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# Compact Wide-Angle Scanning Multibeam Antenna Array for V2X Communications

Muhammad K. Ishfaq<sup>1</sup>, Suleiman. A Babale<sup>2</sup>, Hassan T. Chattha<sup>3</sup>, M. Himdi<sup>4</sup>, Ali Raza<sup>1</sup>, M. Younas<sup>1</sup>, Tharek. A. Rahman<sup>5</sup>, Sharul Kamal A. Rahim<sup>5</sup>, Bilal A. Khawaja<sup>3</sup>

**Abstract**— This paper presents a wide-angle scanning multibeam Planar Inverted-E Antenna (PIEA) array for V2X communication. The compact 4-element PIEA array is designed with  $0.3\lambda_0$  spacing, which achieves  $90^\circ$  wide-angle scanning when a  $135^\circ$  phase shift is applied obtained using a 4x4 Butler matrix (BM). The closeness of the array elements causes high mutual coupling and high cross-polarization at wider scan angles. Therefore, three novel techniques are employed to overcome the high cross-polarization and mutual coupling between antenna elements in this array. To feed the antenna array, a low-cost miniaturised beamforming 4x4 Butler matrix (BM) circuit is designed without the use of phase shifters and conventional crossovers. The total dimensions of the compact PIEA array are just  $0.456\lambda_0 \times 1.12\lambda_0 \times 0.036\lambda_0$  while the overall dimensions of the multi-beam array including Butler Matrix are  $2.731\lambda_0 \times 2.2\lambda_0 \times 0.046 \lambda_0$ . This multi-beam array achieves for the first time the wide-angle scanning angles of  $\pm 87^\circ$  with a 3-dB beam scanning range of  $\pm 120^\circ$  along with the scanning angles of  $\pm 20^\circ$ . This array design can be scaled to use as an antenna array for mm-wave applications.

**Index Terms**— PIEA Array, Wide-angle Scanning, Mutual coupling, Butler Matrix, Modified Coupler, Phase shifter, V2X

## I. INTRODUCTION

The driverless cars and the autonomous driving features in vehicles have greatly increased the interest in Vehicle to everything (V2X) communications (Fig. 1). At present, V2X communication is relying on Dedicated Short-Range Communication (DSRC) 5.9 GHz (5.85-5.925 GHz) band [1-2]. In the future, cellular-vehicle to everything (C-V2X) communication will make use of readily available 5G infrastructure at sub-6 GHz, 28 GHz and 39 GHz bands [3]. To bring V2X to fruition, wide coverage antennas, MIMO, compact switched beam arrays and beamforming arrays are the key enabling antenna technologies [3,4]. The Switch Beamforming Network (SBFN), which is an arrangement of antenna array capable of generating a highly directive beam and steer it to desired directions [5]. There are several types of SBFN, such as the Blass matrix [6], the Rotman lens [7], the Nolen matrix [8], and the Butler matrix (BM) [9]. The most

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popular among these techniques is BM for having a relatively simple configuration and low-power dissipations [10-13]

For designing compact arrays, mutual coupling severely degrades the performance of the beamforming arrays [14]. The research works in [14],[17] present compact designs but have a limited scanning range using high-cost phase shifters. The design in [15] is a compact phased array using high-cost phase shifters, but it had limited scanning and very high cross-polarization around 0 dB at  $70^\circ$  scan-angle making it unable to be used for wide-angle scanning. The research in [16] presented a wide-angle scanning array using reconfigurable pattern elements with a scanning range of  $\pm 75^\circ$ . However, the design is not compact (spacing,  $1.2\lambda$ ).

