



**HAL**  
open science

## **Physico-chemical stone-mortar compatibility of commercial stone-repair mortars of historic buildings from Paris**

P. Lopez-Arce, M. Tagnit-Hammou, Beatriz Menendez, J. D. Mertz, M. Guiavarc'h, A. Kaci, S. Aggoun, A. Cousture

### ► **To cite this version:**

P. Lopez-Arce, M. Tagnit-Hammou, Beatriz Menendez, J. D. Mertz, M. Guiavarc'h, et al.. Physico-chemical stone-mortar compatibility of commercial stone-repair mortars of historic buildings from Paris. *Construction and Building Materials*, 2016, 124, pp.424-441. <10.1016/j.conbuildmat.2016.07.076>. <hal-03266051>

**HAL Id: hal-03266051**

**<https://hal.science/hal-03266051v1>**

Submitted on 7 Jan 2022

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



HAL Authorization

1 **Physico-chemical stone-mortar compatibility of commercial stone-repair mortars**  
2 **of historic buildings from Paris**

3 P. Lopez-Arce\*<sup>1,2</sup>, M. Tagnit-Hammou<sup>2,3,4</sup>, B. Menendez<sup>2</sup>, J.D. Mertz<sup>3</sup>, M. Guiavarc'h<sup>3</sup>,

4 A. Kaci<sup>4</sup>, S. Aggoun<sup>4</sup>, A Cousture<sup>4</sup>

5 <sup>1</sup>Museo Nacional de Ciencias Naturales (CSIC), C/ Jose Gutierrez Abascal, 2, Madrid, 28024, Spain

6 <sup>2</sup>Géosciences et Environnement Cergy, GEC, Université de Cergy Pontoise, France

7 <sup>3</sup>Laboratoire de Recherche des Monuments Historiques (CRC-LRMH USR3224), 29 rue de Paris F-77420 Champs  
8 sur Marne France, France

9 <sup>4</sup>Laboratoire de Mécanique et Matériaux du Génie Civil, L2MGC, Institut des Matériaux, Université de Cergy  
10 Pontoise, F-95000 Cergy Pontoise, France

11 **ABSTRACT**

12 The physico-chemical compatibility of the most frequently used commercial stone-  
13 repair mortars applied to repair surface damage of a common limestone (Euville stone)  
14 employed in the basements of historic buildings from Paris was assessed. The  
15 characterization of anhydrous raw mortar materials, of stone and mortar samples  
16 collected from these buildings and laboratory specimens was carried out.

17 The presence of chlorides and sulfates (gypsum and mixtures of calcium and sodium  
18 sulfates) with minor amounts of nitrates in mortar samples collected from the buildings  
19 suggest an origin of salts caused by contamination/pollution coming from past  
20 restoration products and environmental pollution. The mortar containing quartz, marble  
21 aggregates, portlandite and hydraulic components (C<sub>3</sub>S, C<sub>2</sub>S and C<sub>2</sub>AS) with addition of  
22 aluminosilicate micro-spherical particles with cementitious properties, and no  
23 phyllosilicates, shows a better chemical compatibility with the stone. The mechanical  
24 properties of this mortar are also closer to those of the limestone. However, some  
25 differences in the hydric properties due to their different pore systems and aesthetic  
26 features should be improved in further restoration works.

27 **Keywords:** *stone-repair mortars; natural stone; historic buildings; compatibility;*  
28 *physico-chemical properties*

## 29 **1. Introduction**

30 From many architectural purposes, mortars can be used as plasters or renders covering  
31 the whole surface of walls or building facades, as bedding, jointing or pointing between  
32 stone ashlars or bricks, or even they can be used for rebuilding a decayed structure in  
33 restoration works. Some kinds of repair mortars can be applied for surface repairs of  
34 architectural surfaces. Various terms are used for these specific mortars, *stone repair*  
35 *mortar*, *reconstitution mortar* or *'plastic' repair mortar*, which have the same or very  
36 similar meaning to *surface repairs*, *plastic repairs*, *surface fills*, *loss compensation*  
37 *mortars* or *artificial stone mixtures* [1]. During restoration of heritage buildings,  
38 mortars are frequently used for the repointing of joints or for the “plastic” repair of  
39 stone, which are designed to fill in missing parts of stone. These mortars are moldable  
40 mortars that can be applied in situ, and sets into place by its own adhesion to the  
41 substrate [2]. From all the possible terms that can be assigned to this kind of mortars,  
42 we have chosen *'stone-repair mortar'*, since it is the clearest name for the purpose of  
43 our research, which involve mortars that have been used for repairing or reconstruction  
44 of surface damaged stone from restoration works that were carried out in historic  
45 buildings. A missing part of an original material is modelled by a new material, which  
46 is pliable when applied, and therefore can be adapted into various shapes and finished  
47 with required surface textures [1].

48 Repair mortars used for stone restoration are assumed to be highly compatible with  
49 historic materials in terms of physical, chemical and mechanical properties in order to  
50 assure the durability of masonry on the long term. A systematic approach for the  
51 characterization of historic mortars and materials to be repaired has been defined by

52 RILEM TC 167 COM which offers a valuable tool to identify mortar components,  
53 nature of binder, aggregate, additives, and their relative proportions [3,4]. Ashurst in  
54 1990 [5] described some decision factors on surface repairs, whereas Hughes and Valek  
55 in 2003 [6] reviewed the compatibility concept. These mortars must meet a series of  
56 requirements from a Cultural Heritage preservation point of view to avoid accelerated  
57 deterioration of original material. Material compatibility between repair mortars and the  
58 original material suggests that no damage should be caused to the repaired material. For  
59 example, the incompatibility among building materials due to the combination of  
60 sulfate-bearing mortars and magnesium-rich stone and mortars applied in XVIII  
61 restoration works lead to extensive weathering on a historic Monastery (XII century) by  
62 magnesium sulfate crystallization processes [7].

63 Nowadays, most professionals turn to commercial pre-mixed mortars. There are many  
64 available commercial mortars ready to use in restoration works, from local and  
65 international companies. The advantage is that these are prefabricated, and the  
66 manufacturer can guarantee that the content's mix is standardized, creating the same  
67 workability and properties for each batch, with consistent composition and working  
68 properties. This is much appreciated by restoration architects and contractors [8,9].  
69 However, this advantage can be a disadvantage as well. The specially designed mortar  
70 for one specific stone can work just for stones with the same or similar physico-  
71 chemical characteristics. Furthermore, in cases where the stone is very heterogeneous,  
72 and properties can differ greatly from one stone sample to another, the standardized  
73 process will be less successful when aiming to achieve a compatible mortar [10].  
74 Besides, these mixes present an uncertainty about the ingredients they contain. In  
75 restoration studies using commercial mortars, aggregates are frequently added to solve  
76 the problem of stone heterogeneity [11]. In the case of ready-mixed mortars, powders

77 can simply be added with the required amount of clean water. However, is important to  
78 know the physical properties of the commercial product in order to assure the  
79 compatibility with the stone.

80 The selection of a binder is a starting point of the mix design as it predetermines the  
81 physical and mechanical properties of the mortar mix, as well as the capacity of the mix  
82 to be adapted to the appropriate form and appearance [1]. Natural Hydraulic Lime  
83 mortars (NHL) are produced from a naturally occurring ‘impure’ limestone/chalk.  
84 Typically, the impurities are those from clay minerals and other sources of alumina and  
85 silica. NHL mortars have been manufactured since the XVIII century by burning these  
86 limestones below the clinkering point. These NHL are able to set and harden even under  
87 water, as the mechanical strength development is mainly driven by hydration.  
88 Carbonation of the slaked lime contributes to the hardening process as well.

89 Hydraulic Limes mortars (HL) are produced by artificially blending calcium hydroxide,  
90 calcium silicates and calcium aluminates. This is commonly achieved by blending  
91 mixtures of clays and pure limestone, or calcium hydroxide with suitable pozzolanic  
92 materials. Pozzolans or pozzolanic materials (fly ash, burnt clays, etc.) are reactive  
93 materials that in the presence of soluble calcium hydroxide form hydrated compounds  
94 which act as binders. These are often added to increase strength gain in hydrated,  
95 hydraulic and natural hydraulic lime based mortars.

96 Greeks and Romans first used hydraulic lime mortars with natural pozzolans in ancient  
97 times [12] and Phoenicians employed these binders in Jerusalem (10th century BC)  
98 [13]. NHL was used mostly during the nineteenth century. They are nowadays used in  
99 restoration of historical buildings because their chemical and physical properties are  
100 similar to those of materials used by the original builders, and because they ensure the  
101 development of superior mechanical properties, without having the general drawbacks

102 of Portland cement. NHL was the precursor of Portland cement. The main difference in  
103 the production of NHL and cement is the burning temperature. Callebaut et al. in 2001  
104 [14] focused on the characterization of nineteenth century hydraulic restoration mortars  
105 used in the Saint Michael's Church in Leuven (Belgium), for restoring weathered mortar  
106 joints. Based on the presence of a calcium aluminosilicate (gehlenite ( $C_2AS$ )), the  
107 dominance of di-calcium silicate (larnite ( $C_2S$ )), the large amounts of portlandite  
108 (calcium hydroxide, CH), together with chemical analyses and historical sources, these  
109 hydraulic mortars were characterized as NHL mortars.

110 The ready-mixed mortars are available as powder materials composed of binders,  
111 aggregates and additives already packed together in appropriate ratios. The mortars  
112 preparation only consists of simple mixing operations with the correct amount of water  
113 (which is usually indicated in the technical data sheets). NHLs are frequently employed  
114 as binders in the commercial mixes because of their quick setting capability and  
115 remarkable mechanical strengths [13,15,16]. The characterization of commercial ready-  
116 mixed mortars, allows verifying their real composition and performance characteristics  
117 [17]. However, these composition and properties often differ from those declared in the  
118 technical specifications supplied by the manufacturers, finding disagreements with the  
119 composition declared by the supplier [18]. There is still a lack for testing the physical  
120 properties and durability of mortars according to European standard tests, especially in  
121 terms of compatibility with stone, and the long-term behaviour of the repaired  
122 mortar/stone interface [11].

123 The aim of this research is to determine the physico-chemical compatibility of the three  
124 most frequently used commercial stone-repair mortars applied to repair the surface  
125 damage of Euville stone, a common limestone used in the basements of historic  
126 buildings in Paris city.

127 **2. Materials and methods**

128 *2.1. Characteristics of selected materials*

129 Three commercial stone-repair mortars (Fig.1a) were selected in this research on the  
130 basis of their application on some damaged surface areas of the same type of stone,  
131 repaired due to salt crystallization processes, in different historic buildings of Paris.  
132 These buildings were repaired in the same period of time corresponding to the  
133 restoration campaign 2008-2010. The selected stone is the so-called Euville limestone  
134 (Fig.1b) that was used in the outdoor basements of the Grand Palais, Palais de la  
135 Découverte and Préfecture de Police historic buildings.

136 *2.1.1. Stone-repair raw anhydrous mortars*

137 Three commercial mortars, ready to mix with water according to recommendations of  
138 the manufacturers, are called in this research *Lit*, *Art* and *Alt* mortars. These are  
139 mixtures of natural and hydraulic lime mortars (NHL, HL) with or without aerial lime  
140 (CL). Lit mortar (*Lithomex Light*) is a material produced by Chaux et Enduits St. Astier  
141 (CESA, France), based on a St. Astier natural hydraulic lime binder (NHL) and it was  
142 used to repair Euville stone at the Grand Palais building (GP). According to the  
143 manufacturer, this is a pure NHL, defined as a natural lime, with hydraulic binders, sand  
144 and specific additives. According to Torney et al., 2015 [9], Lithomex mortar contains  
145 the following components (expressed as percentage of binder): calcium hydroxide 20%;  
146 hydraulic binder (Portland cement) 20%; filler (vermiculite) 5%, fine grained quartz and  
147 calcite aggregates and talc filler. The technical data sheet of *Art* mortar (*ArtoPierre TM*  
148 by Parexlanko, France) indicates that this is mainly aerial lime (CL, binder, 70% in  
149 volume) with hydraulic, mineral and organic additives and mineral pigments.  
150 Aggregates are mainly calcareous and siliceous with grains up to 1.5 mm. This mortar  
151 was used in the Palais de la Découverte building. Finally, *Alt* mortar (*Altar® Pierre* by

152 ECP, France) was used to repair Euville stone in the Préfecture de Police building (PP).  
153 According to the manufacturer, quartz grains, calcium carbonate, hydraulic binder,  
154 additives and mineral pigments, compose this mortar. The mineralogical and chemical  
155 composition of the three mortars, before mixing with water (anhydrous raw materials),  
156 was initially determined in this research. Then, the mineralogy and hydric and  
157 mechanical properties of hardened single mortar specimens (4x4x16 cm) were studied  
158 after 28 curing (Fig.1c).

### 159 *2.1.2. Stone*

160 Euville limestone (Oxfordian, Late Jurassic) is a crinoïdal grainstone almost completely  
161 composed of calcium carbonate (98%) with a coarse-grained texture and a syntaxial  
162 cement of calcite. The fabric was formed by an accumulation of coarse crinoïdal  
163 ossicles in submarine dunes. Accessory bivalves and spines of sea urchins are also part  
164 of the fossil fauna. The outcrops of this limestone are situated near Commercy  
165 (Département de la Meuse, France). The Euville limestone is a famous building stone in  
166 France, and also in Belgium, where it is often used in combination with Savonnières  
167 limestone and Lede stone, and it has often been used as a replacement stone in many  
168 historic buildings in several countries in the world

169 [19,20]. As a restoration measure, some surface areas built with this stone affected by  
170 salt crystallization processes have been repaired with several stone-repair commercial  
171 mortars. The stone specimens used in this work were supplied by ROCAMAT quarry in  
172 Euville, France. The specimens where cut parallel to the bedding with dimensions  
173 4x4x16 cm to perform all the hydric and mechanical tests. For the water vapour  
174 permeability test cylindrical specimens 1 cm thick and 4 cm diameter were prepared.

175

176

177 *2.1.3. Stone and mortar samples collected from the historic buildings*

178 Three historic buildings from Paris city where the three types of mortars were used to  
179 restore Euville stone were selected in order to collect stone and mortar samples. Two  
180 small mortar samples were collected, from the Gran Palais building (GP) where  
181 Lithomex mortar was used, sample Lit-GP (Fig.2a), and Préfecture de Police building  
182 (PP) where Altar Pierre mortar was applied to repair the stone, sample Alt-PP (Fig.2b).  
183 At the Préfecture de Police building, a small flake sample of Euville stone (Eu-GP) was  
184 also collected from one area with salt crystallization decay that showed efflorescences  
185 on the surface of the stone (Fig.2c). It was not possible to collect samples at the Palais  
186 de la Découverte building, since the studied area corresponded to a delicate sculpted  
187 stone restored with Artopierre stone-repair mortar displaying an apparent good state of  
188 conservation.

