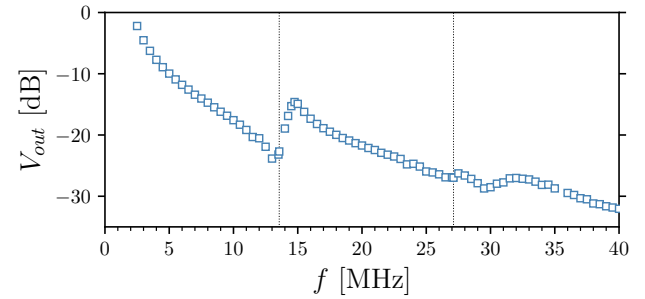


FIG. 5. RF-compensated LP frequency spectrum ( $V_{ref} = 10$  V). Vertical dotted lines indicate 13.56 MHz and 27.12 MHz.

176 measuring.

177 Chokes selection is attained by characterization of their  
 178 impedance frequency spectrum. A  $20 V_{pp}$  sinewave is gener-  
 179 ated by a function generator and fed to one lead of the testing  
 180 choke. The other lead is connected to a 46.52 k $\Omega$  resistor and  
 181 the series circuit closes to the ground. The frequency of the  
 182 input sinewave is swept while the voltage drop across the resis-  
 183 tor is monitored and used to calculate the current flowing  
 184 in the circuit. The frequency at which the current is minimum  
 185 is the choke self-resonating frequency. Functional check of  
 186 the whole probe assembly is performed by applying a  $20 V_{pp}$   
 187 sinewave to the tungsten tip at different frequencies. The  
 188 probe output is recorded by a digital oscilloscope and shown  
 189 in Figure 5 as a function of the input frequency. Local minima  
 190 are evident in correspondence of the harmonic frequencies, as  
 191 desired.

192 The probe is manually displaced within the plasma using  
 193 a single-axis translation stage with a resolution of 10  $\mu$ m and  
 194 a stroke of 150 mm. Probe alignment is ensured by the use  
 195 of a cross-line laser pendulum. I-V curves are recorded us-  
 196 ing a ALP control unit by Impedans Ltd. Thereafter, data is  
 197 post-processed relying on OML theory<sup>34,35</sup>. Assuming local  
 198 quasineutrality, plasma density  $n_p$  is inferred from the linear  
 199 fit of the ion current squared versus the probe potential. The  
 200 ion current fit is then subtracted from the total current to ob-  
 201 tain a better estimation of the electron current. Assuming the  
 202 electrons are described by a Maxwell-Boltzmann distribution  
 203 function, the logarithmic profile of the electron current is lin-  
 204 early fitted, enabling the estimation of the electron tempera-  
 205 ture  $T_e$ . The plasma potential  $V_p$  is computed as the probe bias  
 206 voltage where the first derivative of the I-V curve features its  
 207 peak value.

208 Uncertainty associated with the probe measurements is es-  
 209 timated through a statistical approach. The detailed procedure  
 210 has been previously reported in<sup>11</sup>. The outline of the analysis  
 211 shows that all plasma parameters are measured with a statisti-  
 212 cal deviation as high as  $\sim 2$  %.

#### 213 B. Planar probe with guard ring

214 The ion current density  $j_i$  is measured using a planar probe  
 215 with a guard ring (PPGR). It mainly comprises a disk-shaped

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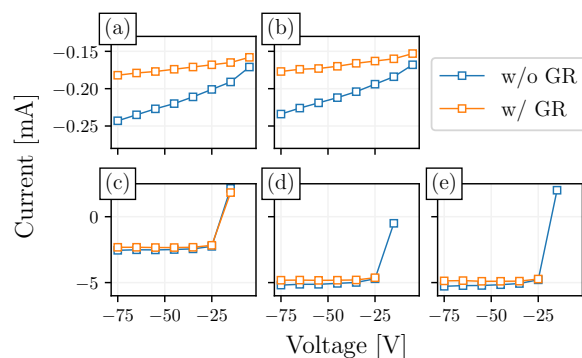


FIG. 6. Ion current profiles at  $(x, y = 0; z = 15 \text{ cm})$ . Subplots denomination is linked to magnetic configurations Conf.s A-E.

216 collector and an outer ring, both made in stainless steel. The  
217 role of the guard ring is to concentrate sheath edge effects far  
218 from the collector, thus ensuring that the ion collection area  
219 exactly corresponds to the collector geometrical area<sup>36</sup>. For  
220 correct functioning of the probe, it is required that *i*) the width  
221 of the guard ring is much larger than the local plasma sheath  
222 thickness and *ii*) the gap between the two electrodes is smaller  
223 than the local sheath thickness to introduce negligible poten-  
224 tial irregularities. The collector is 5.6 mm in diameter and  
225 1 mm in thickness, whereas the ring width is 1 mm. A gap  
226 of 100  $\mu\text{m}$  is maintained between the two electrodes to ensure  
227 electrical insulation. Each electrode features a separated elec-  
228 trical connection for polarization and current measurement.  
229 Voltage is applied to the collector by way of a Keithley 2410  
230 SourceMeter, which is also used to measure the flowing cur-  
231 rent. The guard ring is biased using a TTIEX752M power  
232 supply.

233 Functional check of the probe is carried out by recording  
234 the I-V curves at  $(x, y = 0; z = 15 \text{ cm})$  for the five mag-  
235 netic configurations denominated Conf.s A-E. The curves obtained  
236 with a biased and floating guard ring are compared in Figure  
237 6. Saturation of the ion current is achieved for Conf.s C-D-E  
238 at voltages lower than about  $-40 \text{ V}$ , while no complete satu-  
239 ration is recorded for Conf.s A and B due to the fact that the  
240 guard ring width is not compatible with the local values of  
241 the sheath thickness. This can be confirmed by computing the  
242 local values of the characteristic lengths over the radial coor-  
243 dinate using the values of  $n_p$  and  $T_e$  later discussed in Section  
244 IV. Floating and high voltage sheath thickness,  $s_f$  and  $s_{hv}$  re-  
245 spectively, are computed in accordance with<sup>37</sup>, using  $-75 \text{ V}$   
246 for Conf.s A-B and  $-50 \text{ V}$  for Conf.s C-D-E. Outcomes are  
247 plotted in Figure 7. It results evident that values of  $s_{hv}$  for  
248 Conf.s C-D-E are much smaller than the guard ring width,  
249 whereas those for Conf.s A and B approach its size. It shall  
250 be noted that the attainment of a perfectly flat profile of the  
251 ion saturation current would require a guard ring width  $5 \div 10$   
252 times larger than the actual one. Thus, the overall probe size  
253 would probably lead to serious plasma perturbations. Further-  
254 more, the scope of the presented measurements is not to, e.g.,  
255 focus on indirect propulsive performance estimation but rather

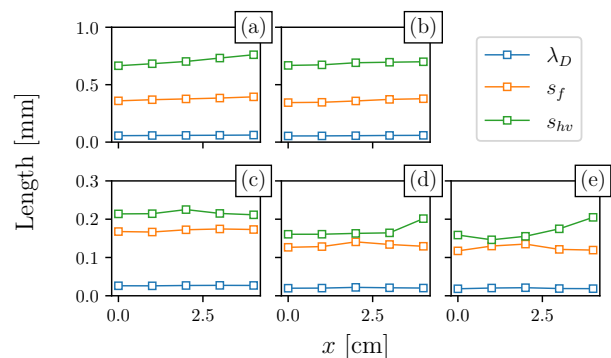


FIG. 7. Debye length, floating and high-voltage sheath thickness at  $z = 15 \text{ cm}$ . Subplots denomination is linked to magnetic configurations Conf.s A-E.

256 to perform a more qualitative-like comparison of the five mag-  
257 netic configurations.

258 Given the high level of reproducibility recorded during pre-  
259 liminary measurements, the uncertainty in  $j_i$  is mainly given  
260 by the uncertainty in the measured current and the probe col-  
261 lecting area. This consideration leads to a value of  $< 8 \%$ .

262 The planar probe is manually actuated from outside the  
263 chamber using the single-axis translation stage described in  
264 Section III A.

### 265 C. Laser-induced fluorescence setup

266 Ions and atoms velocity distribution functions (VDFs) are  
267 measured by means of laser-induced fluorescence (LIF) spec-  
268 troscopy. The technique and the optical bench in use have  
269 been extensively described in previous works<sup>38,39</sup>. Excita-  
270 tion of metastable levels is achieved via an amplified tunable  
271 single-mode laser diode in the 810 – 840 nm spectral range.  
272 The primary laser beam is split in multiple beams with the  
273 purpose of *i*) instantaneous monitoring of the laser mode and  
274 detection of any mode hop by means of a Fabry-Pérot inter-  
275 ferometer, *ii*) laser power check using a photodiode and *iii*) ac-  
276 curate wavelength measurement by way of a calibrated wavem-  
277 eter whose absolute uncertainty is  $\sim 60 \text{ m s}^{-1}$  (80 MHz). Mod-  
278 ulation of the laser beam is achieved using a mechanical chop-  
279 per at  $\sim 1.9 \text{ kHz}$ . The laser is coupled to a 50  $\mu\text{m}$  optical  
280 fiber which allows transporting the laser beam from the optical  
281 bench to the Helicon source setup. Laser is injected inside the  
282 vacuum chamber through a borosilicate glass window located

TABLE I. Kr I and Kr II probed optical transitions.

	Transition	$\lambda_{exc}$ [nm] (vacuum)	$\lambda_{fluo}$ [nm] (air)
Kr I	$5s^2[3/2]_1^{\circ} \rightarrow 5p^2[3/2]_2$	819.23095	760.15457
Kr II	$5p^2D_{5/2}^{\circ} \rightarrow 5s^2P_{3/2}$	820.4959	461.91658

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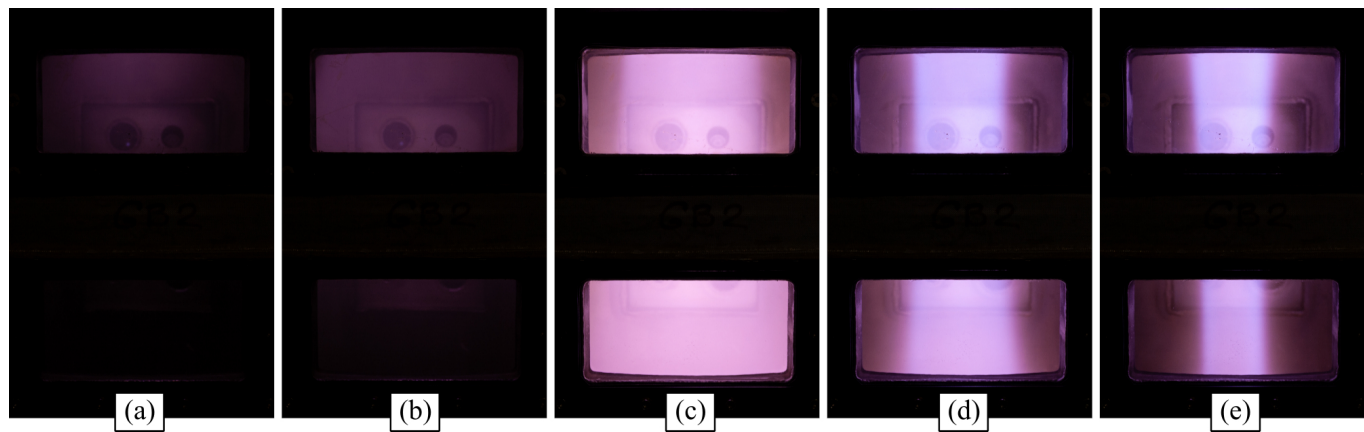


FIG. 8. Photographs of the plasma plume in (a) Conf. A, (b) Conf. B, (c) Conf. C, (d) Conf. D and (e) Conf. E. Windows are centered at  $z = 12$  and  $z = 24$  cm.

at the bottom of the reactor. Note that  $\mathbf{k} \cdot \mathbf{v} < 0$  here, where  $\mathbf{k}$  is the laser wavenumber and  $\mathbf{v}$  the particle velocity. The laser beam is collimated using a combination of a 150 mm and a 1000 mm focal length plano-convex lenses. Uncertainty on the alignment with respect to the HP source axis is estimated to be  $\lesssim 1.6$  deg. In order to ensure a linear regime of the studied optical transitions, the laser power density delivered to the plasma is kept below  $1.2 \text{ W mm}^{-2}$ , a threshold value that has been determined during preliminary measurements. A detection branch is placed perpendicularly to the excitation beam featuring a pair of plano-convex lenses (250 mm and 100 mm focal lengths) focusing on a  $200 \mu\text{m}$  core diameter optical fiber. Both the excitation and detection branches are mounted on a dedicated computer-controlled high precision linear translation stage to enable spatially resolved measurements along the  $y$  axis. The detection optical train can be additionally displaced along the  $z$  axis within a few centimeters using a manual stage. The  $200 \mu\text{m}$  optical fiber transports the fluorescence light to a monochromator which isolates the desired line from the whole spectrum. Afterwards, a photomultiplier tube is used to convert the light signal into voltage, which is fed into a lock-in amplifier operating at the laser modulation frequency to distinguish the signal from the natural plasma emission. The VDFs are inferred by scanning over the laser wavelength  $\lambda$  and computing the particles axial velocity  $v_z$  as  $v_z = c(\lambda - \lambda_0)/\lambda_0$ , where  $\lambda_0$  is the unshifted transition wavelength and  $c$  is the speed of light. The measured LIF profiles result from the Doppler broadened line. The presence of Kr isotopes leads to broadening due to isotopic shift and hyperfine structure<sup>38</sup>. Moreover, due to the presence of a steady magnetic field, the Zeeman effect splits the spectral lines into sub-levels<sup>38</sup>. Nevertheless, since the spectrum is dominated by the  $^{84}\text{Kr}$  isotope and the magnetic field is relatively weak, it is herein assumed that the observed fluorescence line profile images the local VDF.

