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When does a parsimonious model fail to simulate floods? Learning from the seasonality of model bias

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ABSTRACT

Identifying situations where a hydrological model yields poor performance is useful for improving its predictive capability. Here we applied an evaluation methodology to diagnose the weaknesses of a parsimonious rainfall-runoff model for flood simulation. The GR5H-I hourly lumped model was evaluated over a large set of 229 French catchments and 2990 flood events. Model bias was calculated considering different streamflow time windows, from calculations using all observations to analyses of individual flood events. We then analysed bias across seasons and against several flood characteristics. Our results show that although GR5H-I had good overall performance, most of the summer floods were underestimated. In summer and autumn, compensations between flood and recession periods were identified. The largest underestimations of flood volumes were identified when high-intensity precipitation events occurred, especially under low soil moisture conditions.

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1 Introduction

1.1 On the need to improve hydrological models for flood forecasting

Reliable hydrometeorological predictions are important for mitigating the hazards associated with floods, including loss of lives and livelihoods as well as economic losses (e.g. Carsell et al. 2004, Hallegatte 2012, Jeuland et al. 2019). Many operational flood forecasting systems have been implemented around the world to produce streamflow forecasts (Pappenberger et al. 2016) and hydrological models are the basis of these flood forecasting systems (Pagano et al. 2014). However, streamflow predictions produced by these models are still subject to large uncertainties (Roundy et al. 2018). Different sources of uncertainty can affect the predictive capability of hydrological models (e.g. Beven 2016). These uncertainties can be related to the input data, model parameterization or model structural deficiencies, for example. Consequently, advances in hydrological modelling are needed to obtain more accurate estimates of flood peak, timing and volume, and therefore issue earlier and better warnings (e.g. Pagano et al. 2014, Jain et al. 2018). Flood forecasting systems have been improved over the years (e.g. Zanchetta and Coulibaly 2020). For example, the use of continuous models instead of event-based models allowed a reduction of the uncertainty associated with initial conditions (e.g. Berthet et al. 2009, Grimaldi et al. 2020). However, common failures to predict floods are still encountered. For example, the severe floods that occurred in the Seine and Loire rivers and their tributaries (France) in June 2016 were underestimated by our own GRP flood forecasting model (Berthet 2010, Viatgé et al. 2019). Hydrological models are also less reliable in arid or dry areas (e.g. McMillan *et al.* 2016, Melsen *et al.* 2018), especially when flash floods occur (Hapuarachchi *et al.* 2011). Improving the predictive capability of hydrological models is therefore essential for improved flood forecasting.

1.2 Relevance of large-sample model diagnostics

To be able to improve a model, one must first identify situations where the model fails to yield reliable results, i.e. the firstorder factors leading to simulation errors (Gupta et al. 2008). In this regard, various diagnostic methods have been used on hydrological models. Some studies were based on a limited number of catchments (e.g. Butts et al. 2004, Clark et al. 2008, Nicolle et al. 2014). Diagnostics are now increasingly relying on large-sample approaches in order to draw more general conclusions from model performance (e.g. Andréassian et al. 2009, Gupta et al. 2014). Large-sample studies make it possible to establish performance benchmarks, i.e. to determine the current performance of hydrological models across a representative set of catchments (e.g. Seibert 2001, Seibert et al. 2018). The effects of changes in, for instance, model structure or parameterization can then be assessed in light of the performance of the benchmark. Several recently published country-scale studies investigate different model structures over large sets of catchments representing a variety of hydroclimatic conditions. For example, Lane et al. (2019) investigated the predictive capability of four models over 1000 catchments in the UK and the relationships between model performance and catchment attributes, flow regimes and model structures. Knoben et al. (2020) compared the



performance of 38 models over 559 US catchments and highlighted groups of models for which the structural hypotheses were better suited for some catchments rather than others (e.g. seven models had better performance for flashy catchments).

1.3 Model evaluation issues

One of the challenges of large-sample hydrology is related to the advantage of exploiting the robust statistical properties of large samples (Mathevet et al. 2006, 2020) while summarizing the results into an understandable outcome but still maintaining a certain degree of precision to find emerging patterns (Gupta et al. 2014). Many large-sample studies used aggregated statistics to assess model performance across comprehensive datasets (e.g. Perrin et al. 2008, Vaze et al. 2010, 2011, Coron et al. 2012, Andréassian et al. 2014). Some comparative studies of rainfall-runoff models found similar levels of performance between model structures when using aggregated metrics (e.g. Perrin et al. 2001, Van Esse et al. 2013). It has been widely recognized that the use of single aggregated metrics is not sufficient to assess model performance (e.g. Schaefli and Gupta 2007, Euser et al. 2013). For example, Mathevet et al. (2020) compared the performance of two conceptual models across a global set of catchments within a multi-objective framework. They found that while the two models yielded similar overall performance, when looking at sub-period statistics, one model performed slightly better in short-term processes. Furthermore, commonly used performance indicators, such as the Nash-Sutcliffe efficiency criterion (NSE; Nash and Sutcliffe 1970), are known to be biased towards high flows, although their use in model calibration leads to underestimation of flow variability (Gupta et al. 2009) and a limited ability to reproduce extreme flows (Oudin et al. 2006, Crochemore et al. 2015). Therefore they must be used cautiously when evaluating the ability of models to simulate floods.

Hydrological signatures have been found useful in improving the identification of patterns between model performance and our understanding of underlying catchment processes (Yilmaz et al. 2008, Hrachowitz et al. 2014, McMillan et al. 2017). They are used as indicators of situations where models perform well and are suitable for further applications. Consequently, a growing number of studies are using sets of hydrological signatures for model evaluation to emphasize particular aspects of the hydrograph (e.g. Shafii and Tolson 2015, Donnelly et al. 2016, Poncelet et al. 2017, Gnann et al. 2020). Signatures to investigate model performance on high flows can be, for example, the runoff volume above the 80th percentile of the flow duration curve (Yilmaz et al. 2008). Another way to highlight model errors in flood predictions is to evaluate the simulation of peak flows by calculating specific criteria, such as the time to peak or the peak flow ratio. For example, Mizukami et al. (2019) investigated the choice of objective functions to better simulate high flows by calculating the annual peak flow bias.

1.4 A focus on events and seasonality

Event-based models are usually evaluated by their ability to reproduce several flood characteristics, such as rising limb, peak flow magnitude or timing (e.g. Borah et al. 2007, Javelle et al. 2010, Stanić et al. 2018, Stephens et al. 2018). To focus on the ability of continuous models to reproduce floods, model performance can also be assessed against a set of events in streamflow time series. By selecting 3620 flood events in 181 catchments, Lobligeois et al. (2014) identified where and when accounting explicitly for the spatial variability of rainfall and potential evapotranspiration inputs (i.e. by using a semidistributed approach) improved streamflow simulations. Ficchì et al. (2016) showed that the peaks and timing of 2400 floods in 240 catchments were better reproduced at sub-daily time steps than at a daily time step. Vergara et al. (2016) evaluated the regionalization of the parameters of a hydraulic routing function by calculating peak flow and timing errors in the simulation of 47 563 flood events. de Boer-Euser et al. (2017) compared eight hydrological models in one catchment and found similar results in terms of overall performance but clear differences when looking at specific events and metrics. For different purposes, these studies showed that a change of focus in model evaluation, e.g. investigating flood events, can help to identify patterns in the performance of hydrological models.

