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Carlos Pinilla, Aldemar de Moya, Segolene Rabin, Guillaume Morard, Mathieu Roskosz, et al.. First-principles investigation of equilibrium iron isotope fractionation in Fe<sub>1-x</sub>S<sub>x</sub> alloys at Earth's core formation conditions. *Earth and Planetary Science Letters*, 2021, 569, pp.117059. 10.1016/j.epsl.2021.117059 . hal-03371089

**HAL Id: hal-03371089**

**<https://hal.science/hal-03371089v1>**

Submitted on 8 Oct 2021

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# Earth and Planetary Science Letters

## First-principles investigation of equilibrium iron isotope fractionation in Fe<sub>1-x</sub>S<sub>x</sub> alloys at Earth's core formation conditions

--Manuscript Draft--

<b>Manuscript Number:</b>	EPSL-D-21-00042R1
<b>Article Type:</b>	Letters
<b>Keywords:</b>	Isotope fractionation Core Sulfur Iron high pressure
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<b>Abstract:</b>	<p>Iron is one of the most abundant non-volatile elements in the solar system. As a major component of planetary metallic alloys, its immiscibility with silicates plays a major role in planetary formation and differentiation. Information about these processes can be gained by studying the equilibrium Fe isotope fractionation between metal alloys and molten silicates at conditions of core formation. In particular, recent attention has been paid to <sup>56</sup>Fe/<sup>54</sup>Fe equilibrium isotope fractionation at conditions relevant to Earth's core formation and the influence that light elements (O, H, C, Ni, Si and S) have had in this process. Most of these experimental studies relied on the measurement of Fe isotope fractionation from quenched phases of silicate melts and molten iron alloys. The experimental works are extremely challenging, and may suffer different drawbacks. To overcome this, we use ab-initio computational methods to perform a systematic study of the <sup>56</sup>Fe/<sup>54</sup>Fe equilibrium isotope fractionation in molten and solid Fe<sub>1-x</sub>S<sub>x</sub> alloys at conditions of the core formation (60 GPa, 3000 K). We show for the first time, that equilibrium isotope fractionation factors from solid systems can be used as proxies for molten systems with differences between these two methods less than 0.01 ‰ at the relevant P-T conditions. Additionally, we discuss the effect of sulphur concentration on the equilibrium Fe isotope fractionation and show that although there are some structural changes due to atom substitutions, the wide range of studied concentrations produces β-factors that are constant within ~ 0.01‰. Finally, we discuss the implications of our results for the interpretation of recent experiments and the understanding of core crystallization processes.</p>

- Equilibrium isotope fraction factors from solid alloys can be used as proxies for molten systems
- The effect of sulphur on isotope fractionation factors are within a 0.02‰ for all the studied alloys
- Bond type and local environment are the controlling parameters of Fe isotope fractionation in  $\text{Fe}_{1-x}\text{S}_x$  alloys
- No measurable Fe fractionation should be produced between liquid and solid  $\text{Fe}_{1-x}\text{S}_x$  alloys at conditions of Earth's core formation.

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2 **First-principles investigation of equilibrium iron isotope fractionation in Fe<sub>1-x</sub>S<sub>x</sub> alloys at**  
3 **Earth's core formation conditions**  
4

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17  
18 **ABSTRACT**

19 Iron is one of the most abundant non-volatile elements in the solar system. As a major component of  
20 planetary metallic alloys, its immiscibility with silicates plays a major role in planetary formation and  
21 differentiation. Information about these processes can be gained by studying the equilibrium Fe  
22 isotope fractionation between metal alloys and molten silicates at conditions of core formation. In  
23 particular, recent attention has been paid to <sup>56</sup>Fe/<sup>54</sup>Fe equilibrium isotope fractionation at conditions  
24 relevant to Earth's core formation and the influence that light elements (O, H, C, Ni, Si and S) have had  
25 in this process. Most of these experimental studies relied on the measurement of Fe isotope  
26 fractionation from quenched phases of silicate melts and molten iron alloys. The experimental works  
27 are extremely challenging, and may suffer different drawbacks. To overcome this, we use *ab-initio*  
28 computational methods to perform a systematic study of the <sup>56</sup>Fe/<sup>54</sup>Fe equilibrium isotope  
29 fractionation in molten and solid Fe<sub>1-x</sub>S<sub>x</sub> alloys at conditions of the core formation (60 GPa, 3000 K).  
30 We show for the first time, that equilibrium isotope fractionation factors from solid systems can be  
31 used as proxies for molten systems with differences between these two methods less than 0.01 ‰ at  
32 the relevant P-T conditions. Additionally, we discuss the effect of sulphur concentration on the  
33 equilibrium Fe isotope fractionation and show that although there are some structural changes due to

34 atom substitutions, the wide range of studied concentrations produces  $\beta$ -factors that are constant  
35 within  $\sim 0.02\%$ . Finally, we discuss the implications of our results for the interpretation of recent  
36 experiments and the understanding of core crystallization processes.

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## 42 **ARTICLE INFO**

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## 46 **INTRODUCTION**

47 Iron is the major element of solar system planetary cores, in relation with the nucleosynthesis  
48 sequence. Iron plays a major role in every stage of planetary formation and differentiation.

49 Geophysical approaches have confirmed the presence of iron for Earth's core but with almost 10% of  
50 light elements required to make up its mass (Hirose et al., 2013). Traditionally the effects due to the

51 presence of light elements in the core are being inferred by geophysical studies where the density and  
52 sound velocity propagation are studied as function of light element concentration to match those

53 values reported from geophysical models such as PREM. However, recently it has been suggested that  
54 the Fe isotopic composition in the mantle could be used to infer the composition of Earth's core

55 (Bourdon et al., 2018; Craddock and Dauphas, 2010; Craddock et al., 2013; Leshner et al., 2020; Shahar  
56 et al., 2016; Sossi et al., 2016). This is based on the assumption that the presence of elements such as C,

57 O, Si, S should affect the partitioning of iron isotopes between the mantle and the core. Originally, it  
58 has been suggested that core-mantle differentiation will leave imprints on the iron isotope signature of

59 Earth's mantle because of the difference of Fe valence state and coordination in the mantle ( $\text{Fe}^{2+}$ ) and  
60 in the core ( $\text{Fe}^0$  metal) (Polyakov, 2009). That study suggested that the mantle should be enriched in

61 heavy isotopes, product of equilibrium isotope fractionation during differentiation. However,

62 subsequent explanations argue that the bulk silicate Earth is chondritic in its iron isotopic composition

63 and that any difference in isotope composition seen in basalts is due to fractionation during partial  
64 melting of the rock from which they have been formed (Craddock et al., 2013). Indeed, isotope  
65 compositions in natural rocks are scattered in values, with  $\delta^{56}\text{Fe} \sim -0.01 \text{ ‰}$  for carbonaceous  
66 chondrites,  $\delta^{56}\text{Fe} \sim -0.1$  to  $+0.1 \text{ ‰}$  for enstatite chondrites and  $\delta^{56}\text{Fe} \sim +0.1 \text{ ‰}$  for basalts (Craddock  
67 and Dauphas, 2011; Liu et al., 2017; Poitrasson et al., 2013). These scattered values are therefore  
68 interpreted to suggest that the accessible mantle has a Fe isotope composition that is indistinguishable  
69 from chondritic composition (i.e.  $\delta^{56}\text{Fe} \sim 0 \text{ ‰}$ ). Apart from expected evidence of the presence of light  
70 elements in the core due to difference in chemical bonds, one must also consider the effects of  
71 pressure and temperature. It is well known that equilibrium fractionation effects should vanish at high  
72 temperatures. However, in the case of lower mantle and core conditions where pressures are also  
73 high, these fractionation effects might still be important. Recently, Shahar et al. (2016) have carried  
74 out experiments and computational modelling on the effects of pressure and light elements (such as H,  
75 C, O) on the equilibrium isotope fractionation of  $^{57}\text{Fe}/^{54}\text{Fe}$  at the core-mantle boundary. Their work  
76 has found a significant imprint on isotope fractionation due to light elements such as C and H  
77 ( $\delta^{56}\text{Fe} \sim -0.03$ - $-0.05 \text{ ‰}$ ) whilst elements such as O leave almost no imprint ( $\delta^{56}\text{Fe} \sim -0.007$ - $-0.01 \text{ ‰}$ ). Their  
78 results support the suggestions by Craddock et al. (2013) that in order to have a mantle with a  $\delta^{56}\text{Fe}$   
79 near  $0 \text{ ‰}$ , light elements such as C and H that provide a large imprint in fractionation should not be  
80 present in the core at a significant level. Additionally, it favours the presence of O as a light element in  
81 the core. However, the effects of other light elements such as S on equilibrium Fe isotope fractionation  
82 at core conditions are yet unclear as well as any pressure induced magnetic effects that can be of  
83 relevance. There has been recent experimental work by (Ni et al., 2020); Shahar et al. (2015) on the  
84 effects of S on Fe isotope fractionation between solid metal and liquid metal, or between metal and  
85 silicate. In both cases, sulfur enters into the metallic phases and preferentially into the liquid metal  
86 phase. Shahar et al. (2015) found that metal-silicate fractionation increases significantly with the  
87 sulfur content in the metal, whereas Ni et al. (2020) observed that the solid-liquid fractionation in this  
88 system does not depend on the sulfur content of the liquid metal. Obviously, much work needs to be

89 done to understand these effects at temperature and pressure conditions of the terrestrial core, far  
90 away from experimental studies performed below 2 GPa. In this context, the difficulty to carry out  
91 experiments at high pressure and high temperature leads to the use of crystalline phases such as *hcp*  
92 Iron or *14* Fe<sub>3</sub>S as proxies of the molten systems leading to large extrapolations and possible errors in  
93 the interpretation of final results. This approach is used for instance in Liu et al. (2017) where high-  
94 pressure data (up to 206 GPa) suggest a minuscule Fe isotope fractionation between metal and silicate  
95 that is one order of magnitude lower than the one found by Shahar et al. (2015) at 1-2 GPa.

96 In recent years, computational techniques have become useful tools to estimate isotope fractionation  
97 factors in mineral systems. This is particularly true for methods based on quantum mechanics that  
98 allow to describe the vibrational properties of light and heavy isotopes at any pressure and  
99 temperature conditions (Blanchard et al., 2017). However, the weakness of these methods typically  
100 lies in the use of the quasi-harmonic approximation that falls when temperature increases or when the  
101 systems become fully molten. In addition, in dynamical systems such as liquids and melts, it has been  
102 shown that configurational disorder needs to be taken into account in order to obtain meaningful  
103 equilibrium fractionation factors (Blanchard et al., 2017; Pinilla et al., 2015).

104 In this work, we use *ab-initio* computational methods to perform a systematic study of the <sup>56</sup>Fe/<sup>54</sup>Fe  
105 equilibrium isotope fractionation in molten and solid Fe<sub>1-x</sub>S<sub>x</sub> alloys at conditions of the core formation.  
106 By comparing the fractionation factors obtained from solid and molten systems, we estimate the  
107 validity of the experimental approximation consisting in using solid metals as a proxy for molten  
108 alloys. Additionally, we comment on the effects of S concentration on Fe isotope fractionation in liquid  
109 systems. We discuss our findings on view of latest results on equilibrium Fe isotope fractionation and  
110 their relevance for the formation of the Earth's core.

111

112 **METHODS**

## 113 2.1 Equilibrium isotope fractionation factor from harmonic vibrational modes

114 The equilibrium isotope fractionation factor of an element displaying two isotopic forms Y and Y\*  
115 between two phases  $a$  and  $b$  is related to the ratio of the isotope concentration ratios:

$$116 \quad \alpha(a, b, Y) = \frac{\left(\frac{n_{Y^*}}{n_Y}\right)_a}{\left(\frac{n_{Y^*}}{n_Y}\right)_b},$$

117 where  $n_Y$  is the mole fraction of isotopes Y in phase  $a$ . The equilibrium fractionation factor between  
118 two phases can be related to the reduced partition function ratio  $\beta(a, Y)$  of each phase by:  
119  $\ln(\alpha(a, b, Y)) = \ln(\beta(a, Y)) - \ln(\beta(b, Y))$ . Isotopic reduced partition function ratios are usually presented as  
120  $10^3 \ln(\beta(a, Y))$  in permil. The reduced partition function ratio  $\beta(a, Y)$  describes the isotopic fractionation  
121 properties of a given phase normalized to the properties of a classically behaving system. It can be  
122 shown that within the harmonic approximation and using the Teller-Redlich rule for frequencies  
123 (Wilson et al., 1955), the  $\beta(a, Y)$  factor in a solid phase can be written as (Meheut et al., 2007):

$$124 \quad \beta(a, Y) = \left[ \prod_{i=1}^{3N_{at}} \prod_q \frac{v_{q,i}^*}{v_{q,i}} \frac{e^{-hv_{q,i}^*/(2k_B T)}}{1 - e^{-hv_{q,i}^*/(k_B T)}} \frac{1 - e^{-hv_{q,i}/(k_B T)}}{e^{-hv_{q,i}/(2k_B T)}} \right]^{1/NN_q} \quad (2)$$

125 where  $v_{q,i}$  and  $v_{q,i}^*$  are the phonon frequencies of the  $i$ -th branch with wave vector  $q$  for the two  
126 isotopologues.  $N_{at}$  is the number of atoms in the unit-cell and  $N$  is the number of sites occupied by the  
127 Y atom in the unit-cell.  $h$  and  $k_B$  are the Planck and Boltzmann constants respectively, and  $T$  the  
128 temperature. The second product in equation 2 is usually performed on a grid containing  $Nq$   $q$ -vectors  
129 to ensure full convergence of the  $\beta(a, Y)$  value.