The probed optical transitions are reported in Table I. The zero-velocity wavelength for Kr I is estimated from preliminary measurements in the HP source shining the laser along the  $x$  axis. The other listed wavelengths are given in the literature<sup>38–42</sup>.

## IV. EXPERIMENTAL RESULTS AND DISCUSSION

### A. Visual inspection

The very first piece of information regarding the way the plasma responds to the applied magnetic field topology is provided by visual inspection. The photographs of the plasma plume reported in Figure 8 are taken using a common DSLR camera framing the region  $8 < z < 28$  cm and set at  $f/8$  and  $1/40$  s exposure time. It results evident how significant differences characterize the extracted plasma plume when employing the different magnetic topologies. A faint plume is visible when the reactor operates in Conf. A and Conf. B. Instead, a well defined plasma beam is noticed when Conf.s C, D and E are chosen. In the latter cases, the plasma radius visibly delineates the local magnetic streamlines, cf. Figure 2 and Figure 8. It is interesting to notice that the local magnitude of the axial component  $B_z$  is nearly equal for Conf. C and Conf. E at  $z = 12$  cm (see Figure 2), i.e. at the center of the top window in Figure 8. Yet, the two plasma beams show a very different structure. As a matter of fact, local values of the field radial component  $B_r$  and gradient  $\partial B_z / \partial z$  significantly differ. This finding agrees with previous numerical models<sup>26,43</sup> and intrinsically points out that both  $|\mathbf{B}|$  and  $\nabla \mathbf{B}$  have an impact on the plasma behavior.

### B. LP measurements

Plasma properties are characterized using the diagnostics described in Section III. The region delimited by  $0 < y < 4$  cm and  $-4 < z < 21$  cm is probed by means of the rf-compensated LP. I-V characteristics are recorded with a spatial resolution of 5 mm. Data is post-processed as discussed in Section III A and eventually interpolated to enhance visualization. Figures 9, 10 and 11 illustrate normalized 2D maps of  $n_p$ ,  $T_e$  and  $V_p$ , respectively, for the five magnetic topologies. Normalization values are:  $6 \times 10^{17} \text{ m}^{-3}$  as regards to  $n_p$ , 6 eV for  $T_e$  and 25 V for  $V_p$ . The solid black lines

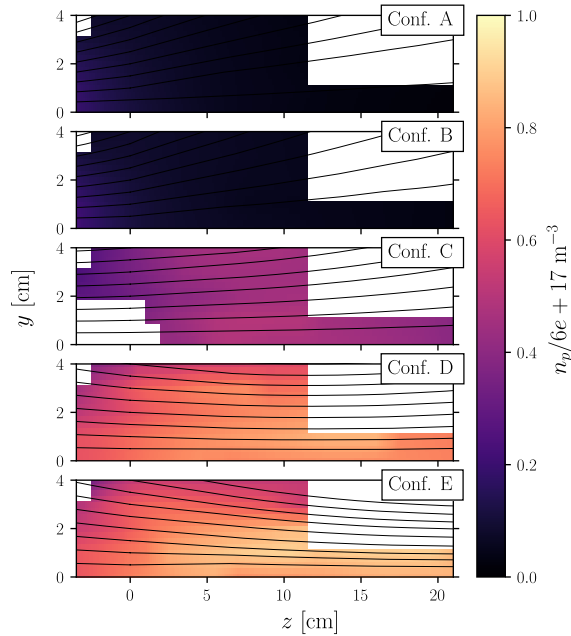


FIG. 9. Normalized plasma density for the five magnetic configurations. Normalization factor is  $6 \times 10^{17} \text{ m}^{-3}$ . Solid black lines represent magnetic streamlines.

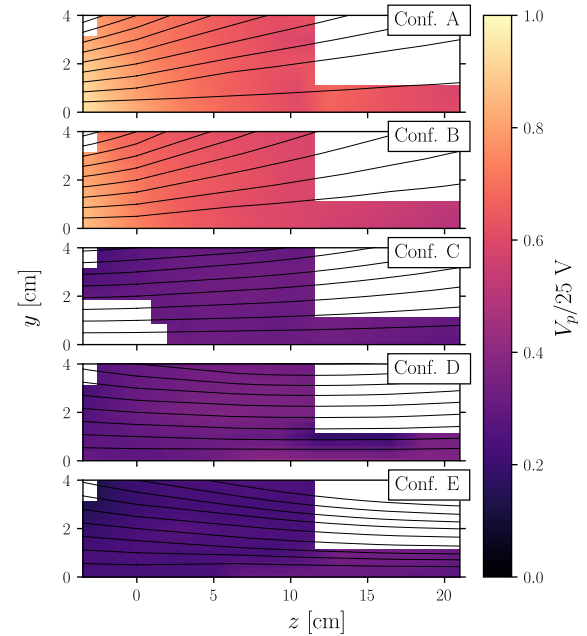


FIG. 11. Normalized plasma potential for the five magnetic configurations. Normalization factor is 25 V. Solid black lines represent magnetic streamlines.

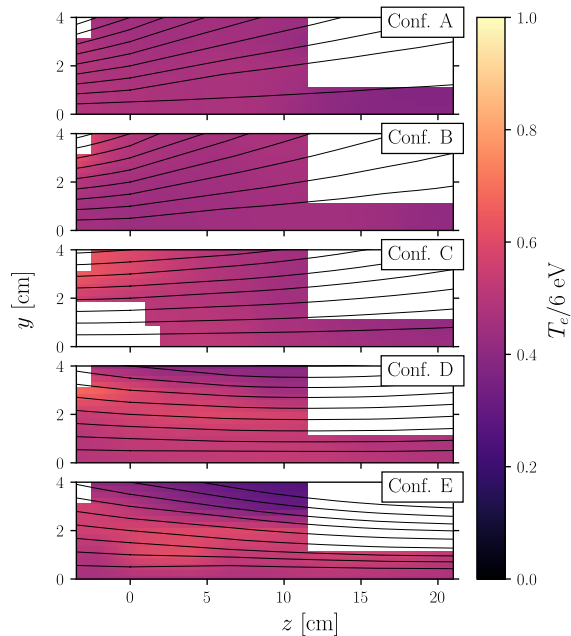


FIG. 10. Normalized electron temperature for the five magnetic configurations. Normalization factor is 6 eV. Solid black lines represent magnetic streamlines.

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357 included in the figures represent the magnetic streamlines de-  
358 limited by the discharge tube edge at  $z = 0$ . Furthermore, on-  
359 axis profiles of  $n_p$ ,  $T_e$  and  $V_p$  are shown in Figure 12. These  
360 experimental measurements show that:

- 361 1. when the HP source operates in Conf. A, the extracted  
362 plasma plume is characterized by a low monotonically  
363 decreasing profile of  $n_p$  ranging between  $\sim 1 \times 10^{17}$   
364 and  $\sim 9 \times 10^{15} \text{ m}^{-3}$  along the reactor axis. The pro-  
365 file of  $T_e$  features a monotonic behavior as well, with  
366 a peak value of  $\sim 3 \text{ eV}$ . In a similar fashion,  $V_p$  drops  
367 from  $\sim 24 \text{ V}$  to  $\sim 15 \text{ V}$ . All plasma properties peak on-  
368 axis at  $z < 0$ . These quantitative observations agree with  
369 the faint light emitted in the nozzle region, as stated be-  
370 forehand. Visual check of the plasma also reveals that  
371 light is instead concentrated within the discharge tube.  
372 It suggests that the radial and back boundaries represent  
373 a major loss term of plasma<sup>26,44</sup>.
- 374 2. when the HP source operates in Conf. B, analogous ar-  
375 guments can be put forward. The profile of  $n_p$  like-  
376 wise peaks on-axis at  $z < 0$  and decays monotonically  
377 downstream. Altogether, slightly larger values of  $n_p$  are  
378 measured with respect to Conf. A. In the bulk of the  
379 plasma,  $T_e$  remains in the order of  $\sim 3 \text{ eV}$  with lower  
380 values downstream. However, a population of relatively  
381 more energetic electrons ( $T_e \sim 3.5 \text{ eV}$ ) appears off-axis,  
382 in correspondence of the magnetic nozzle edge, visible  
383 at  $z < 0$  in Figure 10(b). Although qualitatively very

- 384 similar, the distribution of  $V_p$  for Conf. B presents lower  
385 values with respect to Conf. A of a few volts.
- 386 3. when the HP source operates in Conf. C, results similar  
387 to those previously reported in<sup>11</sup> using the same HP  
388 source are obtained. As a matter of fact, in both the ex-  
389 periments the magnetic throat is located at  $z = 0$ . In  
390 contrast to what was discussed in points (i) and (ii),  
391 all plasma properties peak off-axis. Data acquisition  
392 in the region ( $0 < r < 2, z < 0$ ) was not possible due  
393 to discharge instability possibly induced by the probe  
394 presence. The largest value of  $n_p$  is recorded at  $z > 0$   
395 and it reads  $\sim 3 \times 10^{17} \text{ m}^{-3}$ , whereas  $T_e$  reaches a peak  
396 of 4 eV at  $z < 0$ . The distribution of  $V_p$  is relatively  
397 isotropic, ranging in the  $8 \pm 0.5 \text{ V}$  interval. The rea-  
398 son why  $n_p$  and  $T_e$  present separated regions of the re-  
399 spective maximum values has been explained in<sup>11,45</sup> in  
400 terms of pressure balance. When considering the  $z$  com-  
401 ponent of the electron momentum conservation equa-  
402 tion in the limit of negligible contribution due to mo-  
403 mentum transfer collisions and due to the Lorenz force,  
404 the potential gradient and the pressure gradient balance  
405 each other. In the region where  $B_r/B_z \ll 1$ , i.e. where  
406 the local magnetic field divergence angle is small, the  
407 reduced cross field electron mobility yields a relatively  
408 large axial conductivity, resulting in a nearly null poten-  
409 tial gradient. Hence, for equilibrium reasons, the pres-  
410 sure gradient is required to be small, which results in  
411 a larger  $n_p$  where  $T_e$  is lower and vice versa. Similar  
412 results are numerically found and discussed in<sup>46</sup>.
- 413 4. when the HP source operates in Conf. D, light emis-  
414 sion upstream the antenna is almost absent, hinting that  
415 plasma losses at the back and lateral walls are mitigated  
416 with respect to the previous cases. With reference to  
417 Figure 9(d), it is evident that  $n_p$  follows the axial gra-  
418 dient of  $B_z$ . The maximum value of  $\sim 5 \times 10^{17} \text{ m}^{-3}$   
419 is therefore located in correspondence of the magnetic  
420 throat. In Figure 10(d), it is relevant to notice the dis-  
421 tinct transport pattern of a relatively more energetic  
422 electron population along the magnetic field lines at the  
423 edge of the nozzle, which exhibits  $T_e \approx 3.5 \div 4.2 \text{ eV}$ . A  
424 relatively small  $V_p$  is measured throughout the probed  
425 region, with a peak value in the order of 10 V in the  
426 area of maximum  $n_p$ .
- 427 5. when the HP source operates in Conf. E, similar ob-  
428 servations to those stated in point (4) can be raised.  
429 Profiles of  $n_p$  and  $T_e$  have a strong dependence on the  
430 spatial distribution of  $B_r$  and  $B_z$ . The highest plasma  
431 density value among all the studied magnetic configura-  
432 tions is herein recorded to be  $\sim 5.5 \times 10^{17} \text{ m}^{-3}$  nearby  
433 the magnetic throat. As highlighted in point (4), also  
434 in this case a more energetic population of electrons is  
435 transported along the external surface of the magnetic  
436 nozzle, cf. Figure 10(e). At  $z \cong 10 \text{ cm}$ , all the electrons  
437 with  $T_e \gtrsim 3 \text{ eV}$  are concentrated in a radius of about  
438 3 cm, as visually confirmed by Figure 8(e).

