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# A Method for Series-Resistance-Immune Extraction of Low Frequency Noise Parameters in Nano-scale MOSFETs

Angeliki Tataridou, *IEEE student member*, Gerard Ghibaudo, *IEEE fellow*,  
and Christoforos Theodorou

**Abstract**—This paper presents a new methodology for the extraction of low-frequency noise or random telegraph noise parameters, such as the gate oxide interface trap density,  $N_t$ , and the mobility fluctuations factor,  $\Omega$ , without the influence of the source/drain series resistance,  $R_{sd}$ . The method utilizes the Y-function -which is immune to any first-order degradation, including the series resistance- as well as the intrinsic mobility degradation factors  $\theta_{1,0}$  and  $\theta_2$ . The proposed extraction technique is first demonstrated through numerical calculations and then applied on experimental results of n-channel short length FinFETs. It is shown that if the  $R_{sd}$  impact is not accounted for, the extracted LFN parameters through the classic carrier number fluctuations with correlated mobility fluctuations model (CNF/CMF) can lead to significant extraction errors. This mainly concerns the correlated mobility factor  $\Omega$ , which may be strongly underestimated, but also the extraction of the trap density  $N_t$ .

**Index Terms**—Low frequency noise, Carrier number fluctuations, Correlated mobility fluctuations, FinFETs, mobility degradation, series-resistance, Remote Coulomb scattering

## I. INTRODUCTION

Low-frequency noise (LFN) and Random Telegraph Noise (RTN) effects in MOSFETs [1], [2] have become significant performance limiting factors in advanced nano-scale devices [3] and circuits [4]. The reason is that the amplitude of these trap-related fluctuations is reciprocally proportional to the gate oxide area [2]. Therefore, it is of great importance to properly characterize experimentally these types of noise, and extract the noise model parameters with high accuracy. Apart from helping us gain a better understanding of the fluctuation mechanisms and conclude on interface and material quality, the precise parameter extraction offers a highly valuable input in the development and utilization of noise models in circuit simulations. It is in fact a prerequisite for achieving high accuracy noise-aware circuit design. Traditionally, the main parameters that can be extracted through an LFN experimental characterization in MOSFETs are the volumetric oxide interface trap density,  $N_t$  ( $/\text{cm}^3/\text{eV}$ ), and the remote Coulomb scattering coefficient,  $\alpha_{sc}$  ( $\text{Vs/C}$ ) [5]. Using the carrier number fluctuations (CNF) with correlated mobility fluctuations (CMF) model [5],  $N_t$  can be extracted through the flat-band voltage power spectral

density  $S_{V_{fb}} = q^2 k T \lambda N_t / (W L C_{ox}^2 f)$ , where  $q$  is the elementary charge,  $k$  the Boltzmann constant,  $T$  the temperature,  $C_{ox}$  the gate oxide capacitance per area,  $f$  the frequency and  $W$ ,  $L$  the channel width and length respectively. In recent years, our team has proposed to replace the extraction of the gate voltage sensitive  $\alpha_{sc}$  with the extraction of parameter which is bias-independent for a wide range of drain currents, the factor  $\Omega = \alpha_{sc} \mu_{eff} C_{ox}$ , where  $\mu_{eff}$  is the effective channel mobility [6]. For long channel devices, this extraction can be sufficiently reliable, however in short channel devices, where the source/drain series resistance ( $R_{sd}$ ) becomes important with respect to the reduced channel resistance, the extraction process can be jeopardized. The reason behind this issue is the fact that some static parameters which are utilized for noise parameter extraction, such as the transistor gain  $g_m/I_d$ , are affected by mobility degradation effects as well as access resistance issues. Concerning the latter, in one of our recent works [7] we demonstrated that the presence of  $R_{sd}$  can lead to an underestimation in the extraction of  $\Omega$  and we suggested to exploit the series resistance immunity of the Y-function ( $Y = I_d/\sqrt{g_m}$ ) [8] in the extraction methodology. Nevertheless, the Y-function is also suppressing the intrinsic first-order mobility attenuation factor  $\theta_{1,0}$ , which may cause a different type of error in the extracted parameters. In this work we study in detail how both the mobility attenuation and the  $R_{sd}$ -related degradation can impact the level of LFN in strong inversion, and explore some modeling approaches to present a new parameter extraction method, independent of these effects. An experimental application of the proposed method on short-channel FinFETs is also presented.