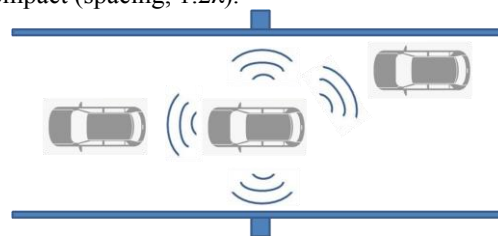


Figure 1: Vehicle-to-Vehicle (V2V) communication example

This work presents a low cost, miniaturized compact multibeam wide-angle scanning array at DSRC 5.9 GHz band for V2X communication. Since compact arrays suffer from high mutual coupling [14] and high cross-polarization at wider scan angles [15]. Therefore, to mitigate mutual coupling and high cross-polarization, three novel techniques are employed, which include employing a reduced size PIEA, etching long slots in-between adjacent array elements, and designing and placing two decoupling meandered line structures in-between the adjacent array elements. To feed the antenna array, a miniaturized BM is designed without the use of phase shifters and classical crossovers. Hence, for the first time, the far beam is achieved at  $\pm 87^\circ$  using the novel compact wide-angle scanning multibeam PIEA array proposed with  $0.3\lambda_0$  spacing. The array design can also be scaled to mm-wave as presented in [18].

## II. WIDE ANGLE SCANNING ARRAY DESIGN

A PIEA array is designed with a  $0.3\lambda_0$  spacing to achieve wide-angle scanning. Using PIEA (a modified dual shorting PIFA) as an array element results in reduced mutual coupling due to the formation of a naturally formed slot antenna in-between the neighboring array elements [19]. However, it suffers from high cross-polarization and poor gain at wider scanning angles [15]. Thus, to overcome high cross-

polarization and high mutual coupling, the following design procedure/techniques are employed:

(i) As a first step, the single PIEA is designed with the compact structure having reduced width to accommodate the increased inter-corner spacing,  $Se$ , while maintaining spacing to  $0.3\lambda_0$ . It helps in reducing radiations due to the naturally formed slot antenna in-between the two adjacent antenna elements.

(ii) To reduce mutual coupling the slots having width  $Se$ , are etched in the ground plane in-between each of the two adjacent array elements. It reduces the coupling current between the two adjacent antennas.

(iii) To further reduce mutual coupling and cross-polarization, two decoupling Meandered Line (ML) structures possessing high inductive reactance are introduced at distances  $Y_{S2}$  and  $Y_{C2}$  from the PIEA corner, in the slots in-between each of the two adjacent array elements, as shown in Fig. 2(c). The ML-structure detailed dimensions are zoomed-in in Fig. 2(c).

To feed the antenna array using BM, a feeding mechanism is designed. All the array elements are fed by a 50- $\Omega$  microstrip feed line ( $L_{f2} \times W_{f2}$ ), etched at  $L_{f1}$ , as shown in Fig. 2(b). The copper of the feed-side ground blocks the slots and decoupling ML structure. To avoid blockage and any variation in the impedance of ML structures, all the copper is etched except which is precisely below the feed line (i.e.  $L_{f2} \times W_{f2}$  as shown in Fig. 2(c)).

Fig. 2 shows the 3D and back view of the proposed compact antenna array having four PIEA elements. Figure 2 (a) shows the configuration of a single element. Roger RT/Duroid 3003 ( $\epsilon_r = 3$ ) is used as the dielectric material (thickness,  $t = 0.25$  mm). Table-1 shows the optimized values of the design parameters of the array.

The  $S_{11}$  &  $S_{22} < -10$  dB in Fig. 3 (a) indicate that the array is performing well from 5.3 GHz to 6.75 GHz. While the mutual couplings  $S_{12}$  &  $S_{23} < -10$  dB show that the techniques employed have effectively suppressed the mutual coupling. The current distribution in Fig. 3 (b) shows that the decoupling ML structure exhibits a high inductance, which reduces the mutual coupling. While the opposite current flowing in the meandered line structure cancels out the radiations, which helps to minimize the cross-polarization.