Streamflow can have strong seasonal variations depending on climate seasonality and catchment characteristics (Berghuijs et al. 2014, Gnann et al. 2020). The seasonal streamflow variations also reflect varying antecedent soil moisture conditions, which can have significant impacts on flood event generation (Blöschl et al. 2013, Berghuijs et al. 2014). In terms of model diagnostics, some studies used signatures to assess the ability of the models to simulate the streamflow regime (e.g. Wang et al. 2008, Massmann 2020). Other model evaluations investigating the seasonality of model performance relied on the analysis of metrics calculated for each season of the year independently (e.g. Muleta 2012, Kim and Lee 2014, Lane et al. 2019).

1.5 Scope of the paper

While it is clear that analysing the performance of hydrological models in simulating flood events can help to characterize model performance, a deeper investigation on the seasonality of model performance considering different streamflow time windows has, to our knowledge, not been conducted to date. In an effort to find patterns of model errors and therefore help target model improvements, we apply a new methodology to assess the simulations of a continuous conceptual rainfall-runoff model over a large sample of flood events at an hourly time step. Bennett et al. (2013) suggested that, to evaluate environmental models, we must first look at basic performance criteria and then refine the analyses depending on the problem at hand. Here we follow these recommendations and aim to probe deeper in the analyses by looking at the seasonality of model bias through different disaggregations of the observed hydrograph. The objectives of this paper are (i) to determine whether investigating the seasonality of model bias through different streamflow time windows can provide information on model deficiencies in simulating high flows and (ii) to identify factors causing model weaknesses in flood simulations.



2 Data

2.1 Catchment set

A total of 229 catchments in France were selected, representing varying hydroclimatic and morphological characteristics (Fig. 1). This catchment selection originates from the work of Ficchì et al. (2016). Snow and human activities have limited impacts on the streamflow of these catchments. Eleven catchments were discarded from the original set because of lowquality data, a too-high percentage of missing streamflows or a high solid precipitation fraction (i.e. with more than 10% of solid precipitation). A summary of the catchment set characteristics is given in Table 1. Further information can be found in the studies by Ficchì et al. (2016) and Ficchì (2017). The baseflow index values higher than 0.9 correspond to two catchments located in the northern part of France, where flow is dominated by the contribution of a dual-porosity chalk aquifer. Two karstic catchments, the Laine River at Soulaines-Dhuy and the Siagne River at Callian, are included in our dataset and have runoff coefficients higher than 1. Flashy catchments, i.e. with high-intensity precipitation and low values of flow autocorrelation, are mainly located in the Mediterranean region and in the Cévennes area in southern France. A large part of the catchments in our dataset are characterized by pluvial streamflow regimes (as defined by Sauquet et al. 2008), where most periods of high flows are in winter and most periods of low flows are in summer. Fourteen catchments are in the transition regime, meaning that high flows occur in winter and spring because of the influence of both rainfall and snowmelt. We chose to keep these catchments for our analyses because Valéry (2010) showed that the sensitivity of model simulations to snow dynamics is limited when the part of solid precipitation is less than 10%.

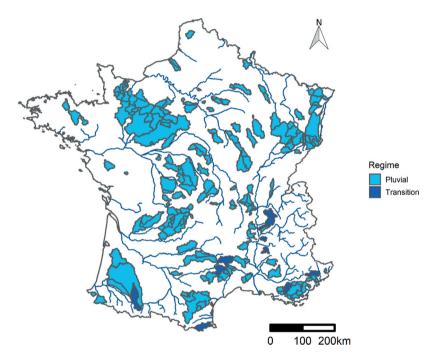


Figure 1. Location of the 229 French catchments selected. The streamflow regimes were determined according to the definition of Sauquet et al. (2008).

Table 1. Distribution of nine hydroclimatic and five morphological characteristics of 229 catchments. P99 is the 99th percentile of daily streamflow.

Characteristic	Definition/reference	Min	Q25	Med	Mean	Q75	Max
Area [km²]	-	3.54	164.1	354.1	680.3	772.3	7918
Average altitude [m]	-	70	198	358	383	519	1060
Average slope [-]	-	0.01	0.03	0.05	0.06	0.08	0.24
Topographic index [-]	Ducharne (2009)	8.19	12.13	13.26	13.13	14.25	17.33
Drainage density [km²]	Le Moine (2008)	0.06	0.3	0.51	1.19	1.08	19.8
Mean flow (Qm) [mm/year]	-	35	262	349	437	524	1398
Mean annual temperature (°C)	-	8.2	9.8	10.4	10.6	11.1	14.3
Fraction of solid precipitation (%)	-	0.5	2.2	3.1	4.1	5.9	9.4
Mean annual precipitation	-	651	818	937	990	1097	2108
(Pm) [mm]	-	594	664	708	739	767	1129
Mean annual potential							
Evapotranspiration (PEm) [mm/year]	-	0.39	0.77	0.84	0.83	0.91	1.00
Flow auto-correlation at 24 h [-]							
Runoff coefficient [-]	Qm/Pm	0.04	0.27	0.35	0.38	0.46	1.71
Aridity index [-]	Pm/PEm	0.66	1.10	1.32	1.37	1.55	3.47
Daily precipitation intensity [-]	P99/Pm	7.58	8.57	9.19	10.56	11.53	19.89
Baseflow index [-]	Gustard et al. (1992)	0.19	0.46	0.57	0.56	0.65	0.95
Rainfall-runoff lag time [h]	Ficchì (2017)	1	8	15	21	26	117



2.2 Hydroclimatic data

Time series of precipitation at an hourly time step were aggregated at the catchment scale from the Comephore product (Tabary et al. 2012), provided by Météo-France at a 1-km over the French metropolitan Comephore offers a quantitative precipitation reanalysis combining all of the available information from weather radars and rain gauges. The time series of daily temperature extracted by Delaigue et al. (2020) from the SAFRAN climate reanalysis database of Météo-France (Vidal et al. 2010) were used to calculate potential evapotranspiration (PE) time series with the Oudin et al. (2005) formula. The daily PE time series were then disaggregated at the hourly time step by assuming a parabolic shape from 6:00 a.m. to 7:00 p.m. (UTC). The maximum PE values are between 12:00 a.m. and 1:00 p.m. Instantaneous streamflow data from the database of the French hydrometric services (Leleu et al. 2014) were interpolated to obtain hourly time series. Precipitation, temperature and streamflow time series covered the period from 1 August 2005 to 31 July 2013. Two independent sub-periods were considered: P1, from 1 July 2005 to 31 June 2009; and P2, from 1 July 2009 to 31 June 2013. For most catchments, these periods are similar in terms of mean runoff coefficient and PE. Differences in the runoff coefficient higher than 5% between P1 and P2 are found in only three tributaries of the Rhône River (downstream): the Ardèche River at Ucel, the Cèze River at Tharaux and at Montclus, and the Argens River at Arcs located in the Mediterranean area.

