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## Role of petrography in durability of limestone used in construction of Persepolis complex subjected to artificial accelerated ageing tests

Mehdi Torabi-Kaveh, Mojtaba Heidari, Hassan Mohseni & Béatriz Ménendez

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### Abstract

Persepolis historical complex hosts palaces and tombs which are constructed by stone blocks. These stones suffer from various weathering. Hence, in this study, physico-mechanical properties of Persepolis stone are investigated in relation to some important weathering factors including freezing–thawing, thermal shock and salt crystallization. This study focused on role of the stone petrography on its durability against the weathering factors. Petrography studies showed that the stone is a nonporous-impermeable bioclastic-packstone which suffered significant diagenesis pressures and contain fractures filled by clay. Based on the obtained results, most of the observed deterioration for the stone is related to freezing–thawing cycles. The freezing–thawing cycles induced significant losses in the stone mechanical properties. Similar variations were recorded after the salt crystallization and thermal shock cycles, although the changes in the stone properties were not to the extent of freezing–thawing. Assessing values of decay constant ( $\lambda$ ) and half-time ( $N_{1/2}$ ) obtained for the stone in relation to the ageing test cycles showed that freeze–thaw and thermal shock have more deteriorative effects on the stone durability than salt crystallization. It is suggested that porosity is the main factor that controls the Persepolis stone durability. Low permeability of the stone inhibits water percolation throughout the specimens, so their deterioration against salt crystallization is negligible. But in case of the freeze–thaw cycles, water uptake by clay minerals, which filled diagenesis fractures in the limestone, could be considered as the main factor for the observed deterioration during freezing–thawing. Also, effect of micro-cracks, caused by the thermal shock cycles, is the best explanation for reducing the mechanical properties of the stone.

### Introduction

Stones are used as construction materials in various buildings and monuments. Hence, evaluation of stone durability is one of the most important subjects in relation to buildings and monuments. Durability of a stone is controlled by its inherent properties and its location. Depends on climatic conditions, various types of weathering factors are threats to monument stones. For example, freezing–thawing, salt crystallization, and thermal shock are considered as the most important factors in deterioration of monument stone (Cárdenes et al. 2014). Freezing the water in the pore spaces of stone leads to overcoming the stresses resulting from ice crystallization on tensile strength and cracking occurs (Fener and Ince 2015). Assessing durability of various rocks in relation to freeze–thaw has been the subject of study by many researchers (e.g.; Karaca et al. 2010; Bayram 2012; Martínez-Martínez et al. 2013; Cárdenes et al. 2014; Ghobadi and Torabi-Kaveh 2014; Fener and Ince 2015; Ghobadi and Babazadeh 2015; Eslami et al. 2018; Benavente et al. 2018; Hashemi et al. 2018; Noor-E-Khuda et al. 2017; Wang et al. 2018). The second deteriorative factor is crystallization of soluble salts inside pore spaces of building and monument stones (Cardell et al. 2003). Several sources can be considered as factors of salt accumulating in stones. For example, ground and surface water which can penetrate into a stone via capillary uptake, absorbing atmospheric moisture, formation of salts in result of interaction of aerosol pollutants with certain minerals (e.g., gypsum) (Marzal and Scherer 2008; Halsey et al. 1995), and salts with internal origin (McKinley et al. 2001). Crystallization and hydration pressures along with hygroscopic water retention are consequences of soluble salt penetration which can deteriorate a stone (Winkler, 1987; Fookes et al. 1988). Salt crystallization destructive effects on building and monument stones have been studied by various

researchers (e.g., Halsey et al. 1995; Cardell et al. 2003; Yavuz and Topal 2007; Zedef et al. 2007; Ludovico-Marques and Chastre 2012; Cárdenes et al. 2014; Modestou et al. 2015; Benavente et al. 2018; Germinario et al. 2017; Jamshidi et al. 2017; Lopez-Arce et al. 2016; Yavuz et al. 2015; Zalooli et al. 2018).

Heating and cooling weathering is considered as another major factor controlling degradation of building materials. Rapid temperature changes throughout the day lead to the creation of thermal shock cycles in rocks (Yavuz 2011). Even if the occurrence of the temperature changes be low, the repeated heating and cooling of the stone can be lead to its deterioration over. Stone characteristics such as grain size, grain shape, grain-to-grain misorientation, thermal expansion, and texture are the main factors determinative rate of thermal degradation (Weiss et al. 2003). Effect of thermal shock on physical and mechanical properties of various types of rocks were studied by many researchers (e.g., Sousa et al. 2005; Yavuz et al. 2006; Takarli et al. 2008; Yavuz 2011; Demirdag 2013; Ugur et al. 2014; Ghobadi and Babazadeh 2015; Lezzerini et al. 2017; Pápay and Török 2018; Wang et al. 2017).

Most of Iran's stony historic monuments including Persepolis were built using limestone. Despite its durability, limestone is susceptible to the deteriorative weathering factors and in some cases it suffers serious damage (Marzal and Scherer 2008). Hence, assessing the parameters controlling limestone weathering is critical. In this regard some researchers studied the behavior of limestone in relation to freeze–thaw, salt crystallization and thermal shock processes (Ghobadi and Torabi-Kaveh 2014; Ugur et al. 2014; Eren and Bahali 2005; Cardell et al. 2008; Walbert et al. 2015; Vázquez et al. 2016; Menéndez and Petráňová 2016; Heidari et al. 2017b). Persepolis is one of the most important monuments in Iran in global scale. Therefore, study of deterioration mechanism of Persepolis stone due to the common weathering factors regarding its petrography is an attractive issue for researchers. Although in some studies various aspects of Persepolis stone have been considered by different researchers. For example, Taghipour et al. (2016) studied durability of limestones used in Persepolis complex against acid solutions, Gallelo et al. (2016) applied non-destructive analytical methods to study the conservation state of Apadana Hall of Persepolis and Heidari et al. (2017a) used fuzzy inference system to determine weathering degree of the Persepolis stone. Hence, the present study will investigate the effects of some common weathering factors including freezing–thawing, thermal shock and salt crystallization on durability and strength of Persepolis stone with emphasis on role of petrography parameters.

#### General information

Persepolis was the ceremonial capital of the Achaemenid Empire (550–330 BC) that in contemporary Persian language is known as Takht-e Jamshid and Parseh, while ancient Persians called it Parsa, meaning the city of Persians. Persepolis is situated 60 km northeast of Shiraz (in the vicinity of the Marvdasht city) in the Fars Province, Iran (Fig. 1). UNESCO (Center 1979) has declared this complex as a World Heritage Site.

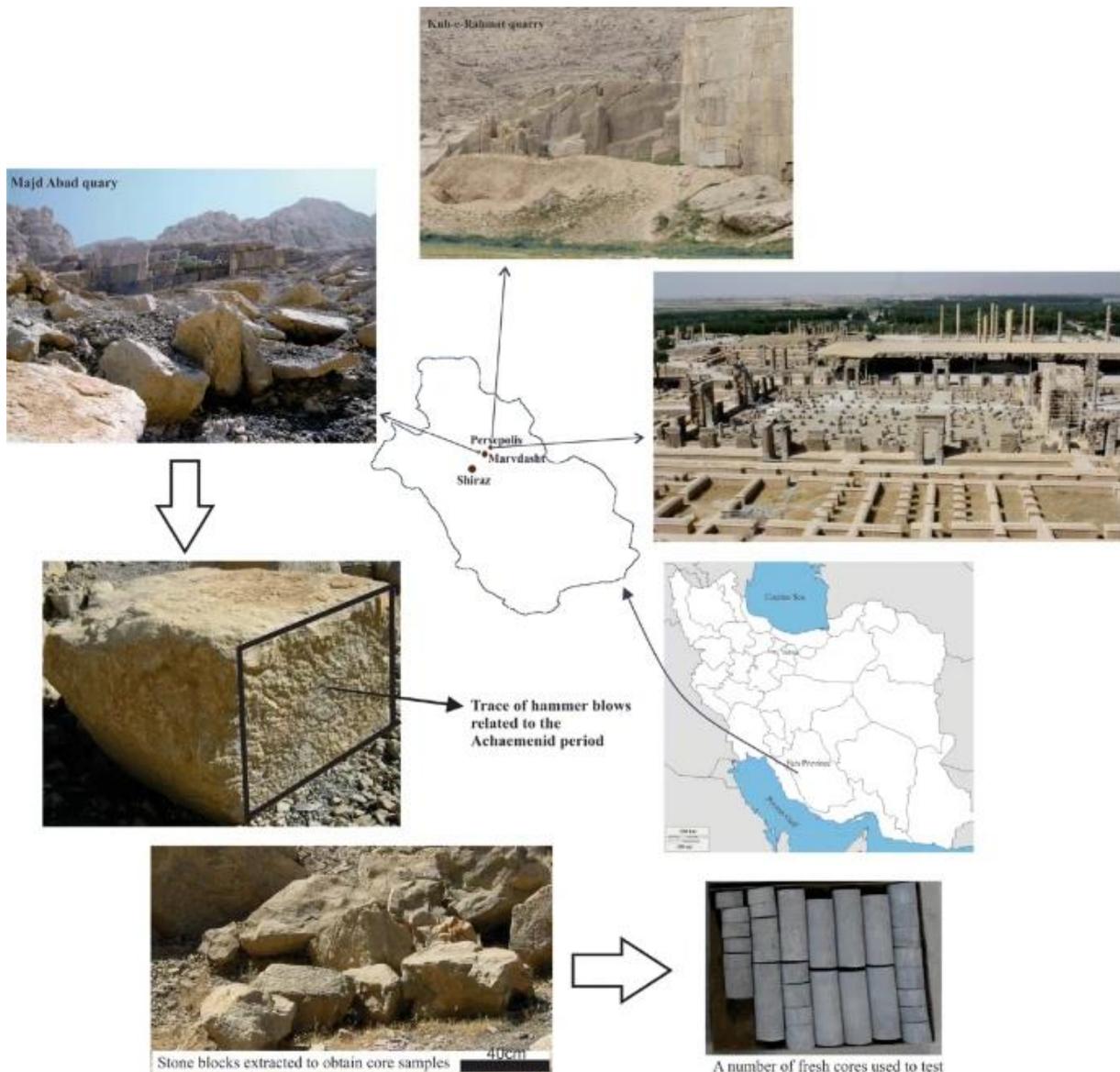


figure1 Remnants of the glorious capital of Persia, Persepolis historical complex (Marvdasht, Fars Province) (photo after <http://www.wondermondo.com>); and a view of the Majd Abad and Kuh-e Rahmat quarries as the main and minor quarries supplying stone to Persepolis construction (existence of hammer blow traces is a reason to introduce Majd Abad as the main quarry)

The Marvdasht city is located 50 km north of Shiraz at 1620 m above sea level. Weather is cold in the city's hilly areas, where Persepolis complex was constructed at there, and moderate climate is dominant in other regions. Marvdasht region has a typical continental climate which is characterized by cold-snowy winters and hot-dry summers. During winter, many days with temperature below  $-4^{\circ}\text{C}$  have been recorded in the region (see Table 1). It shows that freeze-thaw cycles could be expected especially between December and February (Table 1). Also, thermal weathering is expected according to weather data from the region, where daily variation of temperature (temperature differences between day and night) is about  $25.5^{\circ}\text{C}$  (Table 1). It should be said that high relative humidity especially during wet seasons and high evaporation rate in the region suggest occurrence of salt crystallization cycles (see Table 1).