TABLE I: OPTIMIZED DESIGN VALUES OF PIEA ARRAY

Parameter	Value (mm)	Parameter	Value (mm)
$W_{e2}$	0.5	$L_{f1}$	2.5
$W=W_G$	11	$d_e$	15
$L_G$	22.8	$Se$	4
$W_s$	1	$L_{f2}$	12.5
$W_f$	6	$L_{g1}$	2.5
$L$	8.5	$L_{g2}$	8.61
$h$	1.8	$W_2$	0.26
$L_s$	1	$W_3$	0.95
$W_{f2}$	0.615	$W_4$	1.31
$Y_{C2}$	16	$W_5$	0.15
$Y_{S2}$	0.04	$t$	0.25
$Wg\_array$	56	$\lambda_0(5.9\text{ GHz})$	50.8

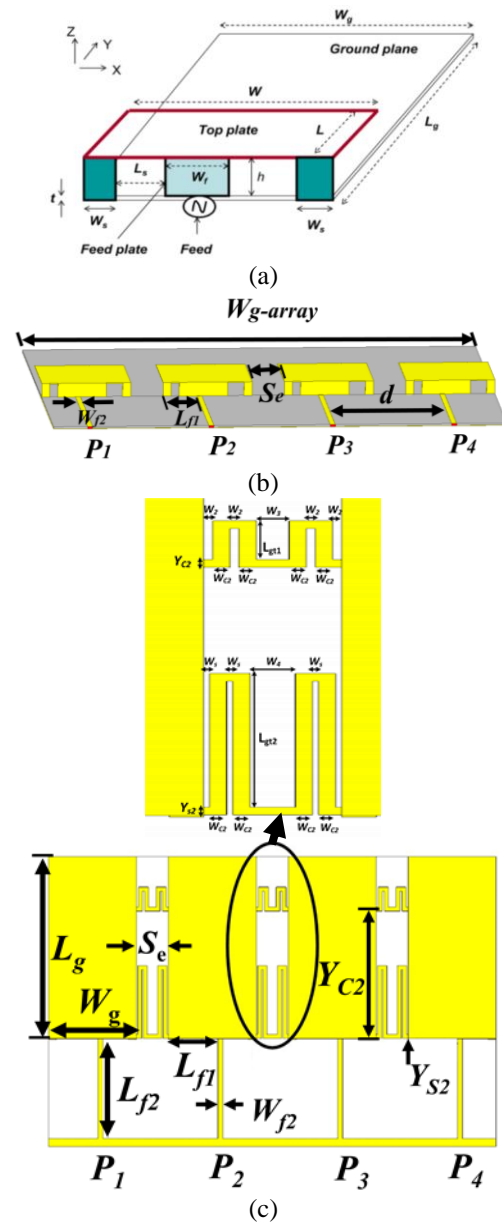


Figure 2: Planar Inverted-E Antenna (PIEA) Array (a) Single Element, (b) Array Top with feeding Part (c) Array Ground plane with Zoom in Highlighting the Decoupling Structure

### III. BUTLER MATRIX DESIGN

Generally, 4x4 BM consists of 90° couplers, 45° phase shifters, and crossovers by combining two 90° couplers [10]. In this work, the BM without phase shifters is designed using the cross-coupled crossover. The 4x4 BM presented in this paper utilizes only the microstrip couplers and a crossover in a planar structure. Employing the modified 45° couplers in this design eliminate the use of phase shifters [20]. This reduces the dimension and transmission loss of the device by shortening the transmission line path, thus reducing the problem of insertion loss and reducing the number of components required in forming BM. The layout of the BM is shown in Fig. 4.