2.3 Selection of flood events

An automated procedure was used to select 2990 flood events in the catchment dataset: 1681 events in P1 and 1309 events in P2. On average, 13 events were selected per catchment. The number of selected events ranges from 3 to 16 events per catchment. Only events with peak flow higher than the 95th streamflow quantile were selected. Flood event periods were taken from the time when streamflow is higher than 20% of the event peak flow to the time when streamflow is lower than 30% of the event peak flow. Each flood event was then visually inspected to avoid overlaps and other errors arising from the automated selection procedure. Figure 2 illustrates some of the flood event characteristics per season. In Fig. 2(c), the ratio of flood volume to total water volume was computed as the ratio between the volume of each flood and the total water volume.

Winter was considered to extend from the beginning of January to the end of March, spring from April to June, summer from July to September, and autumn from October to December. The highest flow peaks relative to mean catchment flow occurred in summer and autumn, mostly in tributaries of the Rhône River and in the Mediterranean region. Summer events are shorter and lower in volume than the other flood events in our dataset. Figure 3 shows that the volume of the selected events ranges from 2% (spring 5th percentile) to 45% (autumn 95th percentile) of the total streamflow volume of the corresponding season. The spring events represent a smaller fraction of the overall spring streamflow volume, whereas autumn events represent a larger proportion of the streamflow volume of the corresponding season.

3 Methods

3.1 Hydrological model and parameter calibration

The continuous GR5H lumped conceptual rainfall-runoff model (Le Moine 2008, Lobligeois 2014) was used to simulate streamflow hourly time series at the outlet of each catchment. We used a version that integrates an interception store (GR5H-I), as formulated by Ficchì et al. (2019). Full mathematical details of the model are given in the Appendix. We performed a continuous split-sample test (Klemeš 1986) to obtain two parameter sets, on P1 and P2, respectively. The model has five free parameters that were estimated for each catchment and each independent sub-period. A warm-up period of 2 years preceding the beginning of each sub-period was applied to initialize the model's states. The hourly precipitation time series of the warm-up period before P1 was built from a uniform disaggregation of the daily time series of the SAFRAN climate reanalysis data. The parameter estimation procedure is based on the algorithm developed by Michel (1991), a local gradient-based optimization procedure preceded by a gross screening of the parameter space (243 parameter sets tested; see the EGD method of Perrin et al. 2008) so as to identify a suitable starting point. We used the same starting parameter sets for each catchment. These parameter sets correspond to the 10th, 50th and 90th percentiles of 900 catchments (see Perrin et al. 2008 for more details). The parameter set that maximized the Kling-Gupta efficiency criterion (KGE; Gupta et al. 2009) was selected with the automated procedure. The interception store capacity was estimated before applying the parameter estimation algorithm. Its value was defined by minimizing the difference between daily and hourly interception fluxes as suggested by Ficchì (2017). Computations were made in the R environment using the airGR package (Coron et al. 2017, 2021).

3.2 Evaluation

GR5H-I simulations were first assessed by looking at the KGE criterion calculated for the whole time series of each calibration and evaluation period. This gives a general overview of the model performance across our large set of catchments. The simulations were then evaluated by calculating the bias considering four levels of hydrograph disaggregation, i.e. different streamflow periods. Bias is a basic but essential indicator when evaluating how the model performs. Several studies showed the importance of investigating model bias, for example, to evaluate the robustness of rainfall-runoff models (e.g. Coron et al. 2012, Fowler et al. 2016). When investigating specific events, it is an indicator of how well a model is able to simulate flood volumes. These four criteria were calculated after model crossvalidation, i.e. model application on P1 and P2 with the parameter sets of P2 and P1, respectively. In other words, the four biases were calculated on P1 with the parameter sets optimized on P2 and on P2 with the parameter sets optimized on P1. The first level of hydrograph disaggregation is the overall bias calculated for the whole time series (including flood flows, but also mean and low flows) of each sub-period independently using the following expression:

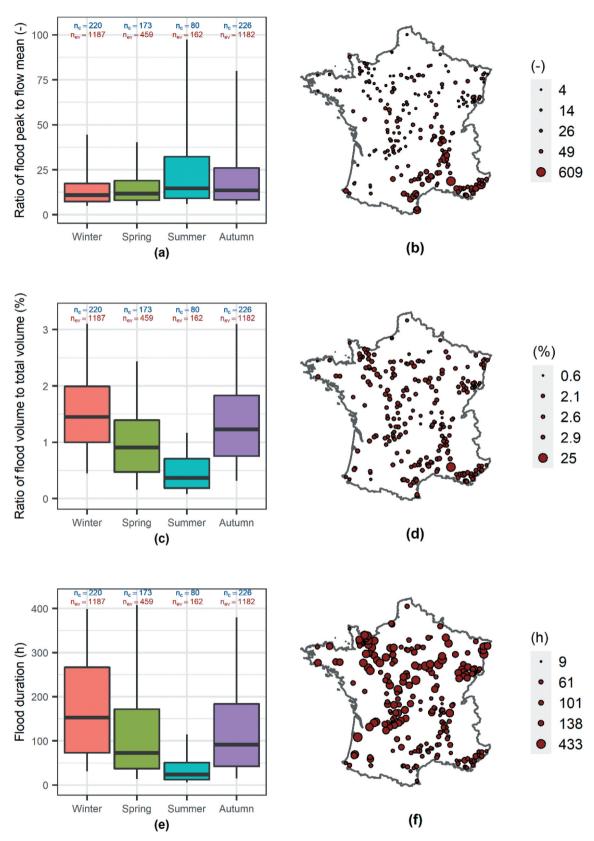


Figure 2. Distribution and localization of the characteristics of 2990 flood events. The distributions are presented between the 5th and 95th percentiles. Parts (b) and (d) present maximum values and part (f) presents mean values. n_{ev} is the number of flood events of each season and n_c is the related number of catchments.

$$\beta_{ts} = \frac{\sum_{i=1}^{p} Q_{sim,i}}{\sum_{i=1}^{p} Q_{obs,i}} - 1 \in [-1, +\infty)$$

with p being the length of the sub-period, and $Q_{\text{sim,i}}$ and $Q_{\text{obs,i}}$ being the simulated and observed hourly streamflows at time i. β_{ts} is a component of the KGE criterion. The second level of disaggregation is defined as the bias calculated for each event

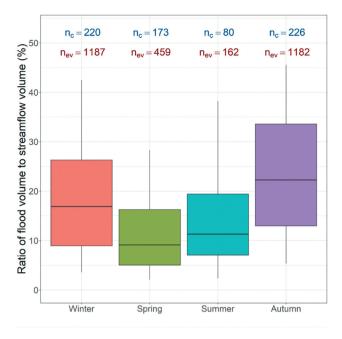


Figure 3. Distribution of catchment seasonal flood volumes compared with seasonal streamflow volume for 2990 flood events in 229 catchments. nev is the number of flood events of each season and n_c is the related number of catchments.