Table 1 Meteorological data of Marvdasht for the period 1998–2017

Months	Jan.	Feb.	Mar.	Apr.	May.	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Annual
No. of days with temperature below $-4^{\circ}\text{C}$	13.65	13.25	1	0	0	0	0	0	0	0	0	3.15	31.00
Daily variation of TEMP $^{\circ}\text{C}$	–	–	–	–	–	–	–	–	–	–	–	–	25.48 <sup>a</sup>
Relative humidity (RH %)	84.55	83.4	78.55	77.15	66.75	49.15	44.55	44.9	53.95	62.7	72.55	83.45	66.80
Evaporation (mm)	18.89	19.18	83.325	134.13	201.71	294.00	341.83	339.03	268.72	178.60	104.23	39.15	168.57
Raining (mm)	65.05	55.63	37.86	44.95	8.38	0.35	0.56	0.66	0.03	0.61	21.99	53.85	24.16

<sup>a</sup>The value was reported by Shekofteh et al. (2018) for Pasargadae site which is located near the Persepolis site

Field observations reveal a wide range of weathering forms such as independent fissures on the stone structure (individual fissures or systems of fissures independent of structural features such as bedding, foliation, banding, etc., Fig. 2a), multiple flakes to multiple scales (transitional form between flaking and contour scaling, Fig. 2b) and break out (Fig. 2c). Probably freeze–thaw and thermal effect processes (Fig. 2a, b) are the main factors in weathering of Persepolis stone. Also, efflorescences are observable on the stones, particularly at the foot of walls and columns where soluble salts in air humidity or ground water (raised from foundations) formed salt crystals near the stone surface (Fig. 2d). Recently, Heidari et al. (2017a) used three quantitative damage indices, which include two indices proposed by Fitzner et al. (2002) (Linear Damage Index, D<sub>lin</sub> and the Progressive Damage Index, D<sub>prog</sub>) and a new index (Cubic Root Damage Index, D<sub>cube-root</sub>), to predict the weathering degrees of the bas-relief of Persian royal guards situated at the entrance of the Throne Hall in Persepolis. They reported slightly weathered degree for the Persepolis stone according to values of D<sub>lin</sub> and D<sub>prog</sub> which were calculated equal to 1.61 and 2.00, respectively, although they believe that D<sub>cube-root</sub> with value of 2.41 is more reliable for description of Persepolis stone weathering which is described as slightly to moderately weathered.

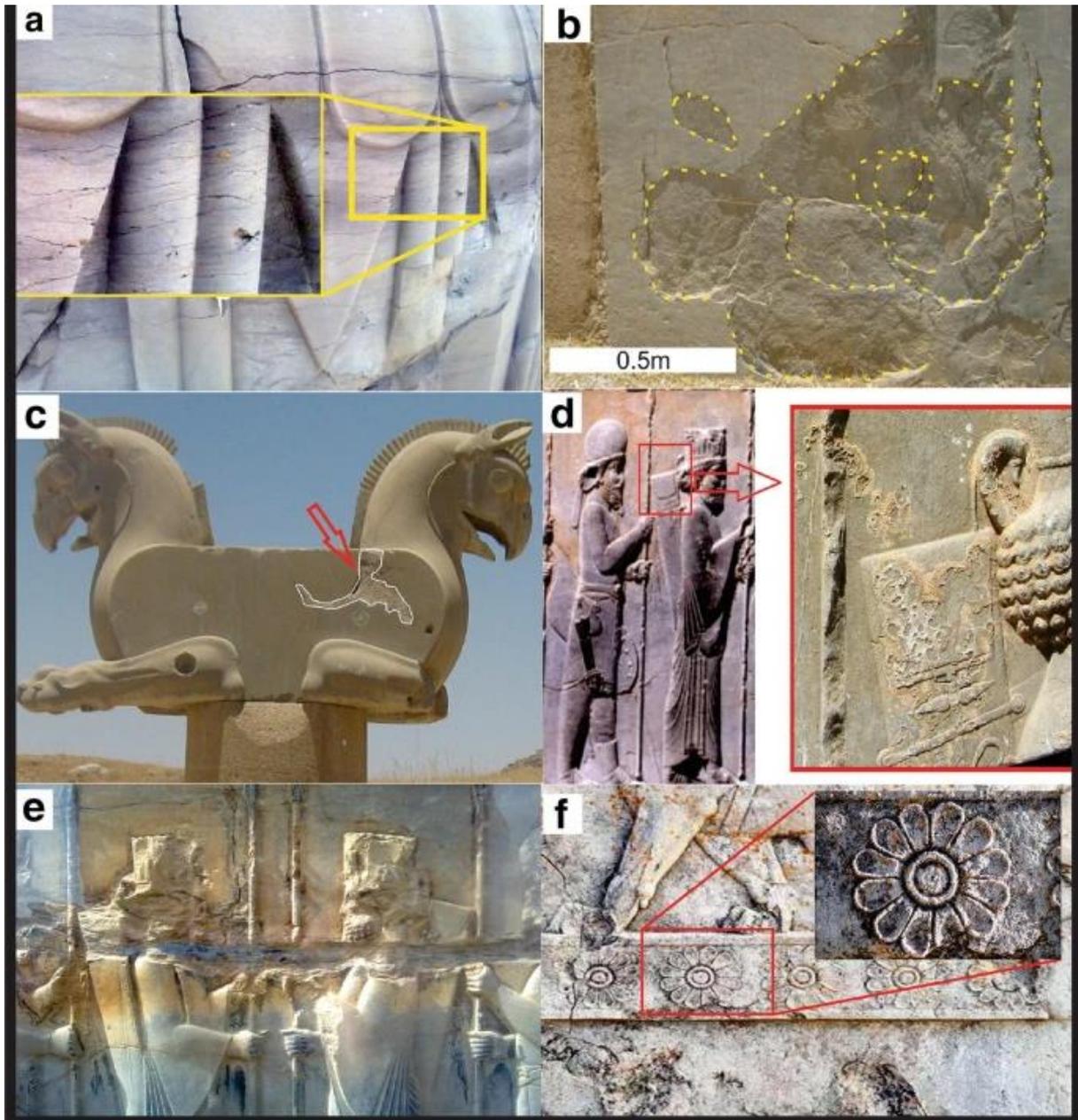


figure2 a Formation of independent fissures on the stone structure; b scaling of Persepolis stone in form of multiple; c break out of a part of Achaemenid griffin due to probably natural weathering; d traces of salt crystallization on a wall in Persepolis complex; e pollutant effects on the Persepolis stone, and f growing lichens on the Persepolis stone

In recent years, various factories were developed near the Marvdasht city such as Shiraz Petrochemical Complex and small units for the production of PVC pipes which considerably created concerns about the future of Persepolis complex. In this regard, it should be said that a significant increase in the weathering rate of the surface of the Persepolis stone has been observed in recent decades due to high increase in air pollution. The contaminating particles cause dirt and stain on the stone surfaces, and since particles containing metal oxides have a catalyzer role and form a hard shell consists of soot and dust, which is the first step in the degradation and gradual destruction of the stone (Fig. 2e). By analyzing the acidity values of rain in different seasons, Ghanbari et al. (2010) reported that the pollutants generated from various industries of the region, as well as pollutants

from the city, including vehicles, have been transferred by the winds of the region to the Persepolis location, and after dissolving within the rain water decompose the monument stones. Based on their report, the pollutant sources of Marvdasht are located in the southeast of Persepolis, and the winds of the region blow from east to west. As a result of this issue, obvious changes in the acidity of the rain were observed by the authors. In case of role of pollutants in deterioration of the Persepolis monuments, a comprehensive study was carried out by Sadeghiyeh et al. (2015). The results showed that the rate of corrosion from the surface of the Persepolis stone due to pollution is 29 g per square meter for 1 year, which is a warning condition. Furthermore, the irregular growth of lichens with different species on surface of the Persepolis stone is another serious concern (Fig. 2f). The main causes of this subject are atmospheric pollutants and high humidity (average relative humidity of 66.8%) in the area. In this regard, Mohammadi and Krumbein (2008) did a comprehensive research study on biodeterioration of ancient stone materials from the Persepolis monuments in.

It is believed that two major quarry were used to supply stone for Persepolis construction. In 25 km south of Persepolis there is a quarry entitled Majd Abad consisting of a black limestone which was used as major site for exploiting the Persepolis complex stones (Fig. 1). The black limestone belongs to the Ilam Formation (Santonian–Campanian, late Cretaceous) (Darvishzadeh 2009). Another quarry is Kuh-e Rahmat quarry, at the proximity of the Persepolis site, consisting of a grey limestone with Aptian age (early Cretaceous) (Darvishzadeh 2009). The existence of a large number of semi-finished and abandoned blocks that have traces of hammer blows (Fig. 1) is one of the most important reasons for introducing this quarry as the main source of Persepolis stones. Considering that most parts of the Persepolis complex were built from materials derived the first quarry, the last type was excluded in our experiments. After coordination with the Cultural Heritage Organization of Fars Province, during a comprehensive fieldwork some blocks with approximate dimensions of  $30 \times 30 \times 40$  cm were collected. A large number of specimens (cylindrical shape) were obtained by drilling the obtained blocks and the samples were prepared to do the accelerated ageing tests.