## II. IMPACT OF DEGRADATION EFFECTS ON LFN

### A. Mobility attenuation factors

The channel mobility degradation effects are typically expressed through the conventional model of the effective mobility by introducing the first and second order attenuation factors  $\theta_{1,0}$  and  $\theta_2$ , respectively, through (1) [9]:

$$\mu_{eff} = \frac{\mu_0}{1 + \theta_{1,0} \left(\frac{Q_i}{C_{ox}}\right) + \theta_2 \left(\frac{Q_i}{C_{ox}}\right)^2} \quad (1)$$

where  $\mu_{eff}$  is the effective channel mobility,  $\mu_0$  the low-field mobility,  $Q_i$  the total inversion charge per unit area.

In order to properly probe the exact impact of these factors on the behavior of LFN, we should begin from the classic carrier number fluctuations with correlated mobility fluctuations (CNF/CMF) approach [5]. According to this generally accepted model, a fluctuation in the oxide charge due to trapping of carriers induces a change in the drain current,  $\Delta I_d$ , directly through the variation in the number of free carriers and indirectly through a change in the effective mobility due to the trapped charge  $Q_{ox}$ . Considering the classical drain current expression in linear region (2), [9], this can be all expressed through (3).

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$$I_{d,0} = \frac{W}{L} \mu_{eff} V_d Q_i \quad (2)$$

$$\Delta I_{d,0} = \frac{\partial I_d}{\partial V_g} \frac{\partial V_g}{\partial Q_i} \Delta Q_i + \frac{\partial I_d}{\partial Q_i} \frac{\partial Q_i}{\partial Q_{ox}} \frac{\partial Q_{ox}}{\partial \mu_{eff}} \Delta \mu_{eff} \quad (3)$$

where  $V_d$  is the applied drain voltage and  $V_g$  the gate voltage. The index “0” refers to the absence of series resistance,  $R_{sd}$ , and  $\mu_{eff}$  is given by (1). After calculations, we obtain:

$$\left. \frac{\Delta I_d}{I_d} \right|_0 = - \left. \frac{g_m}{I_d} \right|_0 \Delta V_{fb} \left( 1 + \Omega \left. \frac{I_d}{g_m} \right|_0 \right) \quad (4)$$

where  $\Omega = \alpha_{sc} \mu_{eff} C_{ox}$  is the CMF factor [6],  $\Delta V_{fb} = Q_{ox}/(WLC_{ox})$  the flat-band voltage fluctuation caused by the trapped charge  $Q_{ox}$ , and  $g_m/I_d$  the transistor gain calculated as follows:

$$\left. \frac{g_m}{I_d} \right|_0 = \frac{C_{gc}}{Q_i} \left( 1 - \frac{Q_i}{C_{gc}} \frac{\theta_{1,0} + 2\theta_2 Q_i / C_{gc}}{1 + \theta_{1,0} Q_i / C_{gc} + \theta_2 (Q_i / C_{gc})^2} \right) \quad (5)$$

where  $C_{gc} = dQ_i/dV_g$  is the gate-to-channel capacitance. One can easily notice in (5) that  $\theta_{1,0}$  and  $\theta_2$  are already accounted for through  $g_m/I_d$  in (4). Indeed, as shown in Fig. 1, regardless the presence of mobility degradation or not, the CNF/CMF model captures well the simulated data from weak to strong inversion. The simulation results were obtained in Python using (2), with  $Q_i$  numerically calculated using the Lambert-W function [10], and the following parameters:  $W = 0.1 \mu\text{m}$ ,  $L = 0.1 \mu\text{m}$ ,  $\mu_0 = 100 \text{ cm}^2/\text{Vs}$ ,  $T = 300 \text{ K}$ ,  $\eta = 1$ ,  $t_{ox} = 1.2 \text{ nm}$ ,  $V_t = 0.2 \text{ V}$  and  $V_d = 30 \text{ mV}$ .

