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### Interseismic Deformation in the Gulf of Aqaba from GPS Measurements

Nicolás Castro-Perdomo<sup>a</sup>, Renier Viltres<sup>a</sup>, Frédéric Masson<sup>b</sup>, Yann Klinger<sup>c</sup>, Shaozhuo Liu<sup>a</sup>, Maher Dhahry<sup>e</sup>, Patrice Ulrich<sup>b</sup>, Jean-Daniel Bernard<sup>b</sup>, Rémi Matrau<sup>a</sup>, Abdulaziz Alothman<sup>d</sup>, Hani Zahran<sup>e</sup>, Robert Reilinger<sup>f</sup>, P. Martin Mai<sup>a</sup>, Sigurjón Jónsson<sup>a,\*</sup>

<sup>a</sup>Physical Sciences and Engineering Division, King Abdullah University of Science and Technology (KAUST), Thuwal 23955, Saudi Arabia

b IPGS, EOST Université de Strasbourg, CNRS, Strasbourg, France

<sup>c</sup>Université de Paris, Institut de Physique du Globe de Paris, CNRS, F-75005 Paris, France <sup>d</sup>King Abdulaziz City for Science and Technology (KACST), Space Research Institute, Riyadh, Saudi Arabia

<sup>e</sup>National Center for Earthquakes and Volcanoes, Saudi Geological Survey (SGS), Jeddah, Saudi Arabia

 $f$ Department of Earth, Atmospheric, and Planetary Sciences. Massachusetts Institute of Technology. Cambridge, Massachusetts, USA

#### Summary

Although the Dead Sea Transform fault system has been extensively studied in the past, little has been known about the present-day kinematics of its southernmost portion that is offshore in the Gulf of Aqaba. Here we present a new GPS velocity field based on three surveys conducted between 2015 and 2019 at 30 campaign sites, complemented by 11 permanent stations operating near the gulf coast. Interseismic models of strain accumulation indicate a slip rate of  $4.9^{+0.9}_{-0.6}$   $mm/yr$  and a locking depth of  $6.8^{+3.5}_{-3.1}$   $km$  in the gulf's northern region. Our results further indicate an apparent reduction of the locking depth from the inland portion of the Dead Sea Transform towards its southern junction with the Red Sea rift. Our modelling results reveal a small systematic left-lateral residual motion that we postulate is caused by, at least in part, late postseismic transient motion from the 1995  $M_W$ 7.2 Nuweiba earthquake. Estimates of the moment accumulation rate on the main faults in the gulf, other than the one

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<sup>∗</sup>Corresponding author

Email address: sigurjon.jonsson@kaust.edu.sa (Sigurjón Jónsson)

that ruptured in 1995, suggest that they might be near the end of their current interseismic period, implying elevated seismic hazard in the gulf area. Keywords: Continental tectonics: strike-slip and transform, Space geodetic surveys, Neotectonics, Transient deformation, Plate motions

#### 1. Introduction

- The highest seismic hazard in Saudi Arabia and Egypt belongs to the areas bor-
- dering the Gulf of Aqaba (Fig. 1). This hazard is due to earthquakes on the off-
- shore extension of the Dead Sea Transform (DST), a major fault system that ac-
- commodates left-lateral motion between the Arabian plate and the Sinai-Levant
- subplate (Freund et al., 1970; McKenzie, 1972). Several major earthquakes are
- known to have occurred along this southernmost portion of the DST during
- the last millennium, with the 1995  $M_W 7.2$  Nuweiba earthquake in the Gulf of

Aqaba being the most recent one (Klinger et al., 1999; Hofstetter, 2003). The decision by the Kingdom of Saudi Arabia to build a megacity in the NEOM area near the gulf has put this region under the spotlight, requiring further research efforts to improve the seismic hazard knowledge of the gulf area.

 The DST formed as a result of the mid-Cenozoic breakup of the Arabo- African plate and today it extends roughly 1000 km from the Red Sea rift to <sup>15</sup> the **East Anatolian fault** (Garfunkel, 1981). The total estimated left-lateral offset of the DST south of the Dead Sea is about 105 km (e.g., Quennell 1958, 1959; Freund et al. 1970; McKenzie et al. 1970; Garfunkel 1981; Joffe and Garfunkel  $18 \times 1987$ ) and the onset of its left-lateral strike-slip motion postdates 19-22 Ma (e.g., Bar et al. 1974; Steinitz et al. 1978; Bartov et al. 1980; Eyal et al. 1981; Joffe and Garfunkel 1987; Ben-Avraham et al. 2012; Nuriel et al. 2017). These estimates 21 translate to an average slip rate between 4.8 mm/yr and 5.5 mm/yr since the initiation of fault motion along the southern part of the DST comprising the Jordan Valley and Wadi Arabah faults.

 The geomorphology along the strike of the DST is marked by a series of pro-nounced depressions, 5-20 km wide, corresponding to pull-apart basins. These

 morphological depressions form at jogs between discontinuous segments of the DST and are usually delimited by both normal and strike-slip faults (e.g., Gar- funkel 1981; Ben-Avraham and Zoback 1992; Klinger et al. 1999; Ben-Avraham et al. 2012). From north to south, these depressions comprise the Ghab and Hula basins, the Sea of Galilee, the Dead Sea and the Gulf of Aqaba (see inset in Fig. 1). These series of pull-apart basins formed by left-lateral shear along left-stepping en échelon fault segments, which results in rhomb-shaped grabens subjected to left-lateral shear and extension (Quennell, 1959; Garfunkel, 1981). Despite being primarily a transtensional fault system (Garfunkel, 1981), a ma- jor ∼200 km long restraining bend characterises the central part of the DST in Lebanon and Syria (e.g., Heimann and Ron 1987; Gomez et al. 2007). This  $\frac{3}{2}$  segment deviates  $20^{\circ}$  -  $30^{\circ}$  from the main trend of the DST and accounts for  $\sim$ 1.6 mm/yr of convergent motion between the Sinai and Arabian plates at that latitude (e.g., Elias et al. 2007; Gomez et al. 2007).

 Historical records, paleoseismic trenching and geomorphological studies in- dicate that many destructive earthquakes have occurred along the DST over  $\bullet$  the past two millennia (e.g., Ambraseys 2009; Agnon 2014; Meghraoui 2015; Klinger et al. 2015; Lefevre et al. 2018). Two successive earthquakes occurred in 363 AD, affecting more than 20 towns in Palestine and Syria (Ambraseys, 2009). According to Thomas et al. (2007), these earthquakes caused extensive destruction at several localities in southern Wadi Arabah. This observation is in agreement with Klinger et al. (2015), who reported an event horizon in a trench located 30 km north of the city of Aqaba (Jordan) that could be related to these earthquakes.

 A major historical earthquake occurred in 1068 AD in the gulf area, de- stroying the town of Eilat (Ambraseys, 2009). Zilberman et al. (2005) reported that the earthquake was strong enough to rupture the surface along the Eilat fault, affecting an irrigation system. Historical records document another violent earthquake in 1212 AD. This earthquake was strongly felt in Eilat, and caused <sup>55</sup> damages to the monastery of St Catherine in the Sinai Peninsula (Ambraseys, 2009). This event was identified in a trench close to the village of Qatar in  southern Jordan (Klinger et al., 2015), and a brecciated layer associated with  $\frac{1}{58}$  this earthquake was also reported by Kagan et al. (2011) in the Dead Sea basin. The last major historical earthquake reported in the gulf area occurred in 1588. Despite its location and magnitude are a subject of debate, intense shaking was documented as far as Cairo and Madinah, suggesting an epicentre in the northern Red Sea region (Ambraseys, 2009). Finally, the largest instrumental 63 earthquake along the entire DST was the  $M_W 7.2$  Nuweiba Earthquake, which struck the Gulf of Aqaba area on November 22, 1995, causing significant dam- age in nearby coastal communities in Egypt, Saudi Arabia, Jordan and Israel (Klinger et al., 1999; Hofstetter, 2003).