#### Experimental procedures

As the aim of this study is assessment of physico-mechanical changes of the Persepolis stone in relation to the artificial accelerated ageing factors, the specimens were tested in two different states. In the first state, sound and fresh specimens were used to examine some properties such as porosity ( $n$ ), P wave velocity ( $V_p$ ), Brazilian tensile strength (BTS), point load strength index ( $I_s$ ), and uniaxial compressive strength (UCS). Then, those properties were measured for the specimens subjected to the artificial ageing tests. Standard methods used in measuring the properties are explained below.

#### Determination of mineralogical, physical and mechanical properties

To examine petrographical parameters of the stone, thin sections from fresh samples were studied by a polarizing microscope (Zeiss Axioskop 40). Also XRD by Philips PW 1140 diffractometer with a Huber Model 631 photographic chamber ( $\text{Cu } \alpha$  radiation) was used to identify minerals of the stone. Moreover, scanning electron microscope (SEM) (JEOL-JSM-840A model) and energy-dispersive spectrometry (EDS) were applied on the samples, coated by gold, with aim of characterizing type of clay minerals in the stone. Routine petrography studies were done also on thin sections from the specimens subjected to the artificial accelerated ageing tests. ASTM standard calcimetry test (D4373-14 2014) was performed to determine carbonate percentages of the samples. ISRM standard (Ulusay 2014) was applied to measure physical properties [porosity ( $n$ ) and weight loss]. Saturation technique was applied to measure porosity (effective porosity) of the specimens. So that after calculating the bulk volume ( $V$ ) of the specimen, it was submerged in water for a period of 48 h, and subsequently, the specimen was removed and a moist cloth was applied to dry its surface. Then its

saturated-surface-dry mass ( $M_{sat}$ ) was determined. In the next stage, measuring grain mass ( $M_s$ ) of the specimen was done after drying that at a temperature of 105 °C and cooling for 30 min in a desiccator. Pore volume ( $V_v$ ) was calculated by dividing the value of  $M_{sat}$  minus  $M_s$  to water density ( $\gamma_w$ ). Finally effective porosity ( $n_e$ ) was defined as ratio of  $V$  to  $V_v$ . Dried and saturated densities were also measured by dividing  $M_s$  and  $M_{sat}$  values to  $V$ , respectively. Also, an E48 Pulse Generator Unit, made by controls and two transducers (a transmitter and a receiver) with a frequency of 54 kHz was applied to measure sound velocity of the specimens. The average values for three times repeating each test on a cylindrical specimen were reported as the P wave velocity. It should be noted that a comprehensive particle analysis was done on the thin sections to evaluate number and average size of particles. ImageJ plugin was applied to automatic determination of particle size distributions.

Strength parameters of the stone specimens in the both states were investigated by three common mechanical parameters including point load strength index ( $I_{s50}$ ), Brazilian tensile strength (BTS) and uniaxial compressive strength (UCS). The parameters were measured by the tests carried out based on ISRM standards (Franklin 1985; Ulusay 2014).

In order to perform the above tests, cylindrical samples were used to determine physical and mechanical properties including five cylindrical samples (with a length to diameter ratio of 2.5–3) for the physical (porosity and P wave velocity) tests and uniaxial compressive strength test, five disk samples (with a thickness to diameter ratio of 0.3–1) for the point load test and five disk samples (with a thickness ratio of 0.5–0.75) for the Brazilian tensile strength test. It should be noted that five samples were used for every ten cycles. It means that 25 samples were used for the cycles of 0, 10, 20, 30 and 40 in total. Since the tests are mostly destructive, it was not possible to assess the changes caused by the ageing tests on a single sample up to 40 cycles.

#### Freeze–thaw test

Freezing–thawing cycles were done according to ASTM standard (D5312 M-12 2013). The specimens after submerging in a container filled with water were frozen under freezing temperature of – 18 °C for 18 h inside a freezer. After that, a water bath at 32 °C was used to thaw the frozen specimens for 6 h. Totally 40 cycles of freezing–thawing were done and the physical and mechanical properties of the specimens were investigated at the end of every ten cycles.

#### Salt crystallization test

Forty cycles of immersion/drying of salt crystallization test were carried out according to the BS EN standard (British Standards Institution 1999). In each cycle the specimens were submerged in a solution of sodium sulfate or magnesium sulfate (14 w %) for 2 h at 20 °C, and dried at 105 °C for 20 h in the oven. Finally, the specimens were cooled at 20 °C for 2 h before the next immersion. The physical and mechanical properties of the specimens were investigated at the end of every 10 cycles.

#### Thermal shock test

Thermal shock tests consist of 40 cycles of heating and cooling were done on the stone specimens according to the standard of BS EN (EN, UNI 2013). Each cycle consists of a stage heating the specimen within an oven (18 h) at 105 °C and cooling the specimens with submerging in water for 6 h. The physical and mechanical properties of the specimens were investigated at the end of every 10 cycles.

#### Results and discussion

## Petrography of the stone

According to Dunham classification (1962), the Persepolis stone is a bioclastic-packstone (Fig. 3a). Subordinate microfossil fragments such as pelagic foraminifera, calcispher, and sponge spicule scattered throughout the stone (Fig. 3a). Content of the fragments is 40–45%. Also, autogenic pyrite crystals are visible in the thin sections (Fig. 3a). For distinction of pore space from pyrite under the microscope, both PPL and XPL photos were studied. It revealed that the dark spots are pyrites which show mostly crystal forms. The stone is almost nonporous and impermeable due to its texture which is homogenous. Analyzing by ImageJ plugin on a thin section image from the stone characterized that the average size of the fragments is about 6  $\mu\text{m}$ , where 3793 fragments were counted (Fig. 4).

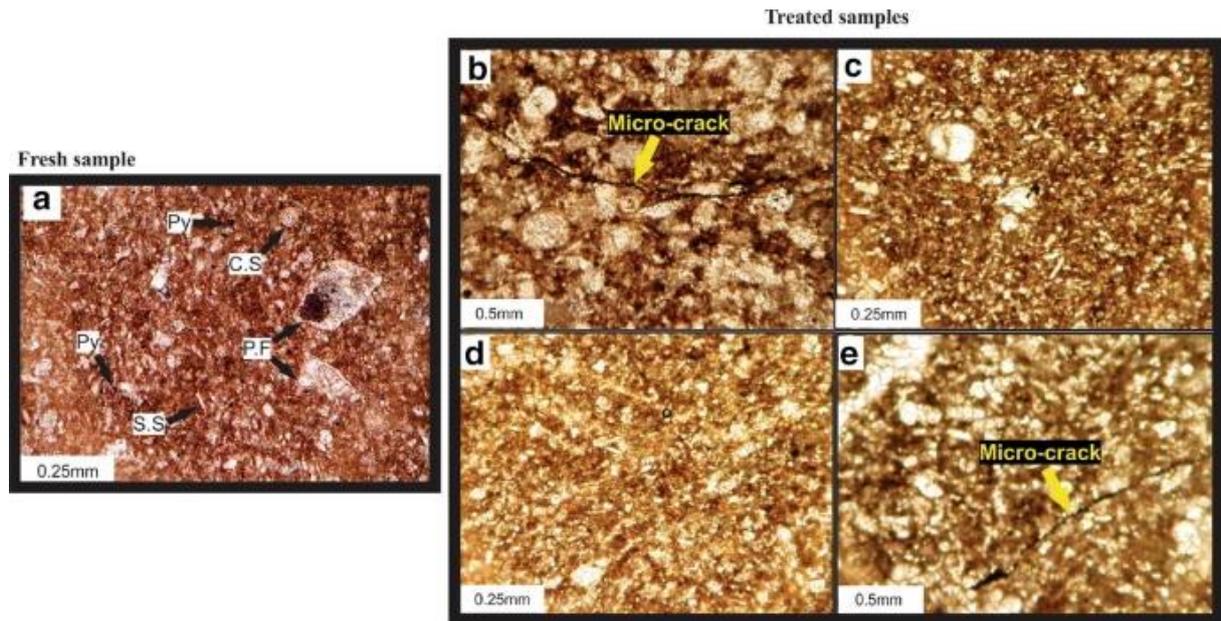


figure3 Photomicrograph of a pyrite (Py) particles and microfossil fragments such as pelagic foraminifera (P.F), calcispher (C.S), and sponge spicule (S.S) scattered throughout the stone; b development of micro-cracks in the stone after 40 cycles of freeze–thaw; c the stone after sodium sulfate salt crystallization test without any visible change; d the stone after magnesium sulfate salt crystallization test without any visible change; and e development of micro-cracks in the stone after 40 cycles of thermal shock