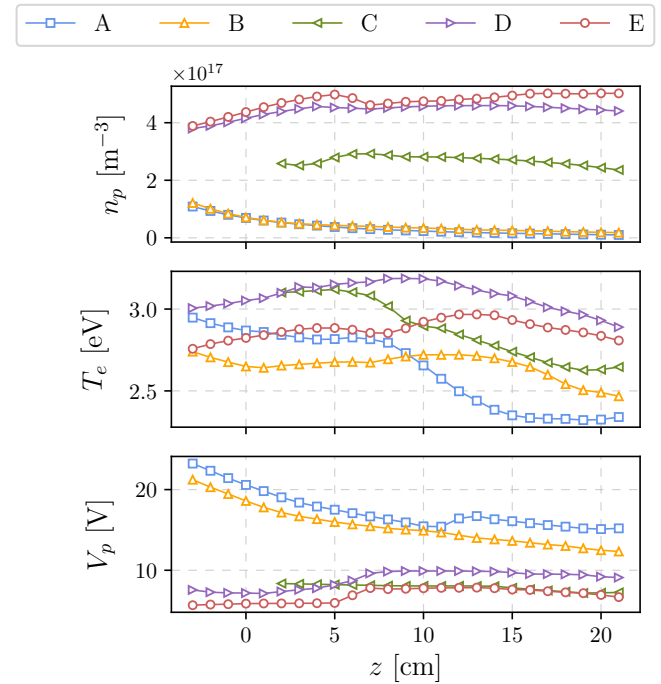


FIG. 12. On-axis profiles of (top) plasma density, (middle) electron temperature and (bottom) plasma potential. Data is extracted from Figures 9-11 and down-sampled to enhance visualization.

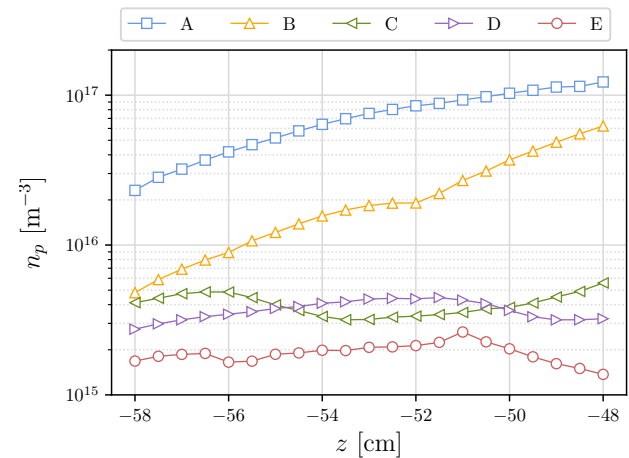


FIG. 13. Ion density profile in the proximity of the back-plate for the five magnetic configurations.

439 Eventually, it is worth observing that the different config-  
440 urations of  $B$  possibly influence the power deposition map.  
441 This, in turn, very likely relates to the different spatial distri-  
442 butions of  $n_p$  and  $T_e$  as discussed in points (1)-(5).

443 In addition to the measurements performed using the rf-  
444 compensated LP, a simple uncompensated LP is inserted on-  
445 axis at the back/injection plate of the HP source to measure  
446  $n_p$  as an indicator of the plasma flux lost in this region. The  
447 probe is biased to scan over the ion saturation branch only.



448 No significant distortions due to rf oscillations are expected in  
449 this part of the I-V curve<sup>33</sup>. For obtaining this particular set  
450 of data, the reactor injection plate has been modified in order  
451 to accommodate the probe and its related wiring. The pro-  
452 pellant is still injected off-axis but it goes through a plenum  
453 first and eventually reaches the discharge tube via a multi-  
454 perforated surface, resulting in a axial gas flow. An uncom-  
455 pensated probe is chosen due to limitations on the available  
456 room. The measured profiles of  $n_p$  are shown in Figure 13  
457 for Conf. A to E. Since the magnetic throat in Conf. A is lo-  
458 cated upstream the antenna, the ions are mostly transported  
459 towards the back plate by following the convergent-divergent  
460 shape of the magnetic field. As the magnetic throat moves far-  
461 ther downstream from the antenna center, lower densities are  
462 measured in the proximity of the injection plate, as expected.

### 463 C. Plasma density profile model

464 Using a simplified description of the plasma, the measured  
465 axial profiles of  $n_p$  can be compared with theoretical profiles  
466 retrieved from the helicon wave dispersion relation, which is  
467 thereafter derived accounting for the non-uniformity of the ex-  
468 ternal magnetic field along  $z$ . This approach implicitly as-  
469 sumes that the plasma production entirely relies on the wave-  
470 mode power coupling. Although the helicon regime is not  
471 proven here by direct measurement of the excited wave, previ-  
472 ous experiments performed on the same device operated with  
473 similar ranges of magnetic field strength and input power have  
474 shown the presence of the propagating wave<sup>11</sup>. Considering  
475 that the electric  $\tilde{\mathbf{E}}$  and magnetic  $\tilde{\mathbf{B}}$  components of the exited  
476 wave are described<sup>47,48</sup> as

$$477 \tilde{\mathbf{E}}, \tilde{\mathbf{B}} \sim \exp[i(m\theta + k_z z - \omega t)], \quad (1)$$

478 where  $m$  is the azimuthal mode number,  $\theta$  is the azimuthal  
479 angle and  $k_z$  is the axial wavenumber, Maxwell equations as-  
480 sume the form

$$480 \nabla \cdot \tilde{\mathbf{B}} = 0, \quad (2a)$$

$$481 \nabla \times \tilde{\mathbf{E}} = i\omega\tilde{\mathbf{B}}, \quad (2b)$$

$$482 \nabla \times \tilde{\mathbf{B}} = \mu_0\mathbf{j}. \quad (2c)$$

483 The electron momentum equation is written as

$$484 -en_p\tilde{\mathbf{E}} = i\frac{m_e}{e}\mathbf{j}_e(\omega + i\nu) - \mathbf{j}_e \times \mathbf{B}, \quad (3)$$

485 where  $\mathbf{j}_e$  is the electron current density,  $\mathbf{B}$  is the external mag-  
486 netic field and  $\nu$  is a collision rate accounting for all dissi-  
487 pation phenomena. Additional comments and derivation of  
488 Equation 3 are reported in<sup>47</sup>. The widespread ideal assump-  
489 tion of perfectly uniform magnetic field is not appropriate in  
490 the actual case. Therefore, although still simplistic, it is as-  
491 sumed that  $\mathbf{B} = B(z)\hat{\mathbf{z}}$ , i.e. only the variation of the magnetic

TABLE II. Helicon wave parameters at  $z = 10$  cm.

	Conf. A	Conf. B	Conf. C	Conf. D	Conf. E
$r_p$ [cm]	7.3	8.1	5.1	4.0	3.5
$k_z$ [cm <sup>-1</sup> ]	0.26	0.26	0.26	0.26	0.26
$\lambda_z$ [cm]	24	24	24	24	24
$\kappa_1$ [cm <sup>-1</sup> ]	0.46	0.41	0.68	0.88	1.03
$\kappa_2$ [cm <sup>-1</sup> ]	0.14	0.17	0.07	-0.01	-0.08

490 field along  $z$  is accounted for. Combining Equation 2a-(2c)  
491 and Equation 3, one obtains

$$\left(\frac{\omega + i\nu}{\omega_{ce}}\right) \nabla \times (\nabla \times \tilde{\mathbf{B}}) + k_z \nabla \times \tilde{\mathbf{B}} + \frac{\mu_0 \omega en_p}{B} \tilde{\mathbf{B}} = \mathbf{0}, \quad (4)$$

492 where the explicit dependence on  $z$  has been omitted,  $\omega_{ce}$  is  
493 the electron cyclotron frequency and the rest is conventional.  
494 Detailed derivation of Equation 4 is likewise included in<sup>47</sup>.  
495 Eventually, in the limit of  $m_e \rightarrow 0$ , the local dispersion relation  
496 is retrieved in the same shape of the well known 0D dispersion  
497 relation, i.e.

$$k(z)k_z = \frac{\mu_0 \omega en_p(z)}{B(z)}, \quad (5)$$

498 where  $k(z)$  indicates the total wavenumber. The wave bound-  
499 ary conditions are fixed by<sup>48</sup>

$$mk(z)J_m[k_r(z)r_p(z)] + k_z J'_m[k_r(z)r_p(z)] = 0, \quad (6)$$

500 where  $J_m$  and  $J'_m$  are the Bessel function of the first kind  
501 of order  $m$  and its derivative, respectively,  $k_r(z)$  is the lo-  
502 cal radial wavenumber and  $r_p(z)$  is the local plasma ra-  
503 dius. The value of  $k_z$  is fixed by the antenna length,  
504 i.e.  $k_z = \pi/d_A, 3\pi/d_A, 5\pi/d_A$ , etc. Pretending that only the  
505 first order axial mode is coupled with the antenna, the compu-  
506 tation algorithm includes:

- 507 • the axial wavenumber is estimated as  $k_z = \pi/d_A$ , there-  
508 fore the axial wavelength is  $\lambda_z = 24$  cm;
- 509 •  $r_p(z)$  is set equal to the radius of the magnetic stream-  
510 line crossing the tube edge at  $z = 0$ , see Figure 2;
- 511 • considering the geometry of the antenna and the direc-  
512 tion of the external magnetic field, it is imposed that  
513  $m = +1$ ;
- 514 • two cases are distinguished:
  - 515 1.  $k_r(z)$  is computed numerically from Equation 6  
516 and it is named as  $\kappa_1(z)$  for the sake of clarity in  
517 the following;
  - 518 2.  $k_r(z)$  is evaluated as  $\kappa_1(z) \sin[\alpha(z)]$  referred to as  
519  $\kappa_2(z)$  hereafter. Here  $\alpha(z)$  is the local magnetic  
520 field divergence angle. The purpose of this heuris-  
521 tic strategy is to provide the model with the in-  
522 formation that the applied magnetic field is not

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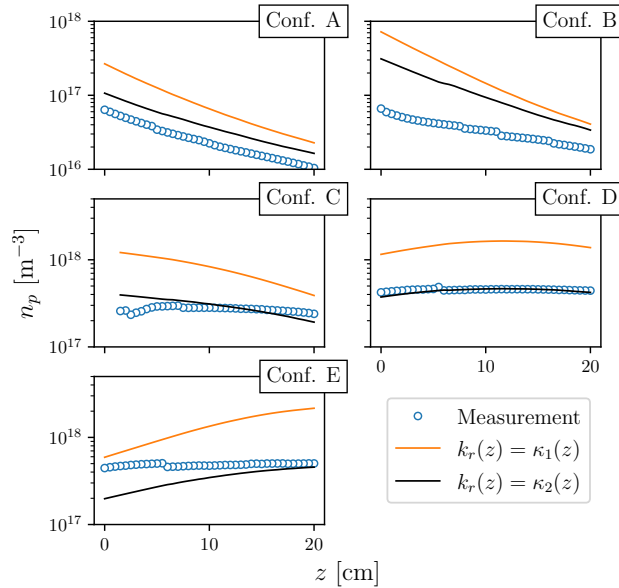


FIG. 14. Plasma density at  $r = 0$  computed using the helicon waves dispersion relation in the  $k_r(z) = \kappa_1(z)$  and  $k_r(z) = \kappa_2(z)$  cases compared to measurement data.

523 purely axial. In doing so, it is postulated that  
 524 the helicon wave resonance cone reduces to a line  
 525 at the magnetic throat, i.e. where  $\alpha = 0$ , thus  $k$   
 526 equals  $k_z$ .

527 • the profile  $n_p(z)$  is consequently computed from Equa-  
 528 tion 5 for the aforementioned two cases.

529 Numerical values of the relevant parameters are reported  
 530 in Table II for all magnetic configurations. In Figure 14, the  
 531 obtained theoretical curves are compared with measurements  
 532 of  $n_p$  extracted from Figure 9 at  $x, y = 0$  for all the tested  
 533 magnetic configurations. In general, it is found that the case  
 534  $k_r(z) = \kappa_1(z)$  provides an overestimation of the plasma den-  
 535 sity. When dealing with Conf.s D and E, the  $k_r(z) = \kappa_2(z)$  case  
 536 is in very good agreement with the data in correspondence  
 537 of the magnetic throat, that is where the strong assumption  
 538  $\mathbf{B} = B(z)\hat{\mathbf{z}}$  is more representative. Ultimately,  $n_p$  measured in  
 539 Conf. C is in relatively good agreement with the latter case.  
 540 It is noted that even the  $k_r(z) = \kappa_2(z)$  case overestimates the  
 541 measured values of  $n_p$  for Conf.s A and B, although match-  
 542 ing the qualitative profile. This suggests that the helicon wave  
 543 is evanescent in this region of the plasma since the measured  
 544  $n_p$  is lower than the one required by the dispersion relation.  
 545 In conclusion, these profiles of  $n_p$  computed from the disper-  
 546 sion relation represent a first effective estimation of the actual  
 547 spatial evolution of plasma density. Therefore, these quanti-  
 548 tative information can be of some convenience for guessing  
 549 the propagation region of helicon waves and for preliminary  
 550 modeling of the plasma dynamics and/or design of the axial  
 551 magnetic field profile.

