

Analysis of morphological variations of flax fibre bundles by Fraunhofer diffraction

Komlavi Gogoli, Florian Gehring, Christophe Poilâne, Magali Morales

▶ To cite this version:

Komlavi Gogoli, Florian Gehring, Christophe Poilâne, Magali Morales. Analysis of morphological variations of flax fibre bundles by Fraunhofer diffraction. Industrial Crops and Products, 2021, 171, pp.113856. 10.1016/j.indcrop.2021.113856. hal-03348176

HAL Id: hal-03348176

https://hal.science/hal-03348176

Submitted on 2 Aug 2023

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Analysis of morphological variations of flax fibre bundles by Fraunhofer

diffraction

1

2

4

- 3 Komlavi Gogoli^{1,*}, Florian Gehring¹, Christophe Poilâne¹, Magali Morales¹
 - 1. Normandie Univ, ENSICAEN, UNICAEN, CEA, CNRS, CIMAP, 14050, Caen, France

5 **Abstract**

The increasing use of plant fibres in industrial applications requires a better understanding of 6 7 their morphologies. Experimental observations have shown that these fibres are characterized by a complex geometry which could affect their mechanical behaviour. Indeed, it is well 8 known that the size and shape of plant fibres cross-section vary from bundle to bundle and 9 along their length. In this study, the technique of Fraunhofer diffraction was used to 10 characterize this morphological heterogeneity of flax fibre bundles. The analysis of the results 11 12 showed a large scattering of the cross-section area (CSA). Lengthwise morphological variations of the bundles were examined and reveal that the CSA varies by a factor of 3.4 over 13 14 a length of 75 mm. It also appears that the cross-section shape of flax fibre bundle can be 15 better approximated by an elliptical model than by a circular model. The ratio between the 16 maximum and minimum cross-section shape factor was found to be approximately 2 over a length of 75 mm. Moreover, the occurrence of cross-section rotations has been shown in case 17 18 of fibre bundles, i.e., the orientation of the major-axis of the ellipse corresponding to the 19 cross-section may be different from one point to another, causing sometimes visible twists 20 along the bundle. These different results allowed us to build a numerical 3D volume 21 considering the evolution of flax fibre bundles outer contour.

Keywords: flax fibre bundle; Fraunhofer diffraction; cross-section area; shape factor; variability; 3D

23 reconstruction

22

E-mail address: alphonse.gogoli@unicaen.fr

^{*} Corresponding author at: Normandie Univ, ENSICAEN, UNICAEN, CEA, CNRS, CIMAP, 14000, Caen, France;

1. Introduction

24

25

26

27

28

29

30

31

32

33

34

35

36

37

38

39

40

41

42

43

44

45

46

47

48

As a response to ecological challenges, there is an increasing use of plant fibres in industry, particularly in the manufacture of composite materials (Dicker et al., 2014; Joshi et al., 2004). As they are biodegradable, renewable and naturally abundant, these plant resources offer real alternatives to petrochemical fibres (Goda and Cao, 2007). Used in particular as reinforcements in organic matrix composite materials, plant fibres such as flax, sisal or hemp have remarkable specific mechanical properties making them very competitive with manmade materials such as glass (Bledzki and Gassan, 1999; Wambua et al., 2003; Yan et al., 2014). In the fight against global warming, these plant fibres are therefore good candidates to replace petrochemicals fibers as their increasing use would help to reduce the ecological cost of industrial processes. However, a large scattering of mechanical properties has been observed, in particular in the distribution of rupture stress and Young's modulus of these fibres (Bourmaud et al., 2013; Haag and Müssig, 2016; Lefeuvre et al., 2015; Shah et al., 2016), which could limits their massive use for the design of structural or semi-structural composite material parts. Also, unlike glass fibres, plant fibres such as flax and hemp have a non-linear mechanical behaviour (Charlet, 2008; Cisse, 2016; Duval et al., 2011). To explain this variability and this complex mechanical behaviour, the morphology, the biochemical composition and the microstructural organization of elementary fibres or bundles are regularly discussed (Del Masto et al., 2017; Placet et al., 2014). Consequently, in-depth understanding of each of these parameters is necessary to allow a more intensive and reliable use of these fibres in industrial processes. Concerning the morphology, various studies have highlighted an important variability of morphological characteristics of plant fibres. Experimental observations have clearly shown that their cross-section is very irregular in size and shape (Charlet et al., 2007; Charlet, 2008; Garat et al., 2018; Thuault, 2015) whereas for man-made fibres the cross-section is more uniform. Moreover, in studies on plant fibres, the cross-section of the bundles is often considered to be circular (Charlet, 2008; Cisse, 2016; Romão et al., 2004; Thuault, 2015). But recent work has shown that the cross-section of flax and hemp bundles can be better assessed by an elliptic model. Indeed, the simplified assumption of circular cross-section is suitable for man-made fibre but lead to overestimate the CSA of flax and hemp fibre bundle (Garat et al., 2018; Haag and Müssig, 2016). It is then clear that the geometric model used to represent the cross-section in the calculations is of major importance and also influences the variability of the mechanical properties of plant fibres (Aslan et al., 2011; Bourmaud et al., 2013; Ilczyszyn, 2013). Based on this observation, in this paper, we presented an elliptical model for a better assessment of flax fibre bundle cross-section. For the measurement of the CSA or the study of plant fibre morphology, there is no standardised technique. Different methods are used by the authors: optical microscopy (Charlet, 2008; Ilczyszyn, 2013; Yue et al., 2019), Scanning Electron Microscopy (Charlet, 2008; Thygesen et al., 2006), laser scan (Garat et al., 2018; Haag and Müssig, 2016), Fraunhofer diffraction (Romão et al., 2004), X-ray tomography (Del Masto et al., 2018) or mathematical modelling combined with experimental data (Grishanov et al., 2006). In the presented study, Fraunhofer diffraction has been chosen because - as non-destructive technique using a laser beam – it allows the morphological study of a sample and the subsequent mechanical testing of the same sample. Also, Fraunhofer diffraction requires less time than tomography and therefore allows more samples to be analyzed. The aim of our investigations is to study the morphological variations of flax fibre bundles and to propose a non-destructive methodology to better assess the morphological characteristics of plant fibres. Thanks to Fraunhofer diffraction, the inter-bundle variability of cross-section and its lengthwise non-uniformity along bundle have been characterised and the non-circularity of the cross-section was investigated by using an elliptical model to calculate

49

50

51

52

53

54

55

56

57

58

59

60

61

62

63

64

65

66

67

68

69

70

71

72

the CSA of the bundles. Furthermore, it is also known that the characterization of the 3D morphology of plant fibres and in particular that of their bundles is a real challenge because of the small size of these samples and the difficulties linked to experimental manipulations. Based on our cross-section measurements, a numerical 3D reconstruction of external contour of flax fibre bundle is finally proposed. The interest of such approach of three-dimensional morphology is to propose a 3D model of a bundle respecting the dispersion of the measured parameters. Also in further studies, by including elementary fibres in the bundle 3D reconstructions as done by (Baley et al., 2018), these models can be introduced into a mesher for finite element method studies that could help to improve the understanding of the mechanics of flax fibre bundles.