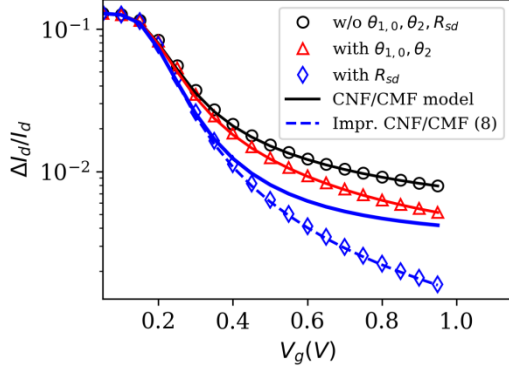


Fig. 1. Simulated data (symbols) and CNF/CMF model (lines) of normalized drain current variation versus gate voltage. Parameters used:  $\theta_{1,0}=1\text{V}^{-1}$ ,  $\theta_2=0.5\text{V}^{-2}$ ,  $R_{sd}=1\text{k}\Omega$ .

### B. Series resistance: a degradation of extrinsic origin

Despite the fact that the effective mobility-related drain current degradation is well accounted for in the CNF/CMF model -as shown in paragraph II.A, this is not necessarily true in the case of an attenuation related to source/drain series resistance,  $R_{sd}$ , because it is an extrinsic effect. The simplest way to express this kind of current degradation is through (6):

$$I_d = \frac{I_{d,0}}{1 + G_{d,0} R_{sd}} \quad (6)$$

where  $G_{d,0} = dI_{d,0}/dV_d$  is the intrinsic channel conductance. It can be easily proven that the total derivative of (6) is:

$$dI_d = \frac{dI_{d,0}}{(1 + G_{d,0} R_{sd})^2} \stackrel{(6)}{\Leftrightarrow} \frac{\Delta I_d}{I_d} = \left. \frac{\Delta I_d}{I_d} \right|_0 \frac{1}{(1 + G_{d,0} R_{sd})} \quad (7)$$

Combining (7) with (4) results in (8):

$$\frac{\Delta I_d}{I_d} = - \frac{g_m}{I_d} \Delta V_{fb} \left( 1 + \Omega \left. \frac{I_d}{g_m} \right|_0 \right) \quad (8)$$

Note how the CNF part ( $g_m/I_d \Delta V_{fb}$ ) includes the impact of  $R_{sd}$ , whereas the parenthesis expressing the impact of CMF is not affected by  $R_{sd}$ . As a result, if we use the measured  $I_d/g_m$  instead of the intrinsic  $I_d/g_{m0}$  (without  $R_{sd}$ ), the model is not expected to fit the measured data. This effect is shown in Fig. 1, where it is evident that although  $\theta_{1,0}$  and  $\theta_2$  are not affecting the model’s accuracy,  $R_{sd}$  can cause a significant deviation from the simulated data, mainly in strong inversion. In fact, there is a perfect fit when we use the improved CNF/CMF as proposed through (8).

It is also interesting to examine how this effect can impact the extraction accuracy of the CMF factor  $\Omega$ .  $\Omega$  is usually extracted using the input-referred gate voltage noise  $\Delta V_g = \Delta I_d/g_m$  (or  $\sqrt{S_{V_g}} = \sqrt{S_{I_d}/g_m}$  for PSD analysis) [5], to take advantage of its linear dependence with  $I_d/g_m$  and extract  $\Omega$  using the slope:

$$\Delta V_g = - \Delta V_{fb} \left( 1 + \Omega \left. \frac{I_d}{g_m} \right|_0 \right) \quad (9)$$