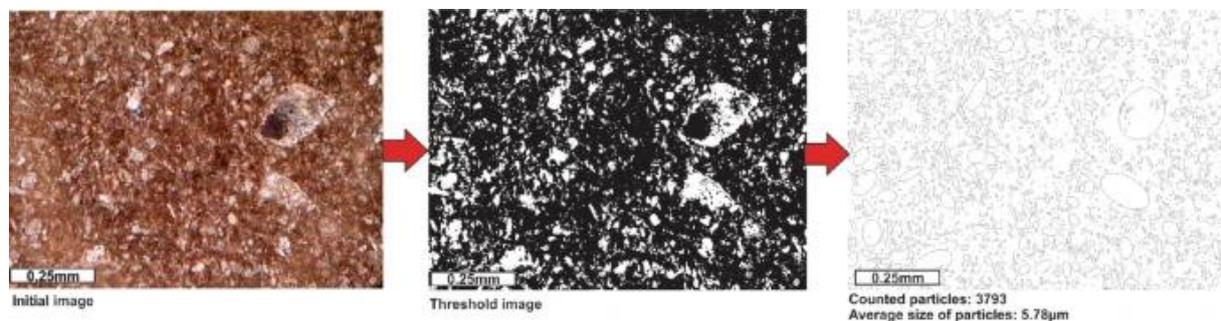
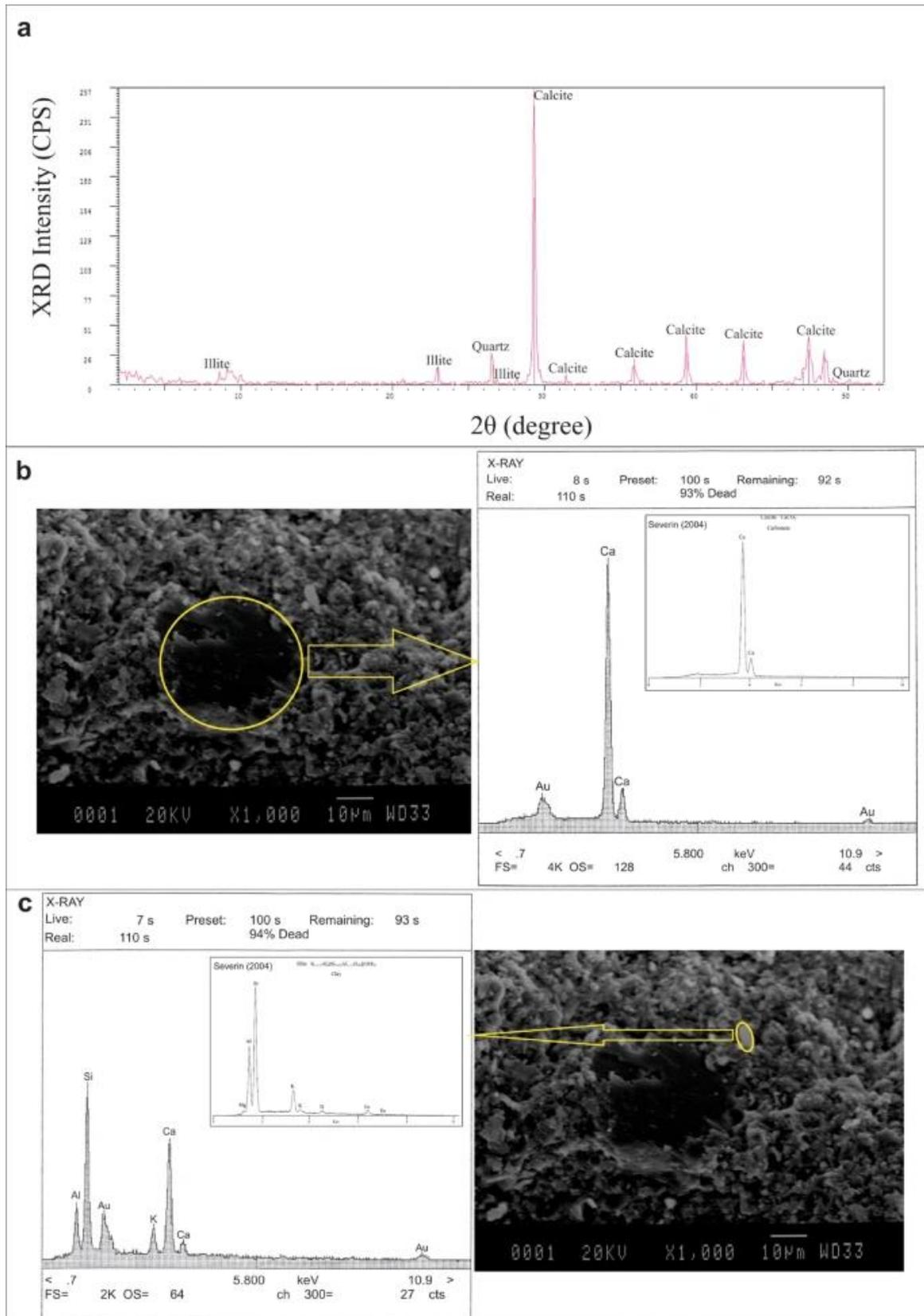


figure4 Particle analyzing on a thin section image from the Persepolis stone

The XRD results show that calcite and clay minerals are main constituents of the limestone, where quartz is also observed as minor constituent (Fig. 5a). The calcimetry also confirmed an average of 80% calcite content in the stone. SEM analyses on the specimens revealed that calcite is the major mineral of the specimens (Fig. 5b), although some clay minerals are visible (Fig. 5c). Furthermore, energy-dispersive X-ray spectroscopy (EDX) performed on the specimens confirmed that the bright spots in the SEM images (Fig. 5c) are illite as they contain Al, Si and K. Also, the observed EDX spectrum is in accordance with the standard EDX spectrum reported by Severin (2004) (Fig. 5c). It should be noted that calcium contents in the EDX spectrum are too high. It may be related to that the sample is unpolished, the analyzed grain is too small in relation to the electron beam size and collected data of characteristic X-ray are partly from the surrounding grains of calcite.



\*after Heidari et al. (2016)

figure5a X-ray diffraction pattern for a sample of Persepolis stone; b dark parts represent calcite; c bright spots represent clay mineral composition. Both are SEM image

## Physical and mechanical properties of the limestone

Table 2 presents the results of physical and mechanical measurements on the specimens in fresh state (before any treatment). As can be seen from the table, the limestone has relatively high density. It is because of lack of significant pore space inside the rock, where average porosity is less than 0.12% for the specimens. Also, the stone has low water absorption (less than 0.38%, Table 2) which suggests high durability against water penetration. High average value of the measured P wave velocity for the specimens is another reason to confirm the obtained density. High density and low porosity affected mechanical properties the limestone. So that, all the three mechanical parameters (UCS, BTS and Is50) have high average values for the limestone (Table 2). In case of UCS, the average value is relatively high (115.6 MPa) which is probably due to existence of high content of quartz in the specimens.

Table 2 Physical and mechanical properties of the stone in fresh state (before any treatment)

Physical properties	Dry density (g/cm <sup>3</sup> )		Saturated density (g/cm <sup>3</sup> )		Water absorption (%)		Effective porosity (%)		P wave velocity (m/s)	
	Ave	STDEV	Ave	STDEV	Ave	STDEV	Ave	STDEV	Ave	STDEV
Value	2.63	0.02	2.64	0.02	0.38	0.09	0.12	0.01	5957	292.7
Mechanical Properties	Uniaxial compressive strength (MPa)			Brazilian tensile strength (MPa)			Point load strength index (MPa)			
	Ave	STDEV		Ave	STDEV		Ave	STDEV		
Value	115.6	4.62		11.2	1.60		4.45	0.60		

## Effects of the weathering factors on apparent shape of the specimens

In general, the weathering effects of freeze–thaw process on the specimens enhanced with increasing cycles of freeze–thaw (Fig. 6a). This is probably due to the formation of new micro-fractures, as the specimens lose their original texture due to freeze–thaw. Although water penetrating through fractures accelerates the weathering of the specimens, multiple fissure networks formed when fissures expand and penetrate deeper into the stone. Due to the existence of clay, it can be concluded that the stone suffered high diagenesis pressure (Bausch 1968), which created veins and fractures. These veins and fractures were secondary filled with clay. This subject controls the development of the fissures (cycles of 30 and 40 in Fig. 6a), where the fissures predominantly developed along the pre-existing fractures of the samples rich in clay minerals (Fig. 7). Regarding the shape and pattern of the fracture propagation in relation to the upper and lower of layering (top and down the core) (Fig. 6a), these weakness surfaces do not relate to sedimentary environments and therefore they are interpreted as a diagenetic structure rather than a sedimentary structure. The formation of these fractures can occur in the late stages of diagenesis (late diagenesis) and during uplifting the sedimentary rocks. It should be noted that although anisotropy could affect deterioration process of a stone, there is no meaningful relationship between degree of deterioration and degree of anisotropy (Fort et al. 2008). Fort et al. (2008) studied effect of anisotropy on the durability of some dolostones from Madrid region (Spain) exposed to salt crystallization process. They reported that anisotropy does not necessarily govern the deterioration process induced by salt crystallization ageing.