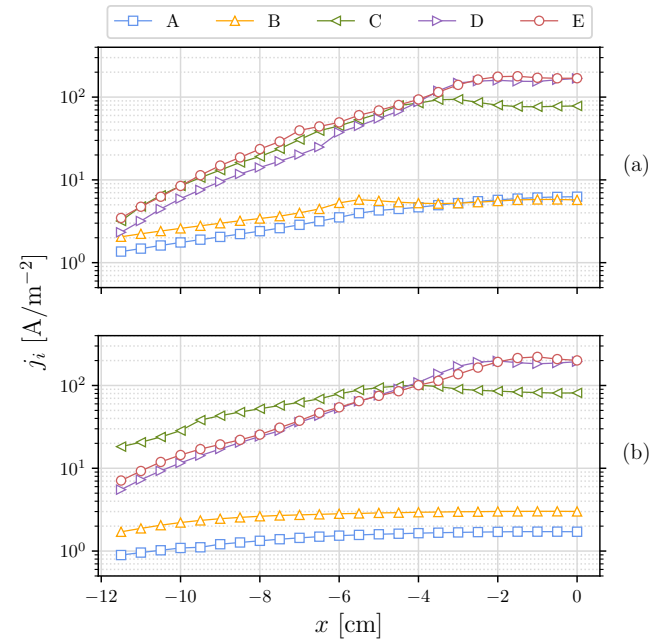


FIG. 15. Ion current density at (a)  $z = 5$  and (b)  $z = 15$  cm for the five magnetic configurations.

TABLE III. Plume divergence parameter  $\delta$  from data in Figure 15.

	Conf. A	Conf. B	Conf. C	Conf. D	Conf. E
$\delta$ at $z = 5$ cm	0.218	0.359	0.041	0.014	0.021
$\delta$ at $z = 15$ cm	0.523	0.567	0.224	0.028	0.035

#### 552 D. PPGR measurements

553 A further insight into the properties of the plasma when  
 554 operating with the different magnetic topologies is ren-  
 555 dered by the employment of the PPGR described in Sec-  
 556 tion III. The probe is displaced radially along the  $x$  axis  
 557 at  $z = 5$  cm and  $z = 15$  cm in order to analyze the diver-  
 558 gence of the extracted plasma plume. The measurements of  
 559  $j_i$  are shown in Figure 15(a-b). Table III gathers the val-  
 560 ues of the divergence parameter  $\delta$  computed as the ratio  
 561  $j_i(x = -11.5 \text{ cm}) / j_i(x = 0 \text{ cm})$ . Results confirm that a low-  
 562 current high-divergence ion beam is extracted from the HP  
 563 source when operating in Conf. A and B. Differently, the ion  
 564 beams related to Conf.s C, D and E feature a similar low-  
 565 divergence profile of  $j_i$  in the proximity of the tube exit, see  
 566 Figure 15(a). Yet, the divergence angle of Conf. C rapidly  
 567 grows as the plasma expands downstream, cf. Figure 15(b).  
 568 The highest value of  $j_i$  is recorded in Conf. E at  $z = 15$  cm,  
 569 in agreement with the largest  $n_p$  probed in the same configu-  
 570 ration. Larger values of  $j_i$  relate well with higher propellant  
 571 utilization efficiency, which is a desirable working condition  
 572 for space propulsion applications.

TABLE IV. Order of magnitude of relevant velocity quantities.

	$\mathcal{O}(v)$
Ion acoustic velocity	$v_B = \sqrt{kT_e/m_i} \approx 2000 \text{ ms}^{-1}$
Thermal velocity	$v_{th} = \sqrt{8kT_i/\pi m_i} \approx 275 \text{ ms}^{-1}$

### 573 E. LIF measurements

574 Using LIF spectroscopy, the velocity distribution functions  
575 of krypton atoms Kr I and ions Kr II are inferred. Informa-  
576 tion about the velocity of the ions is of particular inter-  
577 est for driving conclusions about propulsive performance. On  
578 the other hand, knowledge of the atoms velocity is useful for  
579 modeling of the plasma flow. Table IV exemplifies the order  
580 of magnitude of the relevant velocity terms in the HP  
581 source operating with Kr. Radial profiles of Kr I VDF are  
582 evaluated at  $z = 12 \text{ cm}$  and shown in Figure 16 for all mag-  
583 netic configurations. The spatial resolution is 10 mm. In this  
584 case, the reported data did not require any post-processing as  
585 a adequate signal-to-noise ratio was found. These measure-  
586 ments show that the most probable velocity of Kr I is nearly  
587 unchanged over the different magnetic topologies, reading  
588  $\sim 250 \div 300 \text{ ms}^{-1}$ , therefore in the order of the thermal ve-  
589 locity assuming  $T_i \approx 300 \text{ K}$ , cf. Table IV. No dependence of  
590 the velocity on the radial location  $y$  is recorded. Dissimilar  
591 values of velocity spread are found between the magnetic con-  
592 figurations, with a broader VDF for Conf. C and Conf. D.

593 Axial VDFs of Kr II are probed in the same radial region  
594 with a spatial resolution of 5 mm at three distinct axial posi-  
595 tions, i.e.  $z = 10.5 \text{ cm}$ ,  $z = 12 \text{ cm}$  and  $z = 25 \text{ cm}$ . At some  
596  $y$  locations, the LIF signal was not distinguishable from the  
597 background noise due to small local values of  $n_p$ , therefore  
598 mapping of the VDFs was not possible. For the very same  
599 reason, Conf.s A and B did not allow obtaining an appropriate  
600 signal-to-noise ratio in any of the probed locations. Raw  
601 VDFs are post-processed using a least squares Gaussian fit.  
602 The resulting profiles when the HP source operates in Conf.s  
603 C, D and E are reported in Figure 17, 18 and 19, respectively.  
604 In addition, the most probable velocity is extracted and plot  
605 in Figure 20 thus to facilitate comparison among the various  
606 magnetic configurations. It is noticed that the profiles related  
607 to Conf.s C and D feature a nearly identical trend, whereas the  
608 ion velocity in Conf. E generally retains lower readings. This  
609 is in agreement with the measured values of  $V_p$  which remain  
610 below those concerning Conf. C and D, cf. Figure 11. In the  
611 further upstream regions, namely  $z = 10.5 \text{ cm}$  and  $z = 12 \text{ cm}$ ,  
612 velocities smaller than  $\sim 250 \text{ ms}^{-1}$  are measured, therefore in  
613 the order of the thermal velocity assuming  $T_i \approx 300 \text{ K}$ . Con-  
614 versely, at  $z = 25 \text{ cm}$ , all the velocities increase by a factor of  
615 2 to 3, reaching values as high as  $\sim 500 \text{ ms}^{-1}$ . These small  
616 velocities somewhat concur with the fact that the magnetic  
617 field is weakly divergent in the probed region for Conf.s C and  
618 D, while  $z = 25 \text{ cm}$  represents the throat location for Conf. E.  
619 A weakly divergent magnetic field does not allow for a signifi-  
620 cant momentum gain imparted by the Lorentz force. Measure-  
621 ments farther downstream were prevented due to the limited

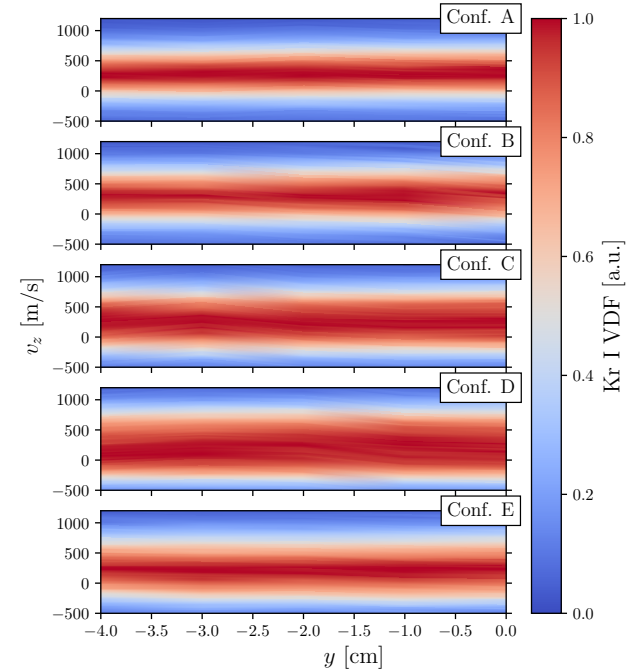


FIG. 16. Kr I velocity distribution function for the five magnetic configurations measured along the  $y$  axis at  $z = 12 \text{ cm}$ .

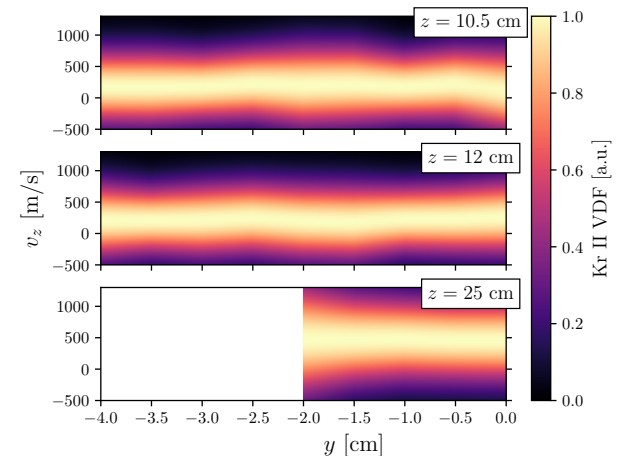


FIG. 17. Kr II velocity distribution function for Conf. C measured along the  $y$  axis at  $z = 10.5, 12$  and  $25 \text{ cm}$ .

622 size of the vacuum chamber. Similar small values of ion ve-  
623 locity are reported in Ref. 49 using LIF on a large scale HP  
624 source. In all of the magnetic configurations, the drop of  $V_p$   
625 is fairly small (in the order of 1 V) within  $z < 21 \text{ cm}$ , cf. Fig-  
626 ure 11. Considering Conf. E for instance, since at  $z < 25 \text{ cm}$   
627 the magnetic field is convergent, it is expected that the favored  
628 inward transport of electrons do not allow for a significant po-  
629 tential drop in this region. In the purely electrostatic case,

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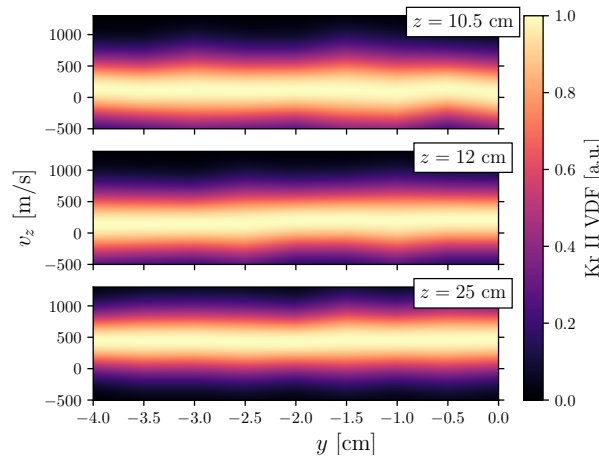


FIG. 18. Kr II velocity distribution function for Conf. D measured along the  $y$  axis at  $z = 10.5, 12$  and  $25$  cm.

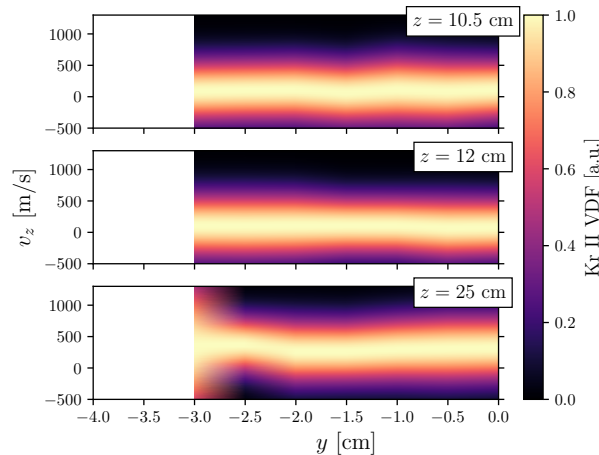


FIG. 19. Kr II velocity distribution function for Conf. E measured along the  $y$  axis at  $z = 10.5, 12$  and  $25$  cm.