This quantity is plotted in Fig. 2, versus both gate voltage overdrive  $V_g - V_t$  and  $I_d/g_m$ . As expected, the CNF/CMF model using the measured  $I_d/g_m$  cannot predict the noise behavior when  $R_{sd}$  is non-negligible. Furthermore, comparing these two figures leads us to conclude that while  $\Delta V_g$  does not seem affected by  $R_{sd}$ , when plotted against  $I_d/g_m$ , it seems as if it was degraded. This can be attributed to the increase of  $I_d/g_m$  with  $R_{sd}$ , which in turn leads to a less steep slope and to an eventual underestimation in the extraction of  $\Omega$ , as shown in [7]. It is also obvious that it might result in an overestimation of  $\Delta V_{fb}$ .

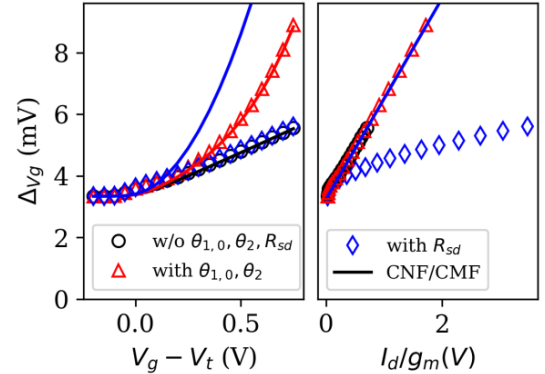


Fig. 2. Simulated data (symbols) and CNF/CMF model (lines) of input-referred gate voltage variation versus gate voltage overdrive (left) and  $I_d/g_m$  (right). Parameters used:  $\theta_{1,0}=1\text{V}^{-1}$ ,  $\theta_2=0.5\text{V}^{-2}$ ,  $R_{sd}=1\text{k}\Omega$ .

## III. PROPOSED METHODOLOGY FOR SUPPRESSING THE IMPACT OF $R_{sd}$

As was demonstrated in part II, in order to achieve an accurate extraction of LFN parameters when  $R_{sd}$  is important, we need a precise estimation of  $I_d/g_{m0}$ . A quantity that is completely immune to  $R_{sd}$  is the Y-function, which is defined through  $Y = I_d/\sqrt{g_m}$ . As shown in [7], in the ideal case when  $\theta_1=\theta_2=0$ ,  $I_d/g_{m0}$  can be very well approximated with  $Y/\sqrt{(\beta V_d)}$ , where  $\beta = W\mu_0 C_{ox}/L$ . However, as

demonstrated in [11], a more accurate approach of  $I_d/g_{m|0}$  is needed to

$$\left. \frac{I_d}{g_m} \right|_0 = \frac{\eta kT}{q} + \frac{Y}{\sqrt{\beta V_d}} \left( 1 + \theta_{1,0} \frac{Y}{\sqrt{\beta V_d}} + \theta_2 \left( \frac{Y}{\sqrt{\beta V_d}} \right)^2 \right) \quad (10)$$

Equation (10) is actually a simplification of (5), which, if inverted, gives:

$$\left. \frac{I_d}{g_m} \right|_0 = \frac{Q_i}{C_{gc}} \left( \frac{1 + \theta_{1,0} Q_i/C_{gc} + \theta_2 (Q_i/C_{gc})^2}{1 - \theta_2 (Q_i/C_{gc})^2} \right) \quad (11)$$

and  $Q_i/C_{gc}$  is well approximated with  $Y\sqrt{(\beta V_d)}$ . However, in the presence of  $\theta_2$ , the Y-function in strong inversion should be corrected as shown in [12]. Thus, for  $V_g > V_t$ , (11) can be evaluated using the corrected Y-function,  $Y_n$ , as:

$$\left. \frac{I_d}{g_m} \right|_0 = \frac{\eta kT}{q} + Y_n \left( \frac{1 + \theta_{1,0} Y_n + \theta_2 (Y_n)^2}{1 - \theta_2 (Y_n)^2} \right) \quad (12a)$$

$$Y_n = Y \sqrt{\frac{(1 - \theta_2 (V_g - V_t)^2)}{\beta V_d}} \quad (12b)$$

Fig. 3 illustrates how (12) can perfectly emulate  $I_d/g_{m|0}$ , and how it can ensure a proper extraction of  $S_{V_{fb}}$  and  $\Omega$  through linear regression.