189 *2.1.4. Hardened mortar specimens manufactured in the laboratory*

190 The water:powder mortar ratios were prepared in the lab, following as much as possible  
191 the recommendations of the manufacturers according to their respective technical data  
192 sheets. The manufacturer's preparation guidelines of Lithomex mortar state that the  
193 materials should be mixed (mechanically or by hand) for between three and five  
194 minutes, with water content of 4.5–5.5 L of water per 25 kg of dry material. We used 5  
195 L of water (W) per 25 kg of dry material (M), i.e. W:M=0.20. In this case, the restorer  
196 who used this type of mortar in the Grand Palais historical building recommended us to  
197 add a handful of sand to the mixture. Since the amount of aggregate fraction between  
198 1.25 and 0.63 mm in this mortar was much lower compared to the other mortars,  
199 according to this information, to grain size distribution analyses and in order to obtain a  
200 mortar as similar as possible to the others, 150 g of normalized sand (fraction 1.25-0.63  
201 mm from Ultibat, EN 12620: 2002 + A1: 2008 [21]), was added to 2000g of raw

202 anhydrous mortar. To prepare Artopierre mortar, between 6 and 7 L of water per 30 kg  
203 of dry material is required according to the technical data sheet. We used 6.5 L per 30  
204 kg of raw anhydrous mortar powder (W:M=0.22). To manufacture Altar® Pierre  
205 mortar, from 4 up to 6 volume of dry material per 1 volume of water was recommended.  
206 To prepare the specimens we used 5 volume of dry material per 1 volume of water  
207 (W:M= 0.13).

208 A mechanical mixture was performed in the three mortars using an industrial mixer  
209 (Controlab, France) during 4 minutes, starting at low speed rotation (62 rpm) during 1  
210 min and finishing at high speed (125 rpm). Then, a jolting apparatus was also used  
211 according to the standard test UNE-EN 196-1:2006 [22], applying 25 blows to  
212 homogenize the mixture and avoiding the formation of air bubbles.

213 Eighteen mortar specimens were prepared, six with each type of mortar, two specimens  
214 for the compression-flexural test, two for water absorption under vacuum test and two  
215 for capillary-desorption test. These were prepared by molding the mixtures in rubber  
216 molds (4x4x16 cm). Besides, to carry out water vapor permeability tests, plastic moulds  
217 filled with each mortar mixture were used. These were big enough to prepare by cutting  
218 at least two circular mortar specimens (50 mm diameter x 10 mm thickness) for each  
219 type of mortar. All the specimens were demolded after two days of curing according to  
220 the standard test NF-EN 1015-11 [23].

221 For hardening the mortar specimens (28 days curing) we tried to simulate the average  
222 annual weather conditions of Paris. The specimens were placed in a ventilated climatic  
223 chamber with CO<sub>2</sub> uptake from the environment (400 ppm approx.) at 11°C and 85%  
224 relative humidity (RH)) during 7 days. Then, RH was changed down to 65% during the  
225 next 7 days, followed by laboratory conditions in a climatic room at 20°C and 50% RH  
226 during 14 days, under environmental CO<sub>2</sub> (400 ppm approx.)). The reason why RH was

227 reduced from 85% down to 65% during the 7-14 curing days was first of all, because  
228 the average annual RH in Paris city was in the range 65-85 % RH approx. In a second  
229 place because these commercial mortars are mixtures of hydraulic and aerial lime.  
230 According to the literature [24,25], a high and a lower RH, respectively, is  
231 recommended to set up suitable curing conditions. The European standard AFNOR EN  
232 1015-11 [23] defines the following optimal conditions of temperature and relative  
233 humidity for the curing of mortar samples in the laboratory at  $T=20\pm 2$  °C and  
234  $RH=95\pm 5\%$  for the first 5 days in the mold, the following 2 days removed from the  
235 mold, and at  $T=20\pm 2$  °C and  $RH=65\pm 5\%$  for the following 21 days. So, 85-65% RH  
236 and 11°C T conditions were selected the first 14 days in order to simulate as much as  
237 possible the environmental curing conditions of Paris and at the same time trying to  
238 perform a laboratory test in a gradual way choosing the most suitable as possible curing  
239 conditions for these type of mortars. The environmental conditions of the final 14 days  
240 to reach 28 curing days had to be performed at  $RH 50\pm 5\%$ ,  $T 20^{\circ}\text{C}$  in a climatic room  
241 only due to availability and space reasons.

## 242 *2.2. Analytical techniques and experimental test methods*

### 243 *2.2.1. Mineralogical and chemical analyses*

244 Polarizing optical microscopy was used to study the main mineralogical constituents  
245 and textures of the mortar samples collected from the buildings and the hardened single  
246 mortar specimens after 28 days curing. The samples were impregnated with epoxy resin  
247 mixed with blue dye to fill the porosity in order to be easily recognized under the  
248 microscope with parallel nicols. The thin sections were studied with an Olympus BX50  
249 polarized light microscope fitted with an Olympus digital camera.

250 X-ray diffraction (XRD) was used to determine the mineralogical composition of raw  
251 anhydrous mortar samples, hardened single mortar specimens manufactured with them

252 after 28 days curing and samples collected from the buildings. Furthermore, soluble  
253 fractions prepared to carry out ion chromatography analyses were left to evaporate and  
254 the product was also analysed by XRD. The analyses were conducted on a Bruker D8  
255 Advance diffractometer with  $\text{CoK}\alpha$  radiation powder. The scanning conditions were  $2\theta$   
256 angles of 5–65°, scan step size 0.05°, time step 1°/s in continuous mode, and beam  
257 intensity of 40 kV and 35 mA. The diffractometer worked with a  $\text{CoK}\alpha$  radiation,  
258 instead of the most common used  $\text{CuK}\alpha$  and so there is a slight variation in the grades  
259 of the  $2\theta$  peaks used to identify minerals. The identification of the mineral phases was  
260 performed using the Bruker AXS DiffracPlus EVA software also used to carry out  
261 semi-quantitative analyses.

262 Scanning electron microscopy (SEM) coupled with Energy dispersive X-ray  
263 spectroscopy (EDS), was used to find weathering products caused by decay processes  
264 and to identify the type of salt efflorescences and sub-efflorescences on the top and  
265 underneath (some millimetres depth) the surface of stone and mortar fragments  
266 collected from the buildings. A SEM microscope Leica S430i was used. The elemental  
267 composition of some selected components from these building samples together with  
268 the raw anhydrous mortar samples was determined by means of EDS semi-quantitative  
269 microanalyses by means of an Bruker micro-analyser spectrometer. Nickel-sputtered  
270 fragments from the samples were studied in secondary electrons mode.

271 In order to perform the chemical composition by EDS analyses of each grain size  
272 fraction of the raw anhydrous mortars (aggregates and binder), the grain or particle size  
273 distribution was carried out by sieving 200g approx. of each mortar according to the  
274 standard test AFNOR NF-EN 1015-1 [26]. The sieve sizes that have been used are the  
275 following: 1.60mm, 1.25mm, 0.63mm, 0.315mm, 0.20mm, 0.16mm, 0.080mm and  
276 0.080mm. Then, the largest sizes (1.60-1.25 mm and 1.25-0.63 mm) were impregnated

277 in epoxy resin and then polished, in order to study their shape and chemical  
278 composition by SEM-EDS analyses. Each grain size range of the finest fractions (from  
279 0.63 down to below 0.080 mm) was pressed in small tablets and then analyzed by EDS  
280 previously sputtering the samples with nickel (Ni).

281 Ion chromatography (IC) analysis was performed to quantify the soluble salts present in  
282 the raw anhydrous mortars and samples collected from the buildings. Some anions ( $\text{Cl}^-$ ,  
283  $\text{NO}_3^-$ ,  $\text{PO}_4^{2-}$  and  $\text{SO}_4^{2-}$ ) and cations ( $\text{Na}^+$ ,  $\text{K}^+$ ,  $\text{Mg}^{2+}$ ,  $\text{Ca}^{2+}$  and  $\text{NH}_4^+$ ) were determined.  
284 Approximately 0.1 g of sample was dissolved in 10 ml of Milli-Q ultrapure water and  
285 placed it for 5 min in an ultrasonic bath at room temperature. The solution with the solid  
286 residue was then left to settle down with a minimum rest period of 24 h. The soluble  
287 salts of raw materials and samples collected from the buildings were quantified on a  
288 Dionex DX-120 ion chromatograph.

### 289 2.2.2. *Physical tests*

290 To determine hydric and mechanical properties, together with physical characteristics  
291 such as density, porosity and color parameters, the following tests were carried out in  
292 the stone and mortar specimens.

293 Water absorption by capillarity was carried out to evaluate the liquid water transfer into  
294 the materials. The capillary coefficients were calculated for the Euville stone and  
295 hardened single mortar specimens. The standard test AFNOR NF EN 1925:1999 [27]  
296 was followed; the results are expressed in  $\text{g}/(\text{m}^2 \cdot \text{s}^{1/2})$  instead of  $\text{kg}/(\text{m}^2 \cdot \text{s}^{1/2})$ . Once  
297 capillarity saturation was reached, the specimens were spun to ease the water drying  
298 under laboratory conditions ( $45 \pm 5$  % RH and  $20 \pm 1^\circ\text{C}$ ) and to calculate desorption  
299 coefficient (water loss or evaporation) weighing the specimens at several intervals of  
300 time.

301 Water vapour permeability test was carried out in the stone and mortar specimens. The  
302 standard test AFNOR EN 15803:2010 [28], with wet cup was followed to calculate the  
303 water vapor permeability ( $\text{Kg}/(\text{m}^2\text{s})$ ). External relative humidity of 50% and  
304 temperature of 23°C were achieved introducing the specimens in a climatic chamber,  
305 setting these conditions during all the duration of the test.

306 Water absorption under vacuum was performed in the stone and hardened mortar  
307 specimens, to determine differences on apparent density ( $\text{kg}/\text{m}^3$ ), bulk density ( $\text{kg}/\text{m}^3$ ),  
308 and to calculate open porosity (%) as described in standard test AFNOR EN 1936:2007  
309 [29].

310 Flexural strength measurements were carried out in the stone and hardened mortar  
311 specimens, with a maximum load of 8 kN and load rate of 0.05 kN/S. Compression  
312 strength measurements were performed in the four fragments obtained from the  
313 breaking of two specimens after the flexural test. A maximum load of 250 kN and load  
314 rate of 2.4 kN/S was applied until breaking, providing values equal or above 7 MPa,  
315 since this is the minimum value detected by the compression cell. A Quantech 3R press  
316 (Quantium<sup>TM</sup>, Researchers & Realisations, France) that follows the standard test  
317 AFNOR EN196-1:2006 [30] was used.

318 Total Hg-porosity and pore size distribution analysis was carried out by mercury  
319 intrusion porosimetry in the stone and mortar samples collected from the building and  
320 the superficial part of hardened mortar specimens manufactured in the laboratory.  
321 Readings were taken at pore radius of 0.003–200  $\mu\text{m}$  under measuring conditions  
322 ranging from atmospheric pressure to 228 MPa on a Micromeritics Autopore IV 9500.

323 Color parameters were measured on the stone and mortar hardened specimens. L\*  
324 parameter, which accounts for luminosity, hue and saturation (chroma, C), a\* and b\*  
325 coordinates (a\* being the red-green parameter and b\* the blue-yellow) were obtained.

326 Total color difference  $\Delta E^*$  was provided as a result of the formula  $\Delta E^* = ((\Delta L^*)^2 +$   
327  $(\Delta a^*)^2 + (\Delta b^*)^2)^{1/2}$ . Measurements were performed with a spectrophotometer Konica  
328 MINOLTA CM-2300d using the CieLab color space; standard illuminant was D65 and  
329 observer angle, 10°.

### 330 **3. Results**

#### 331 *3.1. Characterization of raw anhydrous mortars*

332 The main mineralogical composition of Lit mortar determined by XRD is calcite,  
333 quartz, feldspar and phyllosilicates (clinochlore and talc), followed by hydraulic  
334 components, larnite (i.e.  $C_2S$  or belite), alite ( $C_3S$ ) and traces of gehlenite ( $C_2AS$ ). Art  
335 mortar contains mainly quartz, calcite and portlandite (i.e.  $CH$  or  $Ca(OH)_2$ ) and  
336 hydraulic phases, di-calcium silicate (larnite) and tri-calcium silicate (alite), and traces  
337 of feldspar and calcium-aluminium silicate (gehlenite). A small hump between 10 and  
338 15°  $2\theta$  can be observed in the XRD pattern of this mortar, which might be related to the  
339 presence of clays. Art mortar XRD pattern shows quartz, feldspar, calcite, portlandite,  
340 larnite, alite and traces of gypsum and gehlenite (Fig.3 and Table 1).

341 The SEM-EDS analyses performed in several areas of mineral grains (aggregates) with  
342 sizes between 1.6-1.25 mm and 1.25 mm-0.63 mm of Lit mortar (Fig. 4a) correspond to  
343 phyllosilicates compositions (clinochlore and talc), with and without additional K, Ti  
344 and Cl only detected in the aggregates in the range between 1.6-1.25 mm (Table 2).  
345 Mineral grains of Lit mortar with sizes in the range between 1.25-0.63 mm correspond  
346 to calcite composition with some traces of Mg, Al, Si and Na (Fig. 4b). The results of  
347 these analyses performed in Art mortar show that the mineral grains in the ranges  
348 between 1.6-1.25 mm and 1.25 mm-0.63 mm are mainly, calcite, quartz (that were  
349 deposited in the bottom of the prepared epoxy specimen) and similar phyllosilicates  
350 than those present in Lit mortar (Fig.4c). By contrast, SEM-EDS analyses carried out in

351 the grain sizes between 1.60-1.25 mm and 1.25-0.63 mm of Alt mortar show that these  
352 are only composed by sub-rounded and sharp calcite composition grains, which  
353 partially might correspond to the marble grains added by the manufacturer (Fig.4d).  
354 Some of these grains contain some fissures filled with quartz and some impurities such  
355 as sodium chloride (NaCl). The composition of these largest grain size aggregates in  
356 this latter mortar shows significant differences compared to the other two mortars  
357 (Table 2), since Al, Mg and k are not detected and there is no Fe and Ti in the fraction  
358 between 1.60-1.25 mm.

359 In the three mortars, the composition of the aggregates between 0.63 and 0.20 mm is  
360 mainly siliceous (Si content between 20 and 40 wt. % approx.), and this is especially  
361 marked in Alt mortar (Table 3). Below 0.20 mm the Si content greatly decreases at  
362 expenses of Ca content, which especially increase in Art and Alt mortars (between 27  
363 and 40 wt. % approx.). Besides this, the main difference among the three mortars is the  
364 Na content in Alt mortar which increases with the decrease of grain size (except in the  
365 range between 0.16 and 0.080 mm), from 4 wt. % (between 0.63-0.315 mm) up to 33  
366 wt. % (below 0.080 mm).

367 Ion chromatography analyses show that none of the anhydrous mortars display nitrates  
368 in their composition (Table 4). However, the three have a slight amount of chlorides  
369 (circa 5 ppm). The only one displaying soluble sulfates is Lit mortar (23 ppm approx.).  
370 The concentration in bulk material (wt.%) of the identified total soluble salts (cations  
371 and anions) represents very low percentages in Lit and Alt mortars (2 %) and slightly  
372 higher values in Art mortar (circa 5 %). There is a high amount of soluble  $\text{Ca}^{2+}$  in the  
373 three mortars and this is especially high in Art mortar. No nitrates or phosphates, neither  
374 ammonium have been detected in these samples.