 The gulf itself is about 180 km long and up to 25 km wide (Ben-Avraham et al., 1979; Garfunkel, 1981), and its structure is dominated by three left- stepping en échelon faults bounding a series of pull-apart basins (Ben-Avraham et al. 1979; Ben-Avraham 1985; Ribot et al. 2021, Fig. 1). The northernmost fault segment within the gulf is the Eilat fault. This fault is approximately 59 km long and constitutes the western boundary of the Eilat deep. The central fault segment is the Aragonese fault, which extends approximately 53 km, bounding the Eilat deep to the east and the Aragonese deep to the west. The Arnona fault constitutes the southernmost segment, extending roughly 83 km and forming the western boundary of the Dakar and Tiran deeps. Compelling evidence indicates that the Aragonese fault segment ruptured during the Nuweiba earthquake, while the other segments have not released significant seismic moment in the past several centuries (Shamir et al., 2003; Hofstetter, 2003; Baer et al., 2008; Ribot et al., 2021).

<sup>81</sup> The seismic activity in the gulf is characterised by the occurrence of swarms, <sup>82</sup> which have been observed since the deployment of the first regional seismic networks in the area (El-Isa et al. 1984; Alamri et al. 1991 as cited in Klinger et al. 1999). Significant swarm activity was reported in 1983, 1990 and 1993,  $\epsilon$  reaching  $M_W$  6.1 (El-Isa et al. 1984; Pinar and Türkelli 1997; Klinger et al. <sup>86</sup> 1999, Fig. 2). Most earthquakes in the gulf exhibit predominantly left-lateral <sup>87</sup> motion. However, some of them show significant normal motion, as evidenced by



Figure 1: Mapped faults in the Gulf of Aqaba along with the GPS stations used in this study. Permanent and campaign GPS sites are shown as blue and red triangles, respectively. Fault traces and pull-apart basins are based on Ribot et al. (2021). The inset shows the area of interaction of the Arabian, Nubian, Sinai and Anatolian plates. Shaded topography is based on the SRTM30 PLUS digital elevation model (Becker et al., 2009) and regional-scale fault traces in the inset are compiled from Le Béon et al. (2008). TD, Tiran Deep; TF, Tiran Fault; DP, Dahab Plateau; DD, Dakar Deep; AD, Arnona Deep; ARD, Aragonese Deep; ED, Eilat Deep; GS, Gulf of Suez; GA, Gulf of Aqaba; WAF, Wadi Arabah Fault; DS, Dead Sea; JVF, Jordan Valley Fault; SG, Sea of Galilee; HB, Hula Basin; LRB, Lebanese Restraining Bend; GB, Ghab Basin.

- <sup>88</sup> the pure normal slip reported for the largest event during the 1993 earthquake
- <sup>89</sup> swarm (Klinger et al., 1999; Hofstetter, 2003). More recently, in June 2015,
- $\bullet$  a  $M_W 5.2$  strike-slip earthquake struck the gulf area, causing strong shaking
- <sup>91</sup> in nearby communities and an aftershock sequence that lasted for more than
- <sup>92</sup> two weeks (El-Aal and Badreldin, 2016). Recent seismic data collected by the
- <sup>93</sup> Saudi Geological Survey (SGS) show that earthquakes concentrate along the
- 94 gulf faults,  $\{\text{see } \text{as shown in Fig. 2}\}.$



Figure 2: Earthquake locations ( $M_L \ge 1.5$ ) in the Gulf of Aqaba region from January 2006 to March 2016 with circle sizes scaled according to earthquake magnitude and colours according to date. Focal mechanisms of the 1993  $M_W 6.1$ , 1995  $M_W 7.2$  and 2015  $M_W 5.2$  earthquakes are from the National Earthquake Information Center (NEIC, https://earthquake.usgs.gov), the Global Centroid-Moment-Tensor (GCMT) catalog (Dziewonski et al., 1981; Ekström et al., 2012) and El-Aal and Badreldin (2016), respectively. Seismic stations operated by the Saudi Geological Survey (SGS) are shown as red inverted triangles. Note that the one-sided geometry of the SGS seismic network might bias epicentral locations.

- The present-day crustal deformation along the DST north of the Gulf of
- <sup>96</sup> Aqaba has been extensively analysed in terms of interseismic strain accumu-

#### lation (e.g., McClusky et al. 2003; Wdowinski et al. 2004; Gomez et al. 2007;

 Le Béon et al. 2008, 2010, 2012; Al Tarazi et al. 2011; Sadeh et al. 2012; Mah- moud et al. 2013; Masson et al. 2015; Hamiel et al. 2016, 2018a). However, only <sup>100</sup> four GPS studies have provided slip rate estimates across the fault system in the gulf area. By implementing a back-slip model, Mahmoud et al. (2005) derived a  $\frac{1}{2}$  slip rate of  $4.4 \pm 0.3$  mm/yr, assuming a fixed locking depth of 13 km. A similar approach was followed by Reilinger et al. (2006), who reported a slip rate of 4.5  $104 \pm 0.3$  mm/yr, holding the locking depth fixed to 12 km. ArRajehi et al. (2010) 105 estimated slip rates of  $4.8 \pm 0.2$  mm/yr in the gulf, and, more recently, Gomez  $\frac{1}{106}$  et al. (2020) implemented a back-slip model and reported a slip rate of 4.9  $\pm$  0.1 mm/yr. Unfortunately, these studies were unable to provide locking depth estimates due to the limited geodetic coverage near the gulf.

 In this study, we use previously unpublished geodetic data to derive an up- dated crustal motion velocity field of the gulf. We further implement standard models of interseismic deformation to investigate the fault kinematics along the offshore segments of the DST fault system. Finally, we consider four pos- sible model scenarios of time-dependent viscoelastic deformation produced by the Nuweiba earthquake and discuss whether postseismic transient motions are evidenced in the GPS data acquired near the gulf.

#### 2. GPS Data and Analysis

 A new survey-mode GPS network was installed in 2014 and surveyed three times in February 2015, March 2017 and May 2019 (see Tab. S1 and Fig. S1). This network consists of 27 GPS markers distributed over an area of 150 km by 70 km on the eastern gulf coast, extending from the Strait of Tiran in the south to the Jordan border in the north (Fig. 1). During the surveys, we also occupied three older markers installed by MIT near the municipalities of Al Bad' and Magna (sites BIDA, MAG1 and MAG2). These stations were measured annually between 2010 and 2014 (Gomez et al., 2020), and their data were reprocessed in our study. We also analysed the GPS data collected between 2000 and 2005  at the campaign sites DAHA and NABQ, which are located near the gulf coast on the Sinai Peninsula (McClusky et al., 2003; Mahmoud et al., 2005; Gomez 128 et al., ).