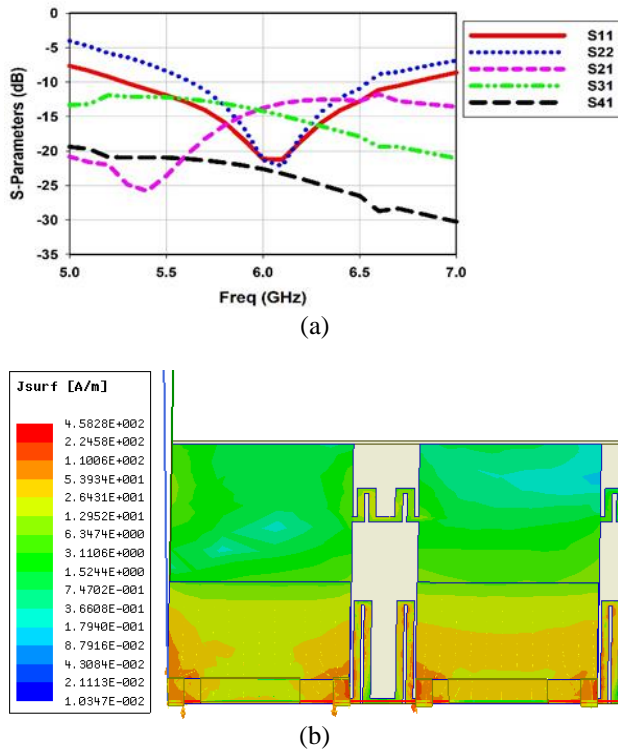


Figure 3: Planar Inverted-E Antenna (PIEA) Array (a) S-Parameters (dB), (b) Current Distribution

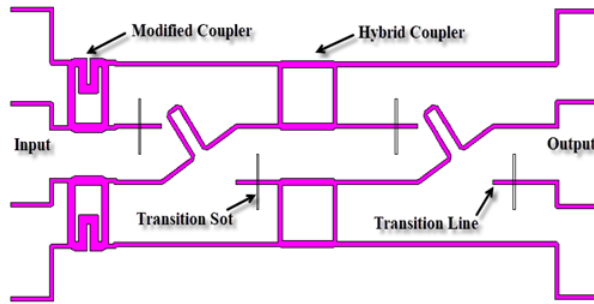


Figure 4: Layout of the cross-coupled BM

Fig. 5(a) shows the reflection coefficient and transmission coefficients when port 1 of the BM is energized. Likewise, Fig. 5(b) shows the S-parameters when port 2 of the BM is energized while the remaining three ports are terminated with a 50 ohms load. Similarly, due to the symmetry of the BM, exciting ports 3 and 4 have a similar effect as ports 2 and 1 respectively. From Fig.5(c), it can also be seen that the progressive phase difference at the outputs of the BM are  $+45^\circ$ ,  $-135^\circ$ ,  $+135^\circ$ , and  $-45^\circ$  at the operating frequency, when ports 1, 2, 3, and 4 are excited respectively. This conforms with the theoretical values.

### III. FABRICATION AND MEASUREMENTS

The proposed multibeam wide-angle scanning PIEA array design was excited using the 4x4 BM designed in section III and the overall system was tested and measured in an anechoic chamber. Fig. 6 shows the complete fabricated prototype of the multibeam antenna array. Fig. 7 shows the simulated and

measured S-parameters of the compact multibeam PIEA array when Port-1 is fed. Between 5.5 to 6.3 GHz, the reflection coefficients and port isolations are below  $-10$  dB, which confirms that the multibeam array performs well for DSRC 5.9 GHz band. When Port 2 and 3 of the BM are excited, the main pattern radiates at an angle of  $\pm 20^\circ$  with a cross-polarization  $< -18$  dB, and when the power is excited at ports 1 and 4, the angle switches to  $\pm 87^\circ$  with a cross-polarization  $< -13$  dB. The output radiation patterns are depicted in Fig. 8. Both the measurements and the simulation results matched with little disparity due to fabrication limitations. Most of the 4x4 BM multibeam array literature shows the multibeam at  $\pm 14^\circ$  and  $\pm 48^\circ$  [9],[10], while this design radiates multibeam at  $\pm 20^\circ$  and  $\pm 87^\circ$ . The reason for this wide scanning angle using 4x4 BM is because of the closeness of the array spacing to  $0.3\lambda_0$ , achieved by employing the novel techniques to effectively reduce mutual coupling and cross-polarization.