## 130 2.2 Equilibrium isotope fractionation factor from the kinetic energy

131 To calculate the equilibrium fractionation factor directly from molecular dynamics simulations of  
132 liquid systems, we can use the equation relating the  $\beta$ -factor to the atomic kinetic energy ( $K$ )  
133 (Polyakov, 1998, 2009):



134 
$$\ln\beta(a, Y) = \frac{\Delta m}{m^*} \left( \frac{K}{k_B T} - \frac{3}{2} \right), \quad (3)$$

135 where  $\Delta m = m^* - m$  with  $m^*$  the mass of the heavier isotope. In this work we have used the definition of  
 136 kinetic energy (K) as a function of the partial vibrational density of states (pDOS) that can be  
 137 computed directly from computer simulations or experiments using nuclear resonant inelastic X-ray  
 138 scattering spectroscopy (NRIXS) (Dauphas et al., 2018; Dauphas et al., 2012; Polyakov, 2009). In this  
 139 way, the kinetic energy of an atomic specie in the phase of interest can be defined as a function of the  
 140 vibrational density of states of this atomic specie,  $g(\nu)$ , as (Vos et al., 2015):

141 
$$K = \frac{3}{2} \frac{\int_{\nu_i}^{\nu_f} g(\nu) \alpha(\nu, T) d\nu}{\int_{\nu_i}^{\nu_f} g(\nu) d\nu}, \quad (4)$$

142 with  $\alpha(\nu, T)$  the kinetic energy of a quantum harmonic oscillator. This last term is defined as:

143 
$$\alpha(\nu, T) = h\nu \left( \frac{1}{e^{h\nu/k_B T} - 1} + \frac{1}{2} \right). \quad (5)$$

144 The vibrational density of states of a system of atoms can be retrieved from the Fourier transform of  
 145 the velocity auto-correlation function (VCF) thermodynamically averaged over all atoms of a given  
 146 specie. The pDOS for a system of N atoms is given by

147 
$$g(\nu) = \int_{-\infty}^{\infty} dt \frac{\langle \mathbf{v}(t) \cdot \mathbf{v}(0) \rangle}{\langle \mathbf{v}(0) \cdot \mathbf{v}(0) \rangle} e^{i2\pi\nu t} \quad (6)$$

148 The VCF has been calculated directly from *ab-initio* molecular dynamics simulations at the  
 149 temperature and pressure of interest.

150

### 151 **2.3 Computational details**

152 The calculations in this work are based on density functional theory as implemented in the VASP code  
 153 developed by Kresse and Hafner (1994) and updated by Kresse and Furthmuller (1996). The exchange

154 and correlation energy was represented by the generalized-gradient-approximation GGA approach in  
155 the version for solids, PBEsol, developed by Von Barth (2004). Electronic wave functions were  
156 expanded on a plane-wave basis with a maximum cutoff energy of 600 eV, which guarantees  
157 convergence of all calculated properties. Pseudopotentials of the projector augmented wave type  
158 (Blöchl, 1994; Kresse, 1999) were used for Fe and S, with an electronic configuration of valence states  
159  $3s^2 3p^6 3d^6 4s^2$  and  $3s^2 3p^4$ , respectively.

160 *Ab-initio* molecular dynamics (AIMD) calculations were performed using a Nosé-Poincaré thermostat  
161 (Bond et al., 1999) and a Parrinello-Raman barostat (Hernandez, 2001) to work at temperatures and  
162 pressures of interest. All systems were thermodynamically equilibrated at core formation conditions  
163 (60 GPa, 3000 K) by means of a NPT ensemble for a minimum time of 2 ps, which was found sufficient  
164 to guarantee fully thermodynamic equilibrium. Once the system was equilibrated to the desired  
165 pressure and temperature, calculations were subsequently performed in a NVT ensemble at the same  
166 temperature, using a Nosé-Hoover thermostat (Hoover, 1985; Nosé, 1984). All AIMD calculations were  
167 carried out with an integration time of 0.5 fs.

168 In order to understand the effect of S on the Fe isotope fractionation, we selected the following  
169 systems: a pure solid hcp iron structure (54 atoms) and its molten counterpart (0 at%S), a solid I4  
170  $\text{Fe}_3\text{S}$  structure (64 atoms) and its molten counterpart (25 at%S) and two liquid alloys with  
171 intermediate compositions of 9.4 at%S and 17.2 at%S (64 atoms each). All calculations besides the one  
172 for pure liquid iron have been carried out at 60 GPa and 3000 K. In the case of pure liquid iron we have  
173 carried out calculations at a higher temperature of 6000 K due to the fact that at this pressure of 60  
174 GPa and 3000 K, the most stable phase of iron is still the solid hcp structure and not a molten system,  
175 as shown by previous phase diagram calculations (Alfé et al., 2002). In order to understand the effect  
176 of temperature on force constants and isotope fractionation factors, we have run an extra AIMD  
177 calculation of solid hcp Fe at 300 K.

178 Additional to the AIMD calculations mentioned above, we have also carried out zero-temperature  
179 structural optimizations of the two crystalline systems, to estimate the  $^{56/54}\text{Fe}$  equilibrium isotope  
180 fractionation factor from vibrational properties using the harmonic approximation through equation  
181 (2). We estimated vibrational frequencies by using first the perturbation theory method as  
182 implemented in VASP to obtain the dynamical matrix. Then, force constants and vibrational  
183 frequencies have been post-processed using the PHONOPY code (Togo and Tanaka, 2015). Phonon  
184 frequencies are given by the eigenvalues of the dynamical matrix. The  $k$ -point for total energy  
185 convergence as well as the  $q$ -mesh used to obtain convergence of vibrational properties used in this  
186 work can be found in Table 1. Using these parameters, frequencies and  $\beta$ -factors are converged to  
187  $0.001 \text{ cm}^{-1}$  and  $0.0001 \text{ ‰}$  respectively. Additionally, we have produced solid solutions at similar  
188 concentration as the two liquid alloys discussed above using the solid solution method reported by  
189 D'Arco et al. (2013); Mustapha et al. (2013). The structures of these solid solutions were found to be  
190 dynamically non-stable and therefore their isotope fractionation factors are not reported in this work.  
191 It should also be noted that we have found magnetic effects to be non-relevant at the studied pressure  
192 and temperature conditions and therefore have not been taken into account in this work (See Valencia  
193 et al. (2020)).

194 Keeping in mind these methodological part, we can now outline the four different methods used in this  
195 work to estimate  $\beta$ -factors and explain the limitations and advantages of each one of them. Firstly, the  
196 trajectories obtained from finite-temperature AIMD calculations have been used to obtain the velocity  
197 auto-correlation function (VCF) and subsequently, the partial density of states (pDOS) using equation  
198 (6). One limitation of the pDOS method lies on the length of the trajectory used to obtain meaningful  
199 results given that the noise in the velocity auto-correlation function increases with the length of the  
200 time interval and could lead to non-converged pDOS spectra. In this work, the reported pDOS are  
201 obtained as an average of several 6 ps trajectories (at least 5 trajectories) obtained over a longer MD  
202 trajectory. We have estimated the kinetic energy and subsequently the  $\beta$ -factor using equations 4 and

203 3 respectively. In this method, the interatomic force constant can also be retrieved from the pDOS,  
204 using the following equation (e.g. Dauphas et al. 2012):

$$205 \quad \langle F \rangle = \frac{m}{\hbar^2} \int_0^{+\infty} g(v) v^2 dv \quad (7)$$

206 This method has the advantage to include anharmonic effects as well as configurational disorder, of  
207 relevance in the case of liquid systems. We will refer to this method as the “pDOS-melt” results.  
208 Furthermore, we have used the same pDOS methodology applied to Fe-hcp and Fe<sub>3</sub>S-I4 crystalline  
209 systems with AIMD calculations performed at 300 K and 60 GPa. The  $\beta$ -factors obtained through this  
210 method will be presented as the “pDOS-solid” results.

211 Using the snapshots from the same AIMD trajectories of the molten systems, we have performed zero-  
212 temperature constant-pressure optimisations of the atomic positions in order to minimise the total  
213 energy. Following this, we have used the relaxed configurations to calculate vibrational properties and  
214 estimate the  $\beta$ -factor using equation 2. This method is similar to the one presented in previous works  
215 by Pinilla et al. (2015) and results obtained from this method will be referred as the “RELAX” results.  
216 In the “RELAX-melt” method the obtained snapshots can be seen as those resembling a glassy system  
217 obtained through rapid quenching and characterised by structural disorder but where bond distance  
218 distribution has been evened out due to optimization of atomic positions. Finally, in the case of  
219 crystalline Fe-hcp and Fe<sub>3</sub>S-I4, we have calculated the vibrational properties within the harmonic  
220 approximation from the optimised structure at zero temperature and used equation 2 to obtain the  $\beta$ -  
221 factor. Results from these calculations will be known as “RELAX-solid” results. It should be noted that  
222 in the case of solid structures, the RELAX-melt method (i.e., AIMD at finite temperature followed by  
223 zero-temperature relaxations) converges to the same results as the RELAX-solid method (i.e., direct  
224 zero-temperature structural relaxation). A summary of the methods used in the present study can be  
225 found in Table 2.

226

## 227 3. RESULTS AND DISCUSSION

### 228 3.1 Iron and sulfur kinetic energies

229 To determine the kinetic energy for Fe and S atoms we calculated the velocity auto-correlation  
230 function (VCF) for all the studied systems as shown in Figure 1. In the case of liquid alloys, the typical  
231 behaviour for dense liquids was observed, with an intermediate negative region produced by atomic  
232 collision and a subsequent rise before oscillating around a zero correlation (Hansen and McDonald,  
233 2005). The fact that the positive part of the VCF is larger than the negative one describes a system with  
234 net diffusion, opposite to what is seen in the case of solids. The corresponding pDOS are also displayed  
235 in Figure 1. It is interesting to note that in the case of solids the pDOS has a zero value at zero  
236 frequency. At low frequency (long times) the pDOS of solids should follow a quadratic trend just like  
237 the one described by the Debye model for the long wavelength limit (Hansen and McDonald, 2005)  
238 and corresponding to acoustic vibrational modes. This is different from what is seen in the case of  
239 liquids where diffusive effects lead to a net pDOS value at zero frequency. Additionally, in the case of  
240 solids we have also displayed pDOS from zero-temperature vibrational frequencies to show the effect  
241 of temperature producing a broader spectrum.

242

243 Using the pDOS we have determined the kinetic energy via equation 4. Figure 2 shows the iron kinetic  
244 energy as a function of temperature for some of the studied systems. We note the large error bars  
245 reported in these results, where kinetic energies for liquid and solid system are close. However, we  
246 observe in details, systematic trends. Fe atoms have a slightly smaller kinetic energy than S atoms with  
247 a  $K_S - K_{Fe} = 0.8$  meV for solid Fe<sub>3</sub>S at 300 K and 60 GPa. An Fe atom in pure solid Fe hcp lattice has an  
248 average kinetic energy  $K_{Fe-solid} = 43.4$  meV at 300 K whereas a similar atom in a Fe<sub>3</sub>S structure has a  
249  $K_{Fe3S-solid} = 44.2$  meV. This difference complies with the fact that the Fe-S bond has a more covalent  
250 nature thus producing a stronger bond than a pure metallic Fe-Fe bond. This conclusion could also be  
251 extended to liquids but with a smaller magnitude. Similar behaviour has been also reported by Morard

252 et al. (2008) in the case of Fe-S-Si liquid alloys. Overall, the Fe kinetic energy of  $\text{Fe}_{1-x}\text{S}_x$  alloys tends to  
253 be slightly higher than those based on pure Fe. Furthermore, the kinetic energy of an Fe atom in a  
254 solid, liquid and gas phase of these alloys is different due to the bond nature, but the trends are not the  
255 same depending on the composition investigated. All systems possess a larger kinetic energy than that  
256 for a free Fe atom ( $3k_B T/2$ ) = 38.7 meV/atom at 300 K, but in the case of pure Fe, the solid has a lower  
257 kinetic energy than that found for the liquid phase, whereas, this effect is reverted in the case of the  
258  $\text{Fe}_3\text{S}$  system. Finally, we can observe that the kinetic energy difference decreases as temperature  
259 increases, leading to a constant value due to the increase of diffusive-like contributions.

260

### 261 **3.2 Iron $\beta$ -factors from solid and molten alloys**

262

263 The  $^{56}\text{Fe}/^{54}\text{Fe}$  reduced partition function ratios ( $\beta$ -factors) obtained from all methods described in  
264 Table 2 are shown in Figure 3. A further insight into our results can be obtained from the iron force  
265 constants displayed in Table 3. We need to differentiate the results estimated from calculations at zero  
266 temperature (RELAX-melt and RELAX-solid methods) from those at finite temperature (pDOS-melt  
267 and pDOS-solid methods). At 3000 K,  $\beta$ -factors from the later methods seem to be  $\approx 0.02$  ‰ lower  
268 than the  $\beta$ -factors from the former one (Fig. 3). Consistently, force constants from pDOS calculations  
269 (pDOS-melt and pDOS-solid) are  $\sim 100$  N/m smaller than those from frequency methods (RELAX-melt  
270 and RELAX-solid) (Table 3). This difference is found to be related to shorter Fe-Fe and Fe-S bonds at  
271 zero temperature as well as to the truncation in the kinetic energy integral to a certain maximum  
272 cutoff value of 246 meV (See SI). This truncation procedure is much on the lines to what is done for  
273 NRIXS experiments (Dauphas et al., 2012).

274 If we now compare solid, glass and liquid results, we can make several observations. For both Fe and  
275  $\text{Fe}_3\text{S}$  compositions, RELAX-melt and RELAX-solid methods present comparable results for the  $\beta$ -factors  
276 (Fig. 3) or the force constants (Table 3). The RELAX-melt method includes some configurational  
277 disorder like in a glass, even if the distribution of bond distances has been diminished by the

278 optimization of atomic positions. Therefore, these results suggest that the isotopic properties of a glass  
279 system, as that given by the RELAX-melt method, may be equivalent to that of a perfect solid structure.  
280 When dealing with liquid systems taking full account of thermal effects such as in the case of the pDOS  
281 calculations, we see that the  $\beta$ -factors extrapolated at conditions of core formation (3000 K, 60 GPa)  
282 from a liquid Fe simulation run at 6000 K and from a solid simulation run at 300 K are comparable  
283 with  $\beta^{\text{Fe}_{\text{solid}}} - \beta^{\text{Fe}_{\text{liquid}}} \approx 0.02 \text{ ‰}$  at 3000 K. The same conclusion can be drawn for the Fe<sub>3</sub>S composition.  
284 Overall, our results highlight that although configurational disorder is different in all systems, bond  
285 type and local environment are the controlling parameters of this modelling. This shows that  $\beta$ -factors  
286 obtained from solid systems may in principle be used in place of molten ones, with differences not  
287 larger than 0.02 ‰ at conditions of core formation. Hence, we can conclude that crystalline or glassy  
288 iron alloys are good proxies for molten systems for deep Earth studies as has already been done in  
289 several experimental works.