630 a potential drop of  $\sim 1$  V translates into an ion velocity in-  
631 crease of  $\sim 1.5$  km s $^{-1}$ . Hence, the acceleration of the ions  
632 throughout the MN does not fully exploit the available en-  
633 ergy. This phenomenon is related to some dissipation phe-  
634 nomenon, e.g. collisions, as later discussed. Moreover, al-  
635 though no sonic condition is achieved at the magnetic throat  
636 in Conf.s C and D, ions experience a further acceleration in  
637 the divergent part of the nozzle, see Figure 20. It suggests that  
638 the sonic point, if ever reached, is shifted downstream, in con-  
639 trast with the ideal postulation of gas-dynamics-like plasma  
640 expansion<sup>50</sup>. In this experiment, the ions might reach the  
641 sonic speed only at the sheath edge that forms downstream  
642 between the chamber wall and the plasma plume. Numer-  
643 ous works focusing on modeling of magnetic nozzle dynam-  
644 ics have assumed that the ion Mach number equals unity at  
645 the throat<sup>51-53</sup>. Albeit this condition conveniently allows sep-  
646 arating the processes of plasma generation and plasma accel-

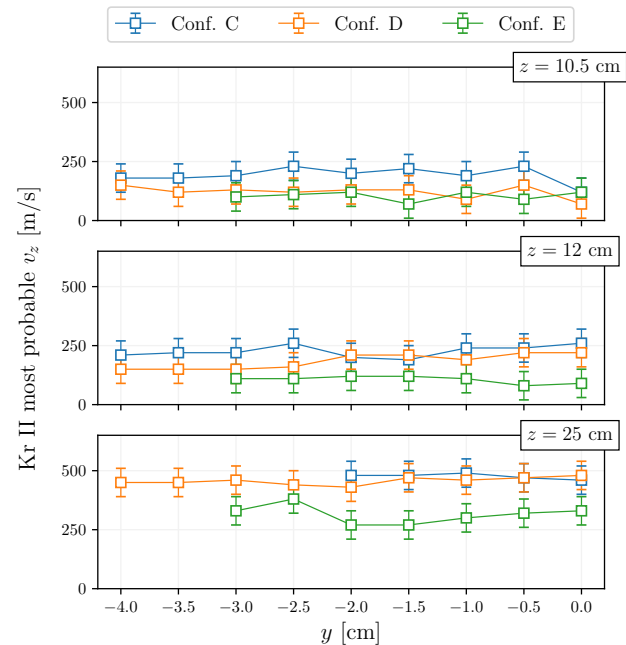


FIG. 20. Kr II most probable axial velocity extracted from Figure 17-19. Error bar is  $60$  m s $^{-1}$  (typical instrument absolute error).

647 eration, it is not representative in this case as well as in some  
648 other plasma beams<sup>24,54</sup>. Collard *et al*<sup>24</sup> have examined a list  
649 of phenomena which are potentially responsible for separation  
650 of the magnetic throat and the sonic point, namely electron-  
651 neutral collisions, charge-exchange collisions and ionization  
652 within the plume. In the device herein analyzed, a combina-  
653 tion of several dissipative phenomena is likely to contribute in  
654 introducing a drag force term that prevents the ions to reach  
655 the sonic speed. In Conf. C, for instance, a significant level  
656 of ionization is localized in the near-field plume downstream  
657 the magnetic throat, as previously noted when commenting on  
658 Figure 9. This suggests that the energy stored in the electrons  
659 is spent for ions generation rather than acceleration.

660 A parametric evaluation of the Kr II axial VDF is addition-  
661 ally performed at  $z = 25$  cm for the purpose of better grasping  
662 the mechanisms occurring within the nozzle. The exploited  
663 parameters are: input power (750 W and 900 W); mass flow  
664 rate ( $0.5$  mg s $^{-1}$ ,  $1$  mg s $^{-1}$  and  $2$  mg s $^{-1}$ ); current in the elec-  
665 tromagnets (6 A and 8 A). The magnetic configuration is fixed  
666 to Conf. D for this experiment because of its divergent shape  
667 at  $z = 25$  cm and larger signal-to-noise ratio with respect to  
668 Conf. C. The resulting VDFs are shown in Figure 21, which  
669 includes the raw data, the Gaussian fittings and the unfold  
670 most probable velocities obtained at each working condition.  
671 The overall tendency results clear. Indeed, higher ion veloci-  
672 ties are attained as the mass flow rate decreases and the mag-  
673 netic field is increased, whereas slower ions are recorded with  
674 larger mass flow rates. These outcomes suggest that collisions  
675 resulting from a larger pressure do play a role in the accel-  
676 eration process. At lower pressures, a larger mean free path is  
677 expected, therefore allowing for greater values of  $T_e$ .

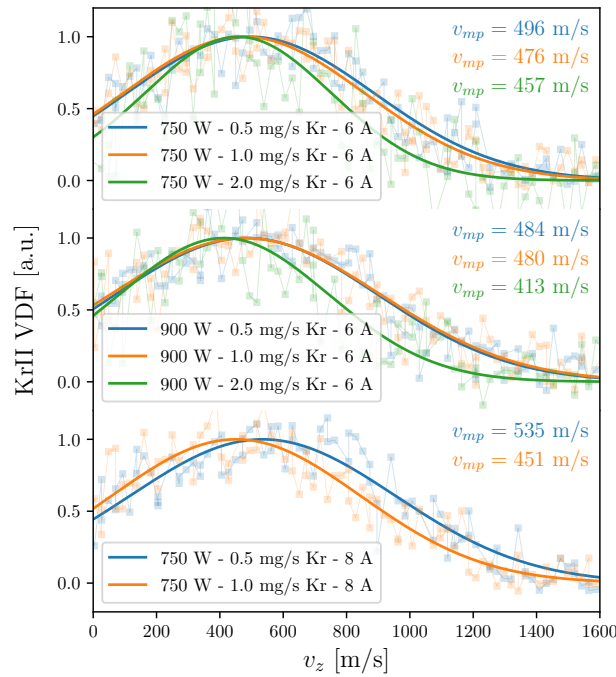


FIG. 21. Kr II axial VDF for Conf. D at  $z = 25$  cm as function of  $P_{IN}$ ,  $\dot{m}$  and electromagnets current. Scatter points indicate raw data, solid lines exemplify least squares Gaussian fittings.

## 678 V. CONCLUSION

679 In summary, several plasma properties are inferred via di-  
 680 rect measurement to establish empirical approaches to thruster  
 681 design and optimization. The magnetic throat is displaced  
 682 along the reactor axis and the resultant plasma is studied in  
 683 the near-field plume using electrostatic diagnostics and LIF  
 684 spectroscopy. It is found that a low-current high-divergence  
 685 plume is extracted from the plasma source when the magnetic  
 686 throat is located upstream or in correspondence of the antenna  
 687 center point. Plasma density measurements at the back plate  
 688 emphasize that, in those cases, the generated plasma mainly  
 689 remains within the discharge tube and is lost at the radial and  
 690 back boundaries. Larger ion currents and higher confinement  
 691 levels are attained when the magnetic throat is located down-  
 692 stream the antenna, namely at a distance at least equal to the  
 693 wavelength corresponding to the first order axial mode of the  
 694 helicon wave. Hence, optimization of the plasma generation  
 695 process in a Helicon thruster would include the separation of  
 696 the magnetic throat from the antenna location in accordance  
 697 with the excited helicon wavelength.

698 Theoretical axial profiles for the plasma density are directly  
 699 derived from the dispersion relation under the hypothesis of  
 700 non-uniform magnetic field. Comparison with probe mea-  
 701 surements show relatively good agreement therefore hinting  
 702 the applicability of this theoretical description for guessing

703 the helicon wave propagation region. Furthermore, prelim-  
 704 inary modeling and design of Helicon thrusters can perhaps  
 705 make use of this approach to shape the axial magnetic field  
 706 profile.

707 The measured ion axial velocities exhibit small values, be-  
 708 ing below the sonic condition at the magnetic throat. By mea-  
 709 suring the most probable ion velocity obtained under differ-  
 710 ent working parameters (input power, magnetic strength and  
 711 mass flow rate), it is concluded that ionization and collisions  
 712 occurring in the near-field plume contribute to limiting the ion  
 713 acceleration process.

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 718 for In-space Applications).

## 719 CONFLICT OF INTEREST

720 The authors have no conflicts to disclose.

## 721 DATA AVAILABILITY

722 The data that support the findings of this study are available  
 723 from the corresponding author upon reasonable request.

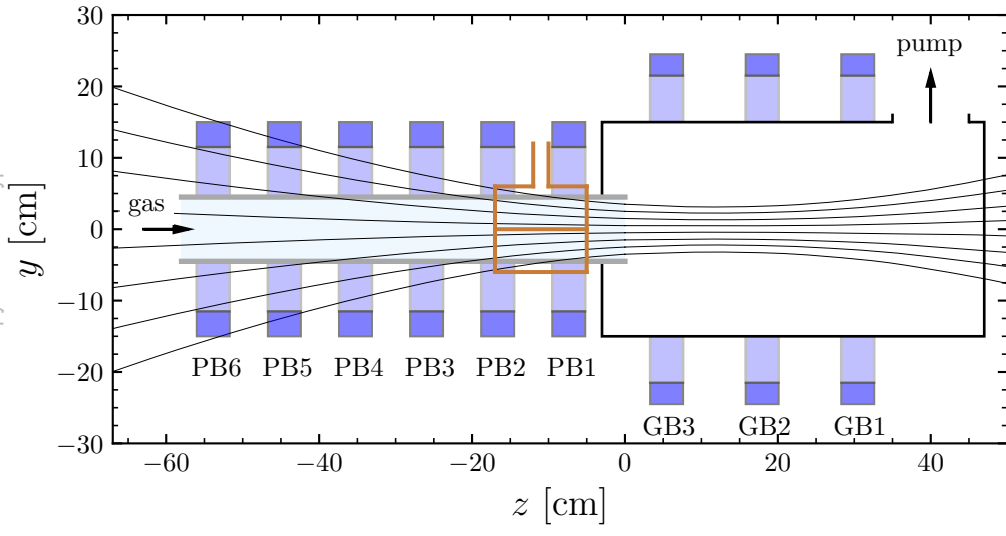
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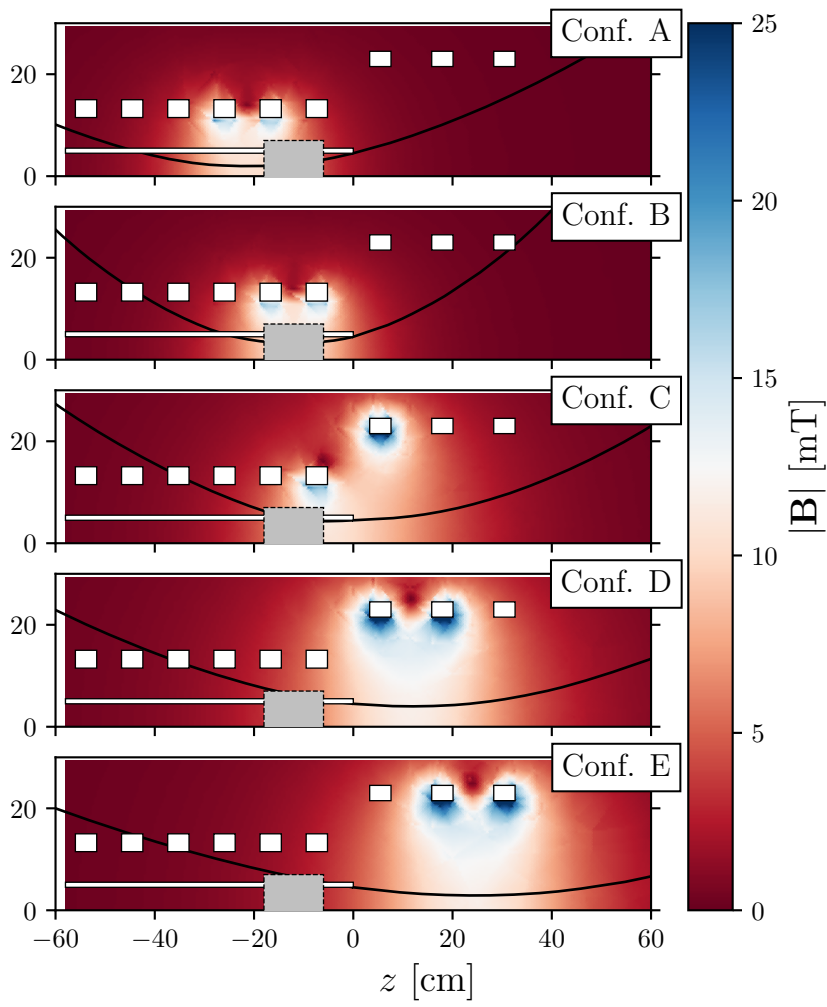
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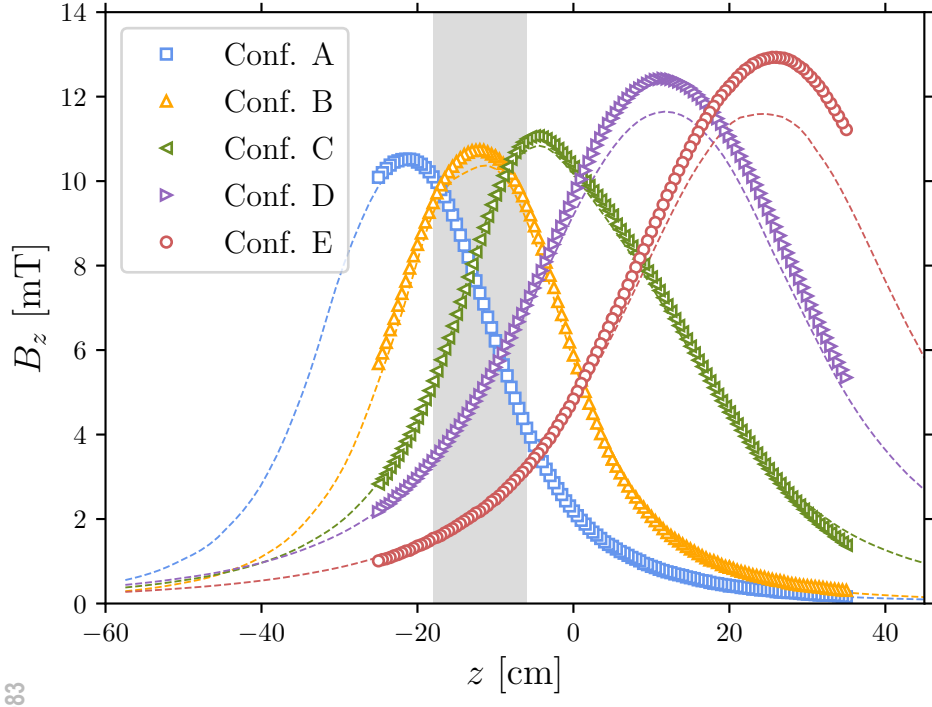
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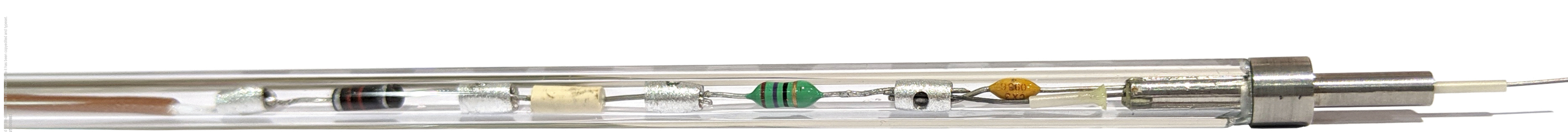