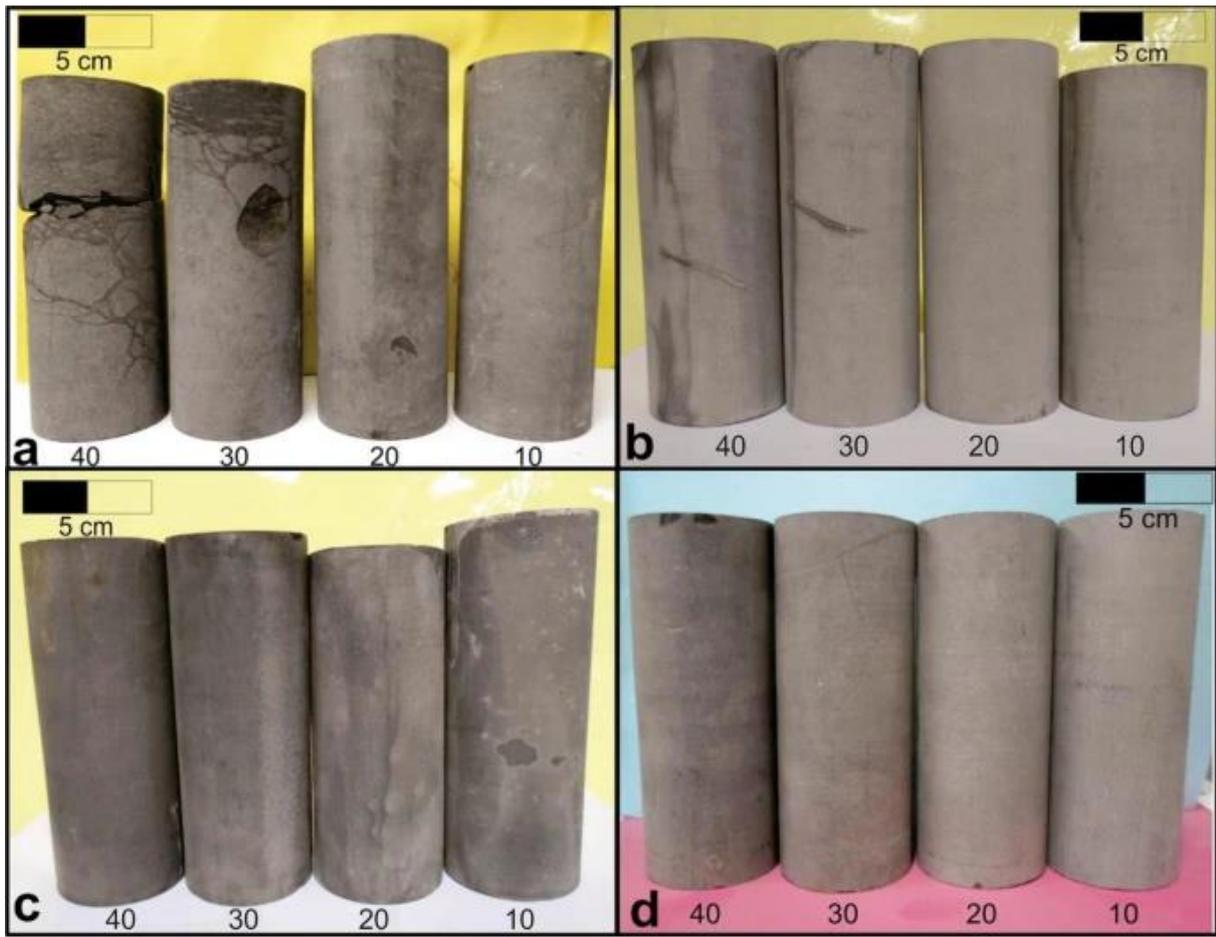


figure6 Visual changes of degradation patterns during a freeze–thaw, b sodium sulfate salt crystallization and c magnesium sulfate salt crystallization and d thermal shock ageing tests

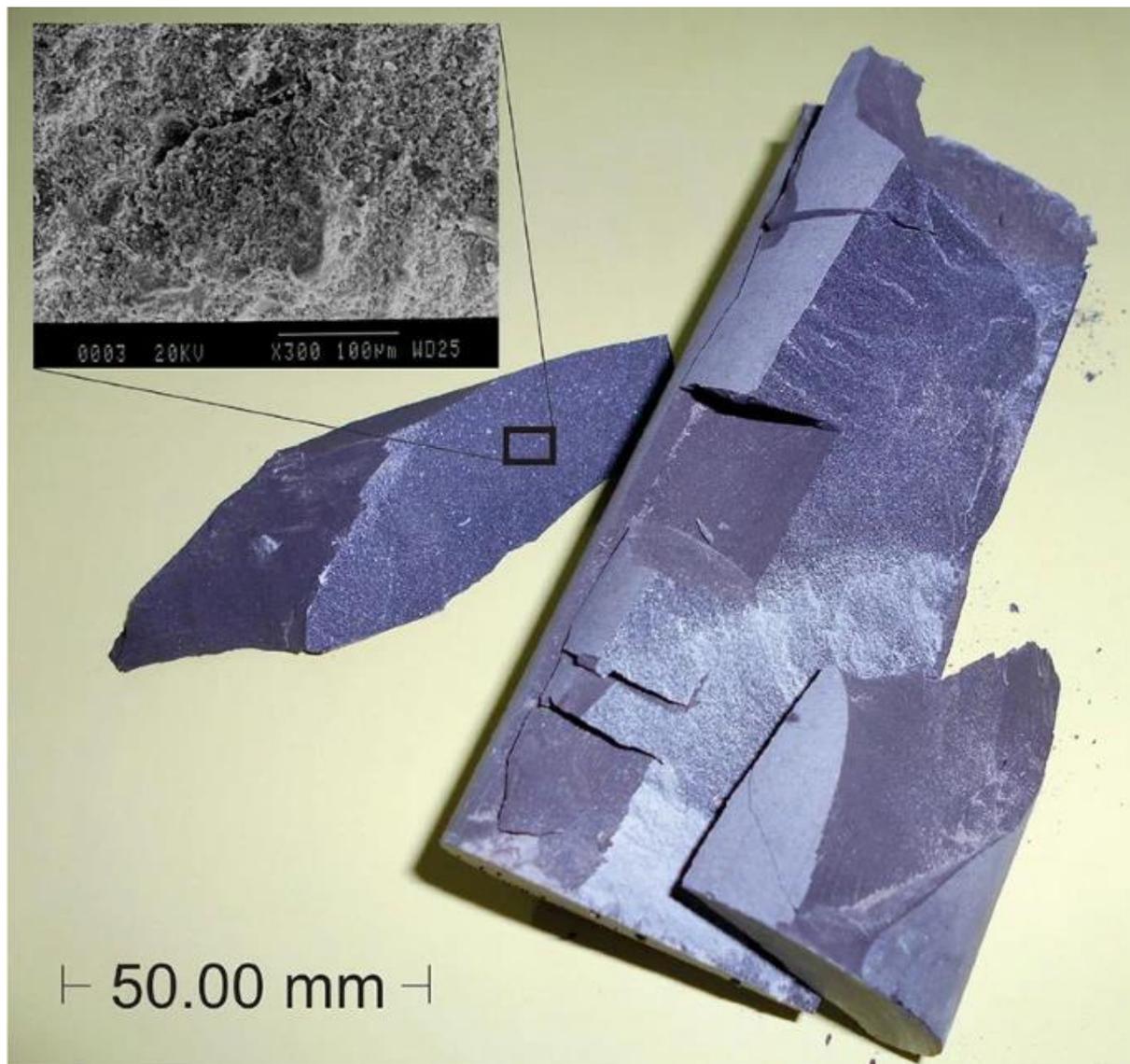


figure7 Breaking the Persepolis stone specimen (treated by freezing–thawing cycles) along the pre-existing fractures filled by clay minerals during uniaxial compressive strength test

Observations showed that the salt crystallization ageing tests have no significant effect on apparent shape of the specimens (Fig. 6b, c). It should be mentioned that some cracks in the specimens were filled by crystallized salts, notably when sodium sulfate solution was applied (Fig. 6b).

Significant visual changes in the specimens were not observed during 40 cycles of thermal shock test, as only slight cracking have been occurred after the cycle of 30 (Fig. 6d) and some parts of the specimen break out (see the cycle of 40 in Fig. 6d) due to the thermal shocking.

Due to the observation of efflorescence on surface of the Persepolis stone, two core specimens were subjected to solutions of sodium sulfate and magnesium sulfate. The specimen's shape changes were monitored every 7 days until 2 months. During drying and evaporation at the specimens, capillary rise leads to crystallization of face salts from solution and producing the white crust known as efflorescence (Fig. 8). The main result is that the sodium sulfate solution rose more than the magnesium sulfate due to capillary after 2 two months (Fig. 8). Higher water absorption capacity of

the sodium sulfate solution in comparison to the magnesium sulfate is a reason for that. Also, it should be noted that the durability of Persepolis stone face to both the salt solutions is high as the specimens exposed to the salt solutions were completely sound after 60 days.

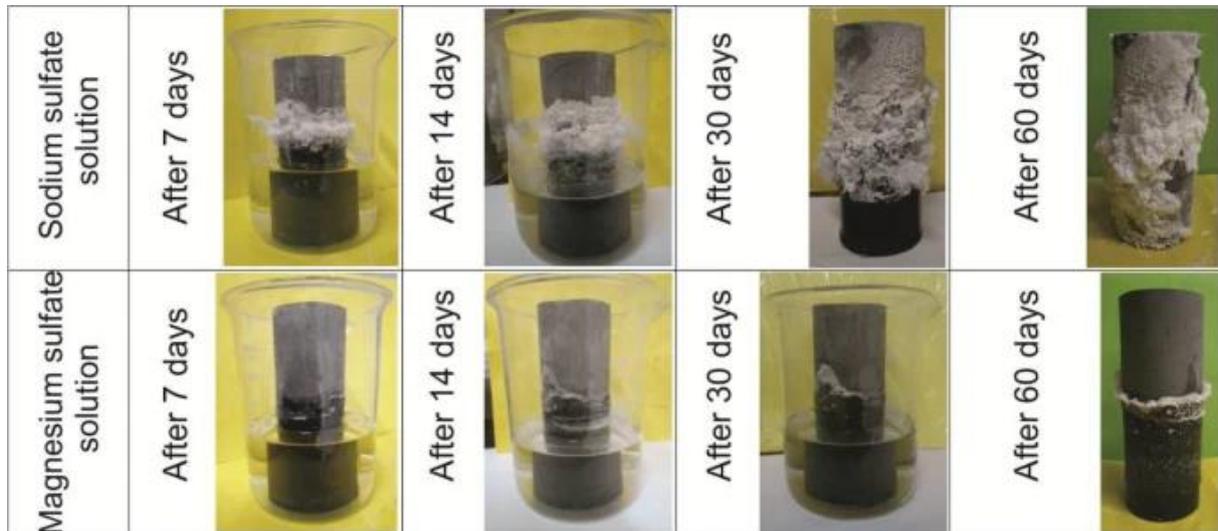


figure8 Photographs were taken from Persepolis stone specimen exposed to the sodium sulfate and magnesium sulfate solutions after 7, 14, 30 and 60 days (diameter of the core specimens is 54 mm)

#### The stone petrography and changes of the specimen's texture due to the weathering factors

It has been observed that the freeze–thaw and the thermal shock tests have relatively significant effects on the stone, as visible micro-cracks were developed in the specimens with width of 2  $\mu\text{m}$  (Fig. 3b, e). While effects of the salt crystallization tests on the stone were negligible (Fig. 3c, d). It should be noted that the micro-crack path crossed through spaces between the fragments, mostly within the clay matrix in both the tests. Considering high purity of the Persepolis stone and difference in linear expansion coefficient value for calcite (in two different directions), the observed damages during thermal shock is expectable. Because calcite is the only mineral that expands due to increasing temperature in one direction, but it contracts in another direction when it cools down (Haynes 2014). Also, it is worth noting that relatively low mobility of salty water in compare to fresh water leads to low penetration of that into rock. In fact, when salt dissolves, positive and negative ions become surrounded by polar water molecules, effectively increasing their size, and producing quite high inter-particle, electric forces. This decreases the mobility of the ions and of the water molecules. Hence, it can be concluded that lack of observable changes in texture of the specimens after the salt crystallization tests is due to that subject.

