



TherMatHT 8, 2-3 sept. 2021

Experimental and numerical study of bubble formation in a borosilicate melt doped with cerium oxide

Luiz Pereira<sup>1</sup>, Annabelle Laplace<sup>1</sup> & Franck Pigeonneau<sup>2</sup> <sup>1</sup>CEA Marcoule, DES, ISEC, DE2D, SEVT/LDMC <sup>2</sup>Mines-Paristech PSL Univ. - CEMEF









#### Primary foam







- Energetic efficiency;
- Wear of the process.



Purpose of the work :

# Bubble dynamics in molten nuclear glass doped in cerium oxide





Purpose of the work :

# Bubble dynamics in molten nuclear glass doped in cerium oxide





Purpose of the work :

Bubble dynamics in molten nuclear glass doped in cerium oxide



- What are the main mechanics of the bubble formation ?
- What are the nature and sizes of bubbles?
- What is the dynamics of the bubble population ?



2. Bubble formation in crucible

3. Numerical predictions

4. Synthesis



- Melting of granular material composed by a borosilicate glass + 0.1wt % of CeO<sub>2</sub>.
- Post morten observation of a crucible section.



Figure 1 – Cross section of the crucible a room temperature.





Figure 2 – Optical microscope sample at  $T = 800 \,^{\circ}\text{C}$  and after 20 min in the furnace.





Figure 3 – Optical microscope images of samples at various temperatures and times.





Figure 4 – Bubble size distribution at  $T = 1000 \,^{\circ}\text{C}$  after 20 minutes of melting.

$$f(x,\zeta,\sigma) = \frac{1}{x\sigma\sqrt{2\pi}} \exp\left[-\frac{(\ln x - \ln \zeta)^2}{2\sigma^2}\right].$$
(1)  
TherMatHT 8, 2-3 sept. 2021

According to Reboul et al.<sup>1</sup>, void volumes in a granular media are log-normal distributed.



Figure 5 – Voids in a granular media (a) and PDF of void volumes (b) according to Reboul et al. (2008).

<sup>1.</sup> N. Reboul/E. Vincens/B. Cambou : A statistical analysis of void size distribution in a simulated narrowly graded packing of spheres, in : Granular Matter 10.6 (2008), p. 457-468.



Figure 6 – Gas composition of bubble at  $T = 900 \,^{\circ}\text{C}$ .





Figure 6 – Gas composition of bubble at  $T = 900 \,^{\circ}$ C.

>> Population of bubbles created by air entrapment.





Figure 7 –  $N_b$  (cm<sup>-2</sup>) vs. *t*.

Figure 8 –  $\langle D \rangle$  (µm) vs. *t*.



$$t_{\eta} = \frac{H\eta(T)}{\rho g \langle D \rangle_0^2};$$
<sup>(2)</sup>



Figure 9 – (a)  $N_b$  (/cm<sup>2</sup>) vs.  $t/t_\eta$  & (b)  $\langle D \rangle$  (µm) vs.  $t/t_\eta$ .



Development of numerical model based on a population balance equation<sup>2</sup>:

$$\frac{\partial n}{\partial t} =$$
 (3)

<sup>2.</sup> D. L. Marchisio/R. O. Fox : Computational models for polydisperse particulate and multiphase systems, 2013.

Development of numerical model based on a population balance equation<sup>2</sup>:

$$\frac{\partial n}{\partial t} + \frac{\partial (\dot{a}n)}{\partial a} + \sum_{i=1}^{N_g - 1} \frac{\partial (\dot{\varpi}_i n)}{\partial \varpi_i} =$$
(3)

mass transfer;

<sup>2.</sup> Marchisio/Fox : Computational models for polydisperse particulate and multiphase systems (cf. note 2).

Development of numerical model based on a population balance equation<sup>2</sup>:

$$\frac{\partial n}{\partial t} + \frac{\partial (\dot{a}n)}{\partial a} + \sum_{i=1}^{N_g - 1} \frac{\partial (\dot{\varpi}_i n)}{\partial \varpi_i} = -\frac{\rho g a^2}{3\eta(T)} n \tag{3}$$

mass transfer; bubble release from the free surface;

<sup>2.</sup> Marchisio/Fox : Computational models for polydisperse particulate and multiphase systems (cf. note 2).

Development of numerical model based on a population balance equation<sup>2</sup>:

$$\frac{\partial n}{\partial t} + \frac{\partial (\dot{a}n)}{\partial a} + \sum_{i=1}^{N_g - 1} \frac{\partial (\dot{\varpi}_i n)}{\partial \varpi_i} = -\frac{\rho g a^2}{3\eta(T)} n + h(\mathbf{x}, t; a, \varpi).$$
(3)

mass transfer; bubble release from the free surface; binary coalescence due to bubble rising  $^3$ :

$$h(\mathbf{x},t;a) = \frac{1}{2} \int_0^a \frac{a^2}{(a^3 - a'^3)^{2/3}} K\left(a', \sqrt[3]{a^3 - a'^3}\right) n(\mathbf{x},t;a') n\left(\mathbf{x},t;\sqrt[3]{a^3 - a'^3}\right) da' - n(\mathbf{x},t;a') \int_0^\infty K\left(a,a'\right) n(\mathbf{x},t;a') da'.$$
(4)

2. Marchisio/Fox : Computational models for polydisperse particulate and multiphase systems (cf. note 2).

3. D. Ramkrishna : Population balances. Theory and application to particulate systems in engineering, San Diego 2000.



Figure  $10 - \mu_0 = N_b/N_b(0)$  vs.  $t/t_\eta$  with and without coalescence at  $T = 1000^{\circ}$ C.





Figure  $11 - \mu_0 = N_b/N_b(0)$  vs.  $t/t_\eta$  with and without coalescence at  $T = 1100^{\circ}$ C.



# 4. Synthesis

- Initial bubbles are due to the atmosphere entrapment during the melting;
- The size distributions are log-normal distributed;
- The dynamics is strongly thermal activated (scaled by the viscosity);
- The bubble coalescence is main phenomenon at short times (confirm the assertion of Cable<sup>4</sup>).

<sup>4.</sup> M. Cable : A study of refining. Part 2 : Mechanisms of refining, in : Glass Technol. 2 (1961), p. 60-70.

# 4. Synthesis

- Initial bubbles are due to the atmosphere entrapment during the melting;
- The size distributions are log-normal distributed;
- The dynamics is strongly thermal activated (scaled by the viscosity);
- The bubble coalescence is main phenomenon at short times (confirm the assertion of Cable<sup>4</sup>).

See the poster!

<sup>4.</sup> Cable : A study of refining. Part 2 : Mechanisms of refining (cf. note 4).