375

376 *3.2. Mortars and stone flake samples collected from the buildings*

377 Petrography of mortars thin sections performed under optical light microscopy shows  
378 that Lit mortar from the Grand Palais building has a large quantity of rounded esparitic  
379 calcite and quartz grains with submillimetric sizes, together with some micas and many  
380 phyllosilicates embedded in a scarce micritic matrix composed by a mixture of calcite  
381 and clays. The ratio binder:aggregate is approximately 1:4 (Fig. 5a and 5b). Feldspar  
382 grains show up with a high degree of cracking at the surface of the mortar that was in  
383 contact with the surrounded environment where the sample was collected. Porosity is  
384 mainly fissural and surrounds the mineral grains and goes through the clay minerals and  
385 through the matrix. Large pores inside the matrix are associated in some areas to the  
386 phyllosilicates showing signs of weathering (Fig.5c and 5d). Thin sections of Alt mortar  
387 from Préfecture de Police building also show a high amount of calcite crystals inside  
388 sharp fragments of fossiliferous micritic and esparitic limestone rocks, bioclasts and  
389 marble fragments of millimetric size. Abundant smaller feldspar and subhedral quartz  
390 grains with cement as syntaxial overgrowths are also embedded in a dense dark matrix.  
391 The ratio binder:aggregate is approximately 1:3 (Fig.5e and 5f). Small rounded (circa  
392 50  $\mu\text{m}$ ) and larger sub-rounded pores (between 200 and 400  $\mu\text{m}$ ), together with small  
393 spherical particles (circa 50  $\mu\text{m}$ ) are present inside this matrix. Some of these particles  
394 seem to be stuffed with an amorphous gel, being difficult to distinguish them from the  
395 matrix, while many others are empty and filled now with the dyed blue resin used to  
396 mark the porosity of the mortar samples (Fig.5g and 5h).

397 The XRD pattern of Lit mortar collected from the Grand Palais building (Lit-GP),  
398 displays the same mineralogy than the obtained in the raw anhydrous mortar, with the  
399 exception of the presence of muscovite ( $\text{K}(\text{Li},\text{Al})_2(\text{Si}_3\text{AlO}_{10})(\text{OH})_2$ ) and gypsum  
400 ( $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$ ) and the absence of larnite ( $\text{C}_2\text{S}$ ) and alite ( $\text{C}_3\text{S}$ ) (Fig.6). The semi-

401 quantitative (%) analyses show different concentrations in all the identified phases  
402 compared to its corresponding raw material (Table 1). The mineralogy of the salts  
403 precipitated from the soluble fraction of Lit mortar prepared to carry out the ion  
404 chromatography analyses, that were left to evaporate (Lit-GP-sf), shows an increase of  
405 gypsum peaks and the appearance of halite (NaCl). Some residues of non-soluble  
406 fraction (quartz, calcite, clinocllore and talc) are also detected.

407 The XRD pattern of Alt mortar collected from the Préfecture de Police building (Alt-  
408 PP) also shows the same mineralogy than the obtained in the anhydrous raw material,  
409 with the exception of no detection of gypsum, the absence of alite ( $C_3S$ ) and the  
410 presence of a minor amount of larnite ( $C_2S$ ). The semi-quantitative (%) analyses also  
411 show different concentrations in all the identified phases compared to its corresponding  
412 raw material, especially in the amount of portlandite (Fig.6). No salts are identified in  
413 the mortar sample collected from this building and neither in the precipitated soluble  
414 fraction. The XRD of Euville stone flake (soluble fraction after evaporation) shows  
415 gypsum, halite and traces potassium-sodium sulfate.

416 The SEM-EDS analyses of the surface of Lit mortar from the Gran Palais, mainly shows  
417 Ca, Mg, C, O, Si and Al as the main components present in all the analyzed zones.  
418 Underneath the surface it shows aggregates of quartz and mainly Si and Ca (i.e. calcium  
419 silicates) as the composition of the binder. There are zones with large amounts of salts  
420 composed by S and Ca (i.e. gypsum) and Na and Cl (i.e. sodium chloride) (Fig.7a, zone  
421 1 and zone 2, respectively). A great number of phyllosilicates is also observed.

422 On the surface of Alt mortar samples from Préfecture de Police building, Si, Ca, Al, C,  
423 O, Na and Cl are the main components, with variable amounts in all the analyzed zones.  
424 There are zones with large amounts of Na and Cl (sodium chloride). Underneath the  
425 surface of Alt mortar, the main composition of the binder is Si and Ca, with Al, C and

426 O. Many micron-size spherical particles can be observed, some of them seem to be  
427 cracked and empty and others seem to be filled with a “viscous” phase. The EDS  
428 analyses show a thin external part mainly composed by aluminosilicates (Fig.7b, zone  
429 1), which might correspond to mullite ( $2\text{Al}_2\text{O}_3\cdot\text{SiO}_2$ ). Some of them display also Ca in  
430 the external part. The analyses of the interior part of these particles show a high increase  
431 in Ca and minor amounts of Na and Mg (Fig. 7b, zone 2). Aggregates of marble  
432 fragments can also be observed. However, they display low amount of C and some Al in  
433 their composition. The EDS analyses of Alt mortar (external and internal parts) indicate  
434 the presence of salts (sodium chloride) together with aluminosilicates, calcium silicates,  
435 calcium aluminosilicates, calcium carbonate and silicon oxides.

436 The surface of Euville stone flake displays salt efflorescences containing S, K, Ca and  
437 Na (Fig.7c, surface zone). Some millimeters depth from the surface, the SEM images  
438 show sub-efflorescences of sodium and calcium sulfate crystals mixed together, which  
439 might corresponds to thenardite and gypsum, respectively (Fig. 7c, interior zone).

440 Table 5 shows the ion chromatography results of soluble salts present in the samples  
441 collected from the buildings. There is a large amount of sulfates in Lit mortar sample  
442 collected from Grand Palais, above 100 ppm. The amount of sulfates in Alt mortar  
443 sample from Préfecture de Police is much lower (21 ppm). The amount of chlorides is  
444 also lower in Alt mortar (11 ppm) compared to Lit mortar (circa 30 ppm). The presence  
445 of nitrates is detected in both mortars, circa 25 ppm in Lit mortar and circa 34 ppm in  
446 Alt mortar. The concentration in bulk material (wt.%) indicates higher percentages of  
447 total soluble salts (cations and anions) in Lit mortar compared to Alt mortar, even  
448 though these values are very small in both cases. The ion chromatography analyses of  
449 the stone flake collected from the Préfecture Police building show a concentration of  
450 sulfates and chlorides of 984 ppm and 17 ppm, respectively. Nitrates were not detected

451 in this sample. The content of soluble  $K^+$  and  $Ca^{2+}$  in this sample is especially high. The  
452 concentration of salts in bulk material in this sample (that contained efflorescences) is  
453 much higher compared to the mortars (circa 12 wt.%). No phosphates or ammonium  
454 were detected in these samples.

455 Figure 8 shows the pore size distribution obtained by mercury intrusion porosimetry in  
456 the mortars collected from the buildings, which have a very different total porosity  
457 accessible to mercury. Lit mortar sample has a higher total Hg-porosity (circa 26%)  
458 compared to Alt mortar (circa 16%). The pore size distribution of the former is mainly  
459 polymodal with the highest volume of pores with radius in the range between 0.1  $\mu m$   
460 and 3  $\mu m$  (Fig.8a). It displays also larger pores with radius in the range between 3 and  
461 10  $\mu m$ , and smaller pores with radius below 0.02  $\mu m$ . Alt mortar porosimetry curve is  
462 mainly bimodal with most of their pores with radius in the range between 0.5 and 1  $\mu m$   
463 and pores below 0.01  $\mu m$  (Fig.8b).

### 464 *3.3. Stone and hardened mortar specimens manufactured in the lab*

#### 465 *3.3.1. Mineralogical characterization*

466 Thin sections of Lit and Alt hardened mortars under optical light microscopy (Fig.9a-b  
467 and Fig.9c-d respectively) show a great similitude with those samples collected from the  
468 buildings (Fig. 5). The matrix or binder of the laboratory hardened mortars show lighter  
469 colors and rounded pores (500  $\mu m$  approx.) that could be related with a lower degree of  
470 maturation and the lack of exposition to weathering agents. The small rounded pores  
471 (around 50  $\mu m$ ) that were observed in the thin sections of Alt mortar from the building  
472 are not observed in the same mortar manufactured at the lab. In the latter, there are  
473 many spherical particles circa 50  $\mu m$  embedded in the matrix that can be clearly  
474 distinguished from it by a thin rim filled with the resin (no blue dyed), which indicate

475 spherical hollow not connected particles. The thin sections of Art mortar show  
476 aggregates of calcite, quartz, feldspars and many phyllosilicates with some micas. There  
477 are many small rounded pores (filled and not filled with the blue dye, which would  
478 represent open and non-connected porosity), together with fissural porosity going  
479 through the matrix, and intra particle porosity associated to phyllosilicates (Fig.9e and  
480 9f). Euville stone thin sections show a larger size of the mineral grains compared to the  
481 mortars (Fig.9g and 9h). Bioclasts, such as crinoids, sea urchins, brachiopods, coral  
482 fragments and pellets can be easily recognized. Syntaxial calcite cement occupies a  
483 large part of the stone that gives rise to the cohesion of the grains. Shell fragments are  
484 filled with calcite sparitic cement and their edges are surrounded by sparitic and micritic  
485 cement in some areas. Heterogeneous macro-pores are left by the syntaxial overgrowth  
486 while micro-pores are mainly intra-particle or located between the micrite and sparite  
487 crystals around shell fragments. Some quartz and clays can be also observed in minor  
488 amounts.

489 The XRD patterns of the 28 days hardened mortars manufactured in the laboratory  
490 reveal the development or increase of portlandite, the decrease of larnite ( $C_2S$ ) and the  
491 disappearance of alite ( $C_3S$ ) regarding to the analyses carried out in their corresponding  
492 raw anhydrous mortars (Table 1 and Fig.10). In all the mortars the decrease of larnite  
493 peaks is evident together with the improvement of crystallinity of portlandite (CH)  
494 reflected by the sharpness and intensity increase of the main CH peak .

### 495 *3.3.2. Physical characterization*

496 A complete characterisation of the physical properties of Euville stone and the 28 days  
497 hardened mortar specimens has been done.

498 Concerning liquid water transfer (Table 6) it can be seen how Lit mortar specimens  
499 display a very low capillarity coefficient compare to the rest of mortar specimens. The

500 total amount of water at the end of the tests (Fig. 11) is also much lower than for the  
501 others mortars (Fig. 11a) and Euville stone (Fig.11c). In Lit mortar specimens,  
502 evaporation (water loss) is also slower than in the rest of materials but the difference is  
503 less important than for capillarity (Fig.11b). Art mortar specimens get more water than  
504 the others and in a very quick way. Alt mortar and Euville stone have a similar  
505 behaviour during the capillarity test: similar velocity and same water content at the end  
506 of the test, but Euville stone losses the water by evaporation much faster than this and  
507 the other mortars (Fig.11d). At the end of the evaporation test Euville stone has lost all  
508 the water taken during the capillarity test. Water vapour permeability is also quite  
509 similar in Alt mortar and Euville stone. Art mortar shows the highest water vapour  
510 permeability values while permeability of Lit mortar is in between the values obtained  
511 in Art and Alt mortars and Euville stone. We can notice that water vapour permeability  
512 and porosity are directly related; roughly we can consider that an  $\times 10^{11}$  factor exists  
513 between vapour permeability and open porosity.

514 Comparing the values of open water porosity and mercury porosity values (Table 7) it  
515 can be observed that the former porosity is between 10 and 20% higher than the latter,  
516 in all the materials except Lit mortar. For Lit mortar, mercury porosity is slightly higher  
517 than water porosity. Bulk density corresponds to the density of “minerals” that form  
518 part of these materials. Euville stone specimens have the highest bulk density  
519 ( $2.55\text{g/cm}^3$ ), slightly lower than the calcite density ( $2.71\text{ g/cm}^3$ ). Comparing the three  
520 mortars, Lit mortar has the highest bulk density, followed by Alt and Art mortars. This  
521 can be explained by its mineralogical composition. Apparent density depends on  
522 porosity and bulk density, showing that Euville stone is more “compacted” than the  
523 mortars. Concerning the mortars, Alt mortar has the highest apparent density, followed  
524 by Lit and Art mortars. Apparent density is inversely related to water open porosity, i.e.

525 the highest the open porosity the lower the apparent density. Apparent density values  
526 obtained by mercury porosimetry correspond very well to values obtained by water  
527 immersion test. For bulk density it can be observed the same pattern than for porosity,  
528 mercury porosimetry values are slightly lower than water porosity values, except for Lit  
529 mortar specimens.

530 Pore size distribution (PSD) is different for all the samples, where it can be considered  
531 two different cases. First, Lit and Art mortars display a clear bimodal PSD which is  
532 quite similar, with an average pore radius circa  $0.10\mu\text{m}$  for Lit and  $0.13\mu\text{m}$  for Art  
533 mortar; median pore radius are about  $0.5\mu\text{m}$  for Lit and  $0.4\mu\text{m}$  for Art, in both cases  
534 the median radius is higher than average radius. Alt mortar and Euville stone show  
535 average pore radius higher than median radius,  $0.04\mu\text{m}$  and  $0.01\mu\text{m}$  for Alt mortar  
536 respectively, and  $1.4\mu\text{m}$  and  $0.8\mu\text{m}$  for Euville stone, respectively. Euville limestone  
537 has larger pores than the mortars, above  $10\mu\text{m}$  (Fig.12). In all the mortars median  
538 radius is smaller than the modal pick, indicating a bias to the smaller pores; Euville  
539 limestone has a median bigger than the mode, reflecting the bias to the biggest pores.  
540 Difference between mode and median is smaller in Euville stone than in mortars,  
541 because it has a more symmetrical PSD. This difference is more important in Alt mortar  
542 and we can observe a big “tail” in the distribution that takes place in the range of  
543 smallest pores.

544 The comparison between capillarity coefficients and pore size distributions for Art and  
545 Alt mortars and Euville limestone, indicates a direct relation between capillarity  
546 coefficients and pore sizes. In order to avoid the effect of water volume absorbed during  
547 the capillarity test, the capillarity coefficient (C) has been divided by the porosity values  
548 (P), in this way, the obtained values correspond to the median pore radius values of  
549  $0.82\mu\text{m}$  (Euville),  $0.41\mu\text{m}$  (Art) and  $0.01\mu\text{m}$  (Alt) (Table 7). A linear regression among

550 these values gives an equation  $C/P = 1.2461 \times (\text{median pore radius}) + 1.9591$ , with a  
551 regression coefficient of  $R^2 = 0.9438$ .