independently, i.e. bias is computed from flows that were observed and simulated during a specific flood event. For a given flood event, the event bias is expressed as follows:

$$\beta_{ev,j} = \frac{\sum_{i=1}^{n_j} Q_{sim,i}}{\sum_{i=1}^{n_j} Q_{obs,i}} - 1 \in [-1, +\infty)$$
 (2)

with n_i the length of the j^{th} event. A single value of β_{ev} was calculated for each of the 2990 events using cross-validation simulations. The third level of disaggregation is a measure of flood volume errors at the catchment level. It allows us to compare the catchments with the same weight – as the number of events differs between catchments - and also to compare event bias with overall bias. For each catchment, we calculated

the bias for all the events combined on each evaluation period. In other words, the bias was calculated for the streamflow time series during the flood events, i.e. without the times at which there is no flood event. The bias was calculated for each subperiod of each catchment (458 values). For a given catchment and one sub-period, the calculation is expressed as follows:

$$\beta_{cEv} = \frac{\sum_{j=1}^{m} \left(\sum_{i=1}^{n_j} Q_{sim,i}\right)}{\sum_{i=1}^{m} \left(\sum_{i=1}^{n_j} Q_{obs,i}\right)} - 1 \in [-1, +\infty)$$
 (3)

with m the number of events of the catchment in a given subperiod. The fourth level of bias is calculated in the flow time series without the times at which floods occurred. It is a measure of how the model simulates the water balance outside the selected flood events, i.e. during mean and low flows.

It will therefore help to identify compensations between streamflow periods. This bias can be expressed as:

$$\beta_{cWev} = \frac{\left(\sum_{i=1}^{p} Q_{sim,i}\right) - \sum_{j=1}^{m} \left(\sum_{i=1}^{n_{j}} Q_{sim,i}\right)}{\left(\sum_{i=1}^{p} Q_{obs,i}\right) - \sum_{j=1}^{m} \left(\sum_{i=1}^{n_{j}} Q_{obs,i}\right)} - 1$$

$$\in [-1, +\infty) \tag{4}$$

Figure 4 illustrates the streamflow time windows that are considered in the calculation of β_{cEv} and β_{cWev} .

A bounded version of these criteria, β^b , is calculated in order to facilitate comparison of results between catchments (Mathevet et al. 2006), as the bias can tend towards very large values when streamflow is overestimated. The highly skewed distribution introduces difficulties in interpreting mean values and dispersion over a set of criteria values.

$$\beta^b = \frac{\beta}{\beta + 2} \in [-1, 1] \tag{5}$$

Table 2 presents the corresponding values of β for some values of β^b . Negative values indicate underestimation of observed streamflow, and positive values indicate overestimation of observed streamflow by the model. A value of 0 indicates that there is no bias. We then refined the level of focus by investigating the seasonality of each bias. To calculate the four

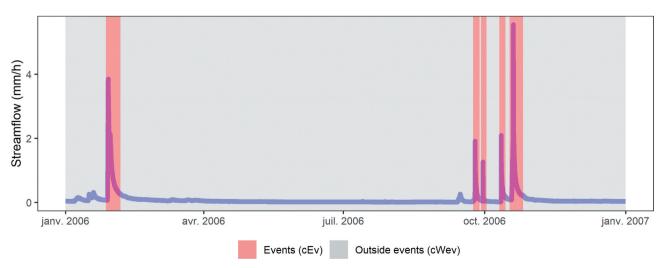


Figure 4. Illustration of the streamflow time windows used to calculate the event bias per catchment and the bias outside periods with events per catchment. The hydrograph presented here corresponds to the Lergue River at Lodève (southern France).

Table 2. Correspondence between bias (β) and bounded bias (β^b) values.

β ^b	β	β	β
- 1	–1	0	0
-0.6	-0.75	0.11	0.25
-0.33	-0.5	0.2	0.5
-0.14	-0.25	0.33	1
-0.05	-0.1	0.5	2

Table 3. List of the relative characteristics used for the univariate analysis. All characteristics are expressed as percentages.

Relative maximum hourly precipitation of the event

Relative maximum event streamflow (or peak flow)

Relative mean SWI index of the event

(ISBA model; Thirel et al. 2010a, 2010b, Coustau et al. 2015)

Relative event runoff coefficient (Q/P)

Relative event duration

seasonal biases (β_{ts} , β_{ev} , β_{cEv} and β_{cWev}), we assumed that a flood occurred in a given season if the time of peak was in that season.

3.3 Linking flood characteristics with model bias

Considering the catchments on which we identified patterns of seasonal event bias, we performed a univariate analysis between event bias and certain flood characteristics. Table 3 lists the characteristics considered in this analysis. Precipitation events were attributed to each flood event. The time window of a precipitation event was set as the time window of the corresponding flood event negatively shifted by the time of concentration of the catchment (see Table 1). The soil wetness index (SWI), calculated by the ISBA surface model (Thirel *et al.* 2010a, 2010b, Coustau *et al.* 2015), was used as an indicator of the soil moisture condition of the catchments. It is defined by Barbu *et al.* (2011) as follows:

$$SWI = \frac{w_{tot} - w_{wilt}}{w_{fc} - w_{wilt}} \tag{6}$$

with w_{tot} being the root soil moisture, w_{wilt} the wilting point and w_{fc} the field capacity. We used the daily catchment-averaged SWI values. We calculated the mean SWI values of each event. Each characteristic was then divided by its

corresponding catchment event average (over both subperiods) to compare the variability of events within catchments. For example, the relative duration of an event is calculated by dividing its duration by the average event duration of the catchment.

4 Results

4.1 Overall model performance

Figure 5 shows the distributions of KGE values over the 229 catchments and calculated for the calibration and validation periods.

The first and third quartiles (Q_1 and Q_3) in calibration mode are between 0.90 and 0.95 in P1 and between 0.91 and 0.95 in P2. In validation mode, Q_1 and Q_3 are between 0.75 and 0.90 in P1 and between 0.79 and 0.91 in P2. As expected, the distributions show a drop in performance between the calibration and validation periods. The distribution of KGE values is more scattered in P1 than in P2. This can be partly explained by a change in the runoff coefficient and cumulative rainfall between P1 and P2 for some of the catchments in our dataset (see Fig. 6).

The lowest KGE values in validation mode correspond to a few catchments located in the Mediterranean region. These results are consistent with previous nationwide studies with the GR models (e.g. Lobligeois *et al.* 2014, Ficchì *et al.* 2016, Poncelet *et al.* 2017). Crochemore *et al.* (2015) showed that KGE values between 0.66 and 0.90 are considered to represent good model performance according to expert judgement. We can therefore consider that the GR5H-I model yields good overall performance in our dataset.