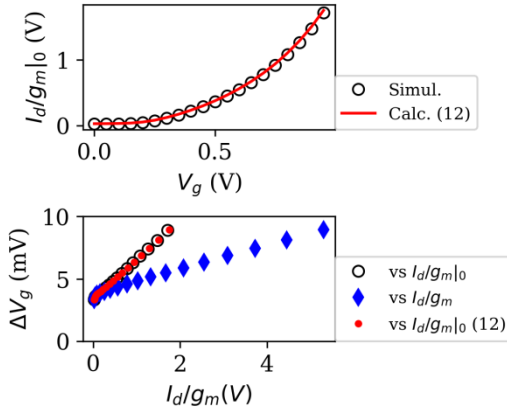


Fig. 3. Comparison between simulated  $I_d/g_{m|0}$  and calculated through (12) (top). Simulated data of input-referred gate voltage variation versus  $I_d/g_m$ , simulated with and without the  $R_{sd}$  impact and calculated through (12) (bottom). Parameters used:  $R_{sd}=1k\Omega$ .

#### IV. EXPERIMENTAL APPLICATION OF THE METHOD

The method presented above requires the extraction of several device parameters from static measurements:  $V_t$ ,  $\beta$ ,  $\theta_{1,0}$  and  $\theta_2$ . Then the  $I_d/g_{m|0}$  can be calculated using (12) and applied on the CNF/CMF model (15). We applied the proposed methodology on n-channel FinFETs fabricated at IMEC-Leuven with number of fins 4, fin height  $H_{fin} = 26$  nm, and fin width  $W_{fin} = 6$  nm. In order to extract the  $\theta_{1,0}$  coefficient we performed  $I_d$ - $V_g$  measurements for 3 different channel lengths,  $L = 44, 70$  and  $90$  nm, in the linear region ( $V_d = 30$  mV), using the programmable bias point probe system NOISYS7 by Synergie Concept [13], combined with a semi-auto 300 mm Cascade Micro Tech probe station. After extracting the  $V_t$  and  $\beta$  parameters using the Y-function method, we extracted the effective mobility attenuation coefficients  $\theta_1$  and  $\theta_2$  from the linear fit of the  $\theta_{eff}$  quantity, as given by (13), versus  $V_g - V_t$  in the strong inversion region [12]. A representative example of the  $\theta_1$  and  $\theta_2$  extraction is shown in fig.4. The extracted values of  $\theta_2$  were between 0.1 and  $0.3$   $V^{-2}$  in all cases.

$$\theta_{eff}(V_g) = \frac{\beta V_d}{I_d} - \frac{1}{V_g - V_t} = \theta_1 + \theta_2 (V_g - V_t) \quad (13)$$

The dependence of  $\theta_1$  on  $R_{sd}$ , as given by (14), allows the extraction of  $\theta_{1,0}$  and  $R_{sd}$  when  $\theta_1$  is plotted with  $\beta$  for different channel lengths as shown in Fig. 4. It should be noted that the static parameters  $\theta_1$ ,  $\theta_2$ ,  $\beta$  and  $V_t$ , were extracted by the average I-V characteristic of 9 devices for the case of channel length 70 and 90 nm and of 41 devices for the 44 nm channel length.

$$\theta_1 = \theta_{1,0} + \beta R_{sd} \quad (14)$$

$\theta_{1,0}$  and  $R_{sd}$ , normalized by the effective gate oxide width, were extracted to be  $0.497$   $V^{-1}$  and  $203$   $\Omega \cdot \mu m$  respectively.