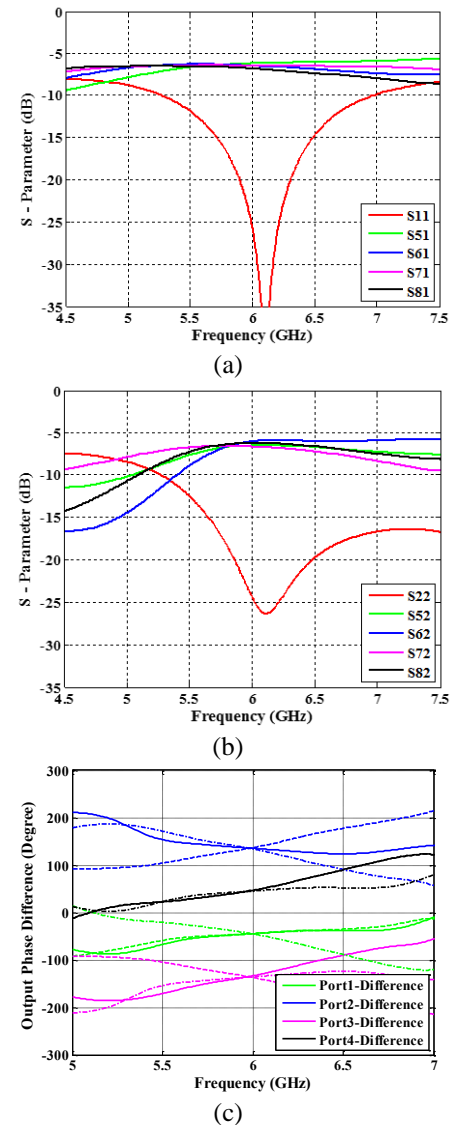


Figure 5: Reflection & Transmission Coefficients When: (a) Port 1 and 3 excited (b) Port 2 and 4 excited, (c) Output Phase Differences (P1-P4)



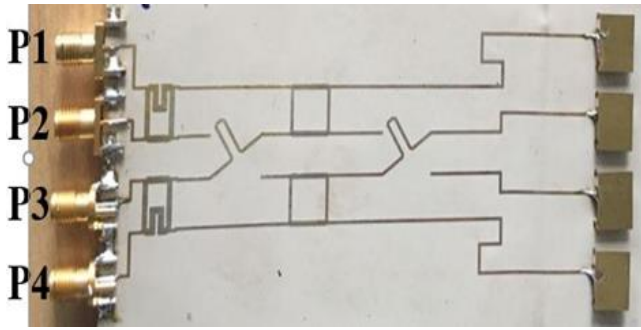


Figure 6: Photograph of the multibeam antenna array

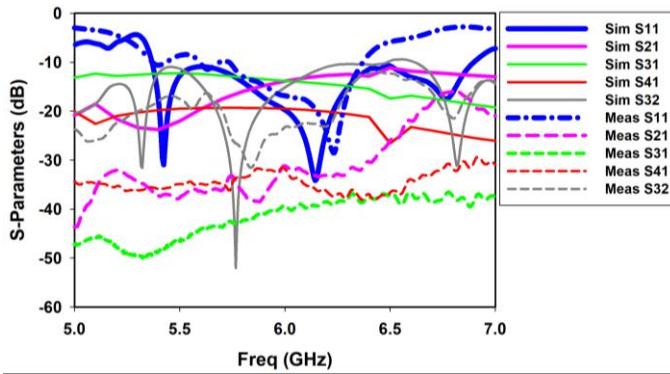
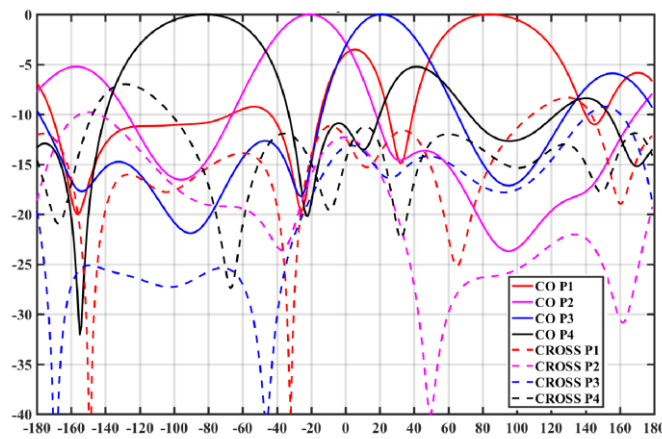