4.2 Model bias on four levels of hydrograph disaggregation

We then refined the analysis and investigated whether the model was able to simulate the 2990 flood events in our catchment dataset. In this regard, the model bias was calculated considering the four levels of hydrograph disaggregation (Fig. 7) defined earlier to enable identification of

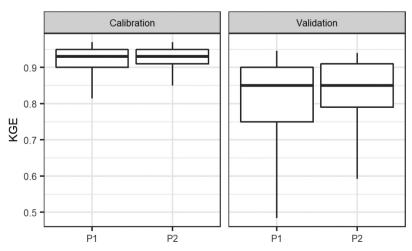


Figure 5. Distribution of GR5H-I performance in calibration and validation periods over 229 French catchments. The distributions are presented between the 5th and 95th percentiles.

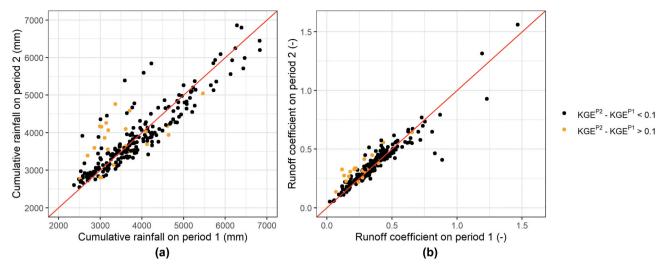


Figure 6. Difference of (a) cumulative rainfall and KGE; (b) runoff coefficient and KGE in validation mode between P1 and P2.

compensations between streamflow periods, i.e. between periods of floods and mean and low flows.

The median event bias $(\beta_{ev}^{\ \ b})$ of the GR5H-I model is equal to -0.03, and its distribution is left-skewed towards negative values. The distribution of catchment event bias $(\beta_{cEv}^{\ \ b})$ is similar to the distribution of event bias, with a median value of -0.02 and a lesser dispersion. When bias is calculated without taking the selected flood events into account $(\beta_{cWev}^{\ \ b})$, the median bias has a value of 0.01. The distribution is wider for positive values outside the interquartile range. The model bias calculated for the entire time series $(\beta_{ts}^{\ \ b})$ has a median value of 0.001 and a distribution similar to the distribution of $\beta_{cWev}^{\ \ b}$. The dispersion of the event bias is wider than the distribution of the three other biases. The dispersion of the bias calculated for the whole time series is narrower than the other distributions. Overall, these results show that there are compensations between periods

where flood events occur and the rest of the hydrograph. The four bias criteria were also calculated in the calibration period and the results showed similar patterns (not shown here).

4.3 Seasonality of model bias

We investigated to what extent certain flood events are better reproduced by the model. As the seasonal variation of streamflow affects antecedent soil moisture conditions, it is a good indicator of the variability in flood characteristics across Metropolitan France. We therefore compared the four bias criteria with the seasonality of floods (Fig. 8(a-d)).

Figure 8(b) shows that more than 75% of the observed summer floods were underestimated by the GR5H-I model. The distribution of event bias shows that the underestimation associated with summer events is much larger than with the other

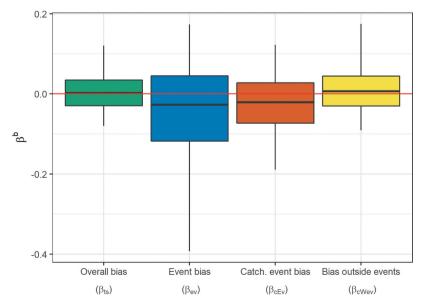


Figure 7. Distribution of GR5H-I bias over 229 catchments and 2990 events. The bias (bounded) was calculated for four levels of hydrograph disaggregation. The distributions are presented between the 5th and 95th percentiles. Calculations were made with cross-validation values, i.e. using simulations on P1 and P2 obtained with the parameter sets optimized on P2 and P1, respectively.

flood events of our dataset. Floods that occur in winter and autumn were less underestimated by the model. The distribution of bias across summer events is wider than the bias calculated for the simulations of the other flood events. The largest overestimations of floods were for autumn events. Large underestimations of summer events explain the skewness of the distribution of GR5H-I event bias presented in Fig. 7. Figure 8(c) shows that the seasonal trend of model event bias is also an intra-catchment pattern. The distributions are less dispersed but the tendency remains similar. The seasonal distribution of model bias calculated in the entire hydrograph exhibits a different pattern (Fig. 8(a)). Summer and autumn bias distributions have positive median values. Winter and spring distributions are similar to the distributions in Fig. 8 (b) and (c) but with a narrower dispersion. When the bias is calculated without flood events (Fig. 8(d)), winter and summer distributions remain similar to the time series bias. Summer and autumn periods are overestimated for 75% of the corresponding catchments. These results indicate compensation between periods

of flood events and periods where there are no flood events in summer and spring. Event bias seems to affect winter and spring periods less in our dataset.

Figure 9(a-h) presents the GR5H-I simulations of eight floods that occurred in tributaries of three major French rivers, the Rhône (Doux and Ardèche tributaries), Seine and Garonne rivers.

The GR5H-I model failed to reproduce the volumes of the summer events (Fig. 9(a, c, e, g)), whereas it was able to reproduce the volumes of four floods that occurred in other seasons (Fig. 9 (b, d, f, h)). The GR5H-I model yielded reasonable performance for the rest of the time series, as assessed by the KGE index.

4.4 Relationship between event bias and flood characteristics

Based on the 80 catchments where flood events occur in summer, we investigated the relationships between model

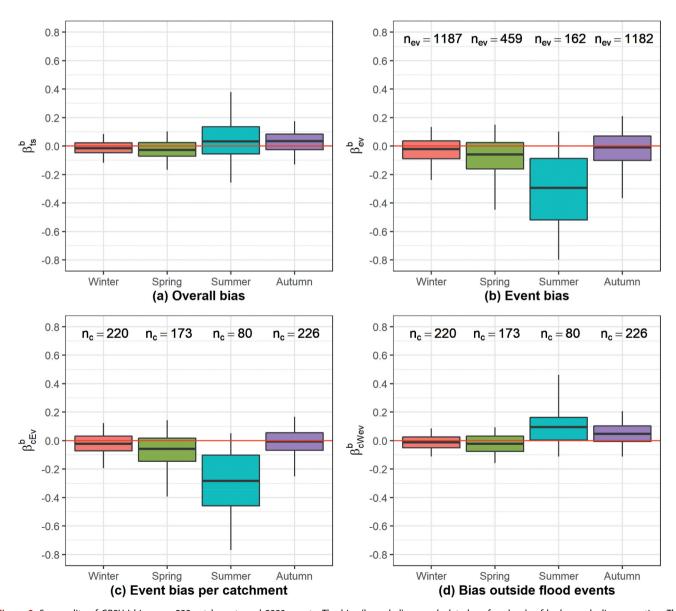


Figure 8. Seasonality of GR5H-I bias over 229 catchments and 2990 events. The bias (bounded) was calculated on four levels of hydrograph disaggregation. The distributions are presented between the 5th and 95th percentiles. Calculations were made with cross-validation values. n_c is the related number of catchments and n_{ev} is the related number of flood events. Part (c) shows the seasonal distributions for all catchments.