552 Results of mechanical tests obtained in these stone and hardened mortar specimens are  
553 presented in Table 8. Art mortar has a mechanical behaviour different from the others,  
554 since the flexural and compression strengths are much lower than the obtained in the  
555 other mortars. The experimental resolution of the mechanical tests machine used is not  
556 adapted to Art mortar specimens. So if this mortar is not considered, a very good linear  
557 regression between flexural strength and apparent density ( $R^2 = 0.999$ ) can be obtained.

558 The spectrophotometry results are compiled in Table 9. The highest total color  
559 difference ( $\Delta E^*$ ) between each mortar and Euville stone is obtained in Art mortar (circa  
560 8), followed by Alt (circa 5) and Lit mortar that shows the lowest differences (circa 3).

## 561 4. Discussion

### 562 4.1. Chemical and mineralogical characterization

563 The original chemical and mineralogical composition of the raw anhydrous mortars  
564 exert a great influence on their final physico-chemical properties in a short and in a  
565 longer term, and hence on the compatibility with the stone to be repaired and their  
566 durability [31]. Quartz, calcite, feldspar and larnite/belite, alite and traces of gehlenite  
567 (hydraulic components,  $C_2S$ ,  $C_3S$  and  $C_2As$ , respectively) are present in the three raw  
568 anhydrous mortars (Fig.3 and Table 1). The main difference in their mineralogy  
569 determined is the absence of phyllosilicates in Alt mortar and the absence of aerial lime  
570 (portlandite) in Lit mortar. The former contains high quantity of portlandite and calcium  
571 and aluminosilicates (larnite, alite and gehlenite) while the latter has abundant  
572 phyllosilicates (clinochlore and talc) and no portlandite. Art mortar composition is in  
573 between the two other mortars, with portlandite, larnite and alite, and some  
574 phyllosilicates (vermiculite, which was only possible to identify in the XRD and

575 petrography of the 28 days hardened mortars and not in the XRD of the raw anhydrous  
576 materials (although the presence of phyllosilicates was inferred by a small hump  
577 between 10 and 15 °2θ in the XRD pattern). The identified soluble salts determined by  
578 ion chromatography represent insignificant values in the concentration in bulk material  
579 (wt.%), around 2 % in Lit and Alt mortar, which should not represent a salt  
580 crystallization problem or development of salt efflorescences, and a slightly higher  
581 content in Art mortar (5%). However, is important to take into account that these  
582 percentages include a high concentration of soluble calcium ( $\text{Ca}^{2+}$ ), which could be  
583 combined with other anions that were no possible to identify with the chromatographic  
584 column used in these analyses. Soluble calcium combined with other anions such as  
585 carbonates ( $\text{CO}_3^{2-}$ ), silicates ( $\text{SiO}_4^{4-}$ ) or hydroxides ( $\text{OH}^-$ ) could form part of these  
586 mortars, especially in Art mortar with a higher concentration of soluble  $\text{Ca}^{2+}$  (Table 4).

587 The characterization of stone and mortar samples collected from the historic buildings  
588 has been useful to know the current composition and texture of the mortars set under  
589 real conditions and five years of hardening and to study the weathering products causing  
590 decay in these materials. The identification of salt minerals by XRD, SEM-EDX and the  
591 quantification of soluble salts by ion chromatography have served to plan the  
592 accelerated ageing test to assess the durability of stone-mortar specimens in the lab [31].

593 The presence of chlorides and sulfates (gypsum and mixtures of calcium and sodium  
594 sulfates) with minor amounts of nitrates suggest an origin of salts caused by  
595 contamination/pollution coming from past restoration products and environmental  
596 pollution (Fig.6, Fig.7 and Table 5).

597 Lit mortar, classified as a NHL according to the manufacturer, displays a high amount  
598 of phyllosilicates that could have favour cracking of the mortar at the interface stone-  
599 mortar observed at the Grand Palais building when mortar samples were collected

600 (Fig.2). In the frame of Dimppa Project [32] on site measurements with non-destructive  
601 techniques were carried out in this building in the same type of mortar and stone. High  
602 salt index values were found at the interface between Lit mortar and Euville stone,  
603 together with large differences on the thermal behaviour between both materials.  
604 Restorers frequently use clay rich sands because they can increase workability and  
605 matching the right colour for the restoration mortar. However, the main effect of clay  
606 fines ( $<63 \mu\text{m}$ ) in aggregates is an increase of the water demand, due to their high  
607 surface area, for a constant mortar consistency that gives rise to a poor quality mortar  
608 [33]. However, it does not mean that NHL produce bad results in this type of restoration  
609 works, it just depends on the type, proportion and grain size of the minerals in the  
610 original composition and the compatibility with the stone substrate. The characterization  
611 of original mortars and plasters from Crete was carried out with the evaluation of the  
612 repairs prepared with NHL as binding material, siliceous sand and crushed brick as  
613 aggregates [34]. After three years of intervention with these NHL-based mortars and  
614 plasters, macroscopic survey and analyses on the applied materials revealed that no  
615 cracks or release of soluble salts occurred.

616 In this case, this NHL mortar collected from the Grand Palais building (Lit mortar) has  
617 a higher total porosity and a polymodal pore size distribution, compared to the HL  
618 mortar collected at the Préfecture de Police building (Alt mortar). The hardened mortar  
619 specimens manufactured and cured during 28 days in the lab, show the presence of  
620 fissural porosity mainly through the matrix of Lit mortar (Fig.9). The XRD patterns of  
621 all the hardened mortars manufactured in the laboratory (Fig.10) reveal the development  
622 of portlandite (CH) in Lit mortar or its increase in Art and Alt mortars, the decrease of  
623 larnite ( $\text{C}_2\text{S}$ ) and the disappearance of alite ( $\text{C}_3\text{S}$ ) regarding to the analyses carried out  
624 in their corresponding anhydrous raw materials (Fig.3). In Art mortar the decrease of

625 C<sub>2</sub>S peaks can be observed together with the improvement of crystallinity of CH peaks  
626 and the appearance of vermiculite or clinocllore peaks. In Alt and Lit mortars there is  
627 also a decrease in C<sub>2</sub>S and disappearance of C<sub>3</sub>S peaks and the improvement of  
628 crystallinity of portlandite reflected by the sharpness and intensity increase of the main  
629 portlandite (CH) peak. This is explained because the hydration of C<sub>3</sub>S and C<sub>2</sub>S produce  
630 CH and some of new CH amount can also crystallize, inside of the CSH (calcium  
631 silicate hydrates) structure being well sheltered [13]. This fact has been related to the  
632 improvement of mortar strength [35-37], while C<sub>3</sub>S contributes to the strength at early  
633 ages, C<sub>2</sub>S and the carbonation process give their strengths at long term [13].

634 The addition of micro spherical aluminosilicate particles (diameter of 50 μm) similar to  
635 fly ash (FA), into Alt mortar was confirmed through the SEM-EDS analyses, where  
636 these appear empty, cracked or filled with a viscous gel rich in calcium (Fig.7b). Using  
637 fly ash with small and spherical shape in mortar or concrete can reduce water demand of  
638 the mixtures [38]. Chemically, fly ash has pozzolanic activity, which is attributed to the  
639 presence of SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>. It reacts with calcium hydroxide (CH) during cement  
640 hydration, to form additional calcium silicate hydrate (CSH), calcium aluminate hydrate  
641 (CAH) [39] and calcium aluminosilicate (CAS) gels. This can also be explained by the  
642 denser and darker color matrix of Alt mortar under light optical microscopy and higher  
643 physico-chemical compatibility with Euville stone compared the other mortars. The  
644 addition of these spherical micro-capsules, seem to have been added to Alt mortar  
645 mixture in order to improve the mechanical properties acting as a self-healing  
646 cementitious material. Besides these spherical particles, the abundant circular air voids  
647 uniformly distributed in the binder's matrix of both Alt and Art mortars, that creates an  
648 apparently high visible porosity is most probably due to the addition of an air  
649 entrainment agent in the mortar mix [17].

650 The binder:aggregate ratio between 1:3 and 1:4 of the mortars from the buildings  
651 (Fig.5) is in agreement with ratios of similar mortars used in restoration works of  
652 historic buildings in other countries. Pecchioni et al. in 2005 [40] study some Florentine  
653 Palaces (Italy) and the analytical results show that the aggregates were composed by  
654 silicate sand and the binder/aggregate ratio ranged between 1:1 and 1:3, with presence  
655 of larnite.

656 Even though petrography and physical properties of Euville stone have been deeply  
657 studied [19,20], due to its high heterogeneity, the petrography and physical properties of  
658 the specific specimens used in this research was carried to study the compatibility with  
659 the stone-commercial mortars. The heterogeneity of this limestone has been also  
660 observed through on-site measurements on historic buildings and in-lab measurements  
661 with non-destructive techniques [32].

#### 662 *4.2. Physical characterization*

663 In this research we have characterized water (liquid and vapour) transfer through  
664 mortars by means of imbibition properties (capillarity rise), evaporation (desorption  
665 test) and water vapour permeability. The results show that capillarity imbibition,  
666 evaporation and vapour permeability values of 28 hardened Art mortar specimens are  
667 higher than in the others mortars. The reason is the high porosity of this mortar with  
668 pore sizes slightly larger than the others. Art mortar specimens have physical properties  
669 close to those of Euville limestone but with a capillarity coefficient lower than the stone  
670 and a very low evaporation degree.

671 The mechanical behaviour of Lit and Art mortar specimens is very different from the  
672 obtained in Euville stone, being less resistant, especially in compression strength; Art  
673 mortar is the only one with higher flexural and compression strength values close to  
674 those of Euville stone.

675 The low open water porosity values of Lit mortar and the slightly higher values  
676 obtained through mercury porosity compared to water porosity can be explained by the  
677 hydrophobic characteristics of this mortar. Among other reasons, such as the content of  
678 clays in its composition, the possible presence of a water-repellent product in the mortar  
679 composition could explain crack formation, observed both at the interface of stone-  
680 mortar repaired areas at the Grand Palais building. Besides, in the case of these Lit  
681 mortar specimens, also a smooth coating is observed on the surface. This surface  
682 coating, 'skin' or 'scum' is known as laitance and is formed when fine lime particles  
683 held in suspension migrate to the outer surface of the wet material. This laitance is  
684 believed to hinder the vapour permeability of lime-based materials, and negatively  
685 impact upon the substrate beneath by causing accelerated masonry decay associated  
686 with entrapment of moisture. Therefore, it is recommended to remove this laitance from  
687 this type of restoration mortar, especially when applied to permeable substrates [9].

688 From the results of the mechanical properties, especially flexural strength, in the case of  
689 Alt and Lit mortars and Euville stone it depend, on the apparent density of the material,  
690 which is a function of porosity and bulk (mineral) density.  $C_2S$  phases, such as larnite,  
691 and the carbonation process provide strength in a longer term, while limestone  
692 aggregates also increase strength, due to the calcite syntaxial growth, which develops  
693 strength thereby enhancing the binder–aggregate interface [13]. This can explain the  
694 highest strength values in Alt mortar specimens with higher content in these mineral  
695 phases.

696 Regarding to spectrophotometry results, the highest total colour difference ( $\Delta E^*$ )  
697 between each mortar and Euville stone is obtained in Art mortar (circa 8), followed by  
698 Alt (circa 5) and Lit mortar that shows the lowest differences (circa 3). According to  
699 suitability criteria used to assess conservation treatments,  $\Delta E^*$  values lower than 5

700 according to the standard NORMAL 20/85 [41], and close to 3 according to other authors  
701 [42,43], would not be visually detectable by the human eye and it would not  
702 significantly affect the colorimetric parameters of the substrate, which only Lit and Alt  
703 mortars would fulfil this criteria after 28 days of hardening.

704 Repair mortars used for stone restoration are assumed to be highly compatible with  
705 historic materials in terms of physical, chemical and mechanical properties in order to  
706 assure the durability of masonry on the long term [3]. In this sense, these characteristics  
707 in Alt mortar are closer to those of Euville stone, compared to the other mortars, with  
708 the exception of some differences in the hydric properties due to their different pore  
709 systems and aesthetic features that should be improved in further restoration works. The  
710 obtained results cannot allow us to conclude which is the best mortar to restore Euville  
711 stone, and further studies about mortar-stone interactions will be necessary. This work  
712 is an essential step on the research concerning the compatibility and the potential  
713 durability of mortars and stone in masonry building restoration.

## 714 **5. Conclusions**

715 The chemical and mineralogical composition of Euville limestone,(mainly composed of  
716 calcium carbonate) and all the studied anhydrous hydraulic mortars (NHL, HL)  
717 composed by di-calcium silicate ( $C_2S$ , larnite/belite), tri-calcium silicate ( $C_3S$ , alite),  
718 traces of di-calcium alumina silicate ( $C_3AS$ , gehlenite) with presence or absence of  
719 phyllosilicates (vermiculite, clinochlore and talc) and aerial lime (portlandite) seems to  
720 be critical in the chemistry of the 28 days hardened mortars. The mortar containing  
721 calcite, portlandite and no phyllosilicates (Altar Pierre) shows better chemical and  
722 mineralogical compatibility with the stone.

723 The soluble salts content of the raw anhydrous mortars is negligible. The presence of  
724 chlorides and sulfates (gypsum and mixtures of calcium and sodium sulfates) with

725 minor amounts of nitrates present in mortar samples collected from historic buildings of  
726 Paris suggest an origin of salts caused by contamination/pollution coming from past  
727 restoration products and environmental pollution.

728 Regarding to physical compatibility, the mortars containing higher amounts of  
729 phyllosilicates (clinochlore and talc) develop cracks on their surfaces or fissures close to  
730 the stone-mortar interface, as observed in Lithomex mortar samples collected from  
731 Grand Palais building. However, the aesthetical compatibility obtained from the total  
732 color difference values between this mortar and the stone indicates that this is not  
733 visually detectable by the human eye.

734 The addition of marble aggregates and 50-micron spherical aluminosilicate particles to  
735 Altar Pierre mortar, favoured hydrolyses reactions and produced a lower porosity matrix  
736 with closer hydric and mechanical properties to those of the Euville stone compared to  
737 the other two mortars. So, the physico-chemical properties of this mortar are closer to  
738 those of the stone, with the exception of some differences in the hydric behaviour due to  
739 their different pore systems and aesthetic features that should be improved in further  
740 restoration works.

#### 741 **Acknowledgements**

742 Thanks to Foundation des Sciences du Patrimoine / LabEx PATRIMA (2014-2015) for  
743 founding the project “Durabilité de l’interaction Mortier-Pierre dans le patrimoine  
744 architectural” (acronym: Dimppa) that allowed to carry out this research and the  
745 postdoctoral contract of Dr. Lopez-Arce. Thanks also to Roland Westphal (Entreprise  
746 Lefèvre) for showing us the restoration works carried out at the Grand Palais. Special  
747 thanks to Mrs Ch. Garrat from Grand Palais and Mrs Keller from Préfecture de Police  
748 for their decisive help during sampling on the monuments. We are also grateful to Lilian  
749 Cristofol and technical engineers that helped in sample preparation and SEM-EDS

750 analyses from the Civil Engineering Dept. Cergy-Pontoise University (UCP) Finally  
751 special thanks as well to Isabell Laureat from the Chemistry Dept. of UCP for all her  
752 help performing the calibration of the ion chromatography (IC) equipment.