2. Materials and Methods

2.1. Materials

The flax fibre bundles used to perform this morphological analysis were supplied by Natup company and come from different flax varieties and batches. Since the origin of flax could impact fibre bundles morphology and properties (Booth et al., 2004; Pisupati et al., 2021), a batch of flax from the same origin could be used to exclude the influence of the plant variety. Such specific study could be used in the futur with the methodology proposed here. The usual treatment stages of plant fibres: retting, scutching and then combing were applied. These bundles have the particularity of having been treated with water spray, to make the natural pectins more flexible and to use them as glue between millions of parallel bundles to form a roll. For the purposes of the study, the bundles are randomly and manually extracted from the roll. The extraction was done carefully to avoid bundle damage. A total of 100 fibre bundles were characterized and their outer shape were reconstructed.

2.2. Method used to characterize the flax fibre bundle cross-section

98

99

100

101

102

103

104

105

106

107

108

109

110

111

112

113

114

115

116

117

118

119

120

121

To determine the dimensions of the cross-sections, the Fraunhofer diffraction technique as illustrated in Figure 1a was used. This technique consists in focusing a laser beam (wavelength λ) on the cross-section to be characterized and collecting diffraction pattern composed of several horizontal spots on a display table placed at a given distance D from the fibre bundle. A visible green laser (class 3B, $\lambda = 532nm$, maximum power = 100mW) was used for the tests. Each fibre bundle whose morphology is to be analysed is glued to a windowed cardboard frame with a free length between the edges of 100 mm. According to (Lefeuvre, 2014), a minimum of 6 measurements is required to have a sufficiently representative cross-section of an elementary fibre. Despite the longer length of our samples, the same method was used in the absence of more precise indication concerning the fibre bundles. Moreover, this number of measurements per bundle allows us to optimize the experiment time as the number of samples to be tested is high. Based on this assumption, along the free length of each bundle, the dimensions of the cross-section are determined at 6 locations equidistant by 15 mm (15 mm, 30 mm, 45 mm, 60 mm, 75 mm, 90 mm). Since the cross-section of fibre bundle is considered to be ellipsoidal in our investigations, the axes (minor-axis and major-axis) d_1 and d_2 of the ellipse must then be determined to assure a reliable elliptical CSA calculation (Table 1). In accordance to that geometry and the mathematical definition of an ellipse, the axes d_1 and d_2 must be determined in two orthogonal directions. To achieve these goals, thanks to a device designed in the laboratory, the laser beam is first focused on the point of the bundle whose cross-section is to be characterised and the width δ_1 of the central diffraction spot on the display table is measured (**Figure 1b**).

Then, keeping the laser beam always focused on the same point, the support on which the cardboard is mounted is rotated by 90° around the longitudinal axis of the bundle and the width δ_2 of the central spot of the second diffraction pattern is also measured. The same operation is repeated for each of the 6 cross-sections along the bundle. This gives a total of twelve axis calculations per bundle. The two orthogonal directions named "Direction 1" and "Direction 2" are fixed in advance and are therefore identical for all samples.

Table 1: Geometric model and formula used to calculate the CSA from diffraction

measurements

Real cross-section Geometric model CSA Calculation formula

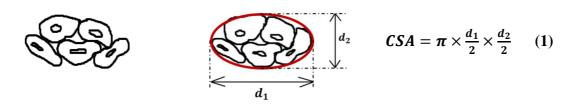


Figure 1: (a) Schematic diagram of the Fraunhofer diffraction principle and (b)

Diffraction pattern recorded on the display table

134 After recording the widths δ_1 et δ_2 , the axes d_1 and d_2 are then calculated using equation (2):

$$d = \frac{2D\lambda}{\delta} \tag{2}$$

137 with:

138

122

123

124

125

126

127

128

129

130

131132

133

 λ : laser beam wavelength

D: distance between the fibre bundle and the display table

 δ : width of the central spot formed by the first two nodes of the diffraction pattern (**Figure**

141 **1b**)

140

143

146

147

148

149

150

151

152

153

154

155

156

157

The smallest axes between d_1 and d_2 is considered to be the minor-axis of the ellipse and the

largest one is considered to be the major-axis. Finally, the elliptical CSA is determined using

the equation (1) shown in the **Table 1.**

For scientific accuracy of later results discussion, it is useful here to recall some significant

consequences of the assumptions made about the cross-sections measurements:

- Since the measurement directions are taken randomly, it is not certain that the two orthogonal dimensions measured correspond to the real axes (major and minor) of the ellipse that would best fit the real cross-section. With the used method, the cross-section is a projection in two orthogonal directions of the real cross-section.
 - Using Fraunhofer diffraction, the disadvantage is that the measure neglects the lumens of elementary fibres which form the bundle. The space occupied by the interfacial lamella between elementary fibres is also not taken into account. However, knowing that in a bundle cross-section, there are usually ten to forty elementary fibres, it follows that the CSA calculated by neglecting the lumen and the interfacial lamella will be slightly overestimated compared to the real CSA. We propose here an estimate of the error made by neglecting the lumens.

Let us assume that at a given point, a bundle is composed of n elementary fibres. The CSA measured at this point, neglecting the lumens is:

$$CSA = \sum_{i=1}^{n} CSA_i \tag{3}$$

161 with:

162 CSA_i : the cross-section area of the elementary fibre of rank i measured by neglecting the area

of its lumen.

The real CSA of the bundle if the total area occupied by the lumens of the elementary fibres is removed become:

166
$$CSA' = \sum_{i=1}^{n} (1 - p_i)CSA_i$$
 (4)

167 with:

179

180

181

182

183

184

185

168 p_i : the surface proportion occupied by the lumen of the elementary fibre of rank i.