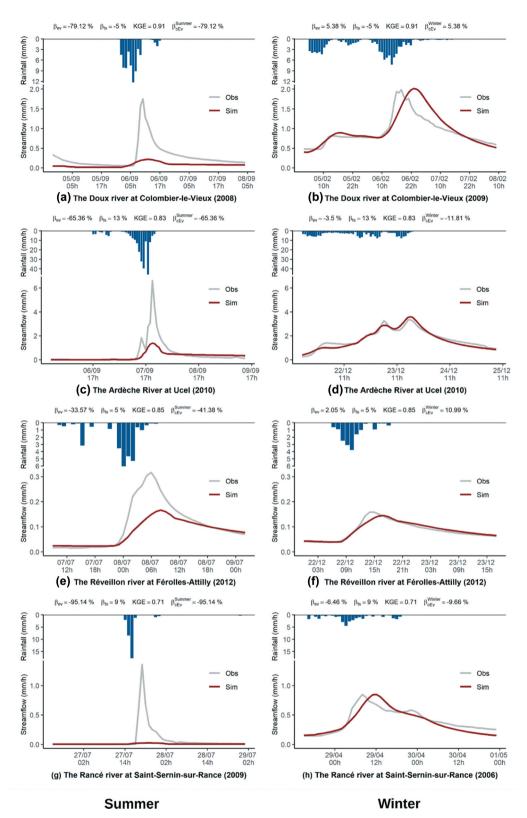


Figure 9. Examples of simulations of summer floods compared with floods that occurred in other seasons. Simulations of GR5H-I are in validation mode. β_{ev} is the flood event bias. β_{ts} and KGE are the bias and KGE index, respectively, calculated for the entire corresponding validation period.

event bias and various flood characteristics. Figure 10 presents the univariate analysis of the links between GR5H-I bias on floods and flood characteristics.

Figure 10(a) shows that GR5H-I bias is lower for flood events for which the maximum hourly precipitation exceeds 130% of the mean of maximum event precipitation. Figure 10

(b) shows that there is no clear relationship between event peak flow and model bias. Large underestimations of flood volumes are associated with low SWI index values (Fig. 10 (c)) and short-duration events (Fig. 10(e)). Interestingly, low runoff coefficient values are associated with larger underestimations (Fig. 10(d)). As expected, the highest correlation

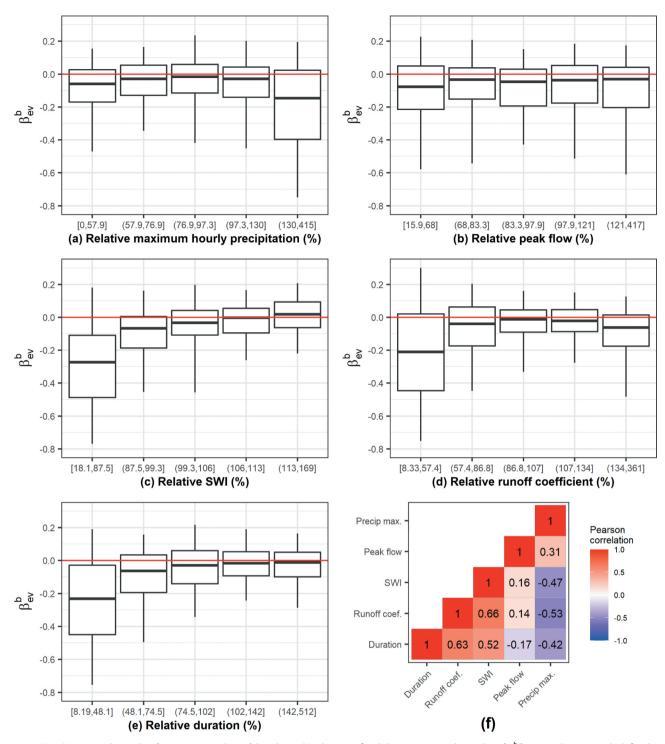


Figure 10. (a) to (e) present the results of a univariate analysis of the relationships between flood characteristics and event bias $\beta_{ev}^{\ \ b}$ for 80 catchments in which floods occur in summer. Each characteristic class contains approximatively 211 events. The flood characteristics presented are relative to the mean flood characteristics of the corresponding catchment. (b) is the linear correlation matrix between the relative flood characteristics.

between flood characteristics is between the SWI index and the runoff coefficient (Fig. 10(f)). The runoff coefficient is also positively correlated with flood duration and negatively correlated with maximum precipitation. These results indicate that the largest underestimations of flood volumes by the GR5H-I model are for short floods occurring in summer under low soil moisture conditions and when high-intensity precipitation events take place.

5 Discussion

Our analysis was based on bias calculations considering different periods of the hydrograph to evaluate the capacity of a conceptual rainfall-runoff model to simulate flood events. By refining the time window of analysis and by using the seasonality of streamflow water balance as a proxy of flood variability, we found patterns of seasonal model bias. These patterns of seasonal model bias are linked to soil moisture conditions and specific characteristics associated with the flood events. We now discuss how informative this analysis can be in light of other existing diagnostics.

5.1 How informative is the KGE index for summer events?

We have shown that calculating the model bias for different streamflow time windows enabled us to highlight compensations between high-flow periods and periods without floods as well as situations where the model was not able to simulate flood volumes. One may wonder whether these results could be obtained with aggregated statistics such as the KGE criterion. In other words, we wanted to know whether the catchments in which the model yielded low KGE values are the catchments in which the summer floods were underestimated. First, the comparison between overall bias and event bias showed differences in the ability of the GR5H-I model to simulate the global water balance and to simulate flood volumes. One reason may be the low water volumes associated with summer events compared with the other floods in our dataset (see Fig. 2). Mizukami et al. (2019) reported similar results when investigating differences in annual peak flow simulations. They showed that improving streamflow bias did not always result in better simulation of flood magnitudes. Furthermore, the results presented in Fig. 11 demonstrate that there is no clear relationship between aggregated KGE values and event bias for catchments in which summer floods occur.

This is consistent with the findings of Brunner et al. (2020), who showed that while the KGE index integrates a flow bias component, it does not explicitly account for high-flow values. These results are also in line with the study by Mathevet et al. (2020), who found that two conceptual models yielded similar results when looking at criteria calculated for the whole time series but found differences in the ability of the model to capture short-term processes when investigating criteria calculated for specific sub-periods. These results show that investigating the seasonality of model bias considering different

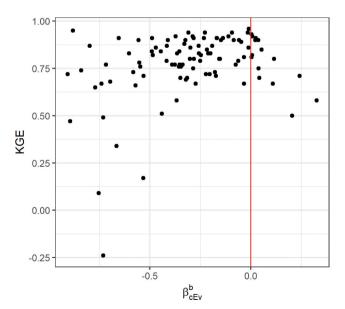


Figure 11. GR5H-I summer event bias per catchment plotted against KGE values for catchments where flood events occurred in summer.

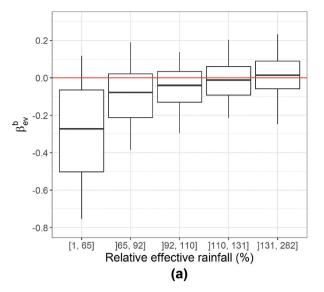
streamflow time windows can offer new information on the ability of a model to simulate specific flood events.