#### Freezing–thawing cycles and physico-mechanical changes of the specimens

Table 2 shows the change in porosity of the specimens subjected to freeze–thaw cycles. Normalized porosity values of the specimens illustrate the porosity variations during the freeze–thaw tests (Fig. 9a). The normalized value is the ratio of the obtained value after testing to that at normal condition (not exposed to freeze–thaw). From cycle 0 to cycle 10 significant changes are observed in the normalized porosity values (Fig. 9a), where lesser variation is visible from cycle 10 to cycle 40. P wave velocities show descending trend with increase in numbers of freeze–thaw cycles ( $R^2 = 0.95$ ) (Fig. 9b), so the velocity stepped down to 4820 m/s, while it was recorded up to 5730 m/s in normal

condition (Table 3). Decrease of the  $V_p$  values is probably due to increase in porosity after freeze–thaw.

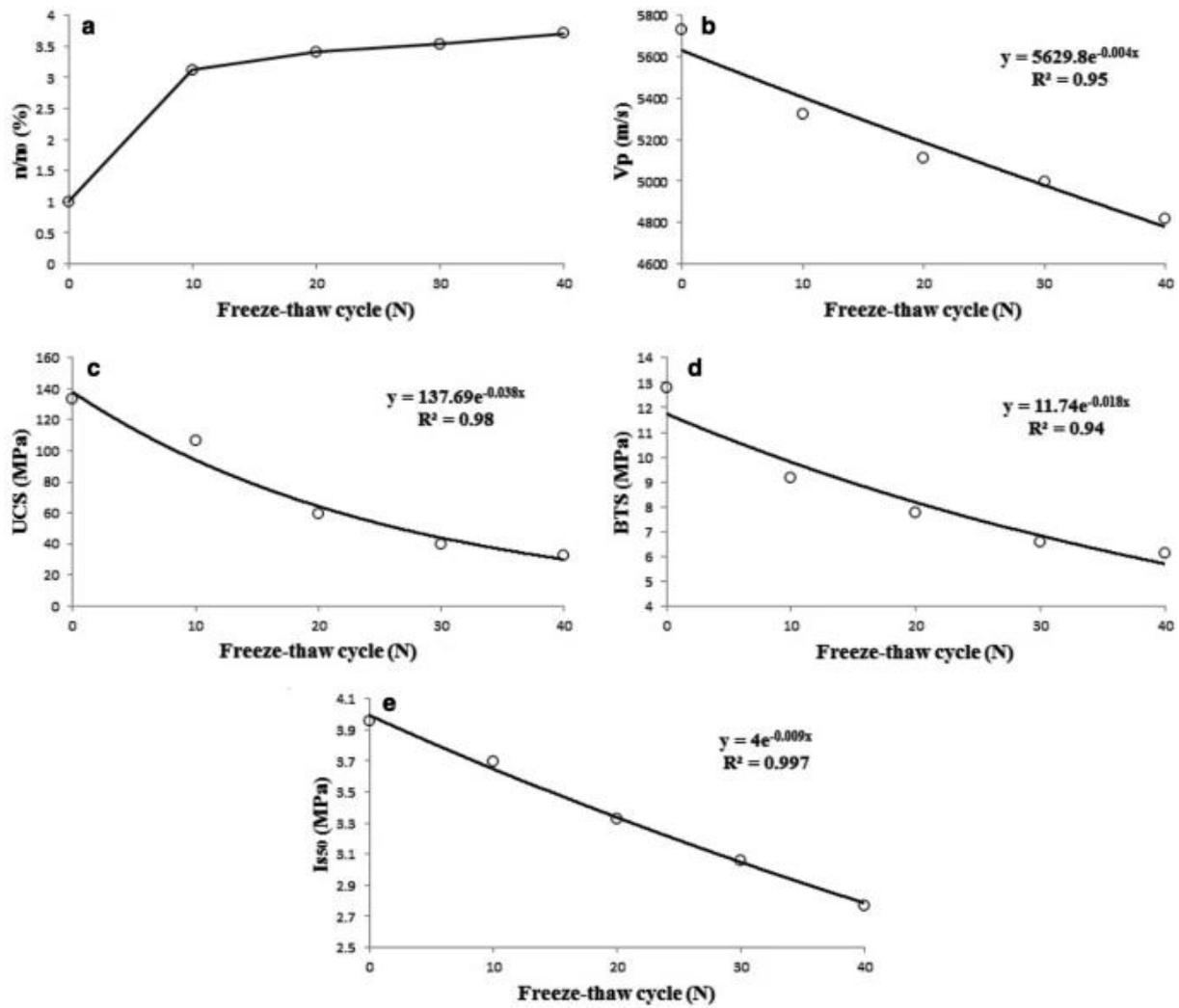


figure9 Changes of physical and mechanical properties of the specimens vs. the numbers of freeze–thaw cycles: a porosity ( $n$ ), b P wave velocity ( $V_p$ ), c uniaxial compressive strength (UCS), d Brazilian tensile strength (BTS), and e point load strength index ( $I_{s50}$ )

Table 3 Average values of physical and mechanical properties of the specimens before and after the freeze–thaw cycles

Physical–mechanical properties	Normal condition	After freeze–thaw			
	Cycle 0	Cycle 10	Cycle 20	Cycle 30	Cycle 40
$n/n_0$	1	3.12	3.41	3.54	3.71
$V_p$ (m/s)	5730	5324	5112	4995	4820
UCS (MPa)	133.5	106.72	59.47	40.16	32.56
BTS (MPa)	12.8	9.16	7.77	6.58	6.12
$I_{s50}$ (MPa)	3.96	3.69	3.33	3.06	2.77

Table 3 presents the measured mechanical parameters for the specimens. Evidently reduction in UCS values was observed with the progress of the freezing–thawing cycles. Significant loss (75.6%) was observed in the average strength from cycle 0 to cycle 40. An exponential relationship with a high determination coefficient ( $R^2 = 0.98$ ) exists between freeze–thaw cycles and UCS values (Fig. 9c). There are similar relationships between freeze–thaw cycles and  $I_{s50}$  and BTS values with  $R^2$  of 0.99 and 0.94, respectively (Fig. 9d, e). In the specimens, all the values of strengths decrease as the freeze–thaw cycles increase. The  $I_{s50}$  value decreased from 3.96 MPa for fresh samples to 2.77 MPa for weathered samples at the end of freezing–thawing cycles (about 30% decrease) (Table 3). Also, the average value of BTS at normal condition is about twice as large as that at cycle 40 (Table 3). These weaknesses of the strength parameters of the specimens could be explained by the developing micro-cracks and fractures. It should be noted that concentration of clay minerals along pre-existing fractures, have also significant role in the observed damages (Fig. 6a). The clay minerals may adsorb water during 40 cycles of freezing and thawing and promoted the development of fractures due to increase in swelling pressure within the specimens.

#### Salt crystallization cycles and physico-mechanical changes of the specimens

Two types of salts were used for the salt crystallization ageing experiments including sodium sulfate ( $\text{Na}_2\text{SO}_4, 10\text{H}_2\text{O}$ ) and magnesium sulfate ( $\text{MgSO}_4, 7\text{H}_2\text{O}$ ). The dry weight of the specimens was not significantly affected by both the sodium sulfate and magnesium sulfate solutions. The weight losses of the specimens after 10, 20, 30, and 40 cycles of the salt crystallization tests are shown in Tables 4 and 5. As could be seen from Figs. 10a and 11a, negligible weight losses were observed in both the sulfate crystallization tests.

Table 4 Average values of physical and mechanical properties of the specimens before and after the sodium sulfate salt crystallization cycles

Physical–mechanical properties	Normal condition	After sodium sulfate salt crystallization test			
	Cycle 0	Cycle 10	Cycle 20	Cycle 30	Cycle 40
Weight loss (%)	0	0.01	0.018	0.025	0.084
$n/n_0$	1	1	1.01	1.06	1.07
$V_p$ (m/s)	5985	5881.11	5732.52	5652.48	5578.41
UCS (MPa)	115.6	110.34	100.22	98.57	93.94
BTS (MPa)	9.15	9	8.47	8.21	7.53
$I_{s50}$ (MPa)	5.35	5.2	5.02	4.96	4.82

Table 5 Average values of physical and mechanical properties of the specimens before and after the magnesium sulfate salt crystallization cycles

Physical–mechanical properties	Normal condition	After magnesium sulfate salt crystallization test			
	Cycle 0	Cycle 10	Cycle 20	Cycle 30	Cycle 40
Weight loss (%)	0	0.023	0.046	0.012	0.028
$n/n_0$	1	1	1.02	1.05	1.05
$V_p$ (m/s)	5667	5575.27	5467.4	5298.58	5205.32
UCS (MPa)	111.3	107.16	103.53	102.26	97.59
BTS (MPa)	9.26	9.1	8.7	8.4	8.36
$I_{s50}$ (MPa)	4.45	4.33	4.1	4.04	3.98