169
$$CSA' = \sum_{i=1}^{n} CSA_i - \sum_{i=1}^{n} p_i CSA_i$$
 (4)

Since it is impossible for us to know the surface proportion of lumen for each elementary fibre in a given cross-section of the bundle, we can take an average value from the literature to estimate the overestimation caused by not taking lumens into account. Let's attribute this average to all the fibres, in this case: $p_i = p$.

$$CSA' = CSA - \sum_{i=1}^{n} p CSA_i$$
 (4)

$$CSA' = CSA - p \times \sum_{i=1}^{n} CSA_i$$
 (4)

$$CSA' = CSA - p \times CSA \tag{4}$$

$$CSA' = (1 - p)CSA \tag{5}$$

Combining different studies (Charlet, 2008; Charlet et al., 2010; Richely et al., 2021), it appears that on average the lumen area is between 0.4 and 10.5% of the CSA of the elementary fibre. In this case the CSA of the bundle measured by neglecting only the lumens of its elementary fibre would be on average overestimated by 0.4 to 10.5% compared to the real CSA (calculated by taking into account the interfacial lamella between the elementary fibres). This gives an idea of the overestimation of the cross-section area due to the negligence of the lumens.

According to (Charlet et al., 2012) the length of the interfacial lamellae is between 5 μ m and 15 μ m and the thickness is about 0.5 μ m. With such data, one could try to estimate a theoretical surface proportion of the interfacial lamella, but the latter depends strongly on the arrangement of the elementary fibres in a given section of the bundle. Therefore, an accurate estimate will need the use of optical methods to measure on several samples: the CSA of a bundle, the CSA of its constituent elementary fibres, the area of the lumens and the thickness of the interfacial lamella between elementary fibres. This is beyond the scope of this work. The mean of the 6 calculated CSAs of the bundle was taken as its representative mean CSA: CSA_{EM} . In total we characterised 100 bundles. For 7 of these bundles, however, the measurements were carried out at 5 points due to elementary fibre detachments along the bundle resulting in 593 cross-sections measurements.

3. Results and discussion

3.1. Scattering of flax fibre bundle axes

With 593 cross-sections characterized by two axes d_1 and d_2 , there are a total of 1186 measurements. Analysis of the results reveals a large scattering of the axes with respectively a mean value of $104\pm38~\mu m$ for minor-axis and $158\pm54~\mu m$ for major-axis (Figure 2a and 2b). The distribution of the axes was characterised by testing different statistical distribution laws using the Anderson-Darling test implemented in Matlab software. Only the log-normal distribution (6) seems to be suitable for the distribution of the axes (**P \leq 0.01).

$$Log(\mu, \sigma): f(x) = \frac{1}{x\sigma\sqrt{2\pi}} exp\left[-\frac{((\ln x) - \mu)^2}{2\sigma^2}\right]$$
 (6)

206 with:

 μ and σ the parameters of the log-normal distribution

This large scattering is quite characteristic of plant fibres because they grow in natural conditions which imply a heterogeneity of their cross-section dimensions, unlike man-made

fibres whose dimensions can be standardised during their industrial production. Compared to other studies on "flax fibre bundle apparent diameter", the mean value of our calculated axes is higher than that obtained by (Haag and Müssig, 2016) and (Garat et al., 2018). Apart from natural causes, the significantly higher length of the bundles tested in our case and the number of cross-sections analysed may be the cause of this discrepancy. This difference may also be due to the treatments applied to the fibre bundles used in the different studies. Harvesting and processing conditions can also influence the geometry of these fibres. Indeed, the more the bundles undergo individualization operations – according to the use that will be made of them - the more the number of elementary fibres per bundle decreases, thus lowering the dimensions of the resulting bundle. Furthermore, it should be noted that other factors such the measurement technique accuracy can also influence the results of calculated cross-section dimensions of plant fibres. In fact, for the same batch of flax bundles, the difference in technique used to measure the crosssection dimensions can lead to an error of up to 175% in the calculation of the tensile stress, due to the bias introduced by each technique (automated laser, microscopy, flat-bed scanning) in the measure (Haag and Müssig, 2016). Simultaneous lengthwise evolution of some bundle axis dimension highlights the noncircularity of the cross-section (Figure 2c). This clearly shows that when the cross-section is considered circular, the "mean apparent diameter" of the bundle which will be calculated will depend on the direction of measurement. For the batch of 100 bundles the relative difference between the two "mean apparent diameters" calculated according to Direction 1 and Direction 2 (considering the cross-section to be a circle of diameter d_1 in Direction 1 or d_2 in Direction 2) respectively is around 20 $\% \pm 17$. This implies that the mechanical properties which will be obtained using each of "mean apparent diameter" will be impacted by this difference. The

211

212

213

214

215

216

217

218

219

220

221

222

223

224

225

226

227

228

229

230

231

232

233

random measurement angle of characterisation chosen by the experimenter is hence a source of variability reported by many studies (Aslan et al., 2011; Bourmaud et al., 2013) in both the cross-section dimensions calculation and the mechanical properties that will be attributed to the bundle. Indeed, the rupture stress and Young's modulus depend directly on the mean CSA of the bundle. This conclusion is obviously valid for elementary fibres.

Figure 2: Characteristics of the axes of the cross-section: (a) Distribution of the minor-axes, (b) Distribution of the major-axes and (c) Lengthwise evolution of cross-section axis for two bundles

3.2. Scattering and lengthwise variation of CSA along the bundle

The 593 cross-sections calculated from the axis measurements were analysed and again revealed a large variability inherent to plant fibres. This cross-section scattering is the logical consequence of the axis scattering discussed in **section 3.1**. In terms of distribution, the cross-section distribution also follows a log-normal distribution ($^*P \le 0.05$) (**Figure 3a**).

Table 2: Calculated geometric parameters of flax fibre bundles CSA

	Min	~Mean	Max
$CSA (\mu m^2)$	836	14062	68267
Minor-axis (μm)	27.8	121.7	251.4
Major-axis (μm)	38.3	147.2	345.9

The mean CSA is $13947 \pm 9331 \, \mu m^2$. Our results are quite similar to those of (Charlet, 2008) who found respectively on two different batches of bundles, mean CSA of $14107 \pm 4555 \, \mu m^2$ and $13881 \pm 4496 \, \mu m^2$ by image analysis. On the other hand, compared to the mean CSA of $6148 \, \mu m^2$ found by (Garat et al., 2018) using optical microscopy, the mean cross-section of this present study is more than the double. To explain the important

difference with the results of (Garat et al., 2018), one can mention again the origin of samples and the individualisation processes they underwent before being characterised. In fact, it is really difficult to conclude on this point because few precise indications are given on this information in the different publications. The variety of flax used in the studies may also be the source of this high difference. But it is unlikely in the light of our knowledge that the difference in variety can justify such a large difference. (Thuault, 2015) studied the "apparent diameters" of seven varieties of flax and concluded from his statistical results that there is no significant different between diameter from one variety to another.