 To better understand the relative motion between the Sinai-Levant subplate and the Arabian plate, we processed data from 20 stations of the GIL network of continuous GPS monitoring in Israel (Wdowinski et al., 2001), covering a 19-year analysis period from 2000 to 2019 (see Fig. S2). Considering the rapid <sub>133</sub> expansion of continuous GNSS GPS networks in Saudi Arabia, we incorporated data from additional 11 permanent stations near the gulf (HAQS, HQLS, TAY1, HAQE, SHRM, BEJD, TB02, TB03, HALY, RASH and TAYS). Our research significantly improves the GPS station coverage near the Gulf of Aqaba com- pared to previous studies, which relied on sparse GPS data in this area (e.g., McClusky et al. 2003; Mahmoud et al. 2005; Reilinger et al. 2006; ArRajehi et al. 2010; Gomez et al. 2020). Nevertheless, near-fault GPS observations are  $\frac{1}{400}$  limited to distances greater than 8 km due to the presence of the gulf itself and 141 the lack of offshore geodetic measurements.

 We analysed the GPS data using the GAMIT/GLOBK software package version 10.70 (Herring et al., 2018) following a three-step approach described in detail by Dong et al. (1998). Daily carrier phase data from campaign and permanent stations were analysed separately to improve the processing efficiency (e.g., Bock et al. 1997). Following this strategy, we obtained two sets of loosely constrained solution vectors and covariance matrices. Both solutions share a set of 16 reference sites with well-determined coordinates and velocities, which we used to tie our final combined solution to the International Terrestrial Reference Frame (ITRF) 2014 (Altamimi et al., 2017). Campaign solutions were then merged with the continuous ones to get a final solution with ambiguities resolved and loose constraints on estimated parameters.

 Combined solutions were used to estimate position time series and site ve- locities in GLOBK. The reference frame realisation was achieved by imposing tight constraints to the coordinates and velocities of 16 sites that comprise the reference network (ZIMM, GRAZ, ONSA, JOZE, WSRT, KIT3, IISC, POLV,  ARTU, POL2, MAS1, RABT, YEBE, DGAR, MBAR, NKLG), minimising in an iterative scheme their position adjustments with respect to their ITRF2014 a priori coordinates by estimating a six-parameter Helmert transformation. Fi- nally, we accounted for time-correlated errors in the position time series by characterising their noise spectrum using the Hector software package version 1.7.2 (Bos et al., 2013). Since campaign stations do not have enough obser- vations to estimate the time-correlated noise in their position time series, we used the mean random walk values obtained for the permanent stations in the 165 study area  $(4.5 \ 10^{-7} \ m^2/yr$  and  $1.5 \ 10^{-6} \ m^2/yr$  for the horizontal and vertical <sub>166</sub> velocity components, respectively). Following this approach, the resulting hori- zontal velocity uncertainties for stations within the new campaign GPS network 168 deployed near the gulf vary between 0.5 and 1.0  $mm/yr$  (see Tab.S2).

#### 3. GPS Velocity Field

 Time series and site velocities realised in ITRF2014 were rotated into stable Sinai reference frame. To perform this rotation, we estimated the Euler pole of the Sinai subplate with respect to ITRF2014 using five reliable stations located on the Sinai subplate at distances greater than 40 km from the DST (CSAR, ALON, YRCM, BSHM and RAMO), as shown in Fig. S2. The SINAI-ITRF2014 175 Euler pole derived here is  $\frac{54.7 \pm 0.7^{\circ} N}{54.7 \pm 0.7^{\circ} N}$ ,  $\frac{347.8 \pm 4.0^{\circ} E}{54.0^{\circ} E}$ ,  $\omega = 0.417 \pm 0.021^{\circ} M a^{-1}$ , which is consistent with Euler vectors estimated in earlier studies (e.g., Wdowin- ski et al. 2004; Le Béon et al. 2008; Sadeh et al. 2012; Hamiel et al. 2016, 2018b,c; Hamiel and Piatibratova 2019). Observed GPS horizontal velocities for the sites on the Arabian plate show NNE motion relative to Sinai (Fig. 3), as reported in previous geodetic investigations (e.g., ArRajehi et al. 2010; Sadeh et al. 2012; Gomez et al. 2020). The velocity field thus reflects the left-lateral motion of the DST fault system. The increasing DST-parallel velocities towards the interior of the Arabian plate in this Sinai-fixed reference frame (Figs. 3-5a), suggest that the coastal areas bordering the gulf faults are currently undergoing interseismic strain accumulation.

 Fig. 4 shows profiles of fault-parallel and fault-normal components of GPS- derived velocities relative to the Sinai-Levant subplate. These projections were 188 performed assuming a single vertical fault with a strike of N16°E extending from the Strait of Tiran in the south to the northernmost tip of the gulf (dashed yel- low line in Fig. 3). Increasing DST-parallel velocities towards the Arabian plate support active interseismic strain accumulation along the coastal areas adjacent to the gulf (Fig. 4a). We further note that the mean fault-normal velocity con-193 sidering all the stations on the Arabian side of the gulf is ∼0.8  $mm/yr$  (Fig. 4b). This observation is consistent with a partly divergent motion between the Sinai and Arabian plates at this latitude, as suggested in previous investigations (e.g., Mahmoud et al. 2005; Reilinger et al. 2006; Gomez et al. 2020). However, the scatter observed in both velocity profiles suggests that the assumption of a sin- gle fault along the full extension of the gulf may be inadequate. This observation led us to consider different fault traces within the gulf based on the structural maps by Ben-Avraham (1985) and Ribot et al. (2021), see below.

#### 4. Elastic Dislocation Model

 We conducted an initial kinematic assessment of the GPS velocity field across the gulf by implementing a screw dislocation model (e.g., Weertman and Weert- man 1964; Savage and Burford 1973). Following this approach, theoretical fault-parallel velocities v can be expressed as follows:

$$
v = a + \frac{b}{\pi} \tan^{-1} \left( \frac{x}{D_L} \right)
$$
 (1)

 where a defines the vertical origin of the arctangent curve, and x is the per- pendicular distance measured from the fault trace. The fault is assumed to be locked during the interseismic period at depths extending from the surface down to a depth  $D<sub>L</sub>$  (often referred to as locking depth), below which free slip occurs at a rate equivalent to the secular relative plate motion b. GPS measure- ments at distances within one-half the locking depth are required to accurately constrain fault locking depths, whereas far-fault observations are important to  constrain secular slip rates (Smith-Konter et al., 2011). This simple interseismic model has been extensively used to investigate kinematic parameters of many strike-slip and transform faults globally (e.g., Lisowski et al. 1991; Wright et al. 2001; Reilinger et al. 2006; Sadeh et al. 2012).

<sup>217</sup> Here we analyse two velocity profiles across the Eilat fault in the north and <sup>218</sup> the Arnona and Tiran faults in the south, which include the largest number of



Figure 3: Horizontal GPS velocities relative to Sinai with 95% confidence ellipses. Permanent and campaign site velocity vectors are coloured in blue and red, respectively. The blue and red boxes indicate the location of the velocity profiles shown in Fig. 5a-b. The dashed yellow line corresponds to the assumed fault location used in Fig. 4a-b. The dashed magenta arc delineates the small circle around the Arabia-Sinai Euler pole derived in this study.



Figure 4: Profiles of a) fault-parallel and b) fault-normal velocities across Gulf of Aqaba assuming a single vertical fault striking N16◦E along the gulf (dashed yellow line in Fig. 3). Site velocities are expressed in a Sinai-fixed reference frame, i.e., positive velocity values on the Arabian plate  $(x > 0)$  represent left-lateral motion in a) and opening in b) across the gulf. The solid orange and blue lines correspond to the best local least-squares fit to fault-parallel and fault-normal velocities, respectively. The least-squares fit was performed using a third-order Savitzky-Golay filter considering 39 data points per window. The pale green and yellow lines represent the fault-parallel and fault-normal velocities predicted by the Arabia-Sinai Euler Pole. Permanent and campaign site velocities are coloured in blue and red, respectively.



 reliably constrain slip rates and locking depths. Moreover, there are no stations constraining GPS rates on the Sinai Peninsula west of the Aragonese fault. For these reasons, the central segment was not considered for slip-rate and locking depth inversions.