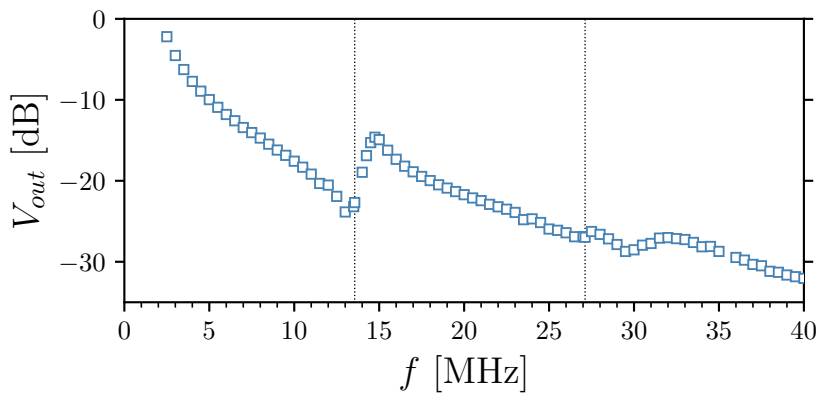
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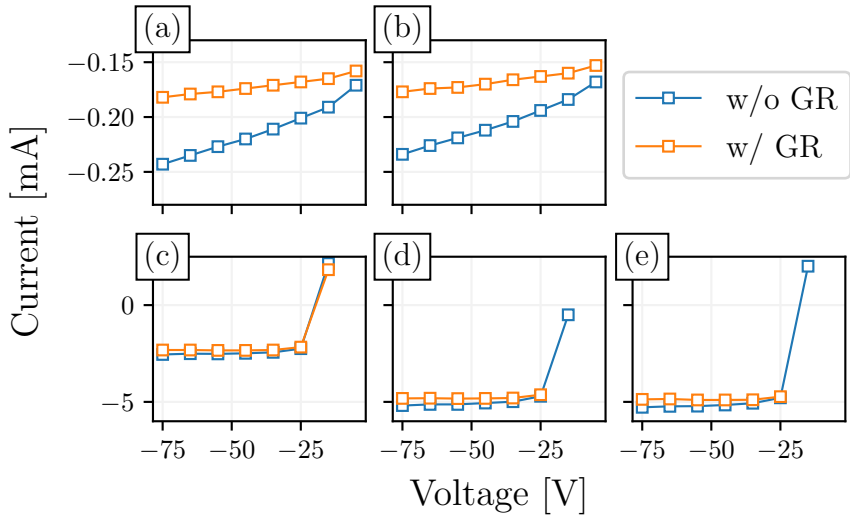




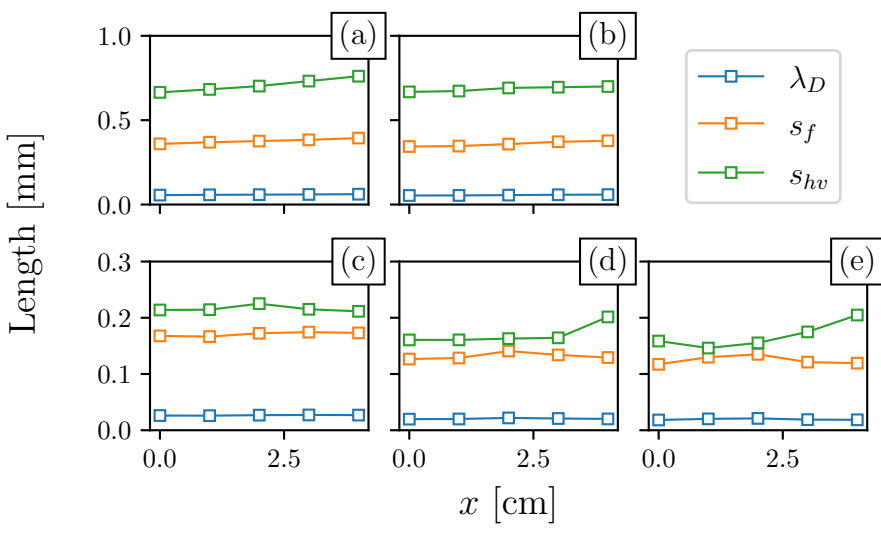
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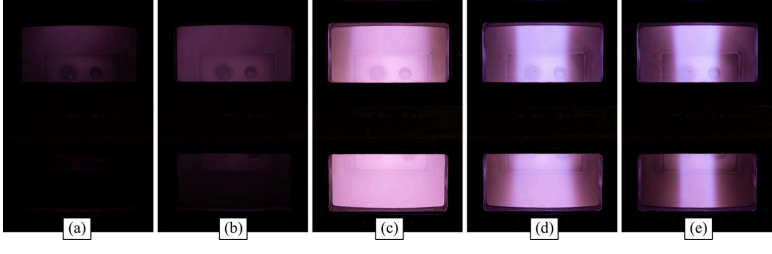
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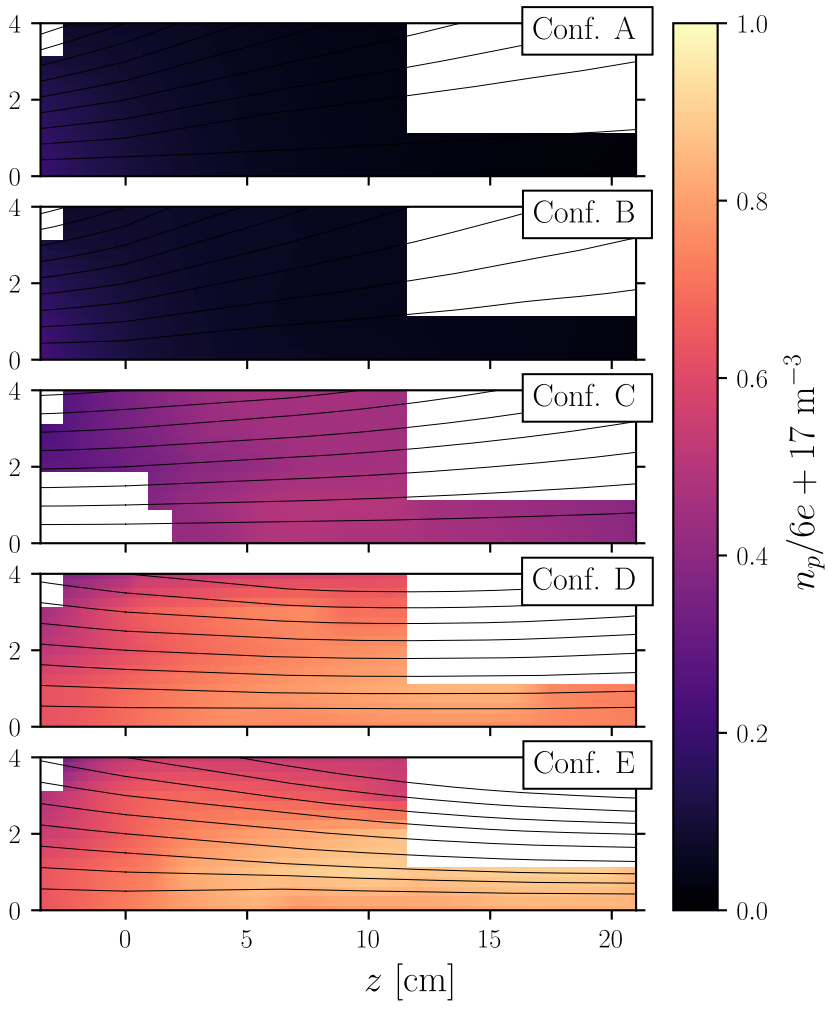
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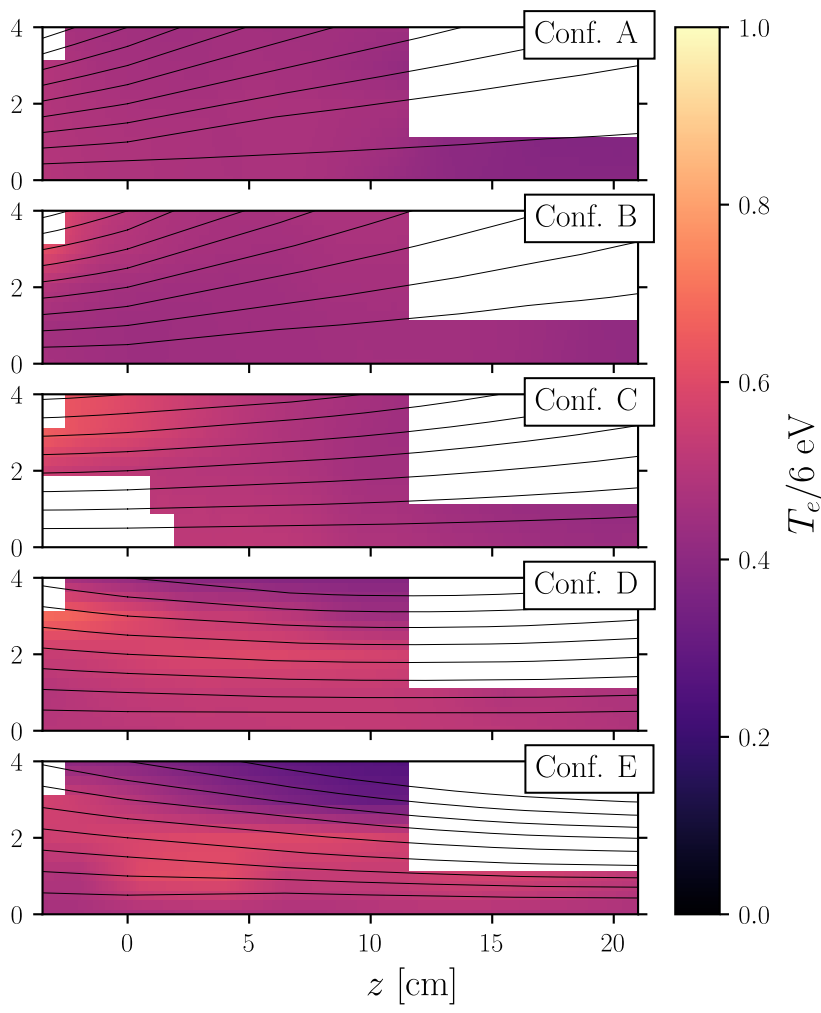
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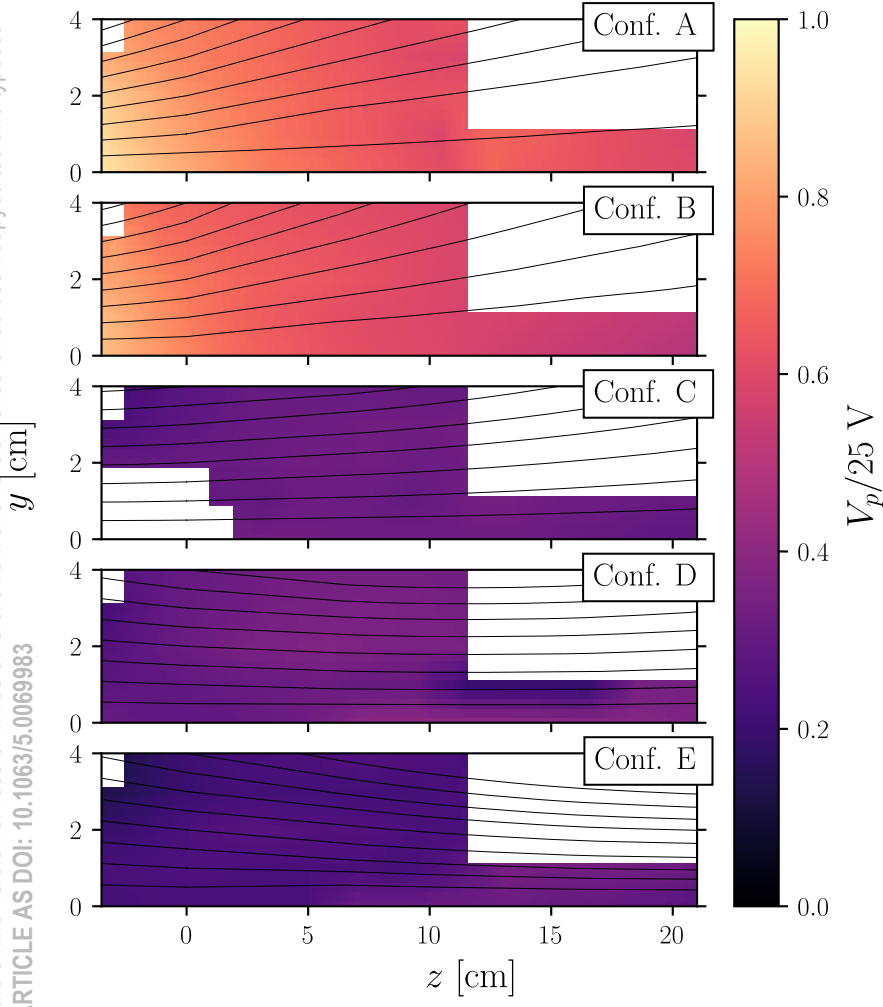
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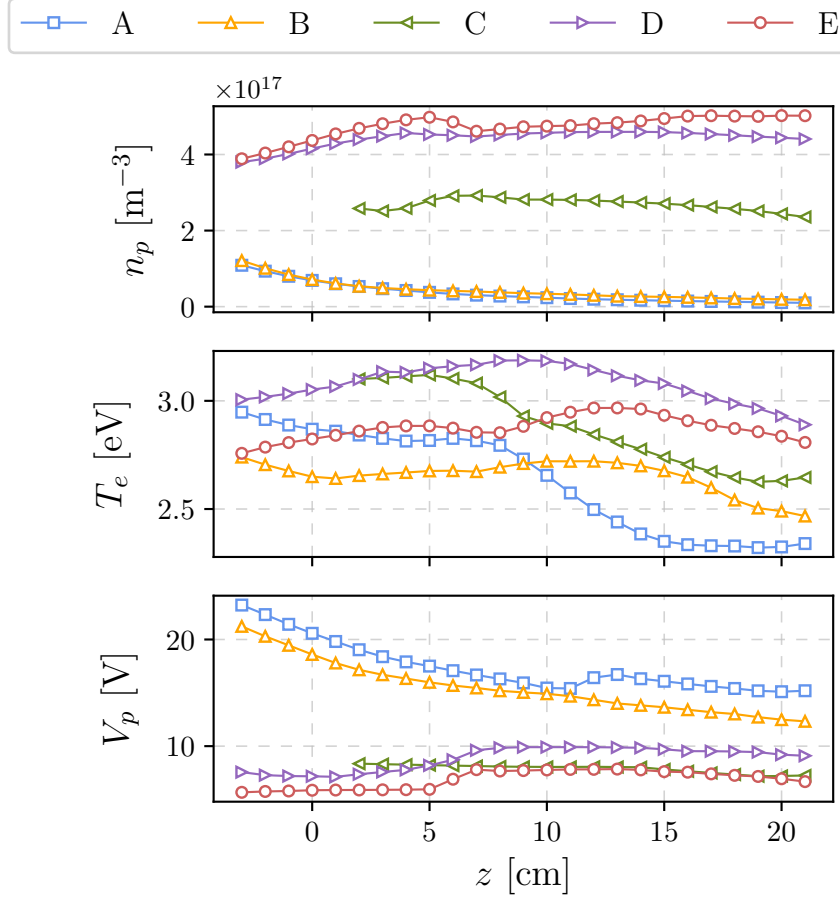