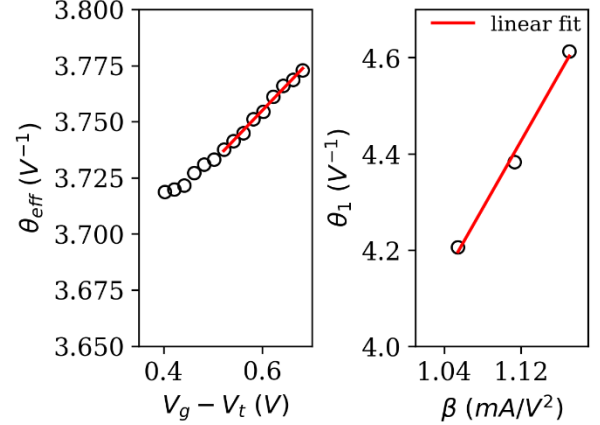


Fig. 4.  $\theta_{eff}$  vs  $(V_g - V_t)$  for channel length 90 nm along with the linear fit (left). First order mobility attenuation factor ( $\theta_1$ ) vs  $\beta$  for 3 different channel lengths (44, 70, and 90 nm) along with the linear fit (right).

In order to avoid the variability effect in our LFN analysis, we measured 41 devices for  $L = 44$  nm, and we extracted an average  $I_d$ - $V_g$  curve, from which we calculated  $g_m$  and the Y-function. The curves and the extracted subthreshold slope SS, which we need in order to calculate the ideality factor  $\eta = qSS / (kT \ln(10))$  [14], used in (12), are shown in Fig.5. The ideality factor was extracted to be  $\eta = 1.13$ .

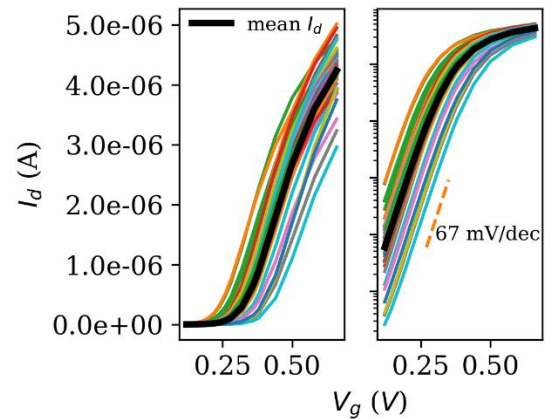


Fig. 5. Current-Voltage characteristics in linear and logarithmic scale of 41 dies along with the average  $I_d$ - $V_g$  curve, extracted by taking the mean value of the drain current of each device.

Detailed LFN measurements were also performed and the input-referred gate voltage noise power spectral density  $S_{V_g} = S_{id}/g_m^2$  was extracted for 41 devices at various gate voltage values. The spectra, along with the average spectrum, extracted by taking the mean logarithmic [15] value of  $S_{V_g}$  of each device, are shown in Fig. 6. The  $1/f$  behavior of the average spectrum allows the application of

the CNF/CMF model as it can be considered that a uniform trap distribution is present for each bias condition.

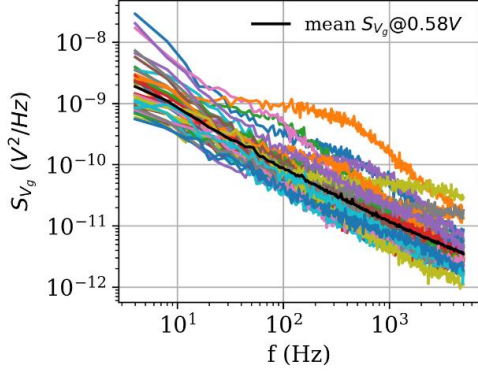


Fig. 6. Input-referred gate voltage noise vs frequency, for 41 devices with  $L = 44$  nm, biased under  $V_g = 0.58$  V.