 We evaluated if observed fault-parallel velocities resemble the theoretical pattern of strain accumulation given by Eq. 1, and excluded from the analy- sis those sites showing anomalous rates with no clear tectonic explanation (grey 237 dots in Fig. 5a-b). We then constrained model parameters (i.e.,  $a, b$  and  $D<sub>L</sub>$ ) and their uncertainties using a grid-search algorithm coupled with a Monte Carlo procedure that accounts for uncertainties in the fault position and stations' velocities. The best fit corresponds to the set of model parameters that results <sup>241</sup> in the lowest root mean squared (RMS) error relative to the actual GPS obser- vations (Fig. 5a-b). To estimate uncertainties in slip rates and locking depths,  $_{243}$  we conducted  $10^4$  Monte Carlo simulations, perturbing the location of the fault <sup>244</sup> randomly within a range of  $\pm 0.5$  km and adding Gaussian noise to the GPS velocities within their 1-sigma uncertainties. In each Monte Carlo simulation, the grid-search explores the misfit (RMS) of the model for a range of values in the parameter domain, and selects the combination of model parameters that results in the lowest misfit. The strike (azimuth) of the fault segments was held fixed during the slip rate and locking depth inversions. However, we explored the effect of small perturbations ( $\pm 5$  degrees) in fault strike on the final inversion results. We found that small variations in fault strike do not have a statistically significant impact on the slip rate and locking depth estimates, as shown in 253 Fig. S3. 254 After performing the Monte Carlo inversion, we derived a  $2\times 2$  covariance <sub>255</sub> matrix from the resulting distribution of slip rates and locking depths. From this

256 covariance matrix, we estimated the width  $(\omega)$  and height  $(h)$  of the confidence <sup>257</sup> level ellipse, which are given by  $\omega = 2 \times nstd \times \sqrt{\lambda_1}$  and  $h = 2 \times nstd \times \sqrt{\lambda_2}$ , where nstd represents the desired confidence level (in standard deviations) and  $\lambda_{12}$  are the eigenvalues of the covariance matrix. Finally We followed this ap**proach to derive**, we estimated the eigenvalues and eigenvectors for the 1-sigma <sup>261</sup> (68%) confidence level ellipses, as shown in Fig. 5c-d.



<sub>277</sub> Fault-parallel rates at stations GA12, GA13 and GA15 disagreed with the <sup>278</sup> expected 1D screw dislocation model within their 1-sigma uncertainties and were <sup>279</sup> dismissed from the analysis. We further implemented an alternative approach, 280 solving for the best-fitting model for a fixed slip rate of 4.5  $mm/yr$ , which cor-<sup>281</sup> responds to the fault-parallel rate predicted by the Arabia-Sinai Euler pole at  $282$  the fault trace (see Fig. 4a). Following this approach, for the northern profile, 283 we obtained a best-fitting locking depth of  $6.2 \; km$  (yellow curve in Fig. 5a).

<sup>284</sup> We also obtained a very shallow locking depth estimate  $(< 2 km)$  for a fixed 285 slip rate of 4.5 mm/yr (yellow curve in Fig. 5b). To further analyse the effect <sup>286</sup> of near-fault station rates on the final locking depth estimates, we considered 287 an additional scenarios assuming a fixed slip rate of 4.5  $mm/yr$  and omitting 288 stations GA01 and GA16 in the northern profile and GA18 in the southern  $289$  profile (blue curves in Fig.  $5a-b$ ) , which moves at full plate rate despite be- $\frac{1}{290}$  ing located ~ 8 km from the fault trace. Our results show that the omission <sub>291</sub> of sites GA01 and GA16 in the northern profile has a minor effect on the slip <sub>292</sub> rate estimate but results in a deeper locking depth of 10.5 km. Similarly, ex**cluding of** station GA18 in the southern profile results in a deeper locking depth estimate of  $3.2 \ km$  compared with the 0.8 km obtained when including GA18  $_{295}$  in the inversion (green line in Fig. 5b). The 68% confidence level ellipses shown in Fig. 5c-d are elongated, showing a clear trade-off between slip rates and fault locking depths. As demonstrated in several studies, higher slip rates require  $\frac{1}{298}$  larger deeper locking depths (e.g., Wright et al. 2001; Meade and Hager 2005; Smith-Konter et al. 2011). This correlation arises from the tight constraint on the near-field velocity gradient imposed by the dislocation model (see Wright et al. 2001 for details).

 Finally, we compared our results with the slip rates and locking depths de-303 rived by Li et al. (2021) based on the implementation of Sentinel 1 burst-over-304 lap interferometry (BOI) in the lands bordering the gulf (light orange curves in <sup>305</sup> Fig. 5<sub>a</sub>-b). Our Taken together, both results indicate shallower locking depths <sub>306</sub> from north to south, towards the Red Sea rift. Our results further suggest that a very shallow locking depth or creeping is required in the southern part of the gulf to account for the low strain accumulation observed in this area. However, the current near-fault GPS data are insufficient to unambiguously discriminate <sub>310</sub> between partial shallow locking and full creep scenarios along the southern fault segments. These results motivated us to implement a more complex model of strain accumulation, which not only considers fault-parallel motions but also allows for tensile motions and rigid block rotations.

#### 5. Back-Slip Model

 Interseismic deformation studies conducted further north along the DST in Is- rael, Jordan, Syria and Lebanon have shown that GPS-derived velocities can be <sup>317</sup> well explained by rigid block movement bounded by a narrow deformation zone that accommodates the relative motion between them (e.g., Mahmoud et al. 2005; Reilinger et al. 2006; Gomez et al. 2007, 2020; Al Tarazi et al. 2011). This view is also supported by the distribution of instrumental and historical



Figure 5: Observed fault-parallel velocities with 1-sigma uncertainties across the Eilat fault (panel a) and Tiran-Arnona faults (panel b) in comparison with predictions from elastic dislocation models in a Sinai-fixed reference frame. Panels c and d depict the results of the slip rate and locking depth inversions and 68% confidence level ellipses. The red curve in both profiles represents the global minimum considering  $a, b$  and  $D<sub>L</sub>$  as free parameters. **Results** from Li et al. (2021), based on burst-overlap interferometric (BOI) observations, are shown in light orange. Outliers are shown as grey dots and were dismissed from analysis, as discussed in the text.

 seismicity, which concentrates along the main fault strands of the DST fault system (Hofstetter et al., 2014). We thus next investigated whether the velocity field in the Gulf of Aqaba area can also be explained using a similar back-slip <sup>324</sup> model.

<sup>325</sup> We adopted the approach described by McCaffrey (2005, 2009) and defined two blocks representing the Sinai and Arabian plates. The boundary between them was modelled as a set of linear fault segments representing the main fault strands of the gulf mapped by Ben-Avraham (1985) and Ribot et al. (2021), with short relay faults connecting the segments (Fig. 7a). Model-predicted ve-locities result from superimposing linear rates due to block rotations and those  associated with the back-slip motion applied on block boundaries, which are estimated following Okada (1985).