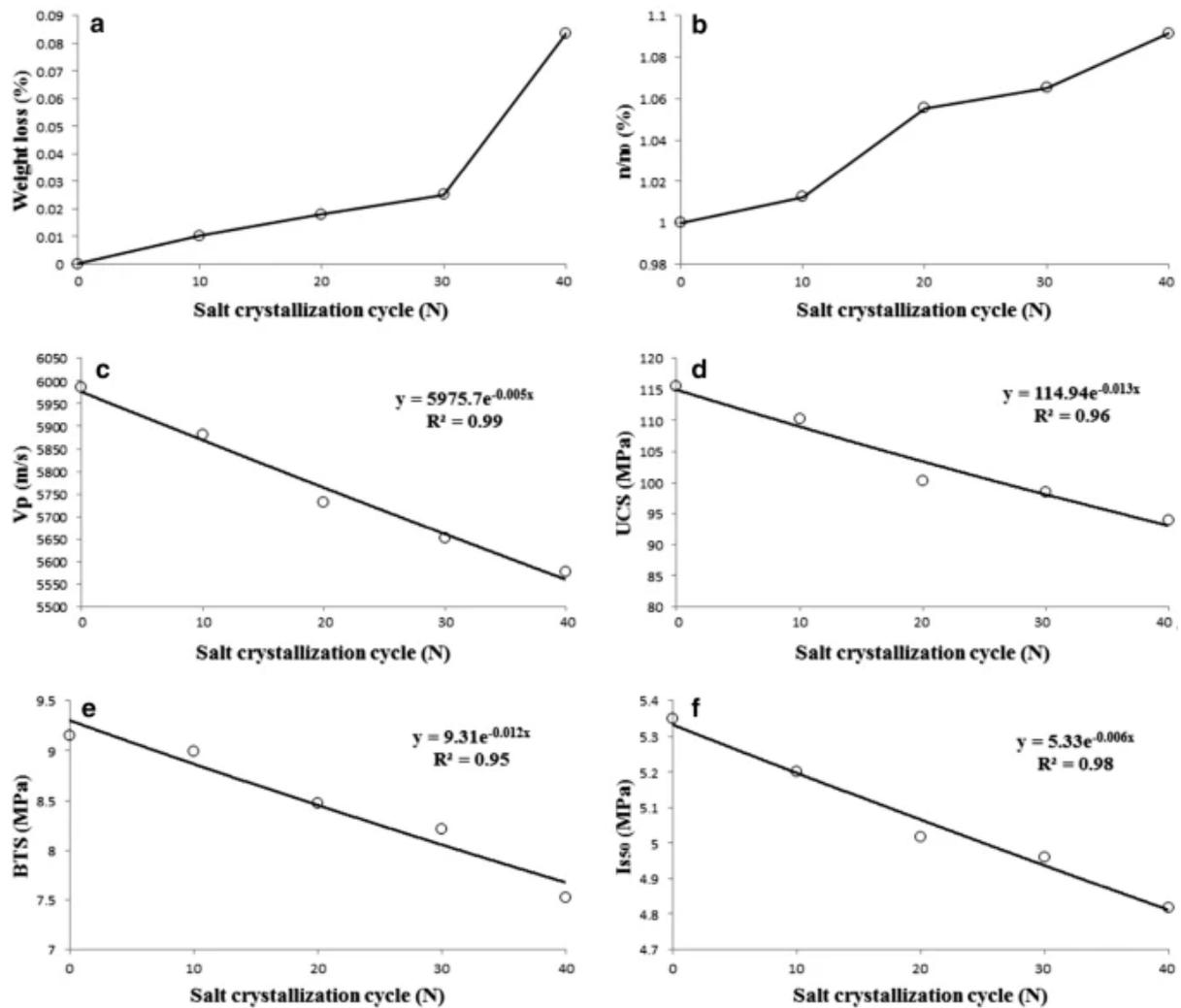


figure10 Changes of physical and mechanical properties of the specimens vs. the numbers of sodium sulfate salt crystallization cycles: a weight loss, b porosity ( $n$ ), c P wave velocity ( $V_p$ ), d uniaxial compressive strength (UCS), e Brazilian tensile strength (BTS), and f point load strength index ( $I_{s50}$ )

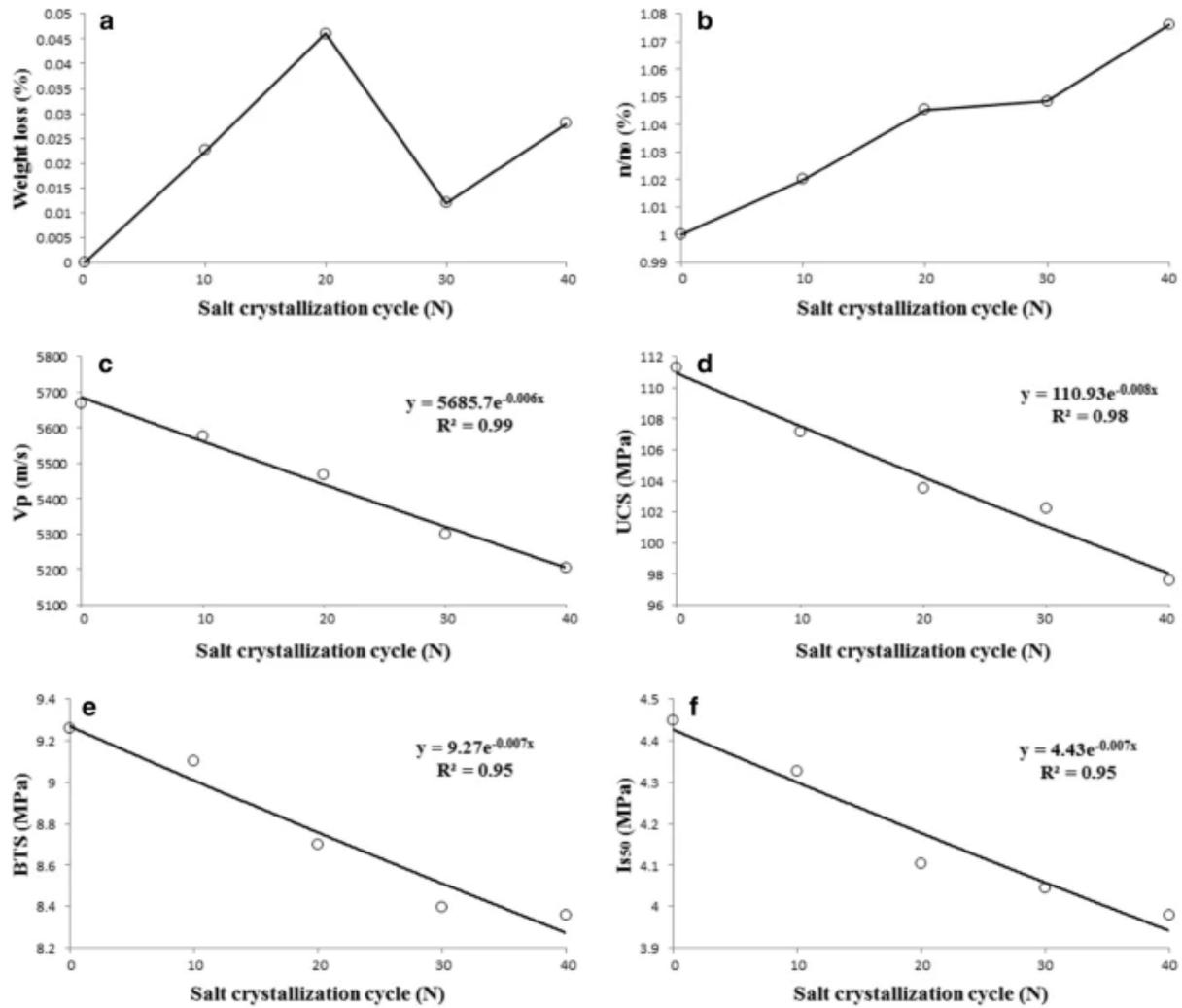


figure11 Changes of physical and mechanical properties of the specimens vs. the numbers of magnesium sulfate salt crystallization cycles: a weight loss, b porosity (n), c P wave velocity (V<sub>p</sub>), d uniaxial compressive strength (UCS), e Brazilian tensile strength (BTS), and f point load strength index (Is<sub>50</sub>)

Tables 4 and 5 show the change in porosity of the specimens after testing. The normalized porosity values of the specimens have direct relationship with the salt crystallization cycles (Figs. 10b, 11b), whereas no significant change was observed in the normalized porosity values from cycle 0 to cycle 40 in both the salts (Figs. 10b, 11b). Although the normalized porosity value shows ascending trend with increasing salt crystallization cycles, its changes are less than that observed in the freezing–thawing process. With developing micro-fractures originating from salt crystal creation within the stone, V<sub>p</sub> of the specimens decreased (Figs. 10c, 11c). Relationship between the V<sub>p</sub> values and the cycle numbers is strong in both the salt crystallization tests and it supports this conclusion (Figs. 10c, 11c).

No significant change in the UCS values of the specimens was observed for all the test cycles (Tables 4 and 5). However, it decreases as the number of the salt crystallization tests increases. There are meaningful relationships between the UCS values and number of the salt crystallization cycles with R<sup>2</sup> of 0.96 and 0.98 for sodium sulfate and magnesium sulfate solutions, respectively (Figs. 11d, 12d).

As the number of test cycles increase, the BTS values also decrease (Figs. 11e, 12e). Sodium sulfate and magnesium sulfate salt crystallization tests caused relatively low reduction in the Is50 values (Figs. 11f, 12f). There are negative correlations between the BTS values and the salt crystallization cycles, as well as between the Is50 values and the salt crystallization tests (Figs. 11e, f; 12e, f).