290

291 Finally, we can compare the values of iron force constants calculated for pure Fe-hcp and Fe<sub>3</sub>S using  
292 the RELAX-melt or RELAX-solid methods to the equivalent NRIXS-derived room-temperature values  
293 reported in previous experimental works by Shahar et al. (2016) and Liu et al. (2017). Calculated and  
294 experimental values are all in good agreement with the largest difference between these values of  
295 about 10% for the pure Fe system (Table 3). It is noteworthy that there are no data for solid alloys at S  
296 concentrations of 5.6 and 10.6 wt% because these solid alloys were found to be dynamically unstable  
297 under the pressure used.

298

### 299 **3.3. Thermal extrapolation of the $\beta$ -factor**

300 The temperature dependence of the  $\beta$ -factor for zero-temperature calculations (RELAX-solid and  
301 RELAX-melt methods) and finite temperature MD simulations (pDOS-solid and pDOS-melt methods)  
302 has been determined using equations 2 and 3 respectively. The procedure of using vibrational  
303 frequencies or the partial density of states obtained at a given temperature to extrapolate the

304 functional behaviour of  $\beta$ -factors to other temperatures is a widely used approach both in theory and  
305 experimental analysis, but can be prone to errors. Here we assess the validity of such procedure by  
306 comparing the  $\beta$ -factors obtained using the pDOS method from AIMD simulations performed at several  
307 temperatures (3000 K, 4000 K, 5000 K, 6000 K and 7000 K) with the values obtained using an  
308 extrapolation procedure (Fig. 4). Our results show that the data extrapolation from a simulation at  
309 3000 K toward higher temperatures is perfectly valid. On the other hand, the data extrapolation  
310 towards 3000 K from simulations performed at higher temperature (4000-7000 K) lead to small  
311 uncertainties. Extrapolated values oscillate from one simulation temperature to the other but globally  
312 these oscillations do not exceed the error bar already calculated for the pDOS-melt method (about  
313  $\pm 0.01$  % at 3000 K, Fig. 4). More critical is the linear extrapolation up to 3000 K of the pDOS-solid  
314 simulation run at 300 K. In order to assess the validity of this extrapolation, we ran an overheated Fe-  
315 hcp structure at 60 GPa and 3000 K. This simulation leads to a  $\beta$ -factor close to the melt one at the  
316 same conditions, suggesting that this extrapolation overestimates the force constant by about 30 N/m  
317 (Fig. 4b) and the  $\beta$ -factor by about 0.01 % (Fig. 4a). Data for pDOS-solid displayed in Figure 6 as well  
318 as Tables 3 and 4 have been corrected to account for this overestimation.

319 Overall, our results suggest that the force constant determined by spectroscopic analysis at room  
320 temperature will be overestimated by 30 N/m when discussing implications at conditions near the  
321 3000 K. This overestimation is of the same order of magnitude as error bars reported in spectroscopic  
322 methods (Dauphas et al., 2012; Roskosz et al., 2015). Therefore, these results warn on the use of solids  
323 as proxies for high-temperature liquids and make this approximation acceptable for a range of  
324 temperatures between 1000-2000 K. It is important to say that the behaviour observed here for the  
325 force constant as a function of temperature is true at the high-pressure regime where this work has  
326 been carried out. However, we expect a more significant correction at low pressures where vibrational  
327 effects, thermal expansion and even magnetic effects might be more pronounced.

328

### 329 **3.4. Correcting for fluidicity effects on estimated $\beta$ -factors**



330 The pDOS methodology described above has been widely used for the NRIXS-based and static  
 331 computation study of isotope fractionation properties in crystalline systems where the harmonic  
 332 approximation is most of the time a good assumption (Bourdon et al., 2018; Dauphas et al., 2018).  
 333 However, a direct extension to liquids may not be appropriate since entropy and fluidicity effects are  
 334 dominated by low-frequency modes. In particular, the pDOS of liquids has a non-zero value at zero  
 335 frequency, which corresponds to the diffusion mode (Fig 1).

336 To assess the effect of fluidicity on the calculated  $\beta$ -factors we have used the two phase approach  
 337 proposed by Lin et al. (2003) and Lin et al. (2010) in which the partial density of states ( $g(\nu)$ ) of a  
 338 system with  $3N$  degrees of freedom can be partitioned into a gas- and a solid-like component:

$$339 \quad g(\nu) = g^g(\nu) + g^s(\nu), \quad (8)$$

340 where the gas-like diffusive component  $g^g(\nu)$  corresponds to  $3N^g = 3fN$  degrees of freedom with  $f$   
 341 being the gas fraction. The remainder,  $g^s(\nu)$ , describes a non-diffuse system in which  $g^s(0) = 0$  (i.e.  
 342 no diffusion). Thus, the degrees of freedom from the system that behaves in a solid-like way are  $3N^s =$   
 343  $3N(1-f)$ .

344 In order to estimate the solid-like density of states, it is necessary to define the gas-like diffusive  
 345 component  $g^g(\nu)$  and the gas fraction  $f$ . In their original paper, Lin et al. (2003) approximate  $g^g(\nu)$  to  
 346 that of a hard sphere fluid defined as:

$$347 \quad g^g(\nu) = \frac{s_0}{1 + \left[ \frac{\pi s_0 \nu}{6fN} \right]^2}, \quad (9)$$

348 where  $s_0$  is the original  $g(\nu)$  zero-frequency value. Likewise, the gas fraction,  $f$ , can be written as

$$349 \quad 2\Delta^{-9/2} f^{15/2} - 6\Delta^{-3} f^5 - \Delta^{-3/2} f^7 + 6\Delta^{-3/2} f^5 + 2f - 2 = 0, \quad (10)$$

350 where

$$351 \quad \Delta(T, \rho, m, s_0) = \frac{2s_0}{9N} \left( \frac{\pi k_B T}{m} \right)^{1/2} \rho^{1/3} \left( \frac{6}{\pi} \right)^{2/3} \quad (11)$$

352 with  $m$  the mass of the particles and  $\rho = N/V$ , the density.  $\Delta$  is a function of the studied alloy. Note that  
 353 through MD calculations, the obtained value  $s_0$  determines  $\Delta$  and subsequently  $g^g(\nu)$  and the gas

354 fraction also called fluidicity factor  $f$ . In this way, any thermodynamic property can be estimated as a  
355 sum of gas and solid contributions.

356 The respective decompositions at conditions of the core formation can be seen in Figure 5. Results  
357 show that the pDOS for a gas decays rapidly and monotonically as frequency increases. This behaviour  
358 is expected since in gases usually the mean free path is larger than the particle diameter. In the case of  
359 a solid-like system, and as shown earlier, the velocity auto-correlation function oscillates around zero  
360 with amplitudes decreasing as time increases. In a single particle system oscillating under a harmonic  
361 potential, this oscillation can be fitted to a cosine function and the  $g^S(\nu)$  resembles a Dirac delta. In the  
362 case of a solid the  $g^S(\nu)$  has several peaks reflecting the ordered nature of crystal structures.  
363 Furthermore, the values of the fluidicity factor  $f$  increases as a function of temperature showing how  
364 the diffusive character of the alloy increases with temperature (Fig. 5c). We have used these results to  
365 estimate the  $\beta$ -factor corrected for fluidicity effects in the case of Fe and Fe<sub>3</sub>S melts. Results are  
366 reported in figure 6. The results with or without fluidicity correction are similar with  $\beta$ -factors  
367 differing by less than 0.01 ‰ among them. Therefore, fluidicity effects present in the pDOS are not  
368 relevant when estimating the equilibrium fractionation factor of Fe in liquid Fe<sub>x-1</sub>S<sub>x</sub> alloys.

369

370

### 371 **3.5. Effect of S concentration on Fe $\beta$ -factor**

372

373 In order to evaluate the effect of S on the iron  $\beta$ -factor we have performed calculations on four systems  
374 with S concentrations ranging from 0.0 to 25 at% (Fig. 6). As already mentioned in part 3.2, results  
375 from zero-temperature methods (RELAX-melt and RELAX-solid) must be discussed separately from  
376 pDOS-based methods. Overall, all methods show a small variation of  $\beta$ -factors (i.e. not larger than 0.02  
377 ‰) over the whole S concentration range. However, calculations show subtle trends where the Fe  $\beta$ -  
378 factor changes continuously with S concentration (see green and black lines in Fig. 6). In addition, the  
379 change seems to be different for the case of crystalline and non-crystalline systems (Figs. 3 and 6). In

380 the case of crystalline systems (RELAX-solid and pDOS-solid results) we see the  $\beta$ -factor for pure Fe-  
381 hcp to be larger than those of Fe<sub>3</sub>S-I4. The same trend is observed for the force constants (Table 3).  
382 Conversely, pDOS-melt and RELAX-melt results show the opposite behaviour where  $\beta$ -factors and  
383 force constants increase with S content. However, we note here that experimental uncertainties likely  
384 exceed these differences calculated here for P-T conditions relevant to the Earth's core formation.

385 The fact that  $\beta$ -factors and force constants depend on concentration in the case of Fe<sub>1-x</sub>S<sub>x</sub> alloys can be  
386 understood from the local structural and chemical environment described through the coordination  
387 number and bond lengths (Smith, 1956). Therefore, we have derived the partial radial distribution  
388 functions and coordination numbers as a function of S content for solid and liquid systems (Fig. 7). In  
389 the case of molten alloys, we see that sulphur shows some covalent bonding with iron in the first shell,  
390 creating shorter Fe-S bonds and increasing slightly the length of the remaining Fe-Fe bonds. Indeed,  
391 Figure 7c clearly shows that the Fe-Fe coordination number (CN<sup>Fe-Fe</sup>) goes from 13.4 at 0 at%S to 9.8 at  
392 25 at%S, showing a decrease in the number of Fe atoms surrounding another Fe atom. Likewise, the  
393 Fe-S coordination number increases from 0.0 in absence of sulphur to 3.1 at 25 at%S. By adding the  
394 Fe-Fe and Fe-S coordination numbers together, we see that the total number of atoms surrounding a  
395 Fe atom in molten systems is fairly constant through all the S concentration range, suggesting that S  
396 atoms substitute readily for Fe atoms within the melt. Therefore, the nearly constant total  
397 coordination number and the increase in the number of shorter Fe-S bonds with sulphur  
398 concentration lead to an increase of  $\beta$ -factors and force constants for all molten alloys. In contrast, in  
399 crystalline systems, atoms are more localized around their equilibrium position and as a result, bond  
400 length distributions tend to be narrower than in melts, as seen in figure 7. Additionally, Fe<sub>3</sub>S-I4  
401 displays an average Fe-Fe distance significantly larger (+6%) than in Fe-hcp (Fig. 7) while the total  
402 coordination number remains nearly the same. This observation explains why crystalline Fe<sub>3</sub>S  
403 presents a smaller  $\beta$ -factor and force constant than Fe-hcp.

404 A closer look at Fe<sub>3</sub>S-I4 shows that this structure has three distinct Fe crystallographic sites: FeI, FeII  
405 and FeIII whose  $\beta$ -factors are 0.094, 0.103, 0.117 %<sub>0</sub> at 60 GPa and 3000 K respectively. The first

406 coordination shell of the FeI site displays 12 Fe atoms (average distance  $d_{\text{FeI-Fe}}=2.44 \text{ \AA}$ ) and 2 S atoms  
407 (average distance  $d_{\text{FeI-S}}=2.08 \text{ \AA}$ ). FeII site is surrounded by 10 Fe atoms ( $d_{\text{FeII-Fe}}=2.40 \text{ \AA}$ ) and 4 S atoms  
408 ( $d_{\text{FeII-S}}=2.14 \text{ \AA}$ ) while FeIII site is surrounded by 10 Fe atoms ( $d_{\text{FeIII-Fe}}=2.38 \text{ \AA}$ ) and 3 S atoms ( $d_{\text{FeIII-}}$   
409  $s=2.13 \text{ \AA}$ ). Iron in site III has the highest  $\beta$ -factor because its total coordination number is the lowest  
410 (13) and is dominated by iron with the shortest Fe-Fe bonds. Between sites I and II, displaying the  
411 same total coordination number of 14, iron in site II has the highest  $\beta$ -factor in relation to a larger  
412 number of S neighbours and a shorter average bond length.  
413 Results thus suggest that the small changes seen in the force constants and  $\beta$ -factors when S  
414 concentration increases in  $\text{Fe}_{1-x}\text{S}_x$  alloys are mainly due to a combination of attenuated structural  
415 changes related to atomic coordination and bond stiffness. The geochemical implications and possible  
416 reappraisals of existing experimental data related to these small variations are discussed below.

417

### 418 **3.6. Implications in the context of terrestrial core formation**

419 Our theoretical calculations alleviate a number of controversies and speculations in the field of HP-HT  
420 behaviour of Fe isotopes in solid and liquid alloys. To a certain extent, these conclusions likely hold for  
421 other isotopic systems.

422 First of all, it is commonly proposed that solids and glasses could be considered as representative of  
423 molten counterparts as a first approximation (Liu et al., 2017; Shahar et al., 2016; Yang et al., 2019).  
424 This was obviously proposed for lack of better alternatives. For pure iron, the simple close-packed  
425 structure of liquids, the similarities between density and compressibility relative to its solid phase  
426 under core conditions made this assumption reasonable (Laio et al., 2000). Similar assumptions were  
427 also made for silicates for which structural data also indicates strong similarities between glasses and  
428 melts at the local scale (Dauphas et al., 2014; Mysen and Pascal, 2005; Sanloup et al., 2013). Our results  
429 demonstrate, in the case of pure iron and iron sulphides that this assumption holds at least in the high  
430 pressure and temperature conditions prevailing during the Earth's core formation.