 The number of near-fault GPS observations is insufficient to reliably invert <sup>334</sup> for the locking fraction distribution along the fault segments within the gulf. <sup>335</sup> even for sparse discretisations of the fault planes. Hence, to further investigate <sub>336</sub> the fault kinematics in the gulf's southern region, we considered three forward back-slip model scenarios defining the locking fraction of the fault segments in <sup>338</sup> this area a priori. In the first scenario, we imposed full interseismic locking to all the faults in the gulf (Fig. 6a). In the second scenario, we considered creep on the Arnona and Tiran faults (Fig. 6b). Finally, in the third scenario, we  $\frac{1}{241}$  imposed creep on the Tiran fault only (Fig. 7). Locked faults were modelled as <sup>342</sup> near vertical extending down to  $\frac{87}{km}$ , based on our best-fit estimate across the Eilat fault. Creeping faults were modelled as free-slipping boundaries that do <sub>344</sub> not produce any elastic strain. To evaluate the effect of implementing different fault geometries in our back-slip models, we ran an additional scenario assuming <sup>346</sup> a dip angle of 65<sup>°</sup> for the Aragonese fault, as proposed by Baer et al. (2008). By <sup>347</sup> comparing the resulting back-slip model residuals with those obtained assuming  $\alpha$  a vertical fault (Fig. 7), we show that the variance difference is not large enough to be statistically significant, as depicted in Fig. S5.

 Considering that most stations in the gulf area have short time series (< 5 years), we did not optimise for rotation parameters during the back-slip mod- elling. Instead, we defined the Arabia-Sinai Euler pole a priori using the Sinai- ITRF2014 Euler vector derived in this study and the Arabia-ITRF2014 rotation pole reported by Altamimi et al. (2017). In this way, the back-slip applied on each locked fault in the gulf was determined by the Arabia-Sinai rotation pole 356 (35.00°N, 8.78°E,  $\omega$ =0.105°Ma<sup>-1</sup>), assuming that no aseismic slip occurs dur- ing the interseismic period on those faults. Finally, we compared observed and back-slip predicted velocities in the gulf area and analysed the residual rates.

 Our modelling results indicate that the coastal areas bordering the Arnona fault are undergoing strain accumulation. This is supported by the good fit to <sup>361</sup> the data on the Arabian side of the gulf obtained by imposing full interseismic <sup>362</sup> locking to the Arnona fault in the first model scenario (Fig. 6a) and the small but coherent southward residuals obtained in the second scenario, where creeping <sub>364</sub> is assumed along the Arnona and Tiran faults (Fig. 6b). We analysed these residuals quantitatively, showing that when the Arnona fault is assumed to be fully locked, near-fault velocity residuals are close to zero (panels a and b in Fig. S6). In contrast, full-creep on the Arnona fault leads to a systematic bias 368 of ∼0.4 mm/yr and ∼0.2 mm/yr in the North and East velocity components, **respectively (panels c and d in Fig. S6)**. We also noted that the fit to the data across the Tiran fault degrades if this fault is assumed to be locked during the interseismic period. This observation suggests that creeping might be required to explain the low interseismic strain accumulation observed across this fault. We found that the best fit to the data is obtained by implementing scenario 3, which considers full locking along all the fault segments except Tiran fault, 375 which is modelled as a creeping fault. Scenario 3 explains the interseismic strain accumulation observed across the Arnona fault and the full-plate rate exhibited by near-fault GPS stations across Tiran fault (see Fig. 7a).

378 Our results further suggest a fault-parallel slip-rate of  $\sim$ 4.5 mm/yr and a  $\frac{379}{100}$  tensile component of ~0.3 mm/yr along the main fault strands in the gulf, as 380 determined from the the relative plate motion (see Fig. 7a). The back-slip model 381 succeeds in fitting **13 out of 17 GPS rates** roughly  $80\%$  (76%) of observed veloci- ties within their 95% confidence ellipses in the southern region of the gulf (east of <sup>383</sup> the Arnona and Tiran fault traces). Nevertheless, our modelling results reveal an apparent reduction in the quality of the fit for most sites located in northern Gulf 385 of Aqaba (east of the Aragonese fault  $trace$ ), where less than  $60\%$  of residuals lie  $\frac{386}{100}$  within velocity uncertainties only 12 out of 23 observations (52%) of observed velocities were fitted within their 95% confidence ellipses. Interestingly, residual velocities are not randomly distributed but are instead systematically directed towards the East-Northeast on the Arabian side of the gulf. This observation led us to investigate in more detail the nature of these residuals and their spatial distribution. For this purpose, we estimated descriptive statistics of the misfits, discriminating between stations in the northern and southern regions of the gulf.



Figure 6: Panel a shows residual velocities after implementing the first back-slip model scenario assuming full interseismic locking on all the fault traces. Panel b shows the residuals obtained after implementing the sec Figure 6: Panel a shows residual velocities after implementing the first back-slip model scenario assuming full interseismic locking on all the fault traces. Panel b shows the residuals obtained after implementing the second scenario assuming full creep along the Arnona fault and the Tiran fault (TF). Orange and grey lines represent locked and creeping fault traces, respectively. Residual rates of seven near-fault stations within the blue dashed boxes are analysed in Fig. S6.



Figure 7: Residual velocity vectors after implementing the third back-slip model scenario (panel a), which assumes full creep on only the Tiran fault (TF). Histograms of fault parallel and perpendicular residuals for the Figure 7: Residual velocity vectors after implementing the third back-slip model scenario (panel a), which assumes full creep on only the Tiran fault (TF). Histograms of fault parallel and perpendicular residuals for the northern part of the gulf (north of the blue dashed line) are shown in panels b-c and for the southern part in panels d-e, with both the bias and RMS values reported.

 The misfit distributions depicted in Fig. 7b-e quantitatively demonstrate that the magnitude of residual velocities differs between the northern and south- ern regions on the Arabian side of the gulf. Notably, the average magnitude of the 396 east component of residual velocities in the northern area is about 0.7  $mm/yr$ . This value contrasts with that observed east of the Arnona fault in the southern region of the gulf, where the east component of residual velocities is roughly zero. Similarly, but to a lesser extent, we observe a small discrepancy in the north component of residual velocities. The mean magnitude of the north component 401 of residual velocities east of the Aragonese fault is  $0.15$   $0.11$   $mm/yr$ , while the average value of the same velocity component observed east of the Arnona fault 403 in the southern region of the gulf is  $-0.11 - 0.14$  mm/yr. Our results thus suggest the existence of a left-lateral residual motion across the gulf that cannot be explained by block rotations and interseismic strain accumulation alone. These results drove us to study the potential influence of postseismic transient motions  $\frac{407}{407}$  caused by the 1995,  $M_w$ 7.2 Nuweiba earthquake in the lands bordering the gulf. Fig. 7a also shows consistent misfits for stations DAHA and NABQ in the Sinai Peninsula. Both stations show significant residuals directed towards the west-southwest.

#### 6. Postseismic Modelling

 Transient surface deformation has been systematically observed following large earthquakes spanning periods from months to decades (Scholz, 2002). Three time-dependent mechanisms are most often tested to explain such deformation transients: Afterslip on and/or around the ruptured fault plane (e.g., Savage et al. 1994; Bürgmann et al. 1997), poroelastic rebound (e.g., Peltzer et al. 1996; Jónsson et al. 2003) and viscoelastic relaxation of the lower crust and upper mantle (e.g., Pollitz 1997; Freed and Bürgmann 2004). The last one is the only process capable of producing postseismic deformation spanning both large spatial and long temporal scales (Vergnolle et al. 2003 and references therein). Despite considerable efforts aimed at elucidating the underlying nature of the  mechanisms controlling postseismic deformation, discriminating among them using geodetic measurements is challenging and is presently an active area of research (e.g., Jónsson 2008; Liu et al. 2020).