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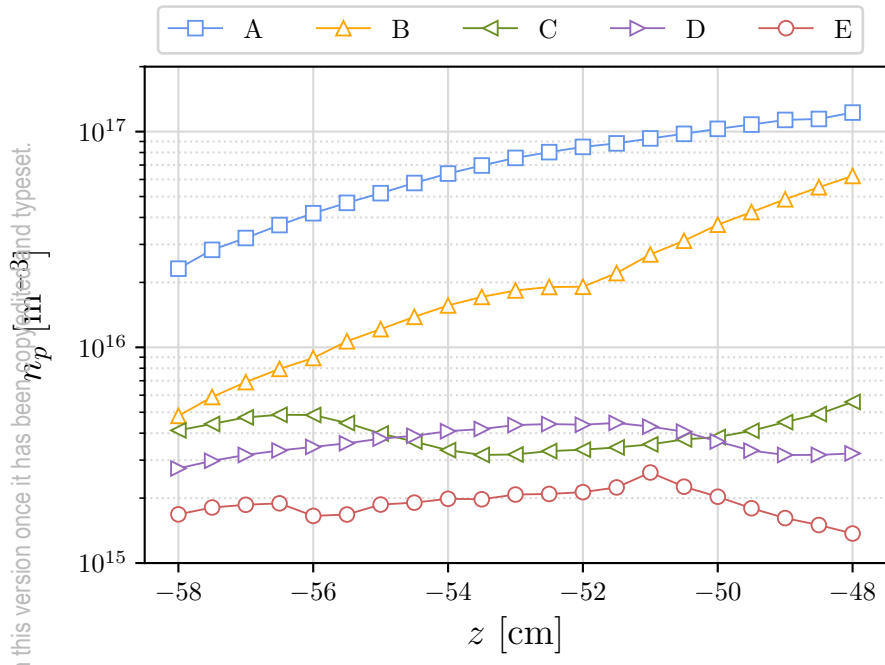
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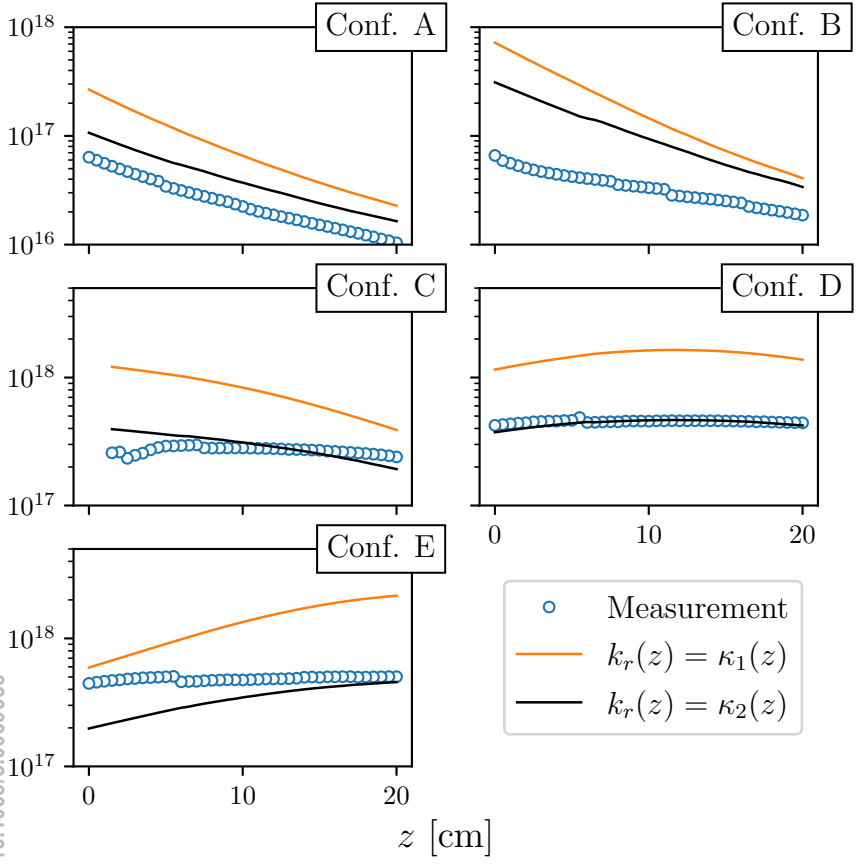
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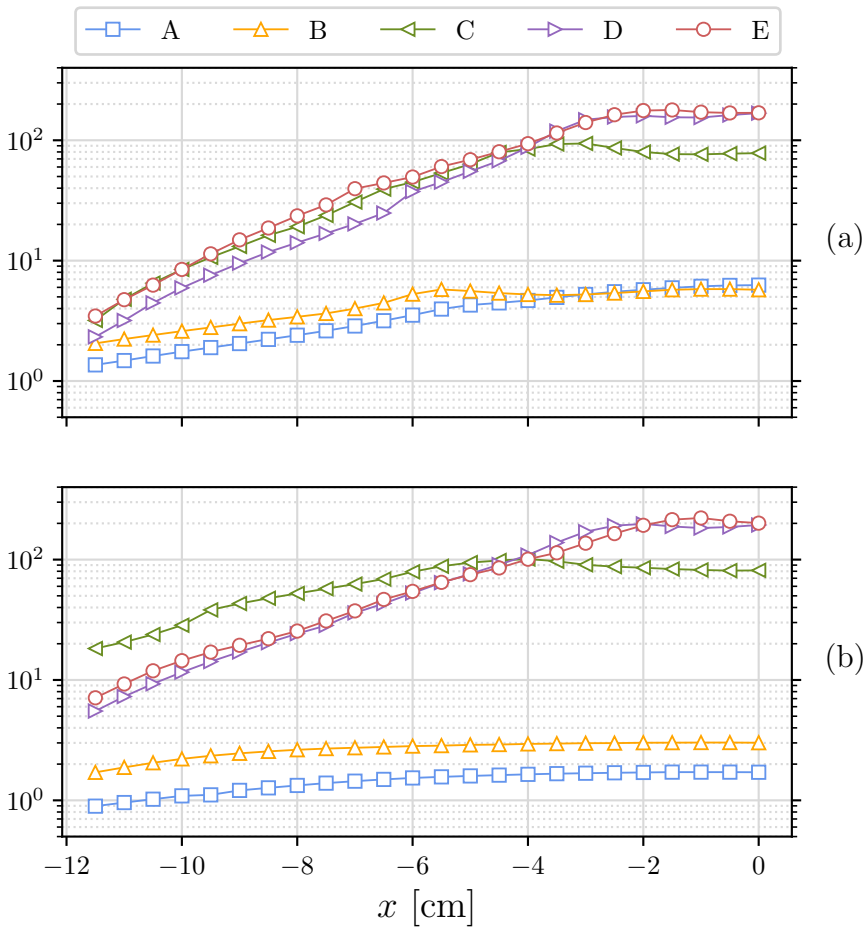
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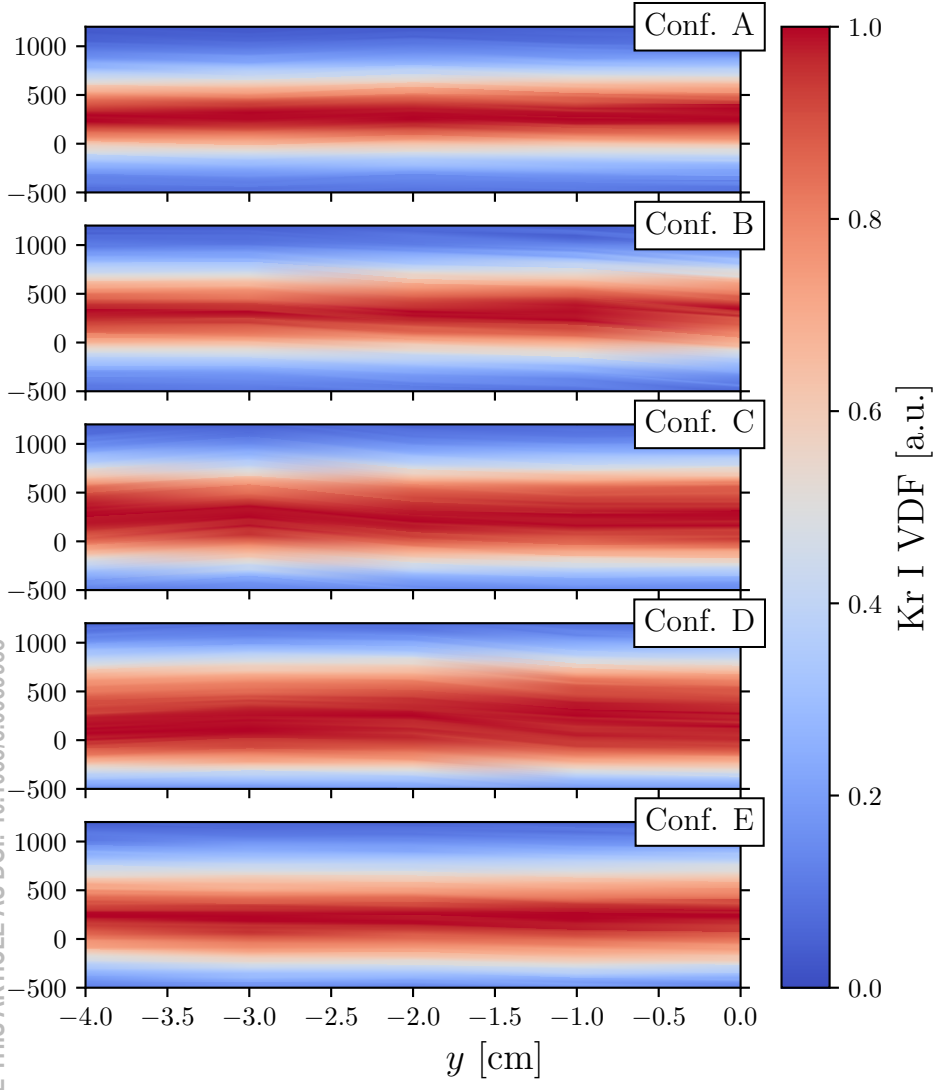