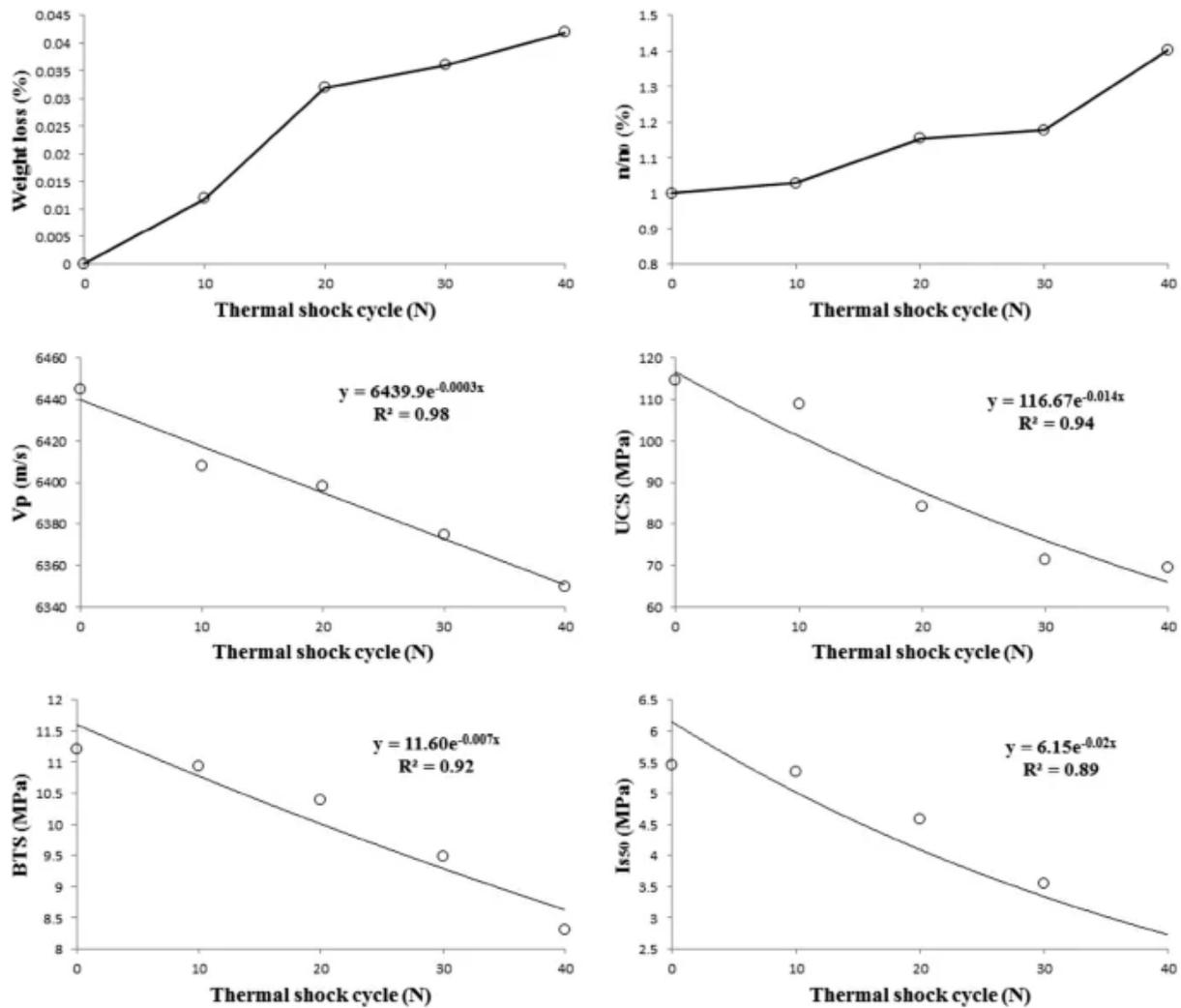


figure12 Changes of physical and mechanical properties of the specimens vs. the numbers of thermal shock cycles: a porosity (n), b P wave velocity (Vp), c uniaxial compressive strength (UCS), d Brazilian tensile strength (BTS), and e point load strength index (Is50)

Slight weathering occurred after the salt crystallization test, as shown in Fig. 6b, c. It seems that the negligible effect of the saline solutions on the properties of the specimens is due to low porosity of the specimens which prohibited further salt solutions percolation throughout specimens. Evans (1969) [cited in Ludovico-Marques and Chastre (2012)] reported that salt degradation is more expectable for high porous rocks. As it was revealed by petrographic examinations on thin sections, the porosity of the specimens is very low, which support our interpretations about the poor degradation effect of the salt crystallization, although lower mobility of saline water in comparison to fresh water is another reason for the poor observed degradation.

Thermal shock cycles and physico-mechanical changes of the specimens

Physico-mechanical changes of the specimens under the influence of 40 cycles of thermal shock test are presented in Table 6. As can be seen from Table 6, slight changes in the physical properties (porosity and P wave velocity values) were created due to the 40 cycles of thermal shock test. As the normalized porosity values were increased with a gradual trend from cycle 0 to cycle 40 (Fig. 12a). The values of  $V_p$  decrease with increase in numbers of thermal shock cycles ( $R^2 = 0.95$ ) (Fig. 12b), so the velocity stepped down to 6350 m/s, while it was recorded up to 6445 m/s in normal condition (Table 6). This slight decrease in the  $V_p$  values is probably related to the development of micro-cracks and subsequent increase in porosity due to the thermal shock cycles.

Table 6 Average values of physical and mechanical properties of the specimens before and after the thermal shock cycles

Physical–mechanical properties	Normal condition	After thermal shock test			
	Cycle 0	Cycle 10	Cycle 20	Cycle 30	Cycle 40
Weight loss (%)	0	0.012	0.032	0.036	0.042
$n/n_0$	1	1.03	1.15	1.18	1.4
$V_p$ (m/s)	6445	6408	6398	6375	6350
UCS (MPa)	114.6	108.84	84.12	71.38	69.39
BTS (MPa)	11.2	10.94	10.39	9.48	8.31
$I_{s50}$ (MPa)	5.45	5.35	4.58	3.56	2.42

For presenting the mechanical test results, UCS, BTS, and  $I_{s50}$  values vs. thermal shock cycles were plotted for 40 cycles (Fig. 12c–e). There are exponential relationships with high determination coefficient between UCS, BTS, and  $I_{s50}$  values with thermal shock cycles (see Fig. 12c–e). Increase in porosity due to the development of micro-cracks is the main reason for observed loss in the mechanical properties.

#### Decay function models for the physical and mechanical properties

Mutlutürk et al. (2004) by performing some ageing tests (freezing–thawing and heating–cooling tests) on different types of rocks proposed a decay function model. They defined two parameters including decay constant ( $\lambda$ ) and half-life ( $N_{1/2}$ ) to measure and describe disintegration rate of rock against the weathering factors. Both these parameters could provide a rapid durability assessment; however, the half-life is a more significant indicator of stone durability (Jamshidi et al. 2016).

Equations 1 and 2 express decay factor and half-life ( $N_{1/2}$ ), respectively:

$$VN = V_0 e^{-\lambda N}, \quad (1)$$

$$N_{1/2} \approx 0.693/\lambda, \quad (2)$$

where  $V_N$  is value of physical or mechanical property of a rock after  $N$  cycles of an ageing test,  $V_0$  is the initial value physical or mechanical property,  $\lambda$  is a decay constant which indicates the average integrity loss of each property by the action of any single cycle of ageing test, and  $N_{1/2}$  is number of cycles necessary to reduce the integrity to half its value. The minus sign in Eqs. (1) and (2) indicates the integrity loss of a physical or mechanical property.

To determine the decay constant ( $\lambda$ ) for the physical and mechanical properties (in this study,  $V_p$ , UCS, BTS, and  $I_{s50}$ ), simple regression analysis with exponential form was applied to express relationship between the values of the properties and number of the ageing cycles (Figs. 9, 10, 11, 12). Considering the high values of determination coefficients, all the relationships are reliable to estimate changes in the limestone's properties after the ageing tests. Values of decay constants of the properties measured for freezing–thawing, thermal shock and salt crystallization ageing tests are presented in Table 7. Also half-life ( $N_{1/2}$ ) values were calculated via Eq. 2 (Table 7). As can be seen from the table,  $V_p$  as a physical property is not much affected by the weathering cycles, so that values of  $\lambda$  and  $N_{1/2}$  are lesser and longer than that for the mechanical parameters, respectively (Table 7). In comparison to the salt crystallization test, freeze–thaw and thermal shock have more impact on the mechanical properties, as they have higher and shorter  $\lambda$  and  $N_{1/2}$ , respectively. For example, average loss of 101 MPa was observed in UCS value after 40 cycles of freeze–thaw in the stone (Table 3); whereas, this value is 21.6 MPa in sodium sulfate salt crystallization test (Table 4). Therefore, the integrity loss rate of UCS after 40 cycles of freeze–thaw is about 4.6 times more than that for sodium sulfate salt crystallization test. As a result, it was revealed that integrity loss rate of the mechanical properties during freeze–thaw and thermal shock cycles is higher than that of salt crystallization cycles.

Table 7 The decay constant ( $\lambda$ ) and half-life ( $N_{1/2}$ ) of the specimens under the ageing tests

Ageing test	Physical and mechanical properties							
	$V_p$		UCS		BTS		$I_{s50}$	
	$\lambda$	$N_{1/2}$	$\lambda$	$N_{1/2}$	$\lambda$	$N_{1/2}$	$\lambda$	$N_{1/2}$
Freezing–thawing	0.004	173.25	0.038	18.23	0.018	38.5	0.009	77.0
Sodium sulfate salt crystallization	0.005	138.6	0.013	53.3	0.012	57.75	0.006	115.5
Magnesium sulfate salt crystallization	0.006	115.5	0.008	86.62	0.007	99.0	0.007	99.0
Thermal shock	0.0003	2310	0.014	49.5	0.007	99.0	0.02	34.65

## Conclusions

Effects of weathering are visible on Persepolis stone. Hence, this study planned some artificial ageing tests (freeze–thaw, thermal shock and salt crystallization tests) to evaluate the durability of Persepolis stone subjected to weathering factors. Limestone specimens obtained from Majd Abad quarry (adjacent to the site of Persepolis) were tested by applying different numbers of freeze–thaw, thermal shock and salt crystallization cycles. At the end of 40 cycles of freezing–thawing, the specimens showed obvious changes in their micro-structure, whereas the salt crystallization tests did not have same effect on the specimens. The UCS, BTS,  $I_{s50}$  and  $V_p$  values decreased due to increase in the porosity of the specimens as a result of the freezing–thawing cycles. During the salt crystallization cycles, physical and mechanical changes were not significant enough to indicate a clear change in the stone properties. However, values of the UCS, BTS,  $I_{s50}$  and  $V_p$  until the 40th salt crystallization cycle slightly decreased as the result of salt crystallization in the initial cracks. In case of the thermal shock test, the recorded changes in the values of the UCS, BTS,  $I_{s50}$  and  $V_p$  are similar to the freeze–thaw test. But intensity of the physical and mechanical changes is significantly less than the freeze–thaw test.

In another part of the study decay function models, based on relationships between physico-mechanical properties and number of the ageing test cycles, were developed with aim of obtaining decay constant ( $\lambda$ ) and half-life ( $N_{1/2}$ ) to evaluate the integrity loss rate of the properties against the ageing tests. Lower  $N_{1/2}$  values were obtained for freeze–thaw and thermal shock tests than that for salt crystallization test. It reveals that those weathering factors are more damaging than salt crystallization for the stone. In justification, it should be said that porosity is the important factor that mainly controls the durability of Persepolis stone. Persepolis stone is not susceptible to salt crystallization due to lack of internal macro-pore structure which prevents further salt solution percolation throughout the stone. Also it revealed that existence of veins and fractures filled with clay is the main weakness factor for Persepolis stone, as the major damage (fractures) after most of the ageing tests predominantly occurred parallel to these weakness surfaces.

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