5.2 On the relevance of event and seasonality analyses to improve simulation of floods

To investigate seasonal patterns in model errors, other hydrological signatures could be based on the hydrological regime (or 365-d rolling mean, e.g. Mathevet et al. 2020) or the flow duration curve (e.g. Yilmaz et al. 2008). However, as presented in section 4.3, the seasonal model bias did not highlight underestimations by the model of flood events observed in summer. The investigation of specific events along with seasonality clearly enabled the identification of patterns in model errors. Another way to identify these patterns would be to derive the flow duration curve in summer periods and calculate differences above the 80th percentile. But the advantage of flood event selection and analysis lies in the possibility to investigate links to various flood characteristics. Floods can have very different seasonal triggers affecting antecedent soil moisture conditions at different time scales (Blöschl et al. 2013, Berghuijs et al. 2014). Therefore, fast processes are not always considered in overall performance analyses. The seasonality of floods is a good indicator of flood triggers in metropolitan France. Our results showed that combining event analysis with streamflow seasonality analysis can help to identify where a conceptual model fails to reproduce flood volumes even when the model yields an aggregated performance considered to be reasonable.

5.3 First-order factors controlling simulation errors

One of the underlying ideas behind diagnosing a model is to be able to identify where model improvement is needed. In the case of the GR5H-I model, our results showed a clear seasonal pattern with an unbiased estimation of floods except in summer, where there is a clear underestimation signal. A central question remains regarding the first-order factors leading to the identified deficiency. Model deficiency can be related to parameter estimation, either because of the choice of objective function (e.g. Mizukami et al. 2019, Brunner et al. 2020) or because of data uncertainty (i.e. wrong parameterization because of uncertainty in forcings or streamflows; see e.g. Beven 2016). However, structural deficiencies may be the underlying cause in the case of our model, as its parsimonious structure could limit its ability to reproduce specific processes occurring in summer, where short-duration processes can take place, such as high-intensity precipitation events. We have seen that this is especially the case under low soil moisture conditions. Furthermore, Fig. 12(a) indicates that the simulation of effective rainfall by the GR5H-I model partly explains the large underestimations of some of the flood events. When the simulation of effective rainfall is low compared with the other floods of a catchment, the model tends to underestimate the flood volume. Figure 12(b) presents the relationship between a measure of precipitation intensity and flashiness of the catchment response and GR5H-I simulation of event effective rainfall. Low values of effective rainfall are associated with



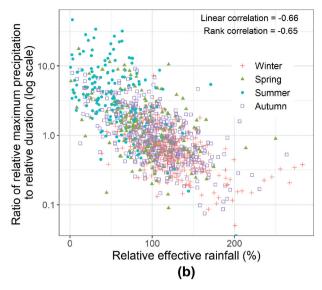


Figure 12. (a) Relationship between GR5H-I simulation of event effective rainfall and event bias (each class contains approximatively 211 events). (b) Relationship between GR5H-I simulation of event effective rainfall and precipitation intensity relative to event duration. The results are for 1054 events that took place in 80 catchments in which floods can occur in summer.

short-duration events with high precipitation intensity (large y-axis values) and mostly for late spring, summer and early autumn events.

Whatever parameter set is chosen, models sometimes do not have the structural ability to reproduce an observed flood. This explanation is consistent with the findings of Mathevet et al. (2020), who reported that the shorter the sub-period of evaluation, the greater the difference in performance between the MRX model and the GRX model (similar to GR5H-I). They concluded that MRX is better able to reproduce short-term processes than GRX because of the more complex structure of the former. The lumped spatial configuration could also be the restraining factor explaining the deficiencies identified, since spatial interactions between precipitations and soil wetness have impacts on flood generation (Tarasova et al. 2020). Short-duration events with high precipitation intensity are sometimes subject to large uncertainties in the input precipitation data (e.g. Zoccatelli et al. 2011, Ruiz-Villanueva et al. 2012, Zhang et al. 2017). If the total amount of rainfall is underestimated during an event, the model cannot simulate the required amount of effective rainfall. This could explain, to some extent, that the model does not perform well on such events. Whatever the first-order factor is, the present methodology, by establishing a finer benchmark for high-flow simulations, helped reveal the difficulties involved in modelling specific flood events. This is particularly relevant to reduce model structure uncertainty and therefore to improve the predictive capability of our model. This work will contribute to future improvements of the GR5H-I model.

6 Conclusion

In this study, we proposed an approach to diagnose the quality of floods simulated by a conceptual rainfall-runoff model over a large set of catchments and flood events. Starting from overall performance criteria calculated for the whole time series, our methodology consisted in computing model bias for selected flood events and looking for seasonal trends and compensations between streamflow periods. From these

seasonal patterns, we aimed to link the model bias to certain flood characteristics. We found that while the model yielded reasonable performance for the dataset in terms of aggregated statistics, patterns in model errors were revealed when investigating performance across selected flood events. Using seasonality as an indicator of the variability of flood characteristics enabled us to identify situations where the GR5H-I model did not manage to reproduce the observed flood volumes. We found that the summer events of our dataset were associated with systematic underestimations by the GR5H-I model. Short-duration processes, such as highintensity precipitation events, associated with low soil moisture conditions are not explicitly taken into account in the structure of the GR5H-I model. For these specific events, this results in a too-low simulation of effective rainfall and therefore underestimation of flood volumes. However, these simulation errors were not detected when considering the KGE index calculated for the entire streamflow time series. By examining both the seasonality of model bias and different streamflow time windows, we have identified compensations between flood events and the rest of the hydrograph in summer and autumn.

Overall, this study confirmed the limitations of using criteria computed on the whole time series to evaluate model performance in simulating high-flow events, even when these criteria are known to be biased towards high flows. The seasonality of streamflow was found to be an indicator of the ability of the GR5H-I model to simulate specific floods that occurred in some of the catchments of our dataset. It enabled us to refine the analyses and look for links to flood characteristics for these catchments. Future developments of the model could focus on improving the calculation of effective rainfall by accounting for summer flood-generating processes. This could be achieved by better considering the spatial variability of rainfall (e.g. Lobligeois et al. 2014, Loritz et al. 2021) or by taking precipitation intensity into account (e.g. Peredo et al. 2021). Multiobjective calibration could also lead to an improved identification of the parameter sets (e.g. Monteil et al. 2020), using, for



example, objective functions that were found to be more suited for flood simulation (e.g. Mizukami et al. 2019).

In this study, we focused on model bias because we considered it a first-order property of model errors. Another perspective on our work could be to further analyse model simulations within a multicriteria assessment framework so as to cover more aspects of model performance (Willems 2009). Also, data uncertainty was not considered for model parameterization or for streamflow result analyses, although it can have an impact on model parameterization and interpretation of model errors (Beven 2016). Finally, further tests on other catchments, such as dry or arid catchments (e.g. in Australia), could improve the generalizability of our results.