431 Second, another common assumption made to extrapolate experimental spectroscopic results to  
432 planetary conditions (Liu et al., 2017; Shahar et al., 2016; Yang et al., 2019) or, conversely to try to  
433 explain flagrant inconsistencies between spectroscopic and experimental results (Shahar and Young,  
434 2020) focusses on the validity of harmonic approximations. Anharmonicity must indeed be present at  
435 some level as it is the mechanism responsible for thermal expansion, which is present in geological  
436 materials. For example, the volume of forsterite expands by 8% when the temperature is increased  
437 from 300 to 2300 K (Bouhifd et al., 1996) and no expansion would be present if the bonds were  
438 perfectly harmonic. If the bonds were perfectly harmonic, then the force constant of those bonds  
439 should not vary with temperature. Conversely, anharmonicity in interatomic potentials would be  
440 manifested as an apparent variation of the force constant of the iron bonds as temperature changes.  
441 Our results show such a variation (Fig. 4b). The Fe force constant decreases from 288 N/m at 300 K to  
442 262 N/m at 3000 K for solid iron, and the force constant for liquid iron decreases from about 255 N/m  
443 at 3000 K to 238 N/m at 7000 K. However, these variations are of the same order of magnitude as  
444 error bars reported in spectroscopic studies. Consistent results were recently produced in the case of  
445 silicate minerals and glasses (Roskosz et al., in prep.). This is an important result because it  
446 strengthens the use of spectroscopic approach to derive isotopic properties of geomaterials at extreme  
447 conditions. It also highlights one more time the unexplained inconsistency between fractionation  
448 factors derived from experimental petrological experiments (e.g. Shahar et al. (2015) and theoretical  
449 and spectroscopic determinations (Liu et al., 2017; Shahar et al., 2016; Yang et al., 2019). To date this  
450 discrepancy remains unexplained but is clearly beyond the effects related to the anharmonic nature of  
451 metallic materials.

452 Third, these data can be used to describe Fe isotopes distribution within core forming materials during  
453 its crystallization. At the studied conditions (60 GPa and 3000 K), our calculations suggest that no  
454 measurable fractionation should be produced between liquids and solids even if incongruent  
455 crystallisation of a Fe-S molten alloy is considered. The limited amount of light alloying element and Ni  
456 should not change this conclusion since NRIXS measurements performed on solid analogues

457 confirmed that reasonable amounts of these elements could not significantly modify the force  
458 constants of the alloy (Liu et al., 2017; Shahar et al., 2016). Moving to milder conditions, experiments  
459 were recently performed to mimic core formation in planetesimals where pressure and temperature  
460 do not exceed a few GPa and 1600 K. Clearly, extrapolations of our calculations to lower temperature  
461 and pressure is limited by phase transitions and no firm conclusion can be drawn in the context of  
462 planetesimal differentiation. Nonetheless, as a first attempt, we have compared our  $\Delta^{56/54}_{solid-liquid}$   
463  $= 10^3(\ln\beta_{solid} - \ln\beta_{liquid})$  results with those recently reported by (Ni et al., 2020) concerning  
464 planetesimal core crystallization (Table 4). We find our results to be about five times smaller than  
465 their reported average value of  $\Delta^{56/54}_{solid-liquid} = 0.09 \pm 0.04$  ‰ at 1573 K for a similar range of S  
466 concentration and much lower pressure. If our predicted very small fractionation is confirmed by  
467 future calculations performed at lower pressure and temperature, then the relatively heavy iron  
468 isotopic signature of iron meteorites could not be explained solely by core crystallization and may  
469 also derive from fractionation associated to processes involved during the exhumation of core  
470 materials.

471

#### 472 4. CONCLUSIONS

473 In this work, we have used computational methods to understand the effect of S on Fe equilibrium  
474 isotope fractionation in  $Fe_{1-x}S_x$  alloys as well as the consequences of using solid metal as proxies of  
475 molten alloys when performing experimental studies. We have shown that although configurational  
476 disorder could be different between these systems, bond type and local environment are the  
477 controlling parameters of Fe isotope fractionation and that  $\beta$ -factors obtained from solid systems may  
478 in principle be used in place of molten ones, with differences not larger than 0.01 ‰ at the high  
479 pressure and temperature conditions investigated here. In addition, while the Fe force constant is  
480 found to decrease with increasing temperature, this consequence of the anharmonicity of the  
481 interatomic bonds remains smaller than the typical error bars of spectroscopically-derived force

482 constants at high pressure. This result makes valid the extrapolation in temperature of such  
483 experimental force constants. Regarding the S concentration effect, we observe changes in Fe  $\beta$ -factor  
484 and force constant much smaller than the estimated error bars even if the subtle and continuous  
485 trends with S concentration can be rationalized by a combination of structural changes related to  
486 atomic coordination and bond stiffness. Our calculations have thus suggested that no measurable  
487 fractionation should be produced between liquid and solid even if incongruent crystallisation of a Fe-S  
488 molten alloy is considered at conditions of the Earth's core formation. However, it is important to note  
489 that the results outlined here for  $\text{Fe}_{1-x}\text{S}_x$  alloys apply to high pressure and high temperature conditions  
490 and that the effect of anharmonicity, S concentration and possibly magnetization on Fe isotopes  
491 behaviour at milder conditions could be larger than what has been found in this work.

492

## 493 **5. ACKNOWLEDGEMENTS**

494 This work was performed using Granado-HPC from the Universidad del Norte, SCARF from the STFC of  
495 the UK, and the HPC resources from CALMIP (Grant 2020 – P1037). The authors acknowledge funding  
496 from COLCIENCIAS (No. 2015-710-51568; Contract No. 023-2016) and ECOSNORD (C17U01, No.  
497 FP44842-143-2017) through research grants.

498

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## Figure captions

**Figure 1.** Calculated velocity correlation function (right) and partial density of states (left) for different molten alloys (top) and solid crystalline systems (bottom). For solid systems, the pDOS were also calculated from zero-temperature vibrational frequencies (violet curves).

**Figure 2.** Iron kinetic energy difference as a function of temperature for the studied solid and liquid systems at 60 GPa. The difference has been taken with respect to the kinetic energy per atom of an ideal gas ( $3k_B T/2$ ). The inset is a closeup of the kinetic energy for the region between 3000K and 6000K.

**Figure 3.**  $^{56/54}\text{Fe}$   $\beta$ -factor in pure Fe and  $\text{Fe}_3\text{S}$  liquid and solid systems estimated using the RELAX-solid (blue circles) and RELAX-melt (green diamonds) methods, and the integration of the pDOS for a liquid (black squares) and solid (red triangles) system. Dashed lines correspond to results from NRIXS experiments reported by Liu et al. (2017).

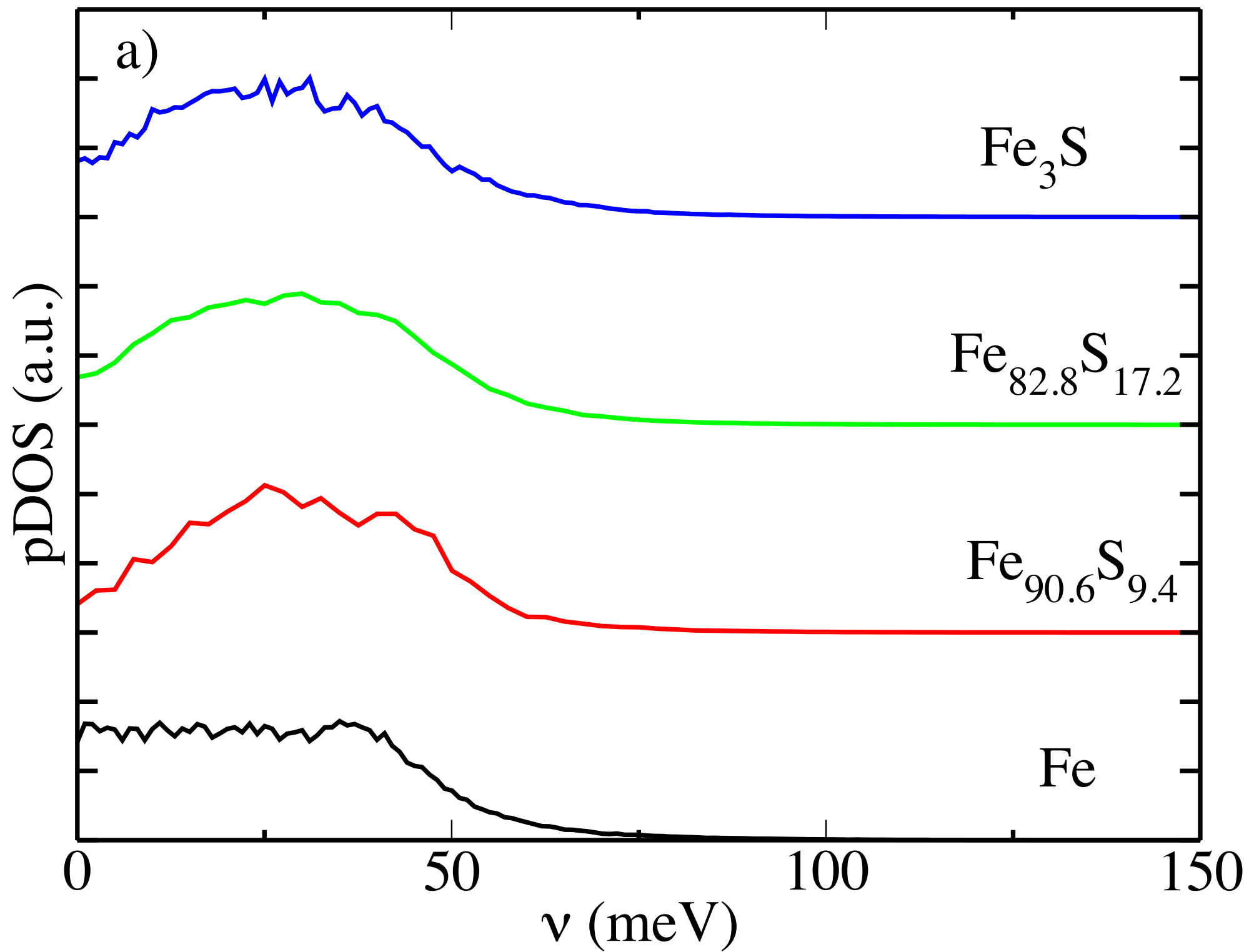
**Figure 4.** a) Temperature dependence of the Fe  $\beta$ -factor estimated using the pDOS-melt method. Colour-circles show values from independent AIMD simulations performed at 3000, 4000, 5000, 6000 and 7000 K. Solid lines correspond to temperature dependences estimated from a single simulation performed at the displayed temperatures, and then extrapolated to other temperatures. Violet dashed line corresponds to results from the pDOS-solid method for Fe-hcp run at 300 K and extrapolated at higher temperatures. b) Fe force constant as a function of temperature in liquid iron (pDOS-melt method). Violet-dotted line and blue-dashed line correspond to values obtained from pDOS-solid at 300 K and 3000 K respectively.

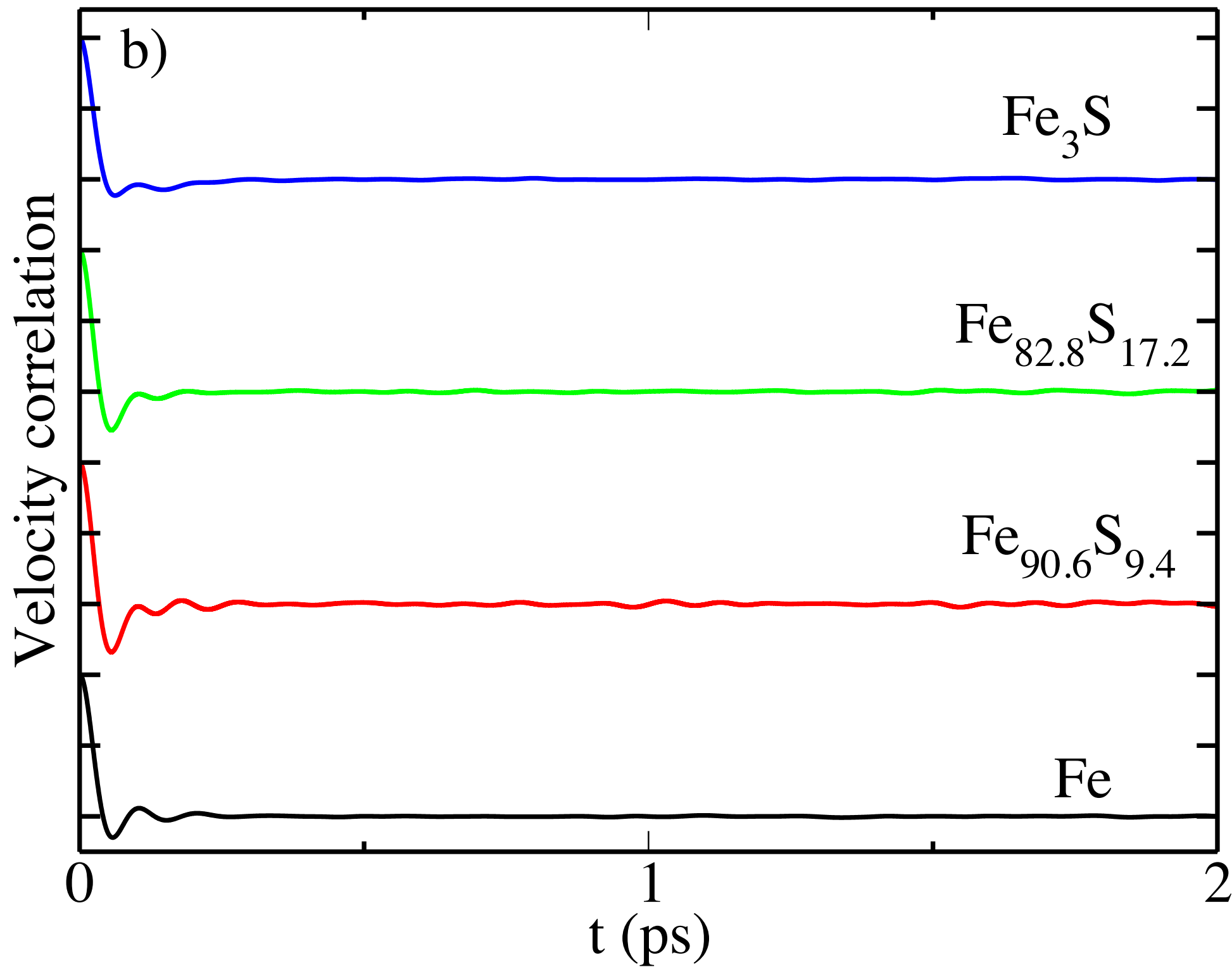
**Figure 5.** Partial density of states for a) pure iron at 6000 K and b)  $\text{Fe}_3\text{S}$  at 3000 K, both at 60 GPa. Black-solid line represents total pDOS, dashed and dash-dotted lines are the solid and gas contributions respectively. c) fluidicity factor  $f$  as a function of temperature for the pure iron system.

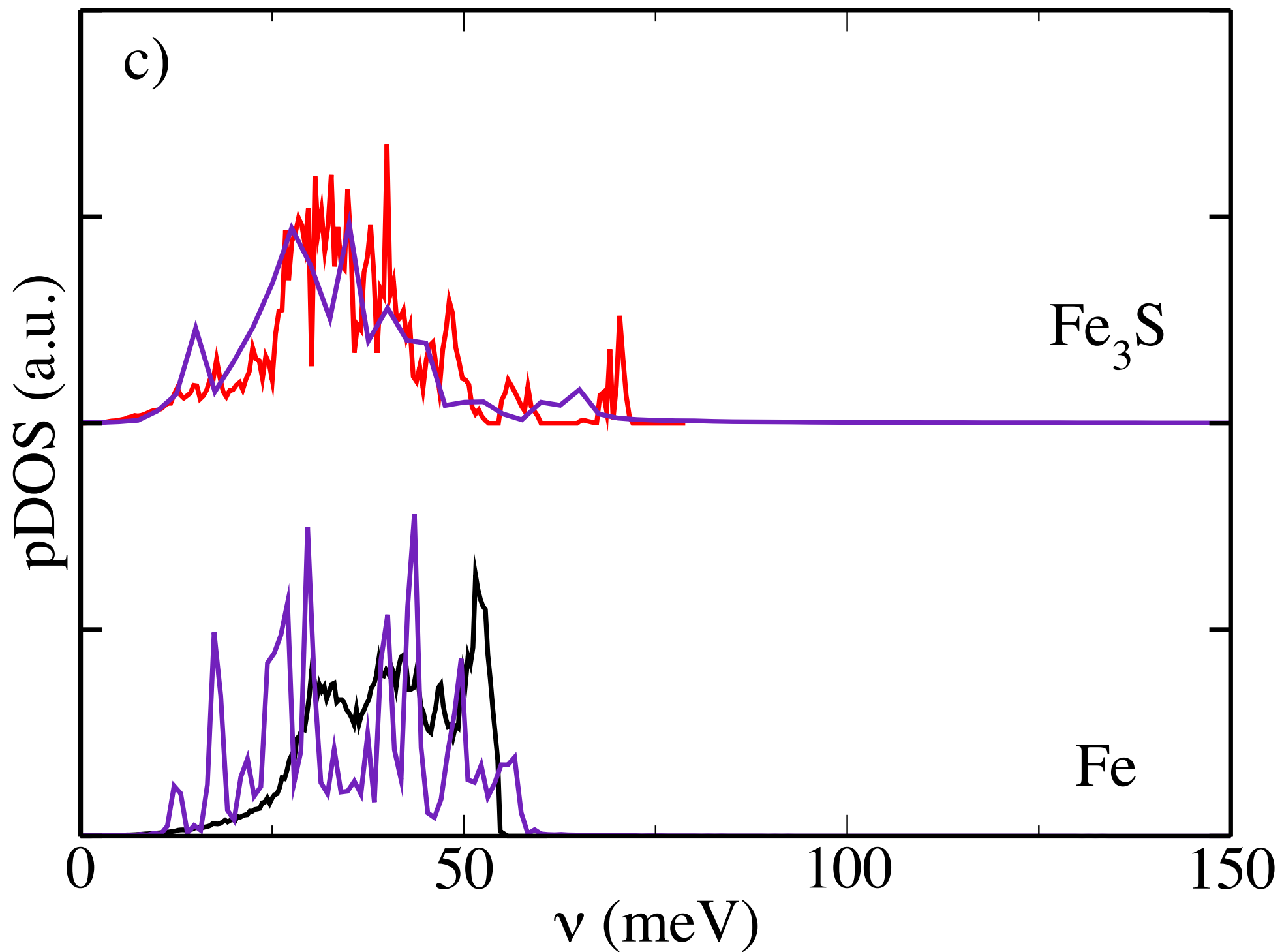
**Figure 6.**  $^{56/54}\text{Fe}$   $\beta$ -factor as a function of S concentration at 60 GPa and 3000 K using different calculation methods. In addition to the four standard methods summarized in Table 2, “pDOS decomp.” corresponds to the pDOS-melt result corrected for fluidicity effects (cf. section 3.5). Experimental results from Shahar et al. (2016) and Liu et al. (2017) are shown for comparison. The small panel on the right hand side corresponds to a zoom up of results obtained at 0 and 25 at% and is displayed to facilitate the reading of the reported values.

**Figure 7.** Structural properties for molten  $\text{Fe}_{1-x}\text{S}_x$  alloys. a) and b) panels correspond to Fe-Fe and Fe-S radial distribution functions respectively for various S concentrations. Dotted and Dashed-dotted lines are values for crystalline Fe-hcp and  $\text{Fe}_3\text{S}$ -I4 at 300K. c) Fe-Fe (black dots)

and Fe-S (red squares) coordination numbers as a function of S concentration. Green line shows the total coordination number for any concentration. Blue values correspond to coordination numbers for Fe-hcp and Fe<sub>3</sub>S-14 crystalline structures.







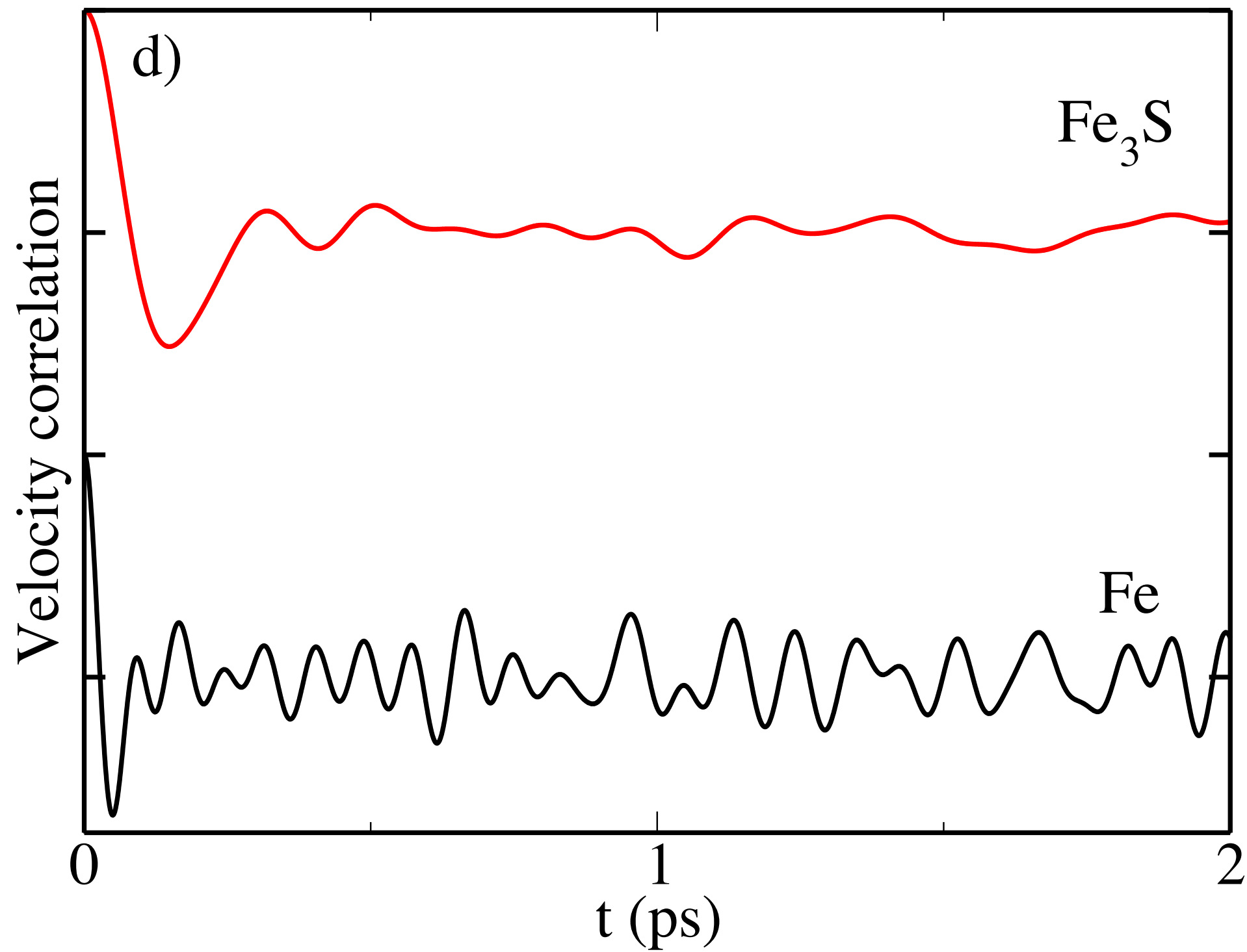
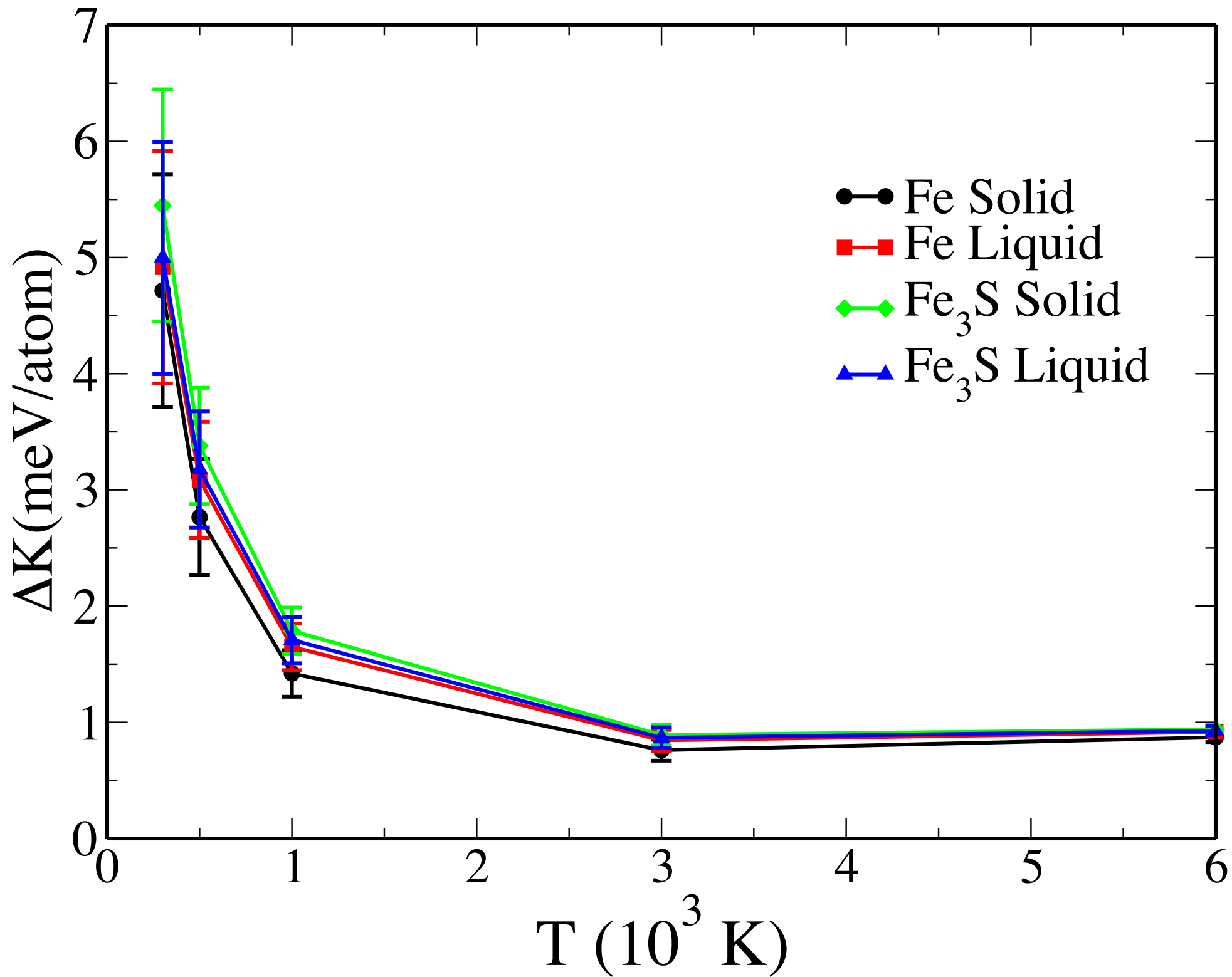
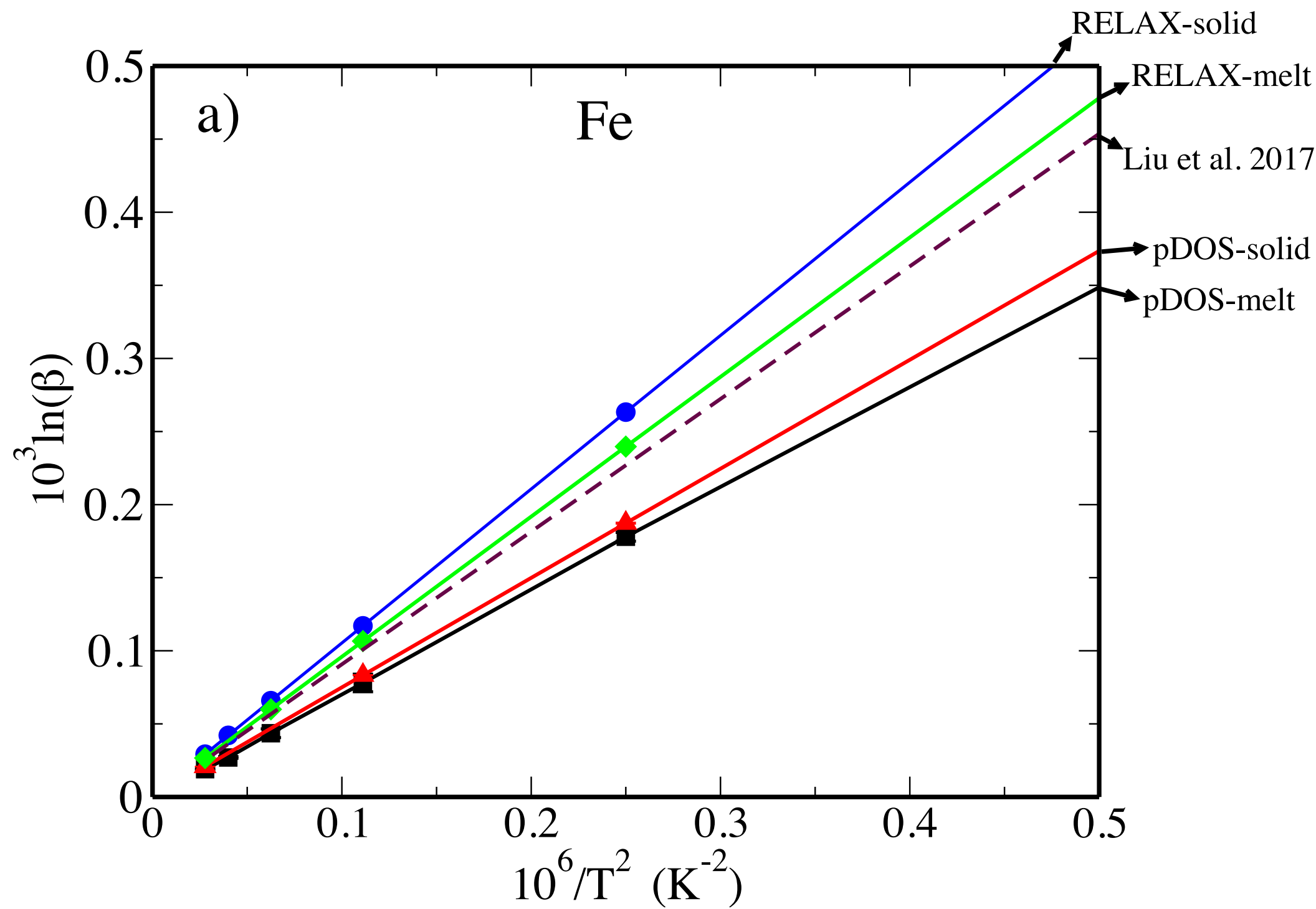




Figure 2





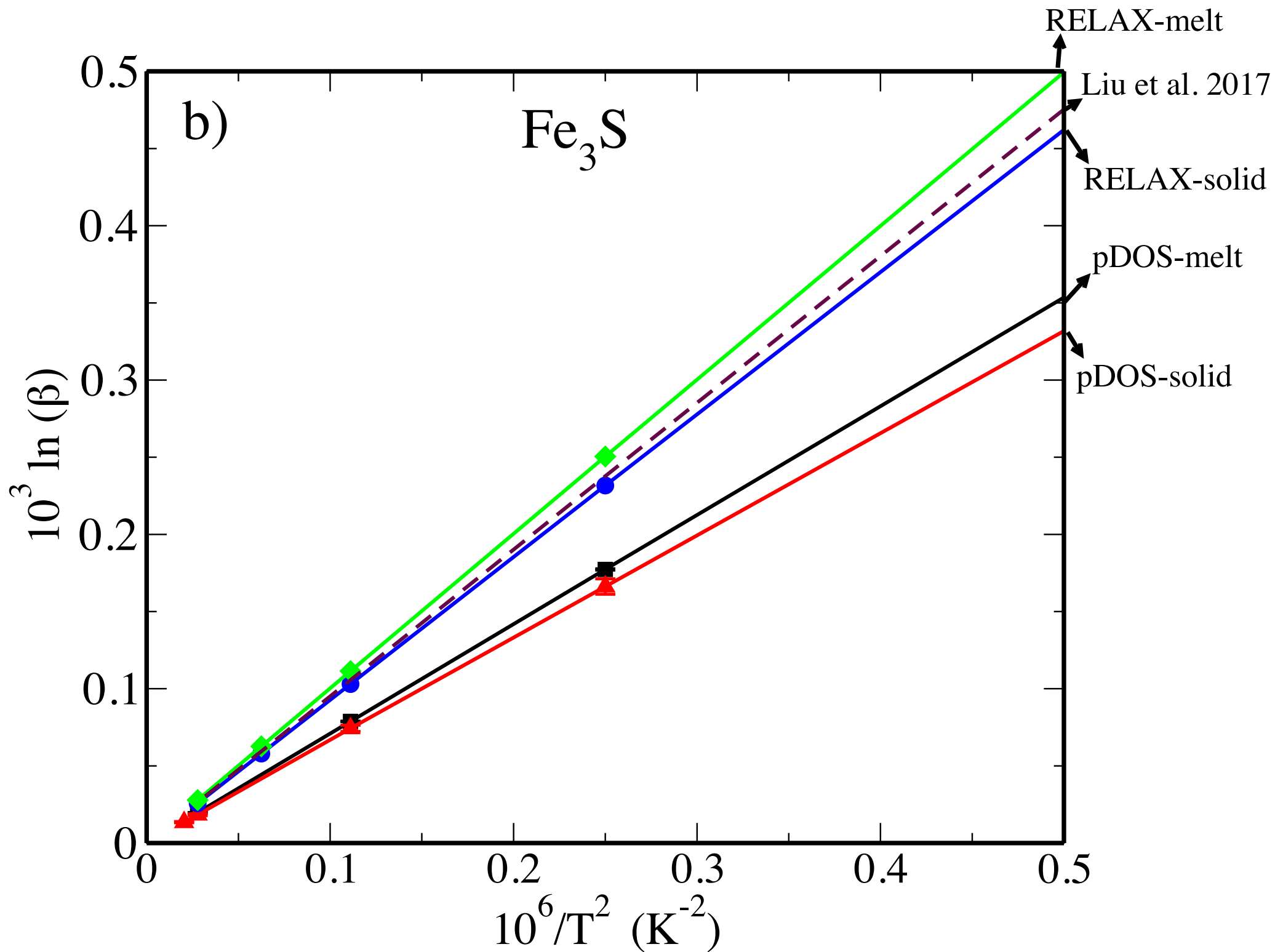
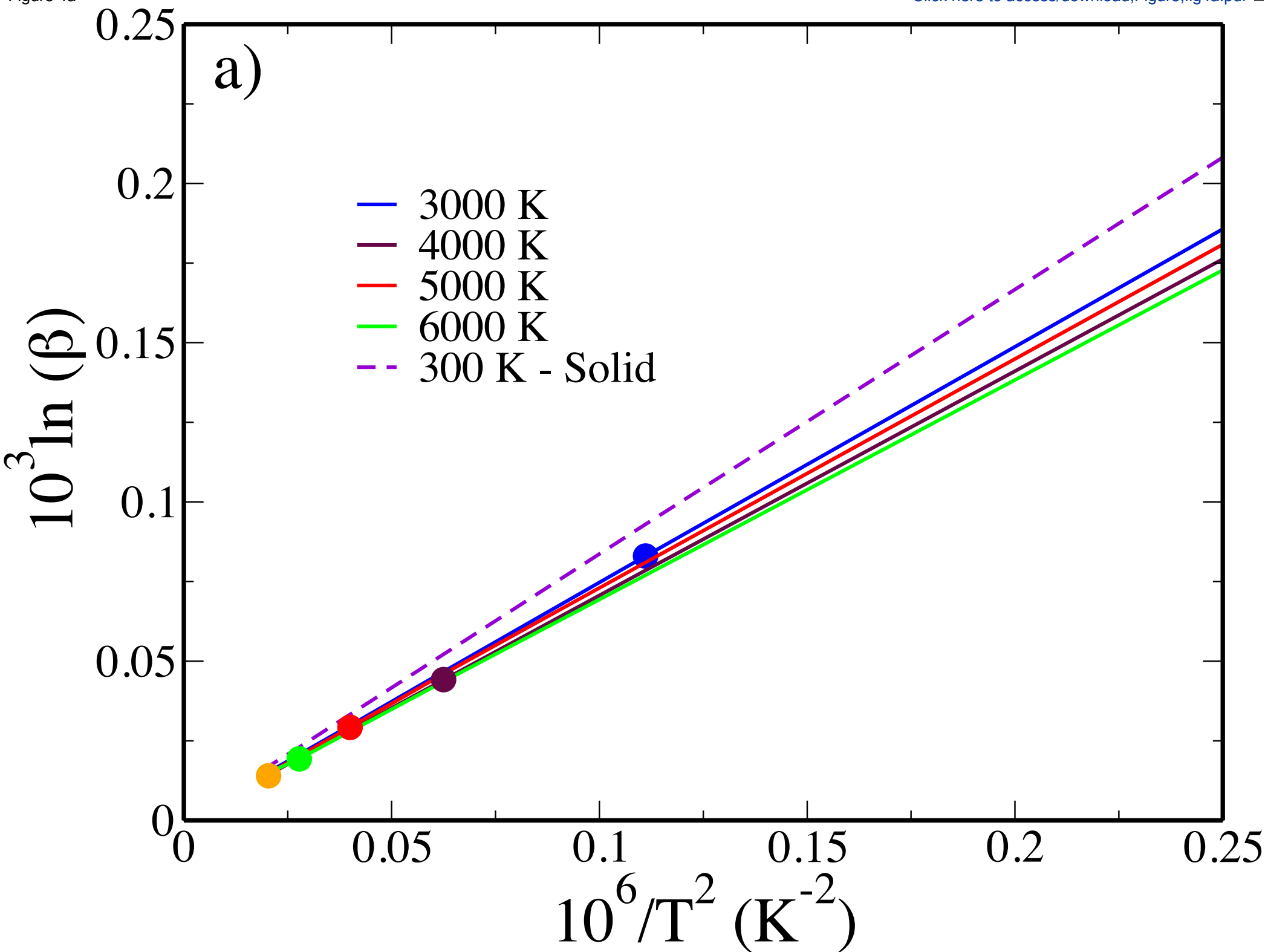
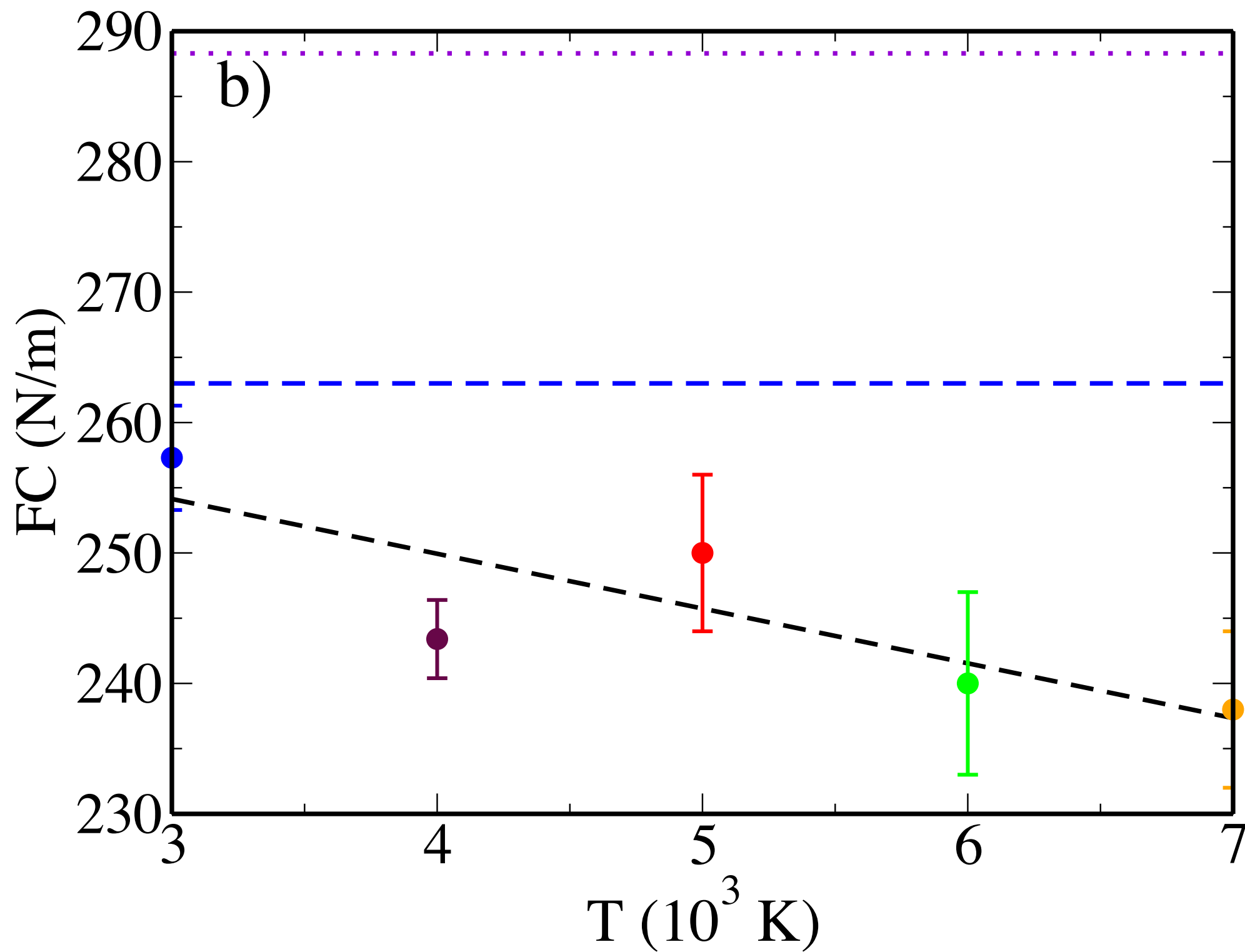
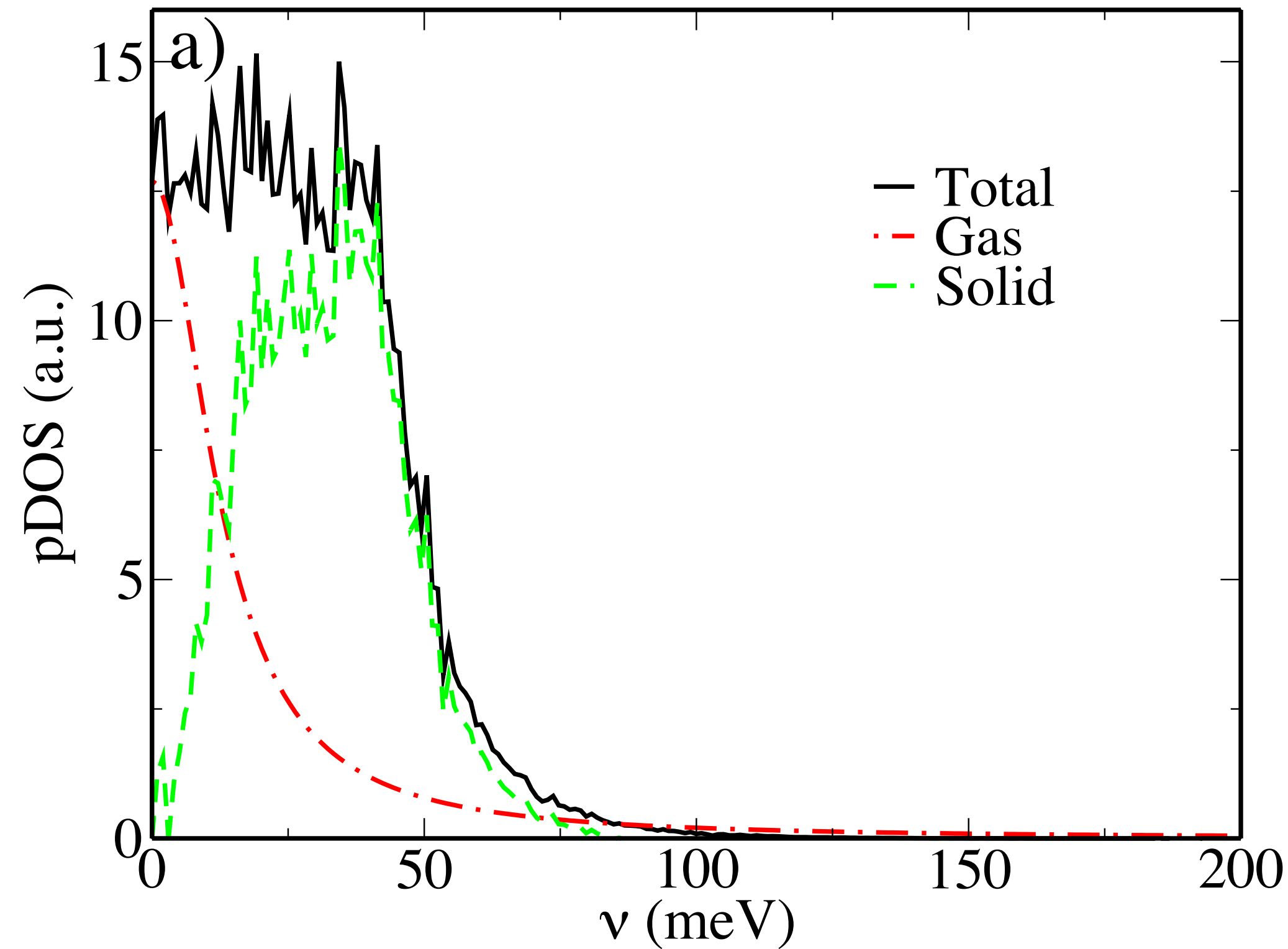


Figure 4a







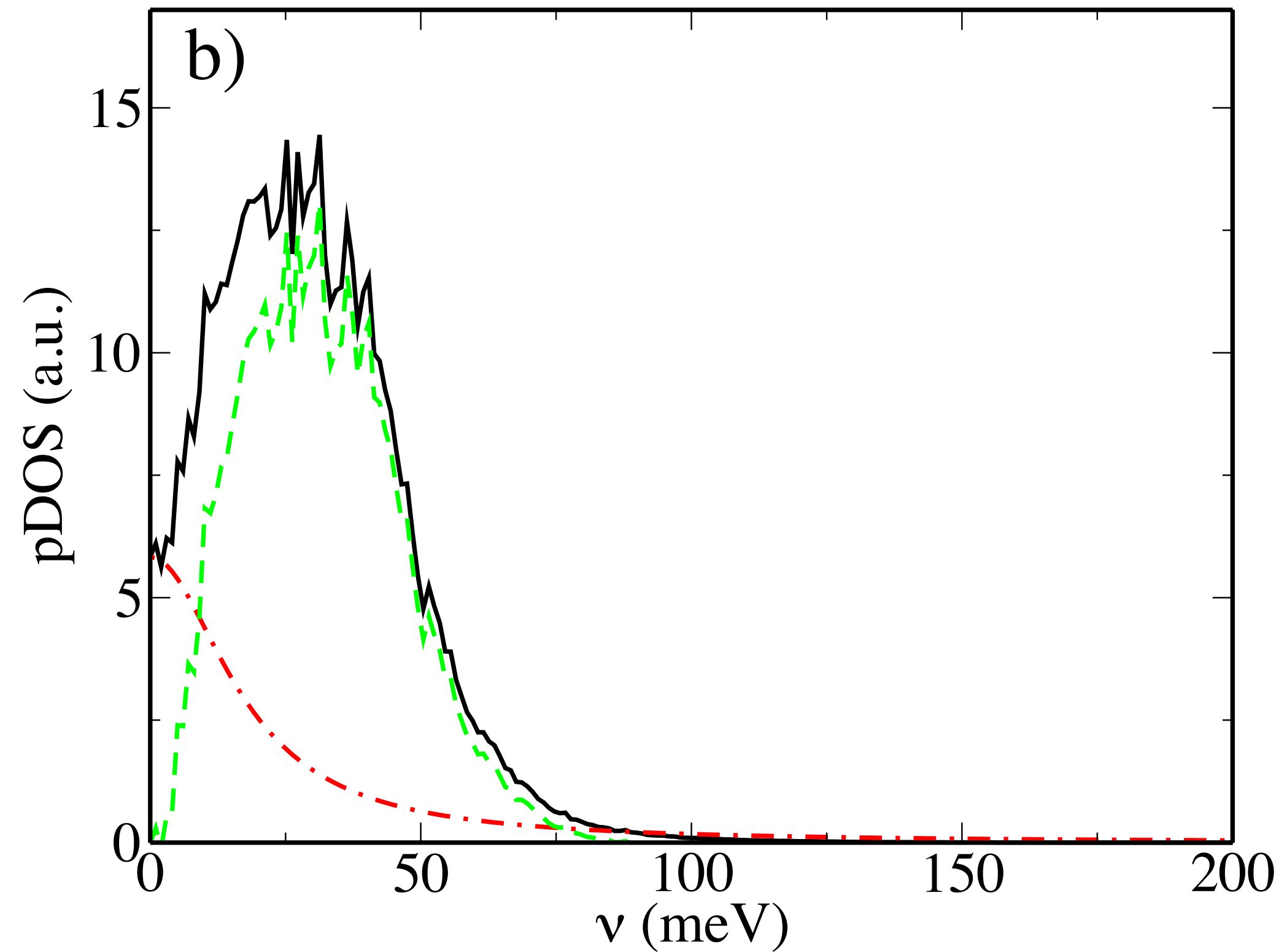


Figure 5c

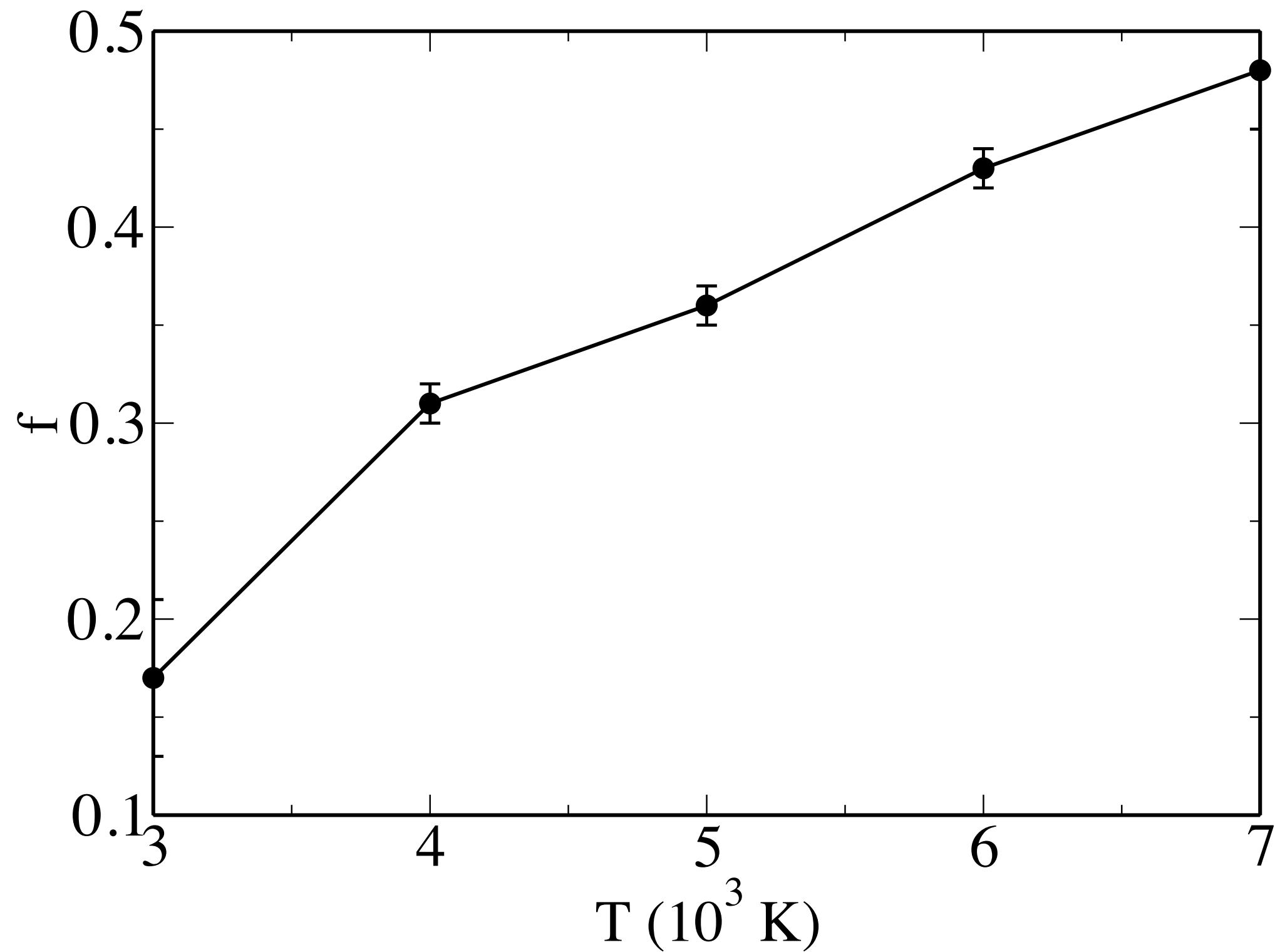
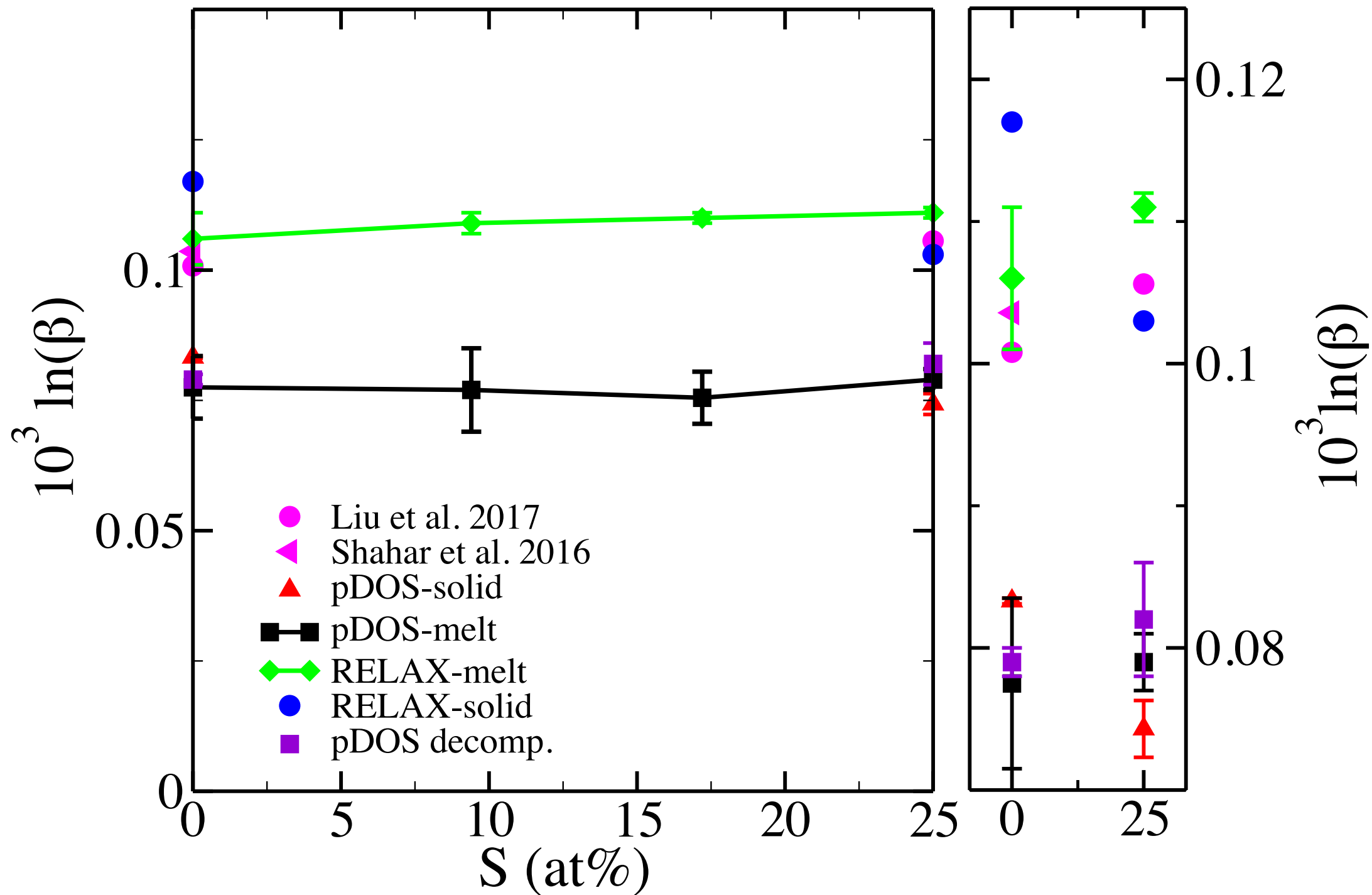
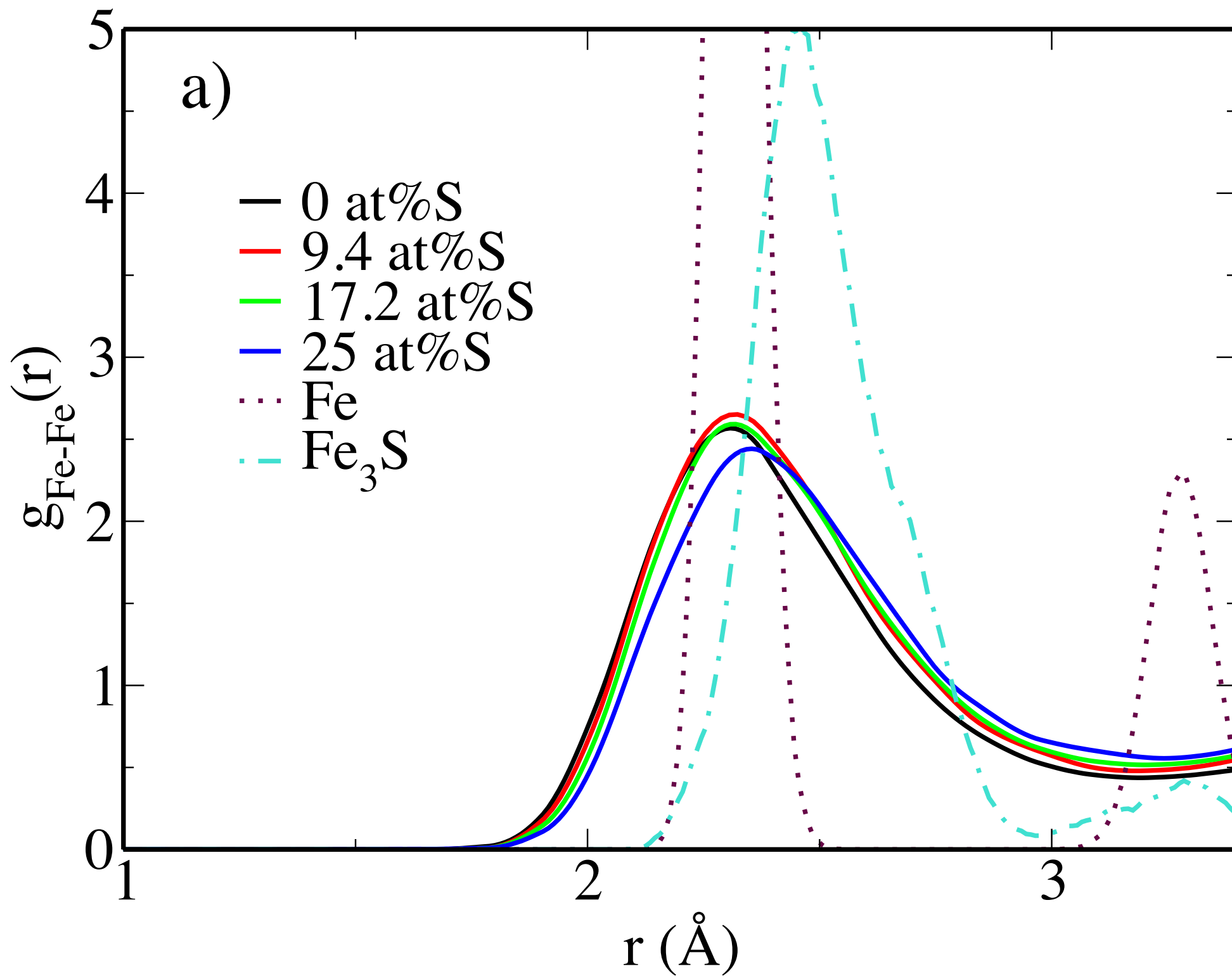
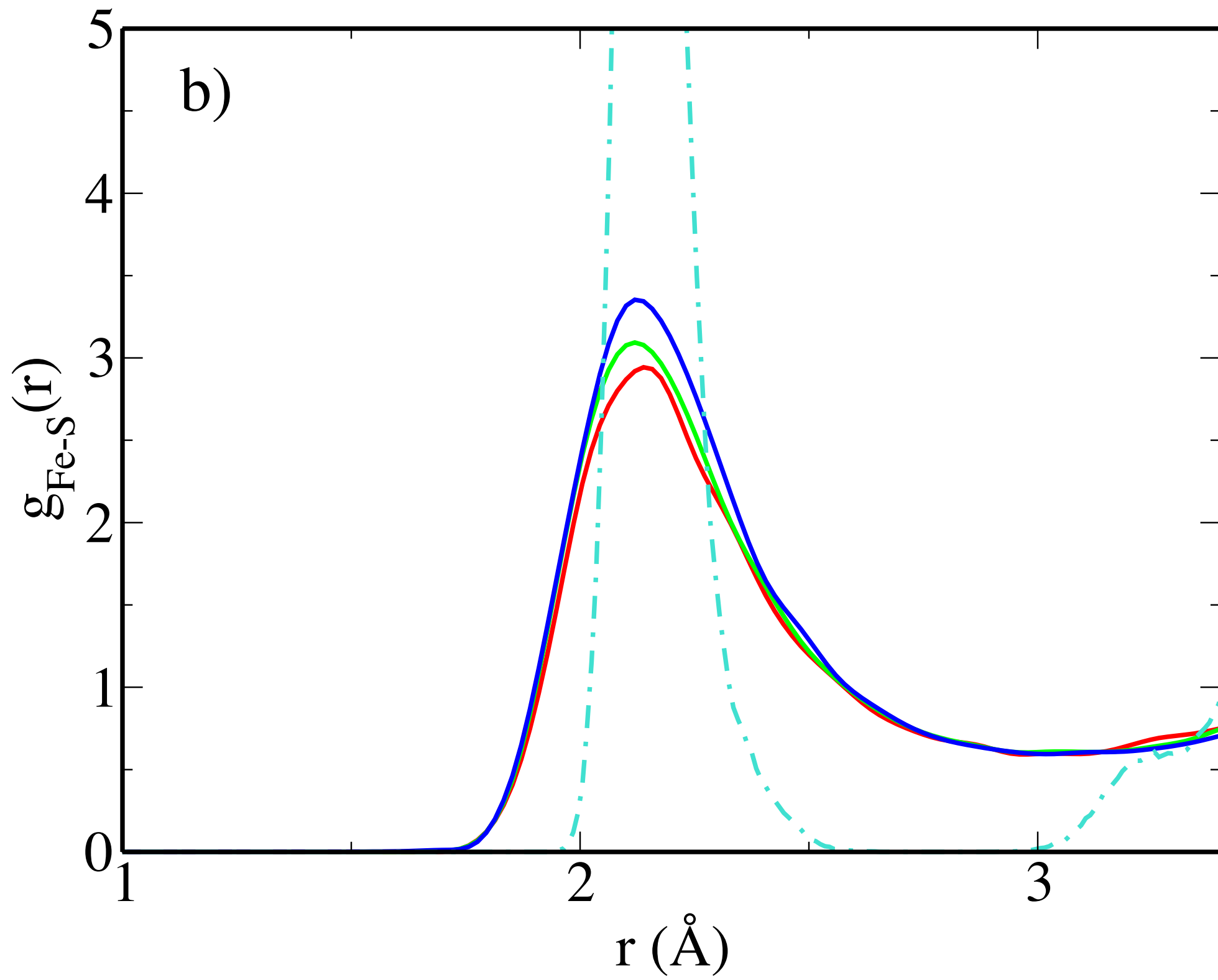


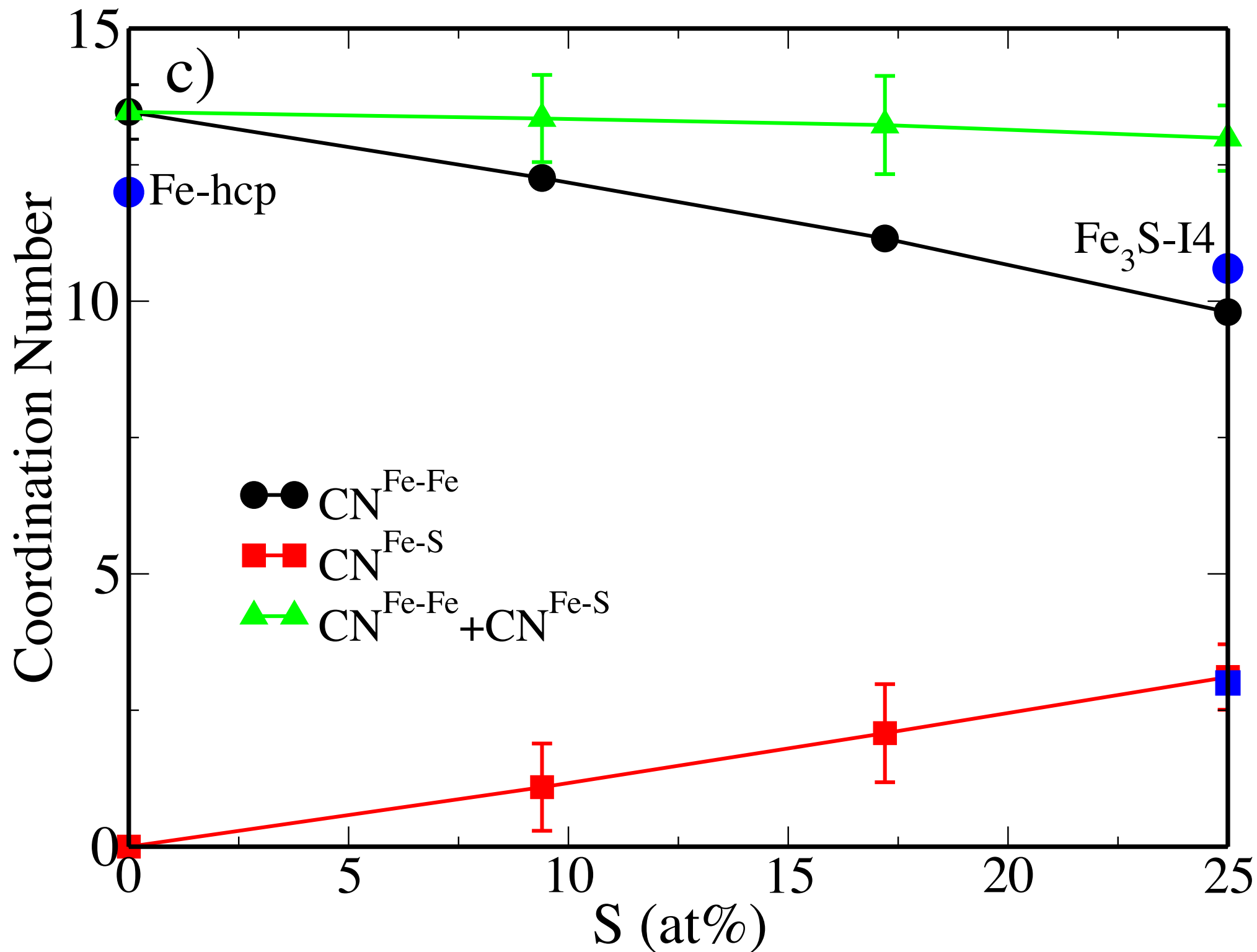


Figure 6









Crystalline system	Supercell size	k-points mesh	q-points-mesh
Fe - hcp	4x4x4	3x3x3	4x4x4
Fe <sub>3</sub> S – I4	2x1x2	1x2x1	6x6x6

**Table 1.** k and q meshes used for the zero-temperature calculation of electronic and vibrational properties of crystalline systems.

Method	Details	$10^3 \ln(\beta)$
pDOS-melt	Full AIMD trajectory at 60 GPa and finite temperature (3000 K for all alloys besides pure molten Fe computed at 6000 K). Anharmonic and configurational disorder effects included.	Calculated using the pDOS and kinetic energy (equations 3, 4 and 6)
pDOS-solid	Full AIMD trajectory at 60 GPa and 300 K. Anharmonic and configurational disorder effects included	Calculated using the pDOS and kinetic energy (equations 3, 4 and 6)
RELAX-melt	Snapshots taken from the liquid AIMD trajectory – structural relaxation at constant P and T = 0 K. Some configurational disorder effects taken into	Calculated using the vibrational frequencies (eq. 2)

	account. Frequencies estimated using the harmonic approximation	
RELAX-solid	Optimization of Fe-hcp and Fe <sub>3</sub> S-14 crystal structures at T = 0 K. Frequencies estimated using the harmonic approximation.	Calculated using the vibrational frequencies (eq. 2)

**Table 2.** Summary of the methods used here for determining the  $\beta$ -factors.

System	pDOS-melt	pDOS-solid	RELAX-melt	RELAX-solid	Other works
Fe	239±7	258±8	330±23	345±19	312 <sup>1</sup> , 321 <sup>2</sup>
Fe <sub>1-x</sub> S <sub>x</sub> with x=5.6 wt%	238±26	----	340±26	----	----
Fe <sub>1-x</sub> S <sub>x</sub> with x=10.6 wt%	232±14	----	344±7	----	----
Fe <sub>3</sub> S	244±5	228±7	352±7	330±29	327 <sup>1</sup>

**Table 3.** Interatomic force constant of iron for Fe<sub>1-x</sub>S<sub>x</sub> alloys in solid, glass and liquid states. Values are given in N/m. NRIXS results from <sup>1</sup>Liu et al. (2017) and <sup>2</sup>Shahar et al. (2016) are shown for comparison.

Typical error value for the displayed NRIXS data is of about 20 N/m.

	$\Delta^{56/54}_{\text{solid-liquid}} (\text{‰})$	$\Delta^{56/54}_{\text{solid-liquid}} (\text{‰})$
	3000 K	1600 K
Fe	0.011±0.005	0.036±0.005
	<i>0.006±0.003</i>	<i>0.021±0.006</i>
Fe <sub>3</sub> S	-0.008±0.001	-0.028±0.001
	<i>-0.004±0.002</i>	<i>-0.016±0.003</i>
Fe <sup>solid</sup> -Fe <sub>3</sub> S <sup>liquid</sup>	0.005±0.002	0.015±0.002
	<i>0.005±0.003</i>	<i>0.019±0.004</i>

**Table 4.**  $\Delta^{56/54}_{\text{solid-liquid}}$  at 1600 and 3000 K calculated using either the RELAX-solid – RELAX-melt methods (first line) or the pDOS<sub>solid</sub> – pDOS<sub>melt</sub> methods (second line).