### 753 **References**

754 [1] J. Válek, Members of RILEM TC-203-RHM, Performance and Repair Requirements  
755 for surface repairs, in: HMC2010 conference and TC 203-RHM final workshop, Prague,  
756 September 22-24 Rilem Publications s.a.r.l., 2010, pp. 1377-1383.

757 [2] J. Griswold, S. Uricheck, Loss Compensation Methods for Stone, JAIC 37 (1998)  
758 89–110.

759 [3] K. Van Balen, E.E. Toumbakari, M.T. Blanco, J. Aguilera, F. Puertas, C. Sabbioni,  
760 G. Zappia, C. Riontino, G. Gobbi, Procedure for a mortar type identification, a proposal,  
761 in: P. Bartos, C. Groot, J.J. Hughes (Eds.), Proceedings of International RILEM  
762 Workshop on Historic Mortars: Characteristics and Tests, Paisley, Scotland, May 12-14,  
763 Rilem Publications s.a.r.l. 1999, pp. 63–72 (1999).

764 [4] C. Groot, G. Ashall, J. Hughes. Report of RILEM TC COM 167: characterisation of  
765 old mortars with respect to their repair. RILEM Report 28, RILEM Publications s.a.r.l.,  
766 France (2004).

767 [5] J. Ashurst. N. Ashurst, Practical Building Conservation, English Heritage  
768 Handbook, Vol.1, Stone masonry, Gower technical Press ltd (1990).

769 [6] J.J. Hughes, J. Válek, Mortars in historic buildings. A review of the scientific and  
770 conservation literature, Historic Scotland, Edinburgh (2003).

771 [7] P. Lopez-Arce, J. Garcia-Guinea, D. Benavente, L. Tormo, E. Doehne, Deterioration  
772 of dolostone by magnesium sulfate salt: An example of incompatible building materials  
773 at Bonaval Monastery, Spain. Constr. Build. Mater. 23 (2009) 846-855.

- 774 [8] I. Papayianni, M. Stefanidou, Strength-porosity relationships in lime-pozzolan  
775 mortars. *Constr. Build. Mater.* 20 (2006) 700–705.
- 776 [9] C. Torney, A.M. Forster, P.F.G. Banfill, E.M. Szadurski, The effects of site practice  
777 on the physical properties of proprietary stone restoration mortar. *Constr Build Mater* 75  
778 (2015) 359–367.
- 779 [10] A. Isebaert, L. Van Parys, V. Cnudd, Composition and compatibility requirements  
780 of mineral repair mortars for stone – A review. *Constr. Build. Mater.* 59 (2014) 39–50.
- 781 [11] B. Szemerey-Kiss, A. Török, Time-dependent changes in the strength of repair  
782 mortar used in the loss compensation of stone. *Environ Earth Sci.* 63 (2011) 1613–1621.
- 783 [12] V. Rahhal, R. Talero, Effect of three natural pozzolans on portland cement  
784 hydration, *Mater. Construcc.* 53 (2003) 29-40.
- 785 [13] J. Lanás, J.L. Pérez Bernal, M.A. Bello, J.I. Álvarez Galindo, Mechanical  
786 properties of natural hydraulic lime-based mortars. *Cem. Concr. Res.* 34 (2004) 2191–  
787 2201.
- 788 [14] K. Callebaut, J. Elsen, K. Van Balen, W. Viaen, Nineteenth century hydraulic  
789 restoration mortars in the Saint Michael's Church (Leuven, Belgium) Natural hydraulic  
790 lime or cement? *Cem. Concr. Res.* 31 (2001) 397-403.
- 791 [15] J.M. Teutonico, G. Ashall, E. Garrod, T. Yates, A comparative study of hydraulic  
792 lime-based mortars, in: P. Bartos, C. Groot, J.J. Hughes (Eds.), *Proceedings of*  
793 *International RILEM Workshop on Historic Mortars: Characteristics and Tests*, Paisley,  
794 Scotland, May 12-14, Rilem Publications s.a.r.l. 1999, pp. 339–349 (1999).
- 795 [16] L. Schueremans, Ö. Cizer, G. Serré, K.V. Balen, Characterization of repair  
796 mortars for the assessment of their compatibility in restoration projects: Research and  
797 practice, *Constr. Build. Mater.* 25 (2011) 4338–4350.

798 [17] D. Gulotta, S. Goidanich, C. Tedeschi, T.G. Nijland, L. Toniolo, Commercial  
799 NHL-containing mortars for the preservation of historical architecture. Part 1:  
800 Compositional and mechanical characterisation, *Cem. Concr. Res.* 38 (2013) 31–42.

801 [18] C. Pelosi, U. Santamaria, G. Agresti, G. De Vivo, D. Bandera, Analysis and  
802 laboratory tests to evaluate the composition and the behaviour of some dehumidifying  
803 mortars used in the restoration field, *Periodico di Mineralogia*, 82 (2013) 557-572.

804 [19] T. De Kock, J. Dewanckele, M. Boone, G. de Schutter, P. Jacobs, V. Cnudde,  
805 Replacement stones for Lede stone in Belgian historical monuments, in: J. Cassar, M.G.  
806 Winter, B.R. Marker, N.R.G. Walton, D.C. Entwisle, E.N. Bromhead, J.W.N. Smith  
807 (Eds.), *Stone in Historic Buildings: Characterization and Performance*, Geological  
808 Society, London, Special Publications 391, 2014, pp. 31-46.

809 [20] J. Dewanckele, T. De Kock, G. Fronteau, H. Derluyn, P. Vontobel, M. Dierick, L.  
810 Van Hoorebeke, P. Jacobs, V. Cnudde, Neutron radiography and X-ray computed  
811 tomography for quantifying weathering and water uptake processes inside porous  
812 limestone used as building material, *Mater. Charact.* 88 (2014) 86-99.

813 [21] EN 12620 + A1:2008 (2002) Aggregates for Concrete.

814 [22] AFNOR EN 196-1 (2006) Méthodes d’essai des ciments Partie 1: Détermination de  
815 la résistance mécaniques, France.

816 [23] AFNOR EN 1015-11, Méthodes d’essai des mortiers pour maçonnerie. Partie 11:  
817 Détermination de la résistance en flexion et en compression du mortier durci, France  
818 2000.

819 [24] A. Arizzi, G. Martínez- Huerga, E. Sebastian-Pardo, G. Cultrone, Mineralogical,  
820 textural and physical-mechanical study of hydraulic lime mortars cured under different  
821 moisture conditions, *Mater. Construcc.* 65 (2015).

- 822 [25] A. Arizzi, H. Viles, G. Cultrone, Experimental testing of the durability of lime-  
823 based mortars used for rendering historic buildings, *Constr. Build. Mater.* 28 (2012)  
824 807-818.
- 825 [26] AFNOR NF-EN 1015-1(P12-301), Méthodes d'essai des mortiers pour  
826 maçonnerie. Partie 1: Détermination de la répartition granulométrique (par tamisage),  
827 France, 1999.
- 828 [27] AFNOR EN 1925, Méthodes d'essai pour Pierres naturelles Détermination du  
829 coefficient d'absorption d'eau par capillarité, France, 1999.
- 830 [28] AFNOR EN 15803, Méthodes d'essai : détermination de la perméabilité à la  
831 vapeur d'eau, France, 2010.
- 832 [29] AFNOR EN 1936, Méthodes d'essai des Pierres naturelles maçonnerie :  
833 Détermination des masses volumiques réelle et apparentes et des porosités ouverte et  
834 totale, France, 2007.
- 835 [30] AFNOR EN 196-1, Méthodes d'essai des ciments Partie 1: Détermination de la  
836 résistance mécaniques, France, 2006.
- 837 [31] P. Lopez-Arce, M. Tagnit-Hammou, B. Menendez, J-D. Mertz, A. Kaci, Durability  
838 of stone-repair mortars used in historic buildings from Paris, *Materials and Structures*,  
839 DOI 10.1617/s11527-016-0846-0
- 840 [32] B. Menendez, J.D. Mertz, M. Guiavarc'h, A. Kaci, S. Aggoun, P. Lopez-Arce,  
841 Durabilité de l'interaction Mortier-Pierre dans le patrimoine architectural (acronym:  
842 Dimppa project). *Foundation des Sciences du Patrimoine / LabEx PATRIMA* (2014-  
843 2015), Final technical report.
- 844 [33] F. Winnefeld, K.G. Böttger, How clayey fines in aggregates influence the  
845 properties of lime mortars. *Mater. Struct.* 39 (2006) 433-443.

846 [34] P. Maravelaki-Kalaitzaki, A. Bakolas, I. Karatasios, V. Kilikoglou, Hydraulic lime  
847 mortars for the restoration of historic masonry in Crete, *Cem. Concr. Res.* 35 (2005)  
848 1577–1586.

849 [35] A. Moropoulou, A. Bakolas, K. Bisbikou, Physico-chemical adhesion and cohesion  
850 bonds in joint mortars imparting durability to the historic structures, *Constr. Build.*  
851 *Mater.* 14 (2000) 35–46.

852 [36] A. Moropoulou, A. Bakolas, K. Bisbikou, Investigation of the technology of  
853 historic mortars, *J. Cult. Herit.* 1 (2000) 45–58.

854 [37] A. Moropoulou, G. Biscontin, A. Bakolas, K. Bisbikou, Technology and behavior  
855 of rubble masonry, *Constr. Build. Mater.* 11 (1997) 119–129.

856 [38] E.P. Mora, J. Paya, J. Monzo, Influence of different sized fractions of a fly ash on  
857 workability of mortars. *Cem. Concr. Res.* 23 (1993) 917–924.

858 [39] L.J. Malvar, L.R. Lenke, Efficiency of fly ash in mitigating alkali silica reaction  
859 based on chemical composition, *ACI Mater. J.* 103 (2006) 319–326.

860 [40] E. Pecchioni, P. Malesani, B. Bellucci, F. Fratini, Artificial stones utilised in  
861 Florence historical palaces between the XIX and XX centuries, *J. Cult. Herit.* 6 (2005)  
862 227–233.

863 [41] *NORMAL 20/85*, Interventi conservativi: progettazione esecuzione e valutazione  
864 preventive, Italy, 1986.

865 [42] D. Benavente, F. Martinez-Verdu, A. Bernabeu, V. Viqueira, R. Fort, M.A. Garcia  
866 del Cura, C. Illueca, S. Ordoñez, *Color Res. Appl.* 28 (2003) 343–351.

867 [43] J.D. Rodrigues, A. Grossi, Indicators and ratings for the compatibility assessment  
868 of conservation actions, *J. Cult. Herit.* 8 (2007) 32–43.

869

870 FIGURE CAPTIONS

871 **Figure 1.** Mortar and stone materials. a) Raw anhydrous ready to mix mortars (left: *Lit* mortar;  
872 center: *Alt* mortar; right: *Art* mortar); b) Euville stone specimen used for water vapour  
873 permeability test; c) 28 days hardened mortars specimens (Left: *Lit* mortar; center: *Alt* mortar;  
874 right: *Art* mortar) after capillarity water absorption test.

875 **Figure 2.** Mortar and stone samples collected from historic buildings of Paris. a) Lit mortar  
876 from Grand Palais building; b) Alt mortar from Préfecture Police building; c) Euville stone  
877 flake from Préfecture Police.

878 **Figure 3.** X-ray diffraction patterns (XRD) of the raw anhydrous mortars (Lit: Lithomex; Art:  
879 ArtoPierre;. Alt: Altar Pierre)

880 **Figure 4.** SEM-EDS analyses performed in several areas of mineral grains with sizes between  
881 1.6-1.25 mm and 1.25 mm-0.63 mm of Lithomex (Litho, Lit), ArtoPierre (Arto, Art) and Altar  
882 Pierre (Altar, Alt) mortars. a) phyllosilicates (clinochlore and talc), with and without additional  
883 K, Ti and Cl with sizes between 1.6-1.25 mm in Lit mortar; b) calcite grains (1.25 mm-0.63  
884 mm) in Lit mortar; c) phyllosilicates (1.25-063 mm) in Art mortar; d) calcite grains (1.25 mm-  
885 0.63 mm) in Alt mortar.

886 **Figure 5.** Thin sections obtained by light optical microscopy in mortar samples collected from  
887 historic buildings of Paris. a) Lit mortar from Grand Palais building (Lit-GP); b) same former  
888 image with crossed nicols; c) Lit mortar, detail of fissural porosity (in blue); d) same former  
889 image with crossed nicols; e) Alt mortar from Préfecture Police building (Alt-PP); f) same  
890 former image with crossed nicols; g) Alt mortar, detail of same sample showing porosity (in  
891 blue).

892 **Figure 6.** X-ray diffraction pattern of mortar samples collected from historic buildings of Paris.  
893 Lit-GP (Lithomex mortar from Grand Palais); Alt -PP (Altar Pierre from Préfecture Police); Lit-  
894 GP-sf (evaporated soluble fraction together with non-soluble residues).

895 **Figure 7.** Scanning electron microscopy (SEM) images and energy dispersive spectroscopy  
896 (EDS) analyses performed on the surface of mortar and stone samples collected from historic  
897 buildings of Paris. a) Lit mortar from the Grand Palais; b) Alt mortar from Préfecture de Police;  
898 c) efflorescences in Euville stone flake from Préfecture de Police.

899 **Figure 8.** Connected porosity and pore size distribution obtained by mercury intrusion  
900 porosimetry in mortar samples collected from historic buildings of Paris. a) Lit mortar from  
901 Grand Palais; b) Alt mortar from Préfecture de Police.

902

903 **Figure 9.** Thin sections observed by light optical microscopy of the 28 days hardened mortars  
904 manufactured in the lab and of Euville stone. a) Lit mortar with parellel nicols; b) same former  
905 image with crossed nicols; c) Alt mortar with parellel nicols; d) same former image with  
906 crossed nicols; e) Art mortar with parellel nicols; f) same former image with crossed nicols; g)  
907 Euville stone with parellel nicols; h) same former image with crossed nicols.

908 **Figure 10.** X-ray diffraction pattern of 28 days (28d) hardened mortars manufactured in the  
909 laboratory (Lit: Lithomex mortar; Art: Artopierre mortar; Alt: Altar Pierre mortar).

910 **Figure 11.** Representation of hydric properties of 28 days hardened mortars and stone  
911 specimens. a) capillarity water absorption of mortars; b) water desorption (water loss) of  
912 mortars; c) capillarity water absorption of Euville stone; d) water desorption (water loss) of  
913 Euville; e) water vapor permeability of mortars; f) water vapor permeability of Euville stone.

914 **Figure 12.** Connected porosity and pore size distribution obtained by mercury intrusion  
915 porosimetry in 28 days hardened mortars and Euville stone.