There is also strong intra-bundle heterogeneity in the cross-sections. The characterisation of this heterogeneity is crucial to set-up the 3D outer contour of the bundles. Here, two levels of study are required: on the one hand, the evolution of the size (CSA) of the cross-section and,

discussed. For a sample, the cross-section heterogeneity ratio r_s – which represents the multiplication factor of the CSA over 75 mm (15 mm to 90 mm) – is calculated by equation

on the other, the evolution of its shape. In the actual section, the first level of the study is

267 (7). It is worth noting that this ratio is computed for each of the six sections of the bundle:

268
$$r_{s} = \frac{\max(CSA_{i})}{\min(CSA_{i})} \quad i = 1; 2 \dots; 6$$

269 (7)

On average the CSA is multiplied by 3.4 over 75 mm. **Table 3** gives the r_s values for 10 representative samples from the batch of 100 bundles characterised. The ratio of the maximum CSA to the minimum CSA can reach values of the order of ten. However, it should be noted that 90% of the r_s values are below 6. Despite the small number of measurement points compared to the length of our samples, this result shows the high variability of CSA along the bundle (**Figure 3b**). This variation in cross-section can cause stress concentrations that would add to the elementary inter-fibre friction that occurs in a tensile test on a plant fibre bundle. Once again, the CSA scattering is one of the reasons which could explain the scattering of mechanical properties since each bundle has a unique morphology that

influences its mechanical properties whatever the sample length, notably through the calculation of the mean CSA.

Figure 3: (a) Cross-Section Area distribution and (b) Lengthwise variations of flax fibre bundle CSA

The explications of this CSA lengthwise variation can be multiple. As the elementary fibres are not continuous and given the length of the bundles tested, the number of elementary fibres per cross-section is very likely to be different. This would result in CSA high variations. Even if between two measuring points, the number of elementary fibres would be identical, the consistency of the CSA is not at all guaranteed.

Table 3: Analysis of CSA heterogeneity for 10 representative bundles of the total batch

289											
	Bundle	L1	L2	L3	L4	L5	L6	L7	L8	L9	L10
	Mean CSA (μm²)	10288	15917	16250	15461	15567	10322	8998	8215	29975	14875
	Standard- deviation	1277	5086	5780	9612	10419	6729	6231	6899	22946	13368
	r_s	1.4	2.2	3.5	4.1	5.4	6.7	7.2	8.6	9.2	12.0

It should be remembered here that even elementary fibre do not have a constant CSA (Charlet, 2008; Thuault, 2015). Using a camera equipped with lenses that can see details at the micrometer scale, the bundles were photographed to highlight these strong lengthwise variations of the CSA (**Figure 4**).

Figure 4: Two different flax fibre bundles section seen in profile

Let now d_{1m} ou d_{2m} be the mean axes of the bundle in the Direction 1 and Direction 2 respectively. A power regression correlation law between the "maximum mean axis" $d_m =$

 $\max(d_{1m}, d_{2m})$ and the mean elliptical cross-section area CSA_{EM} of the bundle was developed (Figure 5a):

$$CSA_{EM} = k \times d_m^{\ n} \tag{8}$$

When the "maximum mean axis" is less than 100 μm, the calculated mean elliptical CSA given by the power law given in equation (8) is very close to the experimental results. This law deviates from calculated mean elliptical CSA for high "maximum mean axis".

3.3. Ellipticity of flax fibre bundle cross-section

The measurements also confirm the ellipticity of the cross-sections. For each of the 593 cross-sections, the ellipticity *e* is calculated to better characterization of the cross-section shape (9):

307
$$e = 1 - \frac{\min(d_{1}, d_{2})}{\max(d_{1}, d_{2})} = 1 - \frac{\min(d_{2}, d_{2})}{\min(d_{2}, d_{2})} = 1 - \frac{\min(d_{2}, d_{2})}{\min(d_{2}, d_{2})}$$
 (9)

From a mathematical point of view, this definition makes it possible to identify the flattening degree of an elliptical curve. The more circular the characterized cross-section is, the more e tends towards 0 since in this case d_1 and d_2 are quite close. Otherwise, the flatter the ellipse corresponding to the cross-section is, the more e tends towards 1. With a range of values from 0 to 0.77, the distribution the ellipticity is highly random compared to those of axes and cross-sections. The mean ellipticity is 0.32 and confirms the relevance of the elliptical model for determining the CSA of flax fibre bundles. On the basis of this result, it can therefore be concluded that, compared to the circular model, the elliptical model seems to be more suitable for determining the CSA of flax fibre bundles.

The comparison with other similar works (Garat et al., 2018; Haag and Müssig, 2016) on plant fibre shape requires the calculation of the shape factor f defined as ratio between the major and minor axis of the ellipse:

$$f = \frac{\max(d_1, d_2)}{\min(d_1, d_2)} \tag{10}$$

It was found for all 593 cross-sections: $f_{mean} = 1.6$, $f_{min} = 1$ et $f_{max} = 4.3$. Our result is similar to that of (Haag and Müssig, 2016) for whom the f_{mean} is 1.76. but lower than the value of 2.58 found by (Garat et al., 2018) for fibre bundle cross-sections. Nevertheless, the three studies lead to the same conclusion: the cross-section of flax fibre bundles is rather elliptical. The ellipse corresponding to the mean shape factor f_{mean} of the present study is drawn on the **Figure 5b** in comparison with a circle whose diameter would be the major axis of the ellipse. The flattening degree of the ellipse close to the real cross-section clearly illustrates the non-circularity of the flax fibre bundle.

The second level of study required to perform the 3D reconstruction of the bundle outer contour is the lengthwise evolution of the cross-section shape. The analysis of the intrabundle heterogeneity shows that the shape factor doubles on average over 75 mm. Not only can the CSA be multiplied by 3.4 over 75 mm, but the cross-section shape factor can be multiplied by 2 on average. These results illustrate the important irregularity exhibited by the morphology of flax fibre bundles.