Figure 7. S-parameters of Multibeam Array

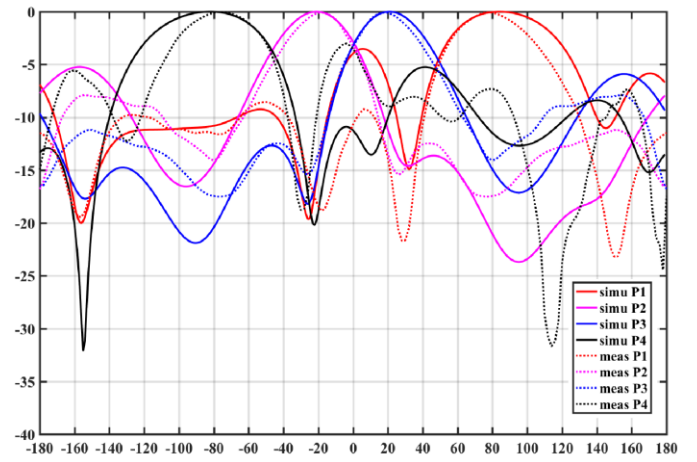
Hence very wide-angle maximum azimuthal scanning angle of  $\pm 87^\circ$  with a 3-dB scanning range of  $\pm 120^\circ$  is achieved using a compact miniaturized multibeam array. Table II shows the simulated and measured beam positions of each beam.

TABLE II: SIMULATED AND MEASURED BEAM-POSITIONS

Port No.		P1	P2	P3	P4
Beam Position( $\theta^\circ$ )	Simulated	+87°	-20°	+20°	-87°
	Measured	+86°	-20°	+20°	-86°
3 dB Beamwidth		71°	45.8°	44.4°	79.2°



(a)



(b)

Figure 8. Multibeam capability (H-plane), (a) Simulated (b) Measured

#### IV. CONCLUSION

This paper has presented a novel miniaturized compact multibeam wide-angle scanning PIEA array with a spacing of  $0.3\lambda$ , designed, fabricated, and characterized for the V2X applications. As a reduced array, inter-element spacing results in high mutual coupling and cross-polarization. Therefore to suppress mutual coupling and high cross-polarization, the design employs novel techniques that are: a compact PIEA designed with reduced width to accommodate an increased inter-corner spacing, the slots etched in between adjacent array elements and two decoupling meandered-line high impedance structures in these slots. This proposed PIEA array design is fed by a compact miniaturized 4x4 Butler Matrix. BM is designed without using phase shifters and conventional crossover. A slot-couple line is designed as a substitution of classical crossovers. With these techniques, when the compact multibeam array is developed, the far beams were successfully achieved, for the first time at  $\pm 87^\circ$ , with a 3-dB beam scanning range of  $\pm 120^\circ$ . Multibeam array produced four beams at  $-87^\circ$ ,  $-20^\circ$ ,  $+20^\circ$ , and  $+87^\circ$ . The wide-angle scanning array design can be used as a phased array by using phase shifters to achieve a continuous 3-dB scanning range of  $240^\circ$  ( $\pm 120^\circ$ ) and can be scaled to mm-wave.

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