 Considering the limited GPS measurements in the years following the 1995 Nuweiba earthquake, the data are insufficient to invert for rheological param- eters. Hence, we set up a series of forward models to analyse the postseismic surface deformation resulting from different lithospheric structures for the Gulf of Aqaba. For this purpose, we studied the viscoelastic relaxation following the methodology proposed by Wang et al. (2006) for a layered viscoelastic Earth model accounting for gravity effects. We used a simplified 1D velocity model of the gulf area from Tang et al. (2016) to define a layered Earth structure consisting of a Burgers viscoelastic half-space underlying a 30  $km$  thick elastic layer, representing the Earth's upper mantle and crust, respectively (see Fig. 8b-d). We 435 also considered a three-layer Earth structure consisting of a 30  $km$  elastic upper crust underlain by a biviscous lower crust and upper mantle (see Fig. 8e). The 437 source of the  $M_W 7.2$  Nuweiba earthquake was modelled using the distributed slip model derived by Baer et al. (2008) from ERS-1 and ERS-2 Interferometric Synthetic Aperture Radar (InSAR) data (see Fig. 9).

 We explored four model scenarios by varying the transient and steady-state viscosities of the Burgers solids. In the first three scenarios, the viscosity of the underlying half-space was set based on the best-fit viscosity reported by **443** Piersanti et al. (2001) for the Sinai-Suez area ( $\sim 10^{18}$  Pa · s). In the fourth scenario, we considered a thin crème brûlée rheological structure consisting on  $\frac{445}{445}$  a 30 km elastic upper crust underlain by a biviscous lower crust and upper mantle. Following the considerations above, in scenario 1, we assigned values of 447 1.10<sup>18</sup> and 1.10<sup>19</sup>  $Pa \cdot s$  to the transient  $(\eta_K)$  and steady-state  $(\eta_M)$  viscosities, **448** respectively. In scenario 2, we fixed  $\eta_K$  to  $2 \cdot 10^{18} Pa \cdot s$  and  $\eta_M$  to  $2 \cdot 10^{19} Pa \cdot s$ . **In scenario 3, we considered a higher transient viscosity of**  $1 \cdot 10^{19} Pa \cdot s$  **and a** 450 steady-state viscosity of  $1 \cdot 10^{20}$   $Pa \cdot s$ . Finally, in scenario 4, we defined steady-451 state viscosities of  $2 \cdot 10^{18} Pa \cdot s$  and  $4 \cdot 10^{19} Pa \cdot s$  for the lower crust and upper 452 mantle, respectively (transient/steady-state viscosity  $= 0.1$ ). We held fixed the **453** ratio between effective and unrelaxed shear modulus  $(\alpha)$  to a value of 0.5 in the <sup>454</sup> first three scenarios, and 0.7 in the last model (see below).



Figure 8: Panel a shows the simplified 1D layered Earth model of the Gulf of Aqaba (adapted from Tang et al. 2016). Panels b, c, d and e are schematic representation of the lithosphere for model scenarios 1, 2, 3 and 4, respectively. Viscoelastic parameters of the Kelvin and Maxwell elements are also given for each scenario:  $\eta_K$  is the transient viscosity (dashpot of the Kelvin solid),  $\eta_M$  represents the steady-state viscosity (dashpot of the Maxwell fluid).  $\alpha$  corresponds to the ratio between effective and unrelaxed shear modulus  $\frac{\mu_K}{\mu_K + \mu_M}$ . The unrelaxed shear modulus  $(\mu_M)$  can be derived from the values of S wave velocities  $(V_s)$  and densities  $(\rho)$ provided in panel a.

 For each model scenario, we computed time series of postseismic displace- ments for the period spanning from the origin time of the 1995 Nuweiba earth- quake to the year 2020. Postseismic velocities were then derived from the average displacement rate over the observation period of each GPS station. As can be seen in Fig. 9, model scenarios implementing lower transient and steady-state viscosities result in slightly higher postseismic rates compared with those includ-ing higher viscosities. The pattern of modelled postseismic velocities in all four



Figure 9: Modelled postseismic velocities computed at the location of GPS stations in the study area. Yellow, green, blue and red vectors represent modelled postseismic velocities for scenarios 1, 2, 3 and 4, respectively. Postsseismic rates were estimated for the observation period at each GPS station (see Fig. S1 for details). The colour-coded grid represents the finite-source model of the Nuweiba earthquake derived by Baer et al. (2008). Note the change in velocity scale from previous figures.

 cases is similar and shows left-lateral motion, which agrees with the coseismic slip prescribed in the finite-fault model. However, unlike the modelled interseis- mic velocities, the predicted postseismic deformation fields exhibit maximum  $\frac{465}{465}$  fault-parallel velocities about 30 km away from the fault trace, with lower rates next to the fault and in the far-field.

<sup>467</sup> To determine whether the back-slip model residuals shown in Fig. 7 can

 be explained by postseismic transient motions from the Nuweiba earthquake, we estimated the misfits resulting from subtracting modelled postseismic rates from the block model residuals. Fig. 10a depicts the misfit vectors obtained for the four postseismic model scenarios considered in our study. As done in the back-slip model, we discriminated between GPS stations located in the northern and southern regions adjacent to the gulf on the Arabian plate. The misfit distributions and RMS values for each postseismic model are shown in Fig. 10b-e.

 Overall, the lowest RMS misfits east of the Aragonese fault were obtained by  $\frac{477}{477}$  implementing model scenario 2 (green vectors in Fig. 10a). Modelled postseismic 478 velocities in the north (east of Aragonese fault trace) lead to a reduction in 479 the RMS misfit by  $\sim$ 11% and  $\sim$ 4  $\sim$ 1% of the east and north rate velocity components, respectively. In contrast, the quality of the fit in the southern region <sup>481</sup> of the gulf (east of the Arnona and Tiran fault **traces**) degraded by  $4\%$  and  $41\%$  in east and north velocity components, respectively. The reduction in the quality of the fit in this area is due to northwestward modelled postseismic velocities, which are not observed in the block-model residuals. As shown in Fig. 7, GPS- derived velocities are well-fit by the back-slip model in the gulf's southern region located east of the Arnona and Tiran faults. Hence, the consideration of any <sup>487</sup> additional postseismic signal in that area the southern region of the gulf results in a degradation of the fit.

 Our results suggest that modelled postseismic velocities induced by the 1995, Mw 7.2 Nuweiba earthquake explain part of the left-lateral residual motion ob- served in the lands bordering the gulf. However, the forward models fail to satisfactorily reproduce the magnitudes of the residual velocity field by under- estimating somewhat the back-slip model residuals in the northeast of the gulf while overshooting observed residuals to the southeast.



best fitting postseismic model (scenario 24). The contrast between the residuals of stations in the No<del>uth northern half of the gulf</del> (East of the Aragonese fault trace) and South (East of the Arnona fault trace) is illust co-seismic fault rupture of the Aragonese fault (after Baer et al. 2008). For visualisation purpose, 95% confidence ellipses are shown only for the Figure 10: Residual velocities after implementing four postseismic model scenarios discussed in the text, with the orange line delineating the 1995 Figure 10: Residual velocities after implementing four postseismic model scenarios discussed in the text, with the orange line delineating the 1995 co-seismic fault rupture of the Aragonese fault (after Baer et al. 2008). For visualisation purpose, 95% confidence ellipses are shown only for the best fitting postseismic model (scenario 2 4). The contrast between the residuals of stations in the <del>North northern half of the gulf</del> (East of the Aragonese fault <mark>trace</mark>) and South (East of the Arnona fault <mark>trace</mark>) is illustrated in panels b-e, with <mark>notched</mark> boxes enclosing data within 25th and 75th percentiles. For each scenario, the median of the misfit distribution is shown as a solid red line and whiskers extend to the most extreme data points not considered as outliers, which are represented by the red crosses. points not considered as outliers, which are represented by the red crosses.