916

917 Table 1. Semi-quantitative (%) X-ray diffraction (XRD) analyses of the raw anhydrous and 28 days hardened mortars together with mortar samples  
 918 from historic buildings from Paris

Mortar	Calcite	Quartz	Feldspar	Gypsum	Clinochlore	Talc	Dolomite	Muscovite	C <sub>3</sub> S	C <sub>2</sub> S	C <sub>2</sub> AS	CH	halite
Lit-raw	20	10	5	Nd*	10	45	traces	Nd*	5	5	traces	Nd*	Nd*
Art-raw	15	50	traces	Nd*	Nd*	Nd*	Nd*	Nd*	5	10	traces	20	Nd*
Alt-raw	20	35	15	traces	Nd*	Nd*	Nd*	Nd*	5	10	traces	15	Nd*
Lit-GP*	14	14	10	5	21	20	Nd*	16	Nd*	Nd*	traces	Nd*	Nd*
Lit-GP <sup>-sf</sup> *	15	5	Nd*	8	49	18	Nd*	Nd*	Nd*	Nd*	Nd*	Nd*	5
Alt-PP	15	60	14	Nd*	Nd*	Nd*	Nd*	Nd*	Nd*	6	traces	5	Nd*
Lit-28D	20	21	5	Nd*	26	28	Nd*	Nd*	Nd*	traces	Nd*	Nd*	Nd*
Art-28D	20	61	9	Nd*	traces	Nd*	Nd*	Nd*	Nd*	5	traces	5	Nd*
Alt-28D	18	50	20	Nd*	Nd*	Nd*	Nd*	Nd*	traces	6	traces	6	Nd*

919 \*Nd: No detected; Lit: Lithomex mortar; Alt: Altar Pierre mortar; Art: ArtoPierre mortar; raw: anhydrous raw mortar; GP: Grand Palais building; PP:  
 920 Préfecture Police building; sf: evaporated soluble fraction; 28D: 28 days hardened mortar; C<sub>2</sub>S: Di-calcium silicate, Ca<sub>2</sub>SiO<sub>4</sub> (Iarnite/belite); C<sub>3</sub>S: Tri-  
 921 calcium silicate, Ca<sub>3</sub>SiO<sub>5</sub> (alite); CH: Calcium hydroxide (portlandite); C<sub>2</sub>AS: gehlenite

922

923 Table 2. Qualitative elemental analyses performed by punctual energy dispersive spectroscopy (SEM-EDS) on several  
 924 grains of the largest grain size fractions (aggregates) of the raw anhydrous mortars embedded in epoxy resin.

Mortar	Lit mortar		Art mortar		Alt mortar	
	1.60-1.25mm	1.25-0.63mm	1.60-1.25mm	1.25-0.63mm	1.60-1.25mm	1.25-0.63mm
Grain size interval						
Normalized wt.%						
Ca	Present	Present	Present	Present	Present	Present
Si	Present	Present	Present	Present	Present	Present
Al	Present	Present	Present	Present	No detected	No detected
Mg	Present	Present	Present	Present	No detected	No detected
O	Present	Present	Present	Present	Present	Present
C	Present	Present	Present	Present	Present	Present
K	Present	No detected	Present	Present	No detected	No detected
Na	Present	Present	Present	No detected	Present	No detected
Fe	Present	Present	Present	Present	No detected	Present
Ti	Present	No detected	Present	Present	No detected	Present
Cl	Present	No detected	Present	Present	Present	Present

925

926

927  
928

Table 3. Semi-quantitative (%) energy dispersive spectroscopy (EDS) analyses performed on the finest grain size fractions (aggregates and binder) of the raw anhydrous mortars pressed on tablets.

Grain size	0.63-0.315 mm			0.315-0.20 mm			0.20-0.16 mm			0.16-0.080 mm			<0.080 mm		
Mortar	Lit	Art	Alt	Lit	Art	Alt	Lit	Art	Alt	Lit	Art	Alt	Lit	Art	Alt
Normalized wt.%															
Ca	13.1	19.7	3.8	11.0	11.3	5.4	9.3	38.3	27.0	7.5	32.6	28.3	3.9	39.7	33.0
Si	19.2	23.0	39.0	20.7	33.1	41.2	11.0	8.0	6.3	5.2	5.5	5.6	8.0	2.4	6.3
Al	0.5	0.4	1.1	0.6	0.6	1.5	0.8	0.4	1.4	1.2	0.5	1.7	1.9	0.5	1.8
Mg	0.5	0.5	0.2	0.4	0.4	0.2	1.2	0.4	1.8	4.8	0.5	2.2	7.7	0.5	1.8
O	52.3	45.6	50.8	50.7	48.0	48.0	59.8	46.7	54.8	61.8	52.5	54.0	61.9	49.1	50.2
C	12.6	10.8	4.6	14.7	6.2	2.5	17.6	5.8	7.1	19.3	7.4	7.3	16.1	7.3	6.0
S	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	1.0	0.3	0.4	0.7	0.4	0.4	0.8
K	0.2	0.0	0.8	0.2	0.4	1.2	0.0	0.2	0.1	0.0	0.2	0.0	0.0	0.1	0.0
Na	0.0	0.0	3.8	0.0	0.0	5.4	0.0	0.0	27.0	0.0	0.4	0.4	0.0	0.0	33.0

\*Lit: Lithomex mortar; Art: Artopierre mortar; Alt: Altar Pierre mortar

929  
930

931 **Table 4.** Soluble salt content determined by ion chromatography analyses of the raw anhydrous mortars

Soluble salts		Anions (ppm)				Cations (ppm)					Wt. (%)
Samples		Cl <sup>-</sup>	SO <sub>4</sub> <sup>2-</sup>	NO <sub>3</sub> <sup>-</sup>	PO <sub>4</sub> <sup>3-</sup>	Na <sup>+</sup>	NH <sub>4</sub> <sup>+</sup>	K <sup>+</sup>	Mg <sup>2+</sup>	Ca <sup>2+</sup>	
anhydrous mortar	Lit	5	23	0	0	22	0.00	3	1	129	2
	Art	5	0	0	0	16	0.00	3	1	534	5
	Alt	6	0	0	0	22	0.00	3	3	165	2

932

933 **Table 5.** Soluble salt content determined by ion chromatography analyses of mortar and stone samples collected from Grand  
 934 Palais (GP) and Préfecture Police (PP) buildings.

Soluble salts		Anions (ppm)				Cations (ppm)					wt.
Samples		Cl <sup>-</sup>	SO <sub>4</sub> <sup>2-</sup>	NO <sub>3</sub> <sup>-</sup>	PO <sub>4</sub> <sup>3-</sup>	Na <sup>+</sup>	NH <sub>4</sub> <sup>+</sup>	K <sup>+</sup>	Mg <sup>2+</sup>	Ca <sup>2+</sup>	(%)
Mortar	Lit-GP	30	105	25	0	22	0	9	5	97	3
From buildings	Alt-PP	12	21	34	0	17	0	2	2	15	1
Stone flake	EU-PP	17	984	0	0	58	0	152	7	261	13

935

936 **Table 6.** Results from hydric characterization of 28 days hardened mortars and stone specimens

Properties / samples	Lit mortar	Art mortar	Alt mortar	Euville stone
Capillary Coefficient (g/m <sup>2</sup> .s <sup>0.5</sup> )	11.63	73.85	43.20	45.60
Desorption Coefficient (g/m <sup>2</sup> .s <sup>0.5</sup> )	-5.16	-29.41	-7.79	-49.80

Water vapour permeability Kg/ (m.s.Pa)	3.08E-11	4E-11	1.79E-11	1.57E-11
Open porosity (%)	31.1 ± 1.1	39.1 ± 1.0	25.0 ± 0.2	16.5 ± 1.0
Apparent density (g/cm <sup>3</sup> )	1.67 ± 0.00	1.58 ± 0.01	1.88 ± 0.03	2.25 ± 0.02
Bulk density (g/cm <sup>3</sup> )	2.45 ± 0.04	2.59 ± 0.00	2.51 ± 0.01	2.69 ± 0.01

937

938 **Table 7.** Mercury intrusion porosimetry results obtained in 28 days hardened mortars and stone

Properties / samples	Lit mortar	Art mortar	Alt mortar	Euville stone
Porosity (%)	32.24	31.77	21.13	14.92
Apparent density (g/cm <sup>3</sup> )	1.69	1.57	1.88	2.17
Bulk density (g/cm <sup>3</sup> )	2.49	2.30	2.38	2.55
Average pore radius (µm)	0.10	0.13	0.04	1.47
Median pore radius (µm)	0.48	0.41	0.01	0.82
Mode pore radius (µm)	0.76	0.95 (0.28)	0.34 (0.25)	0.60

939

940 **Table 8.** Flexural and compression strength of 28 days hardened mortars and Euville stone.

Strength (MPa)	Lit mortar	Art mortar	Alt mortar	Euville stone
Flexural	3.91 ± 0.05	2.22 ± 0.08	4.22 ± 0.16	4.84 ± 0.35
Compression	9.01*	<7	15.65 ± 2.88	27.07 ± 5.25

941 \* In the other specimens compression was <7

942 **Table 9.** Colour parameters (L\*, lightness; a\* and b\* colour coordinates; C\*, Chroma; ΔE\*, total colour difference) obtained in

943 28 days hardened mortar specimens and Euville stone.

Material	L*	a*	b*	C* (D65)	Hue (D65)	ΔE*
Lit	78.44± 0.10	2.35 ± 0.02	11.32 ± 0.04	11.56 ± 0.04	78.30 ± 0.06	3.22
Art	88.05± 0.11	0.93 ± 0.03	6.34 ± 0.08	6.47 ± 0.08	81.72 ± 0.13	7.80
Alt	76.36± 0.06	1.60 ± 0.01	9.56 ± 0.03	9.70 ± 0.04	80.50 ± 0.06	5.16
Stone	81.38± 1.09	2.68 ± 0.28	10.06 ± 1.44	10.41 ± 1.45	74.98 ± 1.46	Reference

944

945

946

FIGURE 1

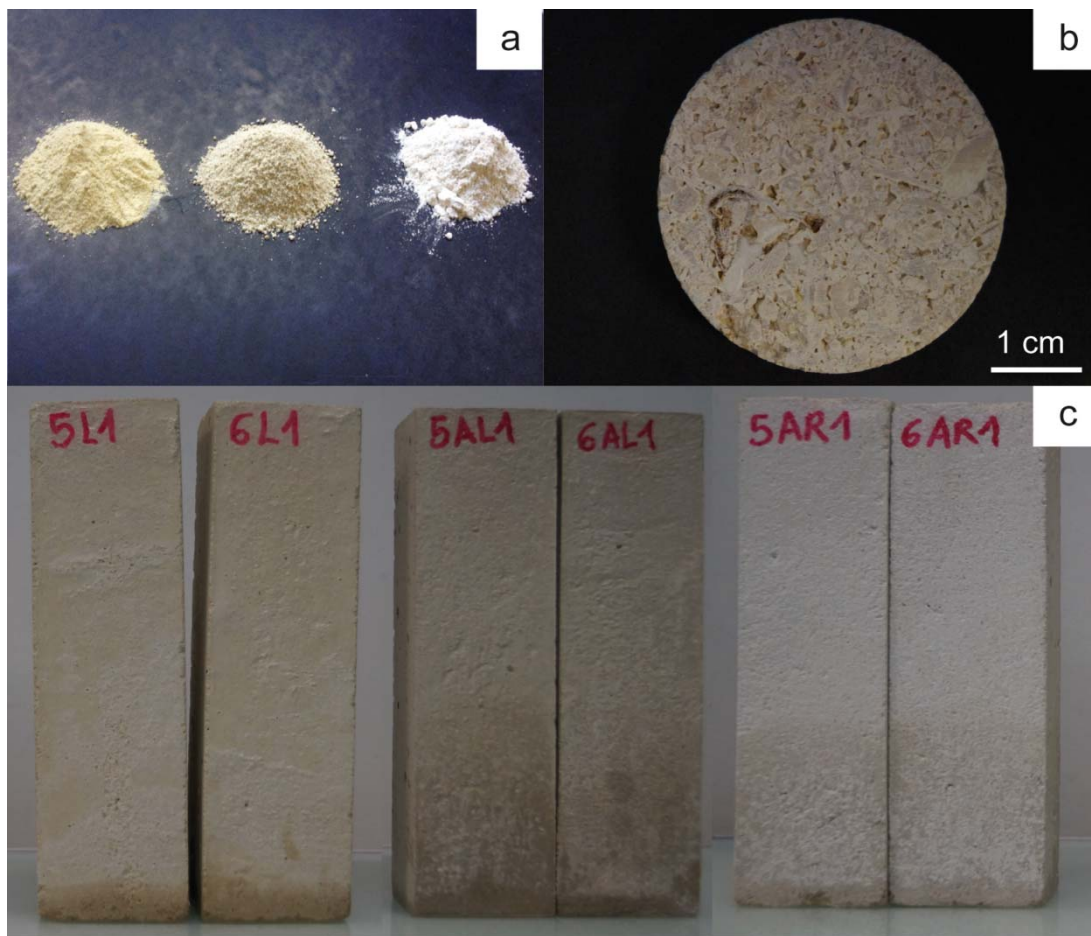
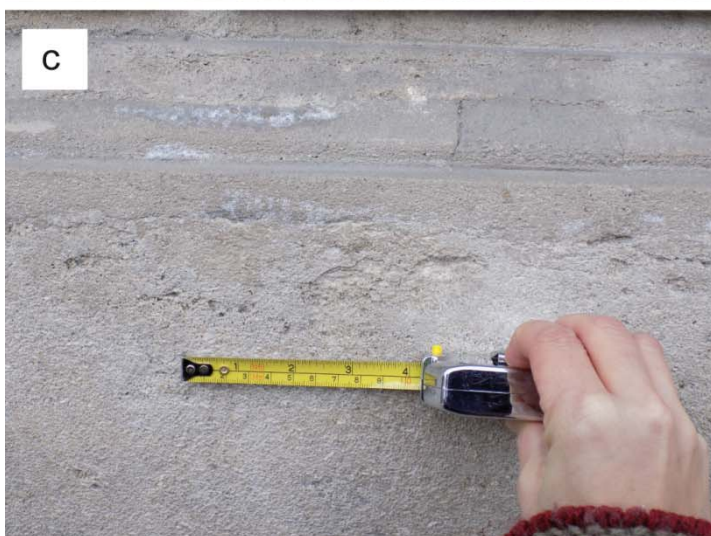
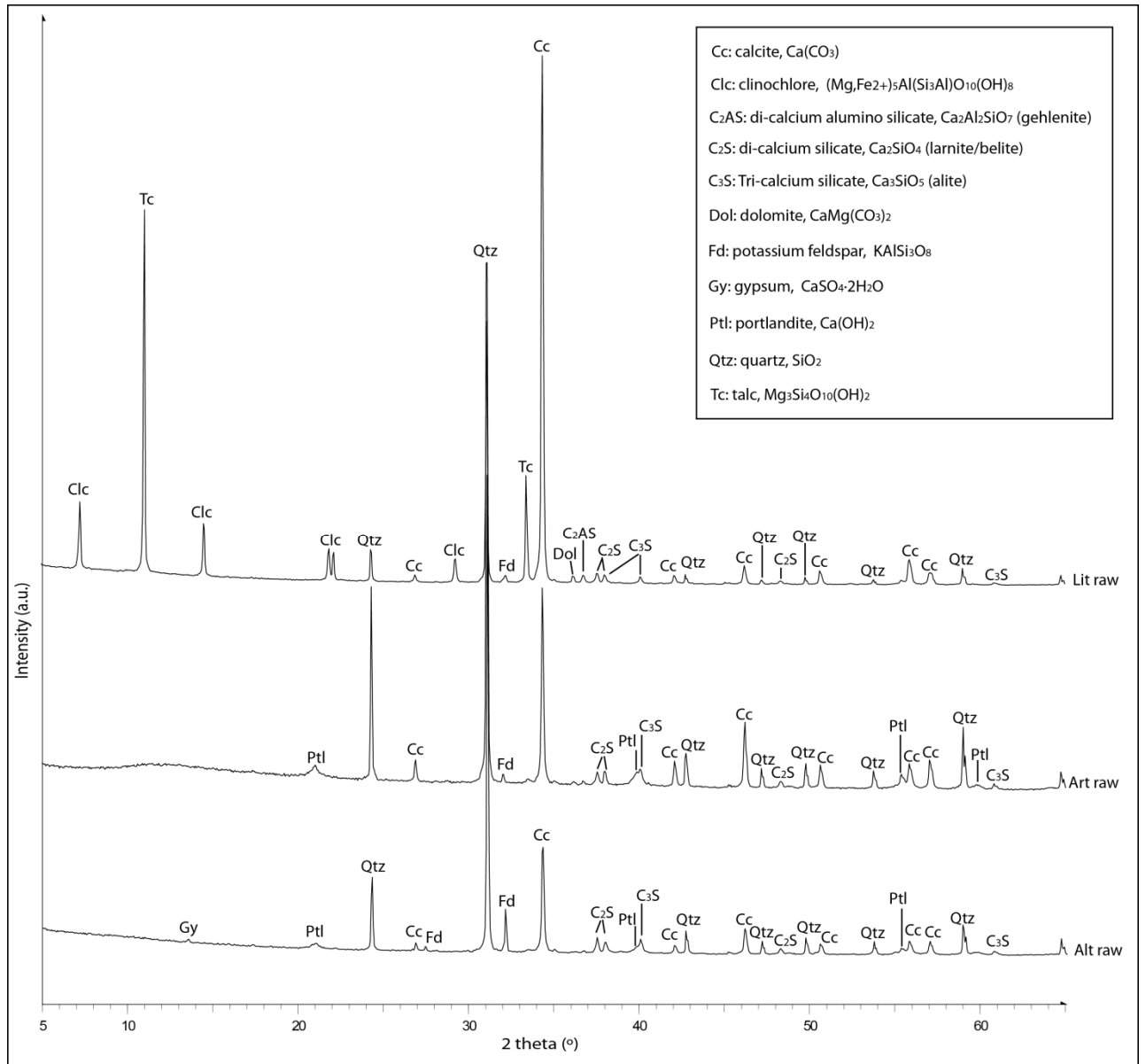