Figure 5: (a) Power law correlation between "maximum mean axis" and mean CSA of the bundle and (b) Illustration of the ellipticity of flax fibre bundle : curves drawn with major axis of the ellipse = diameter of the comparison circle = $100 \mu m$

Although the study of the influence of the geometrical model used to calculate the CSA on the mechanical properties is beyond the scope of this works, these findings confirms that the geometric model directly influences the mechanical properties of the sample (Aslan et al., 2011). For example, in our case, when the mean cross-section of the bundle is calculated by considering a circular cross-section (assuming that the cross-section is a circle of diameter d_1 in Direction 1 or d_2 in Direction 2), there is an average overestimation of 12% compared to the mean cross-section calculated using the elliptical model. Therefore, as suggested by (Virk,

2010), if the circular model is used when measuring cross-section, it would be relevant to determine a "correction factor" for the CSA to take into account the overestimation induced by the geometrical model. This correction factor, which according to our study would be the mean shape factor of 1.6 for flax bundle, is slightly lower than the value of 1.76 proposed by (Haag and Müssig, 2016) but greater than the value of 1.42 proposed for jute fibre bundles by (Virk, 2010).

3.4. Possible rotation of the cross-section along the fibre bundle

The lengthwise evolution of the cross-section has been finely analysed and it was noted that the orientation of the major axis of the ellipse can be different from one cross-section to another. Indeed, for each of the cross-sections, we named d_1 the axis measured along Direction 1 and d_2 the one measured along Direction 2. Considering 2 consecutive cross-sections and assuming that for the first one $d_1 > d_2$ there is no guarantee that in the second cross-section we will have $d_1 > d_2$ but rather the opposite. When this reasoning is extended to each pair of consecutive cross-sections, according to our method of measurements, the orientation of the cross-section can be different from one point to another (Figure 6a). For the 100 bundles, this change in cross-section orientation between two consecutive points occurs on average 2 times when considering 75 mm over a bundle. As evidence of this, we have taken high precision pictures of bundles, where it is clear that some bundles are twisted (Figure 6b).

Figure 6: (a) Illustration of the change of orientation between two consecutive sections and (b) Bundle with local twisting

Using Fraunhofer diffraction or any other laser technique, the number of measurement points per cross-section and per bundle would have to be increased to get an average value closer to reality. The results of our study are indicative since – as we have already reminded – the

ellipse by which we assessed the cross-section corresponds to a view along two orthogonal directions. The change of orientation observed can have several origins according to the following two scenarios. Since a bundle is an assembly of discontinuous elementary fibres, this change in the orientation of the cross-section may be due to the difference in the arrangement of the elementary fibres between two consecutive points (Figure 7a). In other words, depending on the appearance and disappearance of the elementary fibres, the orientation of the cross-section considered as an ellipse could change. In this case, there would be no twisting of the bundle, but just a change in orientation corresponding to the ellipse that best approximates the cross-section. If two consecutive cross-sections of a bundle have an elementary fibre arrangement, as shown in the Figure 7a, it is clear that the orientation of the major-axis of the ellipse corresponding to the cross-section changes between Cross-Section i and Cross-Section i+1. Our calculation method would in this case show a twisting when there is no twisting but only a different disposition of elementary fibre. The other possible scenario is that the growth conditions of the bundles in flax stem or the processing conditions may have favoured an irregular evolution of the orientation of the cross-sections, thus causing twisting along the bundle. Furthermore, the scenario of a bundle of fibres which twists himself after combing should not be a surprise if all the microfibril helices – which act at the main rigid elements inside elementary fibre – are orientated in the same direction (S-helice) (Baley, 2002; Bergfjord and Holst, 2010). In that case, it can be hypothesized that the twisting is due to stress relaxation once the bundle is released. As the microfibrillar angle is much higher in defect areas such as kink-bands than in the rest of the flax fibres (Melelli et al., 2021), it is conceivable that a difference in relaxation ratio may induce or increase such twisting. This twisting revealed by the numerical analysis and the optical observations would probably explain the rotation of the bundle at the beginning of the

368

369

370

371

372

373

374

375

376

377

378

379

380

381

382

383

384

385

386

387

388

389

390

tensile load observed by (Ahmed and Ulven, 2018) using in-situ Scanning Electron Microscopy.

3.5. 3D reconstruction of flax fibre bundles outer contour

392

393

394

395

396

397

398

399

400

401

402

403

404

405

406

407

408

409

410

411

412

413

414

415

The knowledge of the exact morphology of plant fibre bundles and its lengthwise evolution is a very important issue. Indeed, more and more studies are focusing on the propagation of the mechanical behaviour of elementary fibre to the bundle. When performing numerical simulations of bundle mechanical behaviour, taking into the account the disposition of elementary fibres in a circle or ellipse can have an influence on the resulting behaviour of the bundle. For example, numerical simulations by (Del Masto et al., 2017) have shown that the more the ellipticity of a hemp elementary fibre tends towards 0, the more the tensile behaviour of the fibre is non-linear. In addition, a better knowledge of bundle morphology could allow an in-depth study of the effect of twisting on their mechanical behaviour. It is quite possible that there is a mechanical coupling (tensile-torsion) or high stress-concentration during the elongation of these samples. Due to the size of the bundle or elementary fibre the fine description of the morphology remains little investigated. To overcome this experimental difficulty, numerical approaches are increasingly being considered (Mattrand et al., 2014; Ntenga and Beakou, 2011) and make it possible to study the relationship between the complex morphology of plant fibres and their mechanical behaviour (Del Masto et al., 2017). So, based on the results of our morphological analysis, the outer contour of the fibre bundles as made possible by our measurement method was reconstructed numerically. The following basic assumptions are made: - In accordance with the model adopted for our measurements, the cross-section is

- In accordance with the model adopted for our measurements, the cross-section is assumed to be elliptical and the bundle is assumed to have perfect symmetry around its longitudinal axis.

- The morphology reconstructed ignores the disposition of elementary fibres which constitute the bundles. So the bundle is considered as a homogeneous medium.

Three types of bundles were reconstructed (**Figure 7b, 7c and 7d**): a bundle with little morphological variation; a bundle with strong morphological variations, and a bundle reconstructed with mean lengthwise evolution of the cross-section.

Figure 7: (a) Example of elementary fibre disposition which could induce a change of orientation of the cross-section according to our calculation method, (b) 3D reconstruction of the outer contour of bundle with little morphological variation, c) 3D reconstruction of the outer contour of bundle with strong morphological variations, d) A 3D reconstructed bundle with the average values of lengthwise evolution of the cross-section and e) 3D reconstruction of a bundle outer contour by X-ray nanotomography (Del Masto, 2018)

It is possible to compare this purely numerical 3D reconstruction by X-ray nanotomography 3D reconstruction of a bundle outer contour (**Figure 7e**). Note that the number of characterized cross-sections per bundle should be increased to approach more realistic description. However, the heterogeneity of the cross-section highlighted by the measurements is well illustrated in these reconstructions. The models obtained here will be refined and can be used to study by numerical simulations the relationship between the complex morphology of bundles and their tensile behaviour.

4. Conclusion

In this paper, we investigated the morphological variations of flax fibre bundles cross-section using the Fraunhofer diffraction technique. A particular focus was made on the heterogeneity of the morphology of a hundred flax fibre bundles. The first finding is the confirmation of the high intra-bundle and inter-bundle scattering of the cross-section. Over 75 mm of a 100 mm

length bundle, the cross-section area (CSA) is on average multiplied by 3.4 and the shape factor of cross-section doubles. This clearly shows that it is imperative to determine a mean CSA per bundle for later calculation of mechanical properties. Our method has also highlighted the elliptical shape of the bundles cross-sections. Compared to the elliptical model, using a circular model to obtain an "mean apparent diameter" of the bundle is a less relevant method for a reliable estimation of flax fibre bundles CSA. The morphological scattering coupled with the method geometrical model of the cross-section & measurement technique) used to characterize the cross-sections is one of the reasons which explain the dispersion of the mechanical properties reported by different studies on flax fibre bundles. A standardisation of the method using to determine the CSA of plant fibres is strongly required to eliminate the variability introduced by the different techniques used. This would allow a more reliable comparison of results from different studies. The method proposed here for plant fibres is of particular interest if it is essential that the analysed samples keep their morphology undamaged for further testing. Additionally, a possible change in cross-section orientation between two consecutive measurement points along the bundle was revealed. Local twisting of some bundles was thus observed. More detailed analyses, such as an increase in the number of measurement points per cross-section and per – which is possible with automated laser scanning device – would be needed to gain in-depth knowledge of these local bundle twists. These different results allowed us to reconstruct the 3D evolution of the outer contour of flax fibre bundles. Although performed numerically with a low number of cross-sections per bundle given the length of our samples, the reconstruction helps to highlight the significant heterogeneity in the size and shape of the flax fibre bundle cross-section. In future works, by incorporating elementary fibres in the 3D reconstructions, the use of finite element method could help to better understand the mechanical behaviour of the bundles: especially stress

426

427

428

429

430

431

432

433

434

435

436

437

438

439

440

441

442

443

444

445

446

447

448

449

451	concentration phenomena and the shear occuring at the interface of elementary fibres during a
452	tensile test.
453	
454	Funding: This research did not receive any specific grant from funding agencies in the
455	public, commercial, or not-for-profit sectors.
456	
457	
458	
459	
460	
461	
462	References
463	Ahmed, S., Ulven, C.A., 2018. Dynamic in-situ observation on the failure mechanism of flax
464	fiber through scanning electron microscopy. Fibers 6.
465	https://doi.org/10.3390/FIB6010017
466	Aslan, M., Chinga-Carrasco, G., Sørensen, B.F., Madsen, B., 2011. Strength variability of
467	single flax fibres. J. Mater. Sci. 46, 6344-6354. https://doi.org/10.1007/s10853-011-
468	5581-x
469	Baley, C., 2002. Analysis of the flax fibres tensile behaviour and analysis of the tensile
470	stiffness increase. Compos Part A Appl. Sci. Manuf. 33, 939–948.
471	https://doi.org/10.1016/S1359-835X(02)00040-4
472	Baley, C., Goudenhooft, C., Gibaud, M., Bourmaud, A., 2018. Flax stems: From a specific
473	architecture to an instructive model for bioinspired composite structures. Bioinspiration
474	and Biomimetics 13, aaa6b7. https://doi.org/10.1088/1748-3190/aaa6b7
475	Bledzki, A.K., Gassan, J., 1999. Composites reinforced with cellulose based fibres. Prog.
476	Polym. Sci. 24, 221–274. https://doi.org/10.1016/S0079-6700(98)00018-5

- Booth, I., Harwood, R.J., Wyatt, J.L., Grishanov, S., 2004. A comparative study of the
- characteristics of fibre-flax (Linum usitatissimum). Ind. Crops Prod. 20, 89–95.
- 479 https://doi.org/10.1016/j.indcrop.2003.12.014
- Bourmaud, A., Morvan, C., Bouali, A., Placet, V., Perré, P., Baley, C., 2013. Relationships
- between micro-fibrillar angle, mechanical properties and biochemical composition of
- flax fibers. Ind. Crops Prod. 44, 343–351. https://doi.org/10.1016/j.indcrop.2012.11.031
- Charlet, K., 2008. Contribution à l'étude de composites unidirectionnels renforcés par des
- fibres de lin : relation entre la microstructure de la fibre et ses propriétés mécaniques.
- 485 https://doi.org/...
- Charlet, K., Baley, C., Morvan, C., Jernot, J.P., Gomina, M., Bréard, J., 2007. Characteristics
- of Hermès flax fibres as a function of their location in the stem and properties of the
- derived unidirectional composites. Compos. Part A Appl. Sci. Manuf. 38, 1912–1921.
- 489 https://doi.org/10.1016/j.compositesa.2007.03.006
- 490 Charlet, K., Gaillard-Martinie, B., Béakou, A., 2012. Comportement mécanique et
- 491 modélisation numérique de la lamelle mitoyenne de lin. Ann. Chim. Sci. des Mater. 37,
- 492 341–350. https://doi.org/10.3166/RCMA.22.341-350
- 493 Charlet, K., Jernot, J.P., Eve, S., Gomina, M., Bréard, J., 2010. Multi-scale morphological
- characterisation of flax: From the stem to the fibrils. Carbohydr. Polym. 82, 54–61.
- 495 https://doi.org/10.1016/j.carbpol.2010.04.022
- 496 Cisse, O., 2016. Caractérisation du comportement hygro-mécanique des fibres liberiennes
- 497 élémentaires issues du chanvre. PhD Thesis, Université de Franche-Comté, France.
- 498 Del Masto, A., Trivaudey, F., Guicheret-Retel, V., Placet, V., Boubakar, L., 2017. Nonlinear
- tensile behaviour of elementary hemp fibres: a numerical investigation of the
- relationships between 3D geometry and tensile behaviour. J. Mater. Sci. 52.
- 501 https://doi.org/10.1007/s10853-017-0896-x

- Del Masto, A., 2018. Transition d'échelle entre fibre végétale et compositeUD : propagation
- de la variabilité et des non-linéarités. PhD Thesis, Université de Bourgogne Franche-
- 504 Comté, France.
- Dicker, M.P.M., Duckworth, P.F., Baker, A.B., Francois, G., Hazzard, M.K., Weaver, P.M.,
- 506 2014. Green composites: A review of material attributes and complementary
- 507 applications. Compos. Part A Appl. Sci. Manuf. 56, 280–289.
- 508 https://doi.org/10.1016/j.compositesa.2013.10.014
- 509 Duval, A., Bourmaud, A., Augier, L., Baley, C., 2011. Influence of the sampling area of the
- stem on the mechanical properties of hemp fibers. Mater. Lett. 65, 797–800.
- 511 https://doi.org/10.1016/j.matlet.2010.11.053
- 512 Garat, W., Corn, S., Le Moigne, N., Beaugrand, J., Bergeret, A., 2018. Analysis of the
- morphometric variations in natural fibres by automated laser scanning: Towards an
- efficient and reliable assessment of the cross-sectional area. Compos. Part A Appl. Sci.
- Manuf. 108, 114–123. https://doi.org/10.1016/j.compositesa.2018.02.018
- 516 Goda, K., Cao, Y., 2007. Research and Development of Fully Green Composites Reinforced
- with Natural Fibers. J. Solid Mech. Mater. Eng. 1, 1073–1084.
- 518 https://doi.org/10.1299/jmmp.1.1073
- Grishanov, S.A., Harwood, R.J., Booth, I., 2006. A method of estimating the single flax fibre
- fineness using data from the LaserScan system. Ind. Crops Prod. 23, 273–287.
- 521 https://doi.org/10.1016/j.indcrop.2005.08.003
- Haag, K., Müssig, J., 2016. Scatter in tensile properties of flax fibre bundles: influence of
- determination and calculation of the cross-sectional area. J. Mater. Sci. 51, 7907–7917.
- 524 https://doi.org/10.1007/s10853-016-0052-z
- 525 Ilczyszyn, F., 2013. Caractérisation expérimentale et numérique du comportement mécanique
- des agro-composites renforcés par des fibres de chanvre 385. PhD Thesis. Université de

- 527 Technologie de Troyes, France.
- Joshi, S. V., Drzal, L.T., Mohanty, A.K., Arora, S., 2004. Are natural fiber composites
- environmentally superior to glass fiber reinforced composites? Compos. Part A Appl.
- 530 Sci. Manuf. 35, 371–376. https://doi.org/10.1016/j.compositesa.2003.09.016
- 531 Lefeuvre A., 2014. Contribution à l'étude des propriétés des fibres de lin (Linum
- Usitatissimum, variétés Marylin et Andréa) en fonction des pratiques culturales sur le plateau
- du Neubourg. Fibres destinées au renforcement de matériaux composites". PhD Thesis,
- 534 Université de Rouen, France.
- Lefeuvre, A., Duigou, A. Le, Bourmaud, A., Kervoelen, A., Morvan, C., Baley, C., 2015.
- Analysis of the role of the main constitutive polysaccharides in the flax fibre mechanical
- 537 behaviour. Ind. Crops Prod. 76, 1039–1048.
- 538 https://doi.org/10.1016/j.indcrop.2015.07.062
- 539 Mattrand, C., Béakou, A., Charlet, K., 2014. Numerical modeling of the flax fiber
- morphology variability. Compos. Part A Appl. Sci. Manuf. 63, 10–20.
- 541 https://doi.org/10.1016/j.compositesa.2014.03.020
- Melelli, A., Durand, S., Arnould, O., Richely, E., Guessasma, S., Jamme, F., Beaugrand, J.,
- Bourmaud, A., 2021. Extensive investigation of the ultrastructure of kink-bands in flax
- fibres. Ind. Crops Prod. 164. https://doi.org/10.1016/j.indcrop.2021.113368
- Ntenga, R., Beakou, A., 2011. Structure, morphology and mechanical properties of
- Rhectophyllum camerunense (RC) plant-fiber. Part I: Statistical description and image-
- based reconstruction of the cross-section. Comput. Mater. Sci. 50, 1442–1449.
- 548 https://doi.org/10.1016/j.commatsci.2010.11.032
- Pisupati, A., Willaert, L., Goethals, F., Uyttendaele, W., Park, C.H., 2021. Variety and
- growing condition effect on the yield and tensile strength of flax fibers. Ind. Crops Prod.
- 551 170, 113736. https://doi.org/10.1016/j.indcrop.2021.113736

- Placet, V., Cissé, O., Lamine Boubakar, M., 2014. Nonlinear tensile behaviour of elementary
- hemp fibres. Part I: Investigation of the possible origins using repeated progressive
- loading with in situ microscopic observations. Compos. Part A Appl. Sci. Manuf. 56,
- 555 319–327. https://doi.org/10.1016/j.compositesa.2012.11.019
- Richely, E., Durand, S., Melelli, A., Kao, A., Magueresse, A., Dhakal, H., Gorshkova, T.,
- Callebert, F., Bourmaud, A., Beaugrand, J., Guessasma, S., 2021. Novel insight into the
- intricate shape of flax fibre lumen. Fibers 9, 1–17. https://doi.org/10.3390/fib9040024
- 859 Romão, C., Vieira, P., Peito, F., Marques, A.T., Esteves, J.L., 2004. Single filament
- mechanical characterisation of hemp fibres for reinforcing composite materials. Mol.
- 561 Cryst. Liq. Cryst. 418. https://doi.org/10.1080/15421400490479172
- 562 Shah, D.U., Nag, R.K., Clifford, M.J., 2016. Why do we observe significant differences
- between measured and 'back-calculated' properties of natural fibres? Cellulose 23,
- 564 1481–1490. https://doi.org/10.1007/s10570-016-0926-x
- Thuault, A., 2015. Approche multi-échelle de la structure et du comportement mécanique de
- la fibre de lin. PhD Thesis, Université de Caen Basse Normandie, France.
- Thygesen, L.G., Bilde-Sørensen, J.B., Hoffmeyer, P., 2006. Visualisation of dislocations in
- hemp fibres: A comparison between scanning electron microscopy (SEM) and polarized
- light microscopy (PLM). Ind. Crops Prod. 24, 181–185.
- 570 https://doi.org/10.1016/j.indcrop.2006.03.009
- Virk, A.S., 2010. Numerical models for natural fibre composites with stochastic properties.
- 572 PhD Thesis, Plymouth University, England. https://pearl.ply-
- 573 mouth.ac.uk/handle/10026.1/517.
- Wambua, P., Ivens, J., Verpoest, I., 2003. Natural fibres: Can they replace glass in fibre
- 575 reinforced plastics? Compos. Sci. Technol. 63, 1259–1264.
- 576 https://doi.org/10.1016/S0266-3538(03)00096-4