#### 7. Discussion

 Previous estimates of the relative motion between the Sinai and Arabian plates along the Gulf of Aqaba relied on sparse observations at a limited number of GPS sites located on each side of the gulf (e.g., Mahmoud et al. 2005; Reilinger et al. 2006; ArRajehi et al. 2010; Gomez et al. 2020). However, the establishment of 27 survey-mode sites in 2014 and the rapid expansion of permanent geodetic networks in Saudi Arabia during the last decade have allowed us to derive an updated GPS velocity field of this region.

 By implementing a an elastic half-space model, we derived a slip rate of  $\frac{4.9^{+0.9}_{-0.6} \,mm/yr}{10^{-0.9}_{-0.6} \,mm/yr}$  and a locking depth of  $\frac{6.8^{+3.5}_{-3.1} \,km}{10^{-3.5} \,km}$  across the Eilat fault. We  $_{\rm{sos}}$  also estimated a slip rate of  $5.5^{+1.3}_{-0.9}$   $mm/yr$  and a locking depth of  $0.8^{+3.4}_{-0.8}$   $km$  further south across the Arnona and Tiran faults (see red curves in Fig. 5a-b). <sub>507</sub> While the slip rates derived here agree with previous studies, the locking depth <sub>508</sub> estimates is are shallower than that those reported along the Wadi Arabah fault 509 north of the gulf, which range between 12 and 20  $km$  (e.g., Le Béon et al. 2008; Sadeh et al. 2012; Masson et al. 2015; Hamiel et al. 2018b; Gomez et al. 2020).  $\frac{1}{2}$  Further south, stations' rates show no little evidence of strain accumulation despite their proximity to the Tiran fault. This pattern agrees with a very shallow locking depth, which might indicate potential creep along this fault segment (see Fig.  $5b$ ).

 To evaluate the impact of outliers in the slip rate and locking depth inver- sions, we ran additional tests considering all the stations in the profiles including stations with anomalous rates. Inversions including all the GPS stations in the  $\frac{\text{short}}{\text{norm}}$  profile yielded a slip rate of  $6.7^{+0.7}_{-0.7}$  mm/yr and a locking depth of  $\frac{8.8^{+2.2}_{-2.2}}{2.8}$  km. Further south, across the Arnona and Tiran faultts, this test re- $_{520}$  sulted in a slip rate of  $5.9^{+1.3}_{-0.7}$  mm/yr and a locking depth of  $2.5^{+3.2}_{-2.2}$  km. Our results thus suggest that the slip rates seem to be more affected by the outlier rates in the mid- and far-field, than the locking depths (see Fig. S4). Although the slip rates and locking depths for the southern profile are not as well con-strained as for the northern profile, our modelling results show that the buried

### screw dislocation model provides consistent locking depth estimates even in the presence of the outliers, indicating shallower locking depths in the south.

 Previous geophysical studies conducted along the on-land portion of the DST and its offshore extension in the Gulf of Aqaba indicate a systematic thinning of the lithosphere towards the Red Sea (e.g., Ginzburg et al. 1979; Ben-Avraham 1985; Mohsen et al. 2006; El Khrepy et al. 2016a). Ben-Avraham (1985) con- ducted gravity, magnetic and seismic surveys in the gulf, and proposed a thinner crust in its southern region. This observation agrees with earlier investigations indicating higher heat flow values and gradual crustal thinning towards the south (e.g., Ginzburg et al. 1979; Ben-Avraham and Von Herzen 1987). Simi- larly, tomographic inversions and S-receiver function studies revealed that the  $\frac{1}{256}$  lithospheric thickness decreases from 80 km north of the Dead Sea to 65 km in the Gulf of Aqaba, indicating stronger asthenospheric upwelling in the south 538 (Mohsen et al., 2006; El Khrepy et al., 2016a). More recently, Li et al. (2021) im- plemented along-track Sentinel-1 burst-overlap interferometric time-series anal- ysis and reported decreasing locking depths from  $15.9 \pm 1.9$  km of the Wadi  $\frac{541}{100}$  Arabah fault to only  $3.9 \pm 1.5$  km in the southern part of the Gulf of Aqaba. Hence, the locking depth reduction from north to south along the Wadi Arabah and faults within the gulf might be explained by progressive crustal thinning towards the Red Sea.

 $\frac{545}{100}$  We estimated a slip rate of ~4.5 mm/yr along the main fault segments in the gulf based on a forward back-slip model, which implemented the Arabia- Sinai Euler pole derived in this study. This estimate is lower than the best-fit inverted in our screw dislocation models, and could be attributed to potential internal deformation or fragmentation of the Sinai plate as has been reported in recent studies (e.g., Gomez et al. 2020). The present-day slip rate derived from geodetic data in the gulf area agrees well with the long-term geological estimates along the southern on-land portion of the DST, which converge to an 553 average value of  $5 \pm 12$  mm/yr (e.g., Le Béon et al. 2010, 2012). We can thus assume that the present-day slip rate has remained relatively constant over the last millennium. Based on this assumption, the Eilat and Arnona faults  have accumulated significant moment since the last historical earthquakes that struck the gulf area in 1212 AD and 1588 AD (e.g., Ambraseys 2009; Agnon 2014; Klinger et al. 2015; Lefevre et al. 2018).

 We estimated the slip deficit and moment accumulation rate on the major strike-slip faults in the gulf, assuming that they are fully locked during the in- terseismic period. We also considered an additional scenario assuming that the Tiran fault in the southern region of the gulf creeps aseismically. Considering that the 1212 AD and 1588 AD earthquakes cannot be unambiguously assigned to specific fault traces within the gulf, we tested both as potential last earth- quakes on the Eilat and Arnona faults. For this purpose, we evaluated lower and upper bound estimates based on the fault kinematic parameters derived in this research and previous investigations along the southern on-land portion of the DST, corresponding to slip rates ranging between 4.4 and 5.2 mm/yr (e.g., Mahmoud et al. 2005; Reilinger et al. 2006; Le Béon et al. 2008; ArRajehi et al. 2010; Al Tarazi et al. 2011; Sadeh et al. 2012; Masson et al. 2015; Hamiel et al. 2016, 2018a,b; Gomez et al. 2020). For the locking depths, we considered the lower and upper bounds from the 1-sigma uncertainty derived in the gulf's  $\frac{573}{100}$  northern region, corresponding to locking depths ranging between 4 and 10 km (see Fig.  $5a$ ).

 Tab. 1 summarises the parameters considered in our calculations (fault length  $\mathbf{576}$  L, locking depth  $L_D$  and slip rate u) as well as estimates of the slip deficit u,  $\mathbf{F77}$  geodetic moment  $M_0$ , moment accumulation rate  $\dot{M}_0$  and the associated mo- $\mathbf{s}$ <sub>78</sub> ment magnitude  $M_W$  for each fault segment, which was computed based on the scaling regression by Hanks and Kanamori (1979). The slip deficit and mo- ment accumulation rates estimated for the Eilat and Arnona faults suggest that  $\frac{1}{2}$  impending earthquakes could reach  $M_W$  6.7-7.3, assuming that the moment ac- cumulated since the last known historical or instrumental earthquakes ("Last  $EQ'$ ) would be released by an earthquake on each fault strand. Estimates of the slip deficit and moment accumulated on the Aragonese fault are much smaller,  $\frac{1}{100}$  as expected, considering that this fault strand ruptured during the 1995  $M_W 7.2$ Nuweiba earthquake (Klinger et al., 1999; Shamir et al., 2003; Hofstetter, 2003;  Baer et al., 2008; Ribot et al., 2021). Our results thus agree with previous stud- ies suggesting that the Eilat and Arnona faults might be in a late stage of their current interseismic period (e.g., Hamiel et al. 2018b; Kanari et al. 2020; Ribot et al.  $2021$ ).