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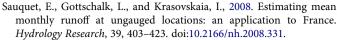
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Appendix. Equations of the GR5H-I model

Here we provide the main equations (integrated over the time step) of the GR5H-I model along with a diagram that depicts the model conceptual storages and fluxes (Fig. A1). Definitions of the variables and parameters are given in Tables A1 and Tables A2, respectively. More information about the model can be found in Le Moine (2008), Lobligeois (2014) and Ficchì et al. (2019).

The following equations provide the detailed computations of the various internal and output variables of the model on a given time step. The sequence can be repeated within a loop to compute a time series of simulated streamflow. Before these computations start, the ordinates of the unit hydrograph must be calculated (see Equations A9 and A10).

Interception store:

At current time step k, evapotranspiration from the interception store E_i is calculated from potential evapotranspiration input E, precipitation input *P* and antecedent interception store level *I*:

$$E_i(k) = min(E(k), P(k) + I(k-1))$$
 (A1)

Then, net rainfall is calculated as follows:

$$P_{th}(k) = \max[0, P(k) - (I_{max} - I(k-1)) - E_i(k)]$$
 (A2)

The interception store level is then updated as follows:

$$I(k) = I(k-1) + P(k) - E_i(k) - P_{th}(k)$$
(A3)

Production store:

The part of net rainfall that fills the production store depends on the antecedent production store level and the net rainfall:

$$P_{s}(k) = \frac{X_{1}\left(1 - \left(\frac{S(k-1)}{X_{1}}\right)^{2}\right) \tanh\left(\frac{P_{th}(k)}{X_{1}}\right)}{1 + \frac{S(k-1)}{X_{1}} \tanh\left(\frac{P_{th}(k)}{X_{1}}\right)}$$
(A4)

In case $E(k) - E_i(k)$ is greater than zero, evapotranspiration from the production store occurs and depends on the antecedent production store level:

$$E_s(\mathbf{k}) = \frac{S(k-1) \cdot \left(2 - \frac{S(k-1)}{X_1}\right) \tanh\left(\frac{E(\mathbf{k}) - E_i(\mathbf{k})}{X_1}\right)}{1 + \left(1 - \frac{S(k-1)}{X_1}\right) \tanh\left(\frac{E(\mathbf{k}) - E_i(\mathbf{k})}{X_1}\right)}$$
(A5)

The production store level is then updated as follows:

$$S^*(k) = S(k-1) + P_s(k) - E_s(k)$$
 (A6)

Percolation from the production store is calculated as:

$$Perc(k) = S^*(k) \cdot \left\{ 1 - \left[1 + \left(\frac{4}{21} \cdot \frac{S(k)}{X_1} \right)^4 \right]^{-\frac{1}{4}} \right\}$$
 (A7)

$$S(k) = S^*(k) - Perc(k)$$
(A8)

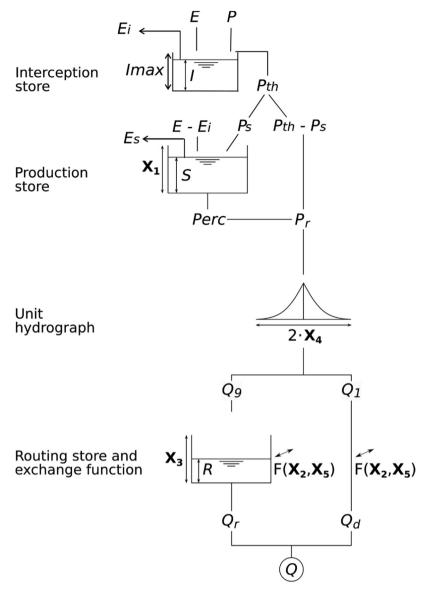


Figure A1. Diagram of the GR5H-I model (modified from Le Moine 2008, Ficchì et al. 2019).

Unit hydrograph (UH):

The S-curve along time *t* is defined independently from the current time step:

$$\begin{cases}
0, & t < 0 \\
-\frac{1}{2} \cdot \left(\frac{t}{X_4}\right)^{1.25}, & 0 < t < X_4 \\
1 - \frac{1}{2} \cdot \left(2 - \frac{t}{X_4}\right)^{1.25}, & X_4 < t < 2.X_4 \\
1, & t \ge 2.X_4
\end{cases} \tag{A9}$$

The resulting unit hydrograph ordinates are calculated by:

$$UH(j) = SH(j) - SH(j-1)$$
(A10)

where j is an integer between 1 and the maximum number of unit hydrograph ordinates (n).

The unit hydrograph ordinates are used to calculate the outflow from the unit hydrograph to the routing store at the current time step:

$$Q_{9}(k) = \frac{9}{10} \cdot \sum_{j=1}^{n} UH(j) \cdot P_{r}(k-j+1)$$
 (A11)

and the outflow from the unit hydrograph to the direct branch:

Table A1. List of the variables of GR5H-I expressed for a given time step (mm or mm/h).

Notation	Definition
Ε	Potential evapotranspiration input
Ρ	Precipitation input
E_n	Net evapotranspiration
E_i	Evapotranspiration from interception store
lmax	Interception store capacity
I	Interception store level
P_{th}	Net rainfall from interception store
E,	Evapotranspiration from production store
P_s	Part of net rainfall that fills the production store
P _s S*	Temporary level of the production store
S	Production store level
Perc	Percolation from production store
P_r	Effective rainfall
Q9	Part of the unit hydrograph outflow that fills the routing store
Q1	Part of the unit hydrograph outflow that does not fill the routing store
F	Potential intercatchment semi-exchange
	Outflow from the routing store
Q_d	Outflow from the direct branch
R*	Temporary level of the routing store
R	Routing store level
Q	Simulated streamflow

Table A2. List of the free parameters of GR5H-I.

Notation	Definition	Unit
<i>X</i> ₁	Production store capacity	mm
X_2	Intercatchment exchange coefficient	mm/h
<i>X</i> ₃	Routing store capacity	mm
X_4	Unit hydrograph time constant	h
<i>X</i> ₅	Intercatchment exchange threshold	-

$$Q_1(k) = \frac{1}{10} \cdot \sum_{j=1}^{n} UH(j) \cdot P_r(k-j+1)$$
 (A12)

Exchange function:

An intercatchment exchange flow is then added (or released) to (or from) both outflows depending on the antecedent routing store level. The potential intercatchment semi-exchange is calculated as follows:

$$F(k) = X_2 \left(\frac{R(k-1)}{X_3} - X_5 \right) \tag{A13}$$

Routing store:

The routing store level is updated as follows:

$$R^*(k) = max[0, R(k-1) + Q_9(k) + F(k)]$$
 (A14)

The outflow from the routing store is then calculated as:

$$Q_r(k) = R^*(k) \cdot \left\{ 1 - \left[1 + \left(\frac{R(k)}{X_3} \right)^4 \right]^{-\frac{1}{4}} \right\}$$
 (A15)

$$R(k) = R^*(k) - Q_r(k)$$
 (A16)

The outflow from the direct branch is expressed as:

$$Q_d(k) = max[0, Q_1(k) + F(k)]$$
 (A17)

Finally, the simulated streamflow is calculated as:

$$Q(k) = Q_r(k) + Q_d(k) \tag{A18}$$