Yan, L., Chouw, N., Jayaraman, K., 2014. Flax fibre and its composites - A review. Compos.

Part B Eng. 56, 296–317. https://doi.org/10.1016/j.compositesb.2013.08.014

Yue, H., Rubalcaba, J.C., Cui, Y., Fernández-Blázquez, J.P., Yang, C., Shuttleworth, P.S.,
2019. Determination of cross-sectional area of natural plant fibres and fibre failure
analysis by in situ SEM observation during microtensile tests. Cellulose 26, 4693–4706.

https://doi.org/10.1007/s10570-019-02428-7

583

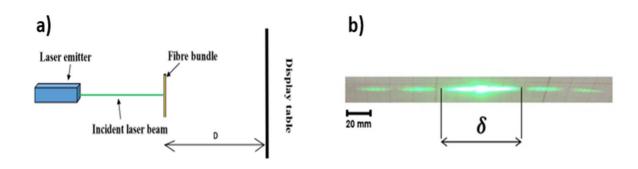
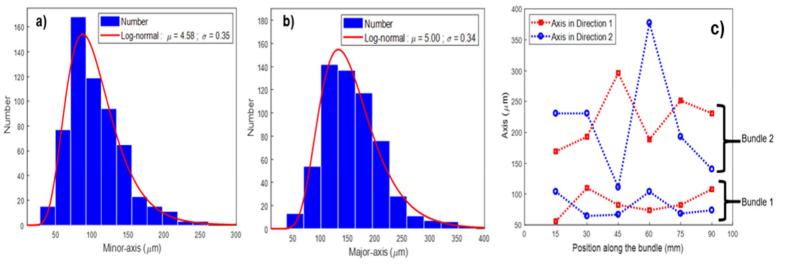


Figure 1: (a) Schematic diagram of the Fraunhofer diffraction principle and (b)

Diffraction pattern recorded on the display table

Figure 2: Characteristics of the axes of the cross-section: (a) Distribution of the minor-axes, (b) Distribution of the major-axes and (c) Lengthwise evolution of cross-section axis for two bundles



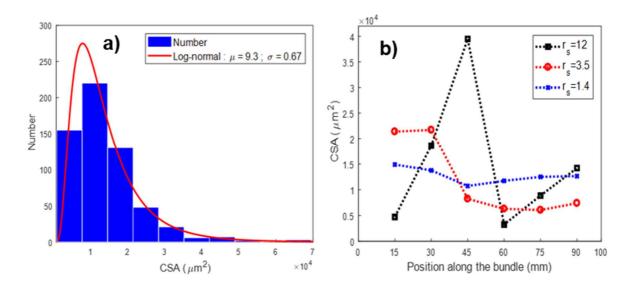


Figure 3: (a) Cross-Section Area distribution and (b) Lengthwise variations of flax fibre bundle CSA

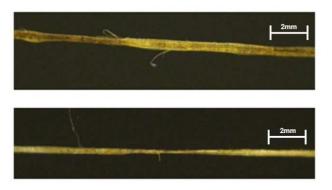


Figure 4: Two different flax fibre bundles section seen in profile

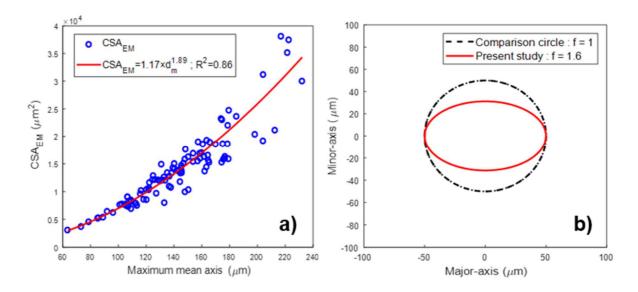


Figure 5: (a) Power law correlation between "maximum mean axis" and mean CSA of the bundle and (b) Illustration of the ellipticity of flax fibre bundle : curves drawn with major axis of the ellipse = diameter of the comparison circle = $100 \mu m$

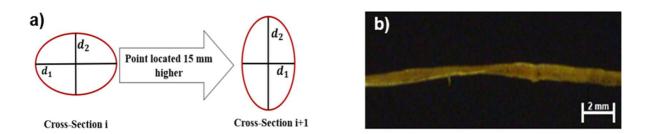


Figure 6: (a) Illustration of the change of orientation between two consecutive sections and (b) Bundle with local twisting

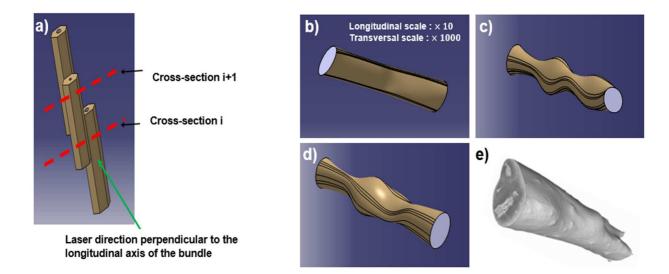


Figure 7: (a) Example of elementary fibre disposition which could induce a change of orientation of the cross-section according to our calculation method, (b) 3D reconstruction of the outer contour of bundle with little morphological variation, c) 3D reconstruction of the outer contour of bundle with strong morphological variations, d) A 3D reconstructed bundle with the average values of lengthwise evolution of the cross-section and e) 3D reconstruction of a bundle outer contour by X-ray nanotomography (Del Masto, 2018)