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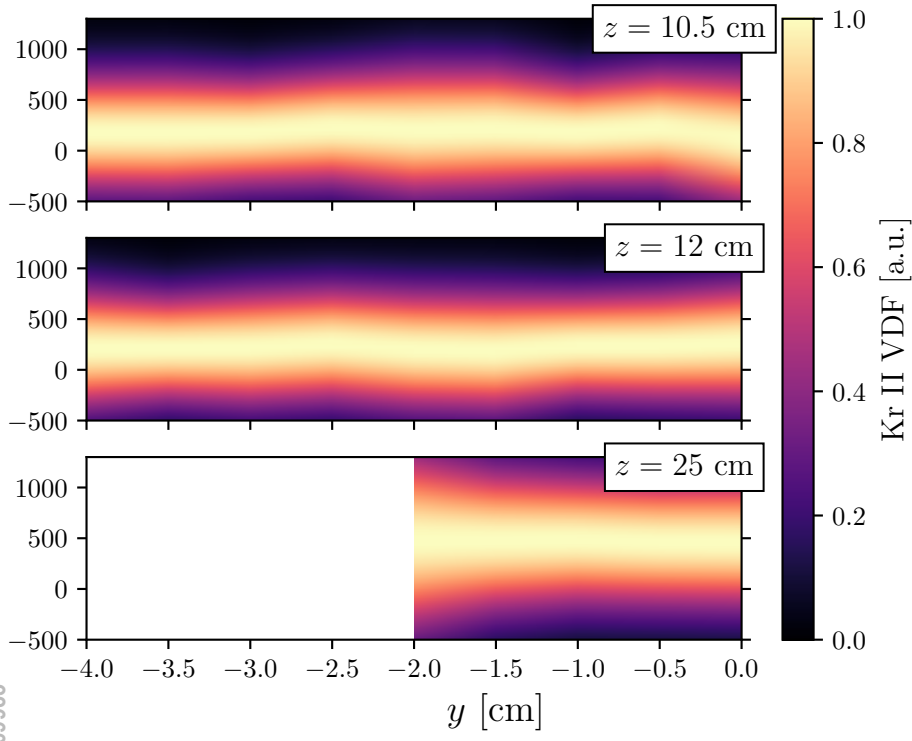


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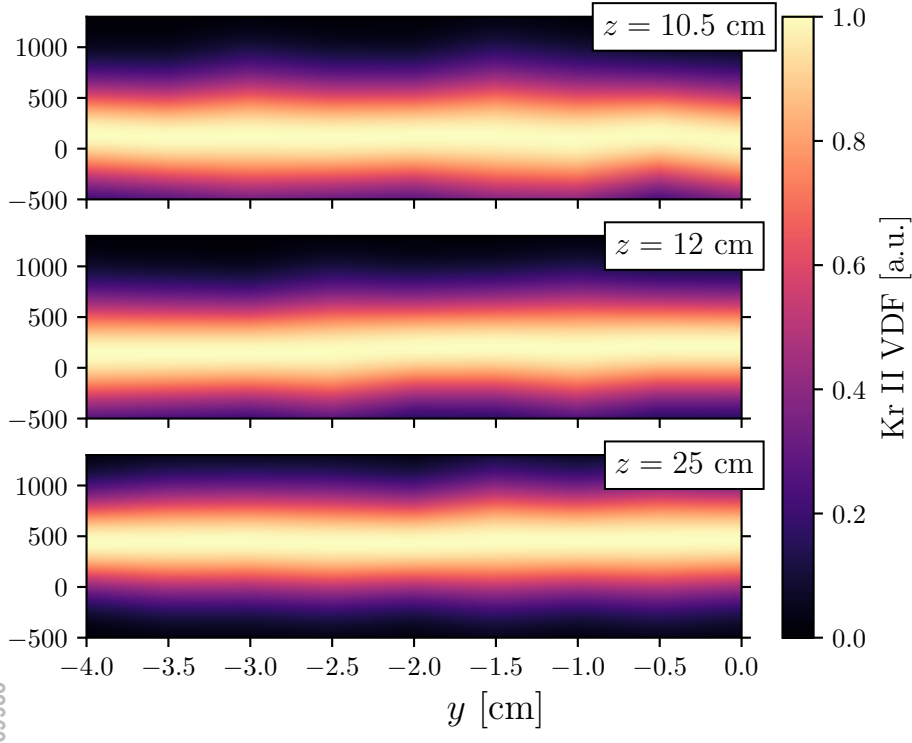
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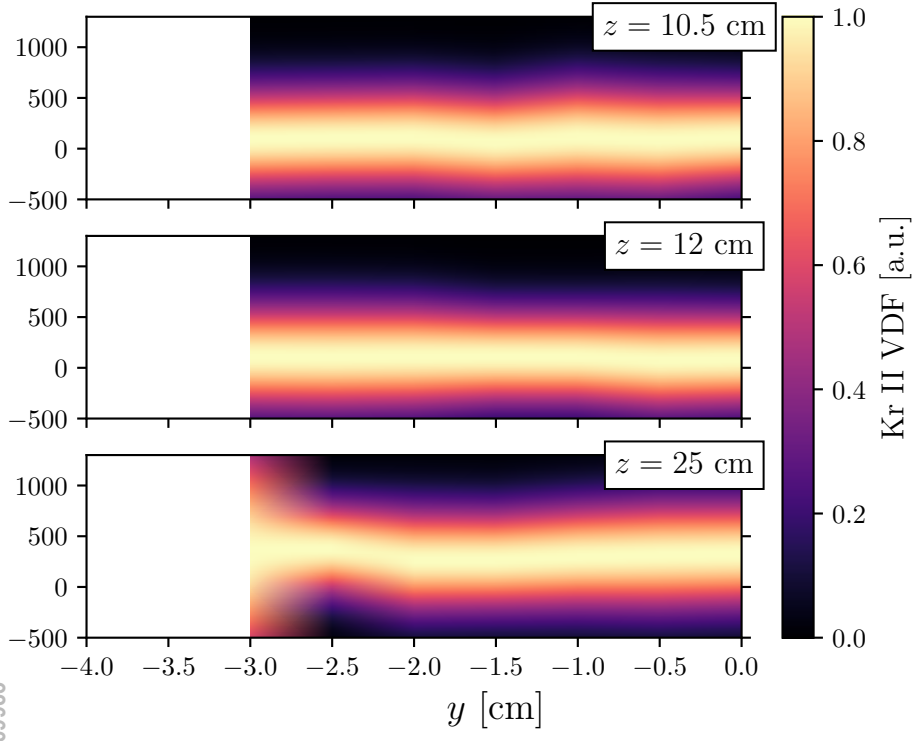


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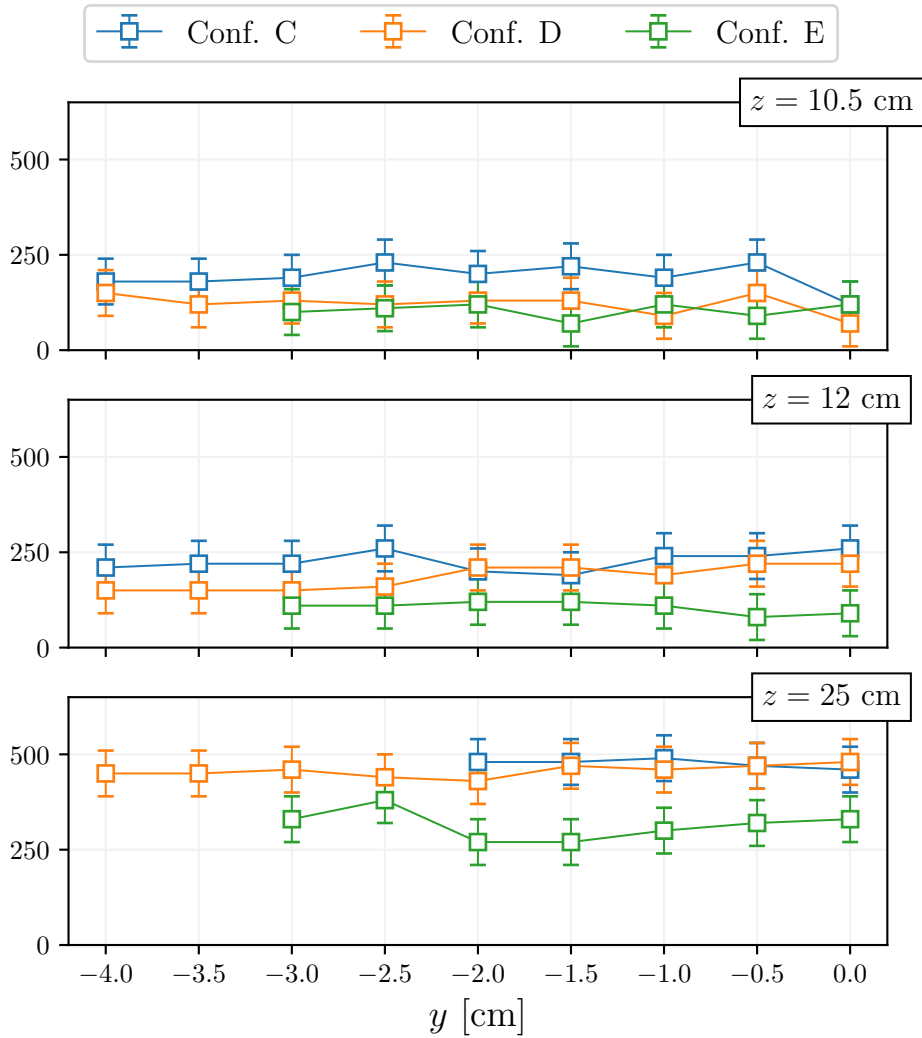




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