FIGURE 2



# FIGURE 3



# FIGURE 4

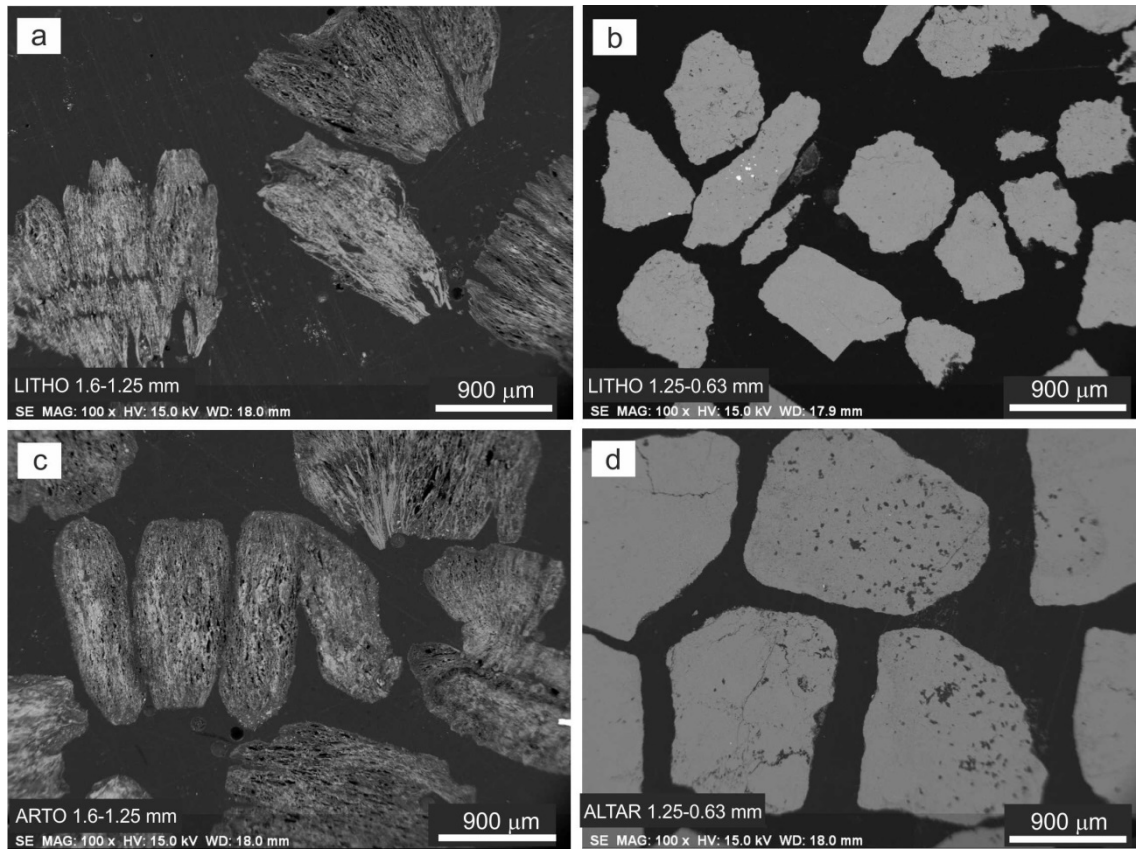
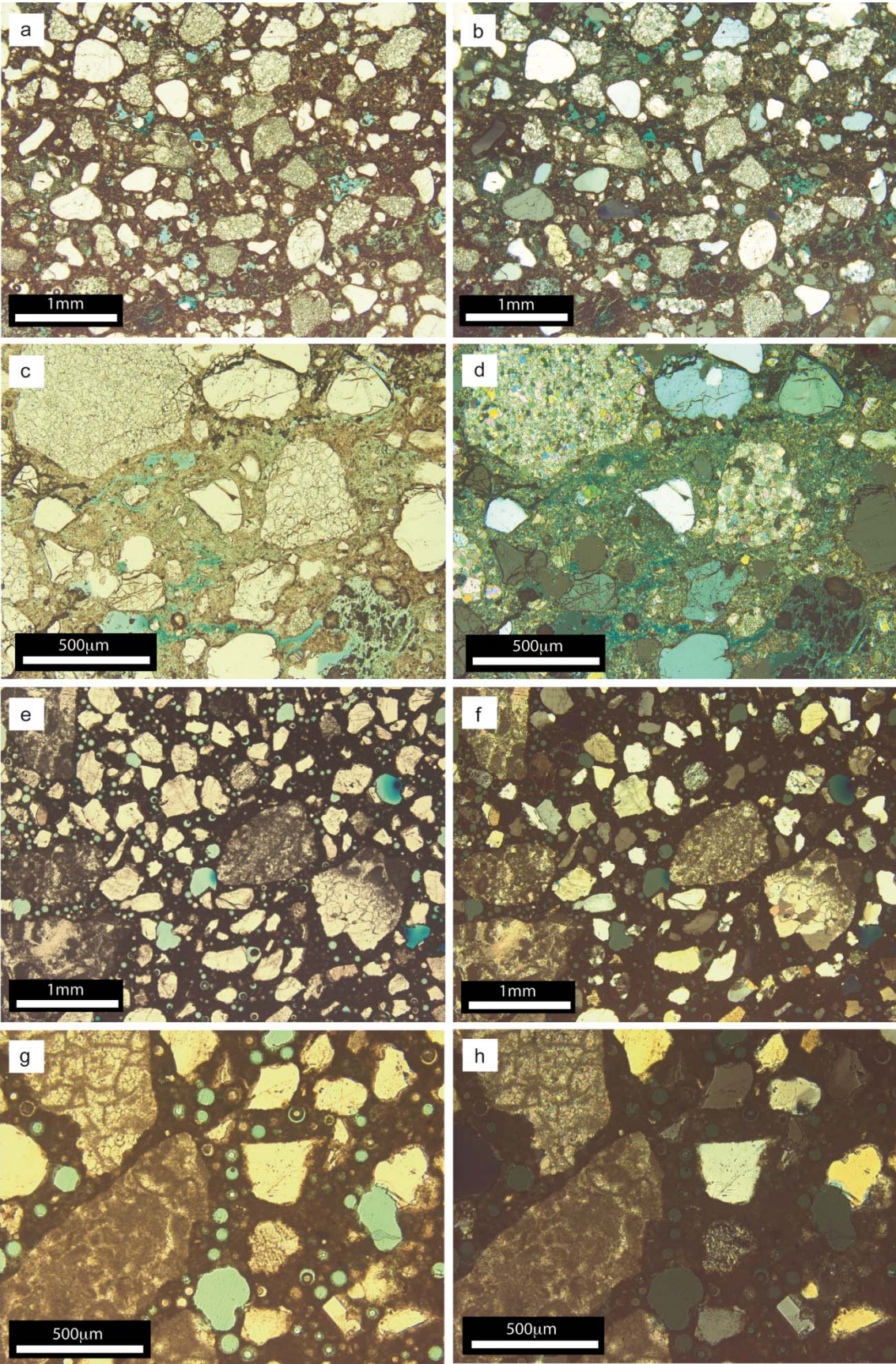
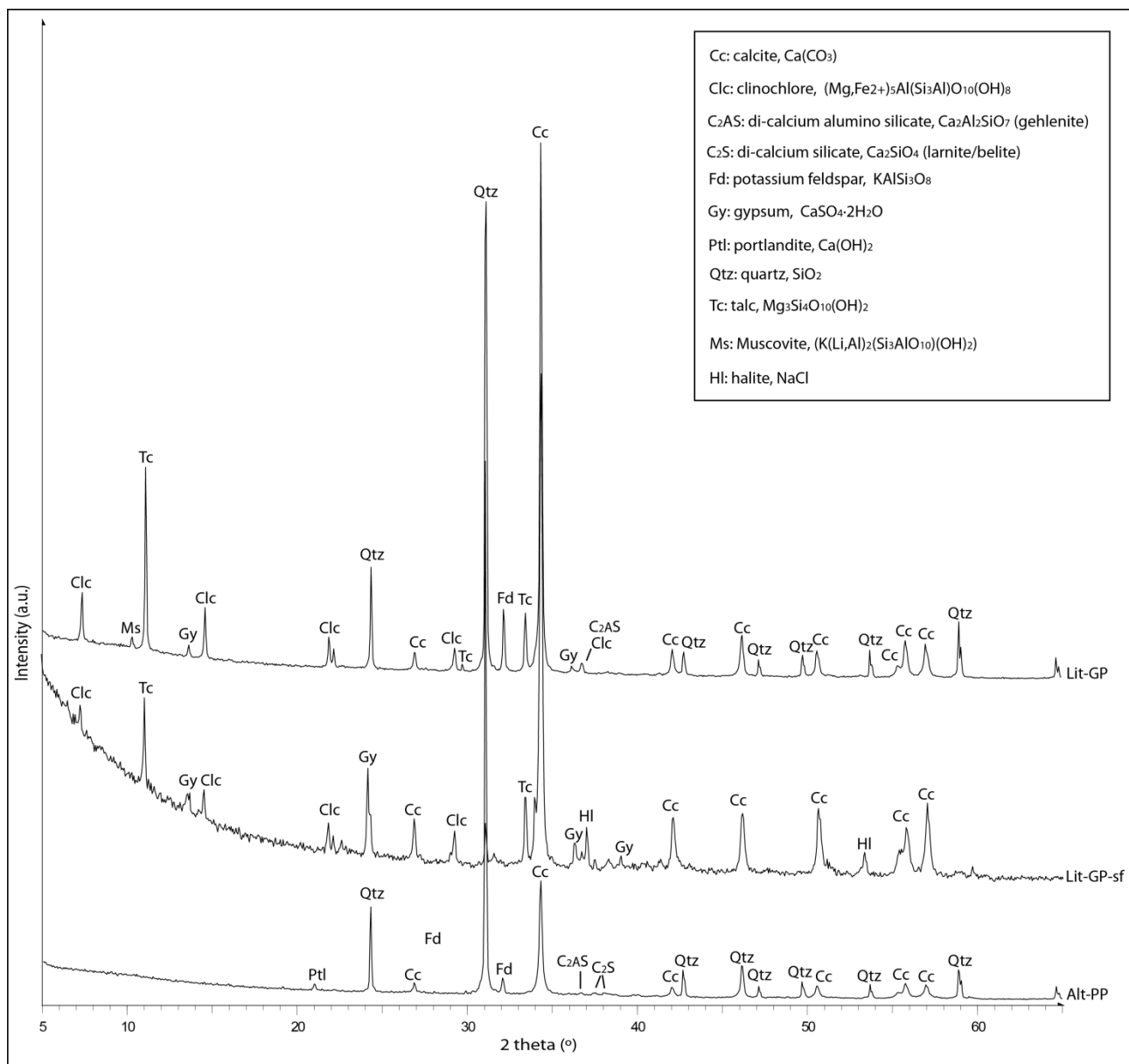


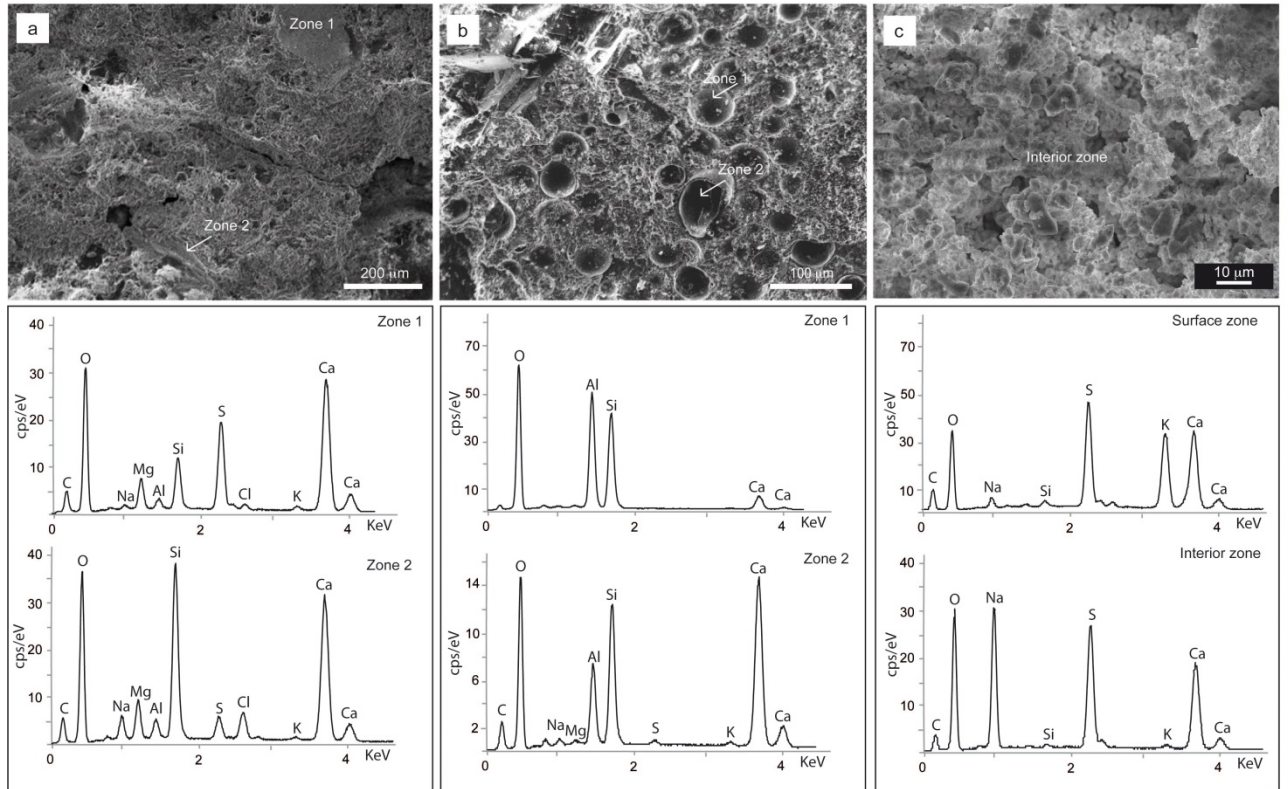
FIGURE 5



# FIGURE 6



# FIGURE 7



# FIGURE 8

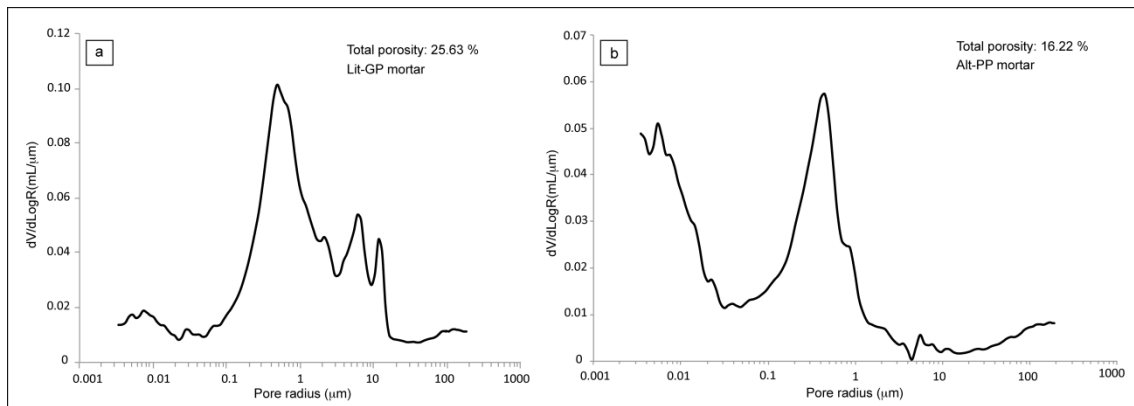
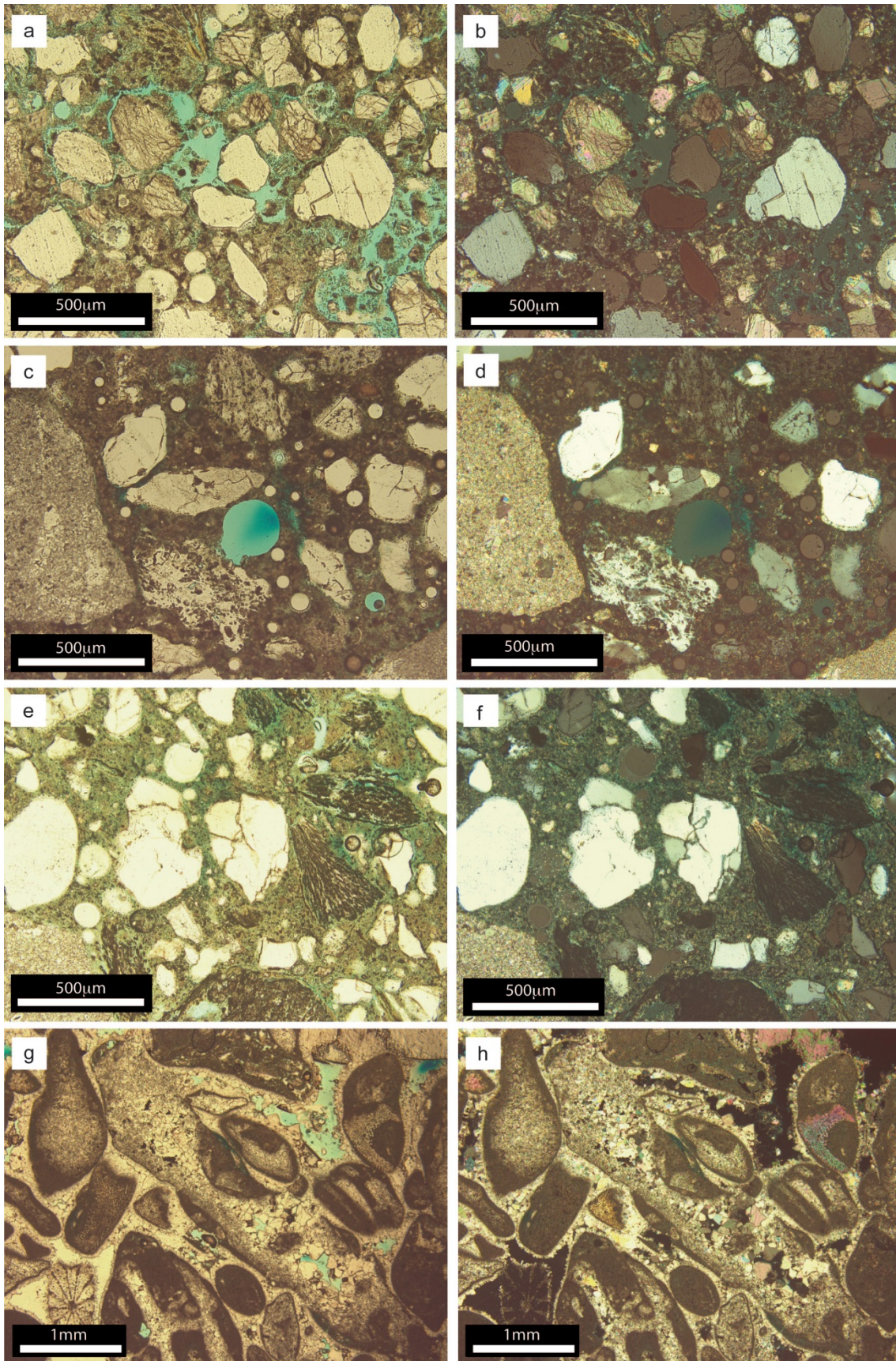
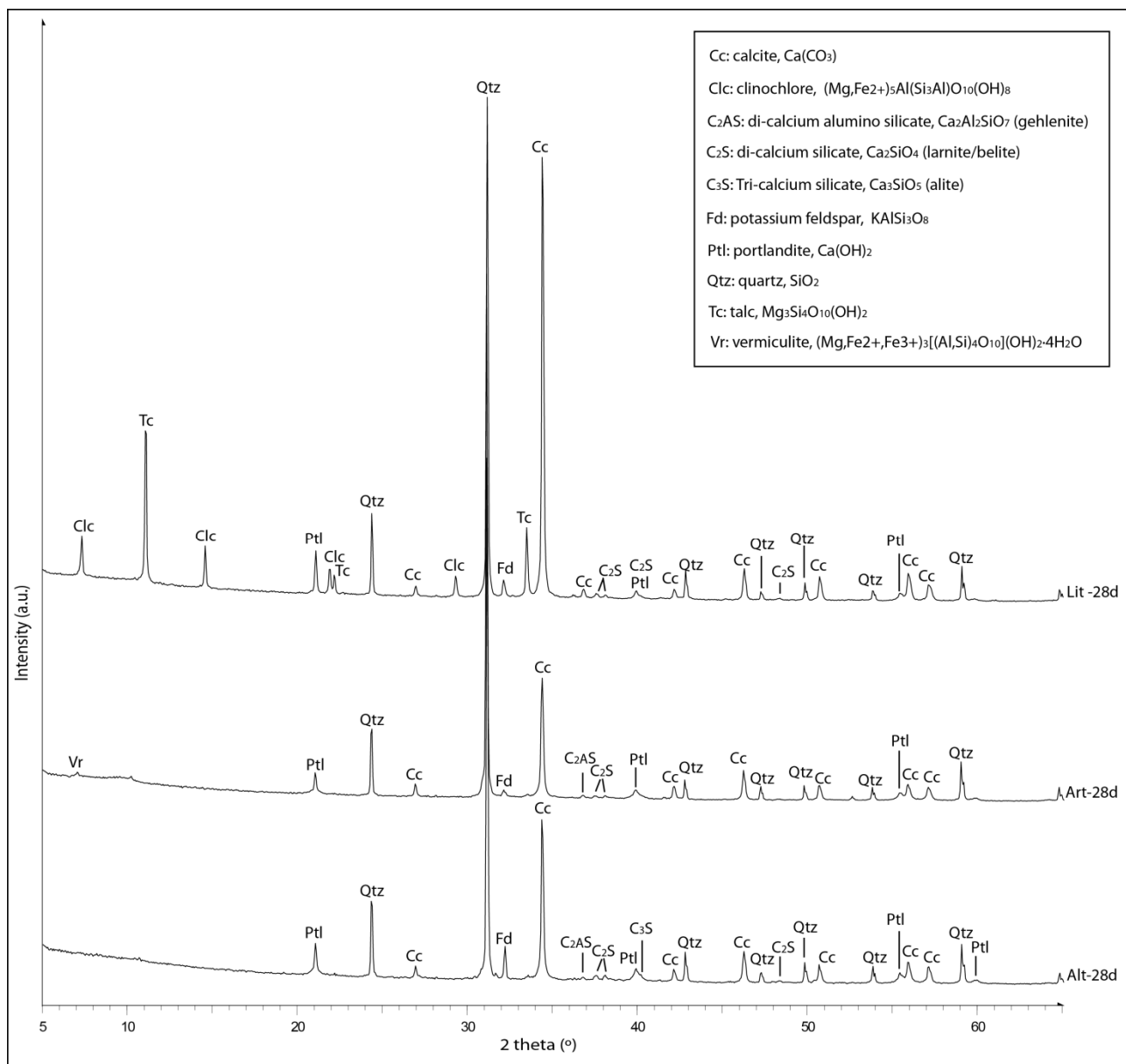


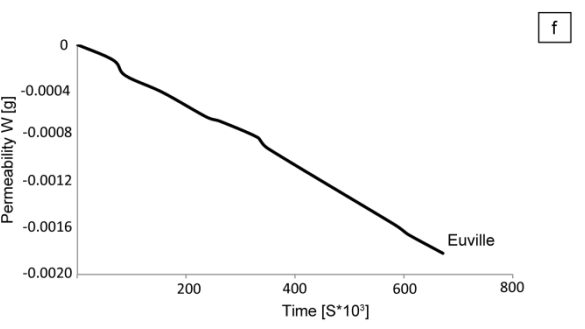
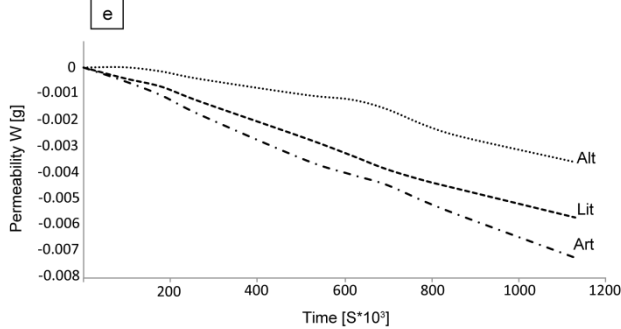
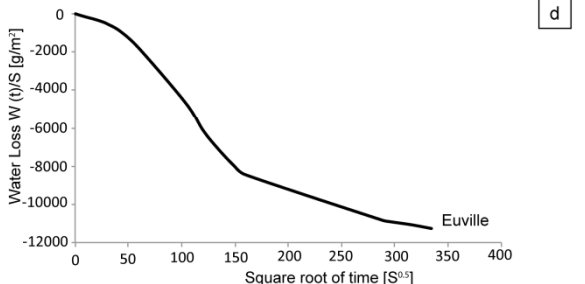
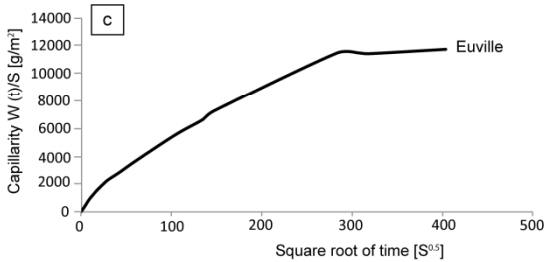
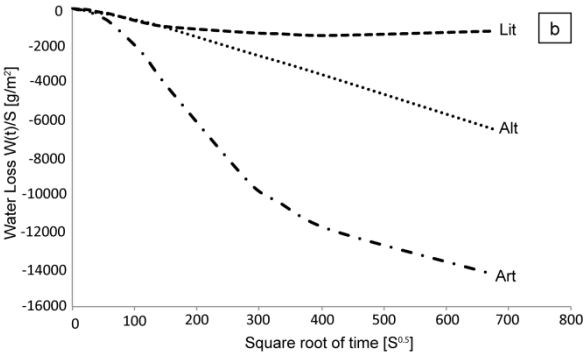
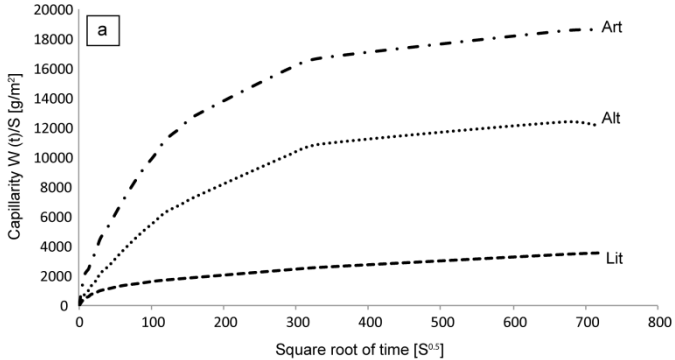
FIGURE 9



# FIGURE 10



# FIGURE 11



# FIGURE 12