Table 1: Fault parameters and estimated earthquake potential for the main strike-slip fault segments in the Gulf of Aqaba.

Fault	$L$ [km]	$L_D$ [km]	$\dot{u}$ [mm/yr]	Last EQ	u[m]	$M_0$ [Nm]	$\dot{M}_0$ $\left[Nm/yr\right]$	$M_W$
Eilat	59	$\overline{4}$ 10	4.4 5.2	1212	3.56 4.20	$2.517\times10^{19}$ $7.437\times10^{19}$	$3.115\times10^{16}$ $9.204\times10^{16}$	6.9 7.2
	59	$\overline{4}$ 10	4.4 5.2	1588	1.90 2.25	$1.346\times10^{19}$ $3.976\times10^{19}$	$3.115\times10^{16}$ $9.204\times10^{16}$	6.7 7.0
Aragonese	53	$\overline{4}$ 10	4.4 5.2	1995	0.11 0.13	$6.996\times10^{17}$ $2.067\times10^{18}$	$2.798\times10^{16}$ $8.268\times10^{16}$	5.9 6.2
Arnona	83	$\overline{4}$ 10	4.4 5.2	1212	3.56 4.20	$3.541\times10^{19}$ $1.046\times10^{20}$	$4.382\times10^{16}$ $1.295\times10^{17}$	7.0 7.3
	83	$\overline{4}$ 10	4.4 5.2	1588	1.90 2.25	$1.893\times10^{19}$ $5.593\times10^{19}$	$4.382\times10^{16}$ $1.295\times10^{17}$	6.8 7.1
Tiran	50	Creep	4.4 5.2					

 Our modelling results reveal a residual left-lateral motion across the gulf that cannot be resolved by standard models of interseismic strain accumulation (Figs. 7 and 10). The nature of these velocity residuals is a subject of debate. While some studies speculate that they could be caused by interseismic elastic strain accumulation along the faults bounding the pull-apart basins in Gulf of Aqaba (e.g., Pietrantonio et al. 2016), others point out that they could be due to postseismic motions induced by the 1995 Nuweiba Earthquake (e.g., Piersanti et al. 2001; Pe'eri et al. 2002; Riguzzi et al. 2006; Gomez et al. 2020).

 We consider four possible explanations for the left-lateral residual motion observed across the gulf. The first possibility is that anomalous misfits are due to poor Euler vector parameters for the Sinai subplate relative to ITRF2014. However, this explanation is not supported by the velocity field obtained for stations of the GIL network in Israel, which exhibit residual velocities close to zero, evidencing the robustness of the Euler vector parameters derived in our study (see Tab. S2 and Fig. S2). A second possibility is that the resulting mis-fits reflect the difference in temporal baselines between stations situated in the  northern and southern regions of the gulf as shown in Fig. S1. This hypothesis might explain the small residuals obtained for stations with longer time series located East of the Arnona fault (sites MAG1, MAG2 and BIDA, RASH, TAYS, TAY1, TB03, SHRM). Nevertheless, it fails to explain the systematic nature of residual motions.

 A third hypothesis is that the relative motion between the Arabian and Sinai plates along Gulf of Aqaba is accommodated by a wide deformation zone extend- ing up to ∼50 km across both plates. Several studies have identified two shear belts composed of anastomosing faults on both sides of the gulf (e.g., Freund et al. 1970; Bartov et al. 1980; Eyal et al. 1981; Garfunkel 1981; Lyberis 1988). Earlier investigations indicate that these faults were active primarily during the first slip stages along the DST and do not affect post-Miocene stratigraphic units (e.g., Bartov et al. 1980; Eyal et al. 1981; Garfunkel 1981). A more recent study reported small-scale normal faults affecting post-Miocene strata and Pleis- tocene coral terraces indicating ENE-WSW extension (Bosworth et al., 2017). However, the seismicity recorded in the gulf area shows that most earthquakes  $\epsilon_{23}$  concentrate along the gulf itself and the coastal plains (e.g., Ben-Avraham et al. 1979; Bartov et al. 1980, Fig. 2), suggesting that recent deformation is confined to those areas.

 Finally, the systematic left-lateral residual signal could reflect ongoing post- seismic deformation caused by the Nuweiba Earthquake. A recent study by Liu  $\epsilon_{28}$  et al. (2020) found that the lower crust exhibits ductility at decadal time scales, and thus postseismic transient motions may be larger and more enduring than previously thought. As noted by Piersanti et al. (2001), the motion of stations DAHA and NABQ on the Sinai side of the gulf is puzzling considering that they exhibit motions that are opposite to the direction predicted by interseis- mic models of strain accumulation (see Fig. 3). Similarly, the updated velocity field presented in this study allowed us to quantitatively identify northeastward residuals east of the Aragonese and Eilat faults, which agree with the overall pattern of modelled postseismic rates.

We speculate that the misfit between the magnitudes of theoretical postseis-

 mic motions and residuals from the back-slip model may arise from structural and rheological complexities in the gulf (e.g., Ben-Avraham 1985; El Khrepy et al. 2016a,b), which were not considered in our forward models. Therefore, postseismic motions and relaxation times could exhibit significant spatial varia- tions depending on the lithospheric structure in different regions of the gulf and the slip distribution used to model the Nuweiba earthquake.

#### 8. Conclusions

 The establishment of 27 survey-mode GPS stations in 2014 and the analysis of up to 19 years of geodetic observations on the Arabian and Sinai-Levant plates allowed us to derive an updated crustal motion velocity field of the lands bor- $\epsilon_{48}$  dering the Gulf of Aqaba. By implementing a an elastic interseismic model, we •• derived a slip rate of  $\frac{4.9^{+0.9}_{-0.6} \,mm/yr}{0.6 \,mm/yr}$  and a locking depth of  $\frac{6.8^{+3.5}_{-3.1} \,km}{0.6 \,mm/yr}$  across the Eilat fault in the gulf's northern region. Our modelling results suggest that either a shallow locking depth or creeping might be required to explain the low interseismic strain accumulation observed in the gulf's southern region across Tiran fault. We identified a systematic left-lateral residual motion across the gulf, characterised by northeastward residuals east of the Aragonese fault and southwestward residuals west of the Arnona fault. We postulate that postseis-656 mic transient motions caused by the 1995,  $M_W 7.2$  Nuweiba earthquake could potentially explain these misfits. Estimates of the geodetic moment accumu- lated on the Eilat and Arnona faults since the last historical earthquakes that struck the gulf area in 1212 AD and 1588 AD indicate that impending earth- $\epsilon_{\rm 60}$  quakes on these faults could potentially reach  $M_W$ 6.7-7.3, posing a significant hazard to the urban centres along the gulf coast. Future studies would benefit from incorporating additional GPS stations on the Sinai side of the gulf, refined slip models of the Nuweiba earthquake and more detailed information about historical earthquakes in the gulf region.

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#### Data Availability

<sup>677</sup> The GPS data underlying this article will be made available on the UNAVCO archive, at <https://www.unavco.org/data/dai/>.

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