Fig. 7 shows the  $\sqrt{S_{V_g}}$  extracted at 10 Hz vs both the measured  $I_d/g_m$  and the calculated  $I_d/g_{m|0}$  using (12), for the extraction of the flat-band voltage power spectral density,  $S_{V_{fb}}$  and the  $\Omega$  component, using the generalized form of (9) for the linear fit in strong inversion.

$$\sqrt{S_{V_g}} = \sqrt{S_{V_{fb}}} \left( 1 + \Omega \frac{I_d}{g_{m|0}} \right) \quad (15)$$

It should be noted that  $S_{V_{fb}}$  is actually the equivalent of  $\Delta_{V_{fb}}$  when going from a single trap to a distribution of traps.  $\Delta_{V_{fb}}$  refers to the electrostatic impact of a trapped charge  $Q_{ox}$  whereas  $S_{V_{fb}}$  is the flat-band voltage power spectral density caused by a fluctuating oxide charge,  $S_{Q_{ox}}$ . Therefore,  $\Delta_{V_g}$  is more useful when simulating the noise amplitude behavior or studying single trapping effects such as RTN, but  $S_{V_g}$  is necessary for studying  $1/f$  noise, where a distribution of trap time constants is involved.

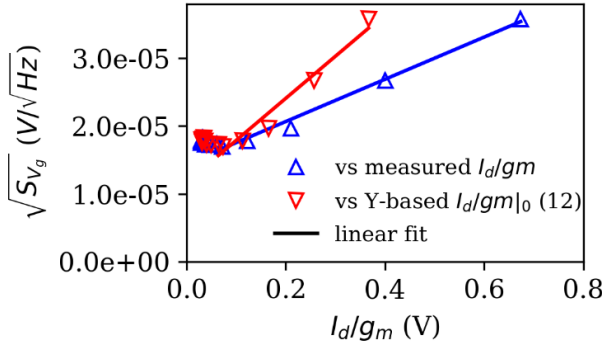


Fig. 7. Square root of input-referred noise,  $\sqrt{S_{V_g}}$ , versus the measured ratio of drain current and transconductance,  $I_d/g_m$ , and the calculated one using (12) along with the strong inversion linear fit based on (9).

Table I shows the extracted values of  $N_t = S_{V_{fb}} WLC_{ox}^2 f / \lambda q^2 kT$  and  $\Omega$  with both the measured  $I_d/g_m$  and the  $R_{sd}$ -free  $I_d/g_{m|0}$  (12). As it can be seen, there is a slight overestimation of  $N_t$  with the classical method. More importantly, the  $\Omega$  component seems to be highly influenced by the  $I_d/g_m$  values used, as explained in part II. In fact, the new  $\Omega$  is more than two times higher, revealing a much more critical magnitude of the remote Coulomb scattering.

TABLE I  
 $N_t$  AND  $\Omega$  EXTRACTED VALUES

	Measured $I_d/g_m$	$I_d/g_{m 0}$ as calculated by (12)
$N_t$ (eV/cm <sup>2</sup> )	$5.13 \times 10^{16}$	$3.36 \times 10^{16}$
$\Omega$ (V <sup>-1</sup> )	2.15	5.29

## V. CONCLUSION

A complete,  $R_{sd}$ -immune methodology has been proposed for the accurate extraction of CNF/CMF noise model parameters, such as  $N_t$  and  $\Omega$ . An  $I_d/g_m$  independent of  $R_{sd}$  is extracted using the the Y-function properties, thus any questionable issues on the accuracy of the LFN extracted parameters due to the  $R_{sd}$  presence have been overcome. This method was successfully applied in experimental measurements performed on short-channel n-FinFETs. It was revealed that the extraction of  $\Omega$  using the classical method, with no suppression of the series resistance impact, was underestimated by more than a factor of two.

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## REFERENCES

- [1] G. Reimbold, "Modified  $1/f$  Trapping Noise Theory and Experiments in MOS Transistors Biased from Weak to Strong Inversion—Influence of Interface States," *IEEE Trans. Electron Devices*, vol. 31, no. 9, pp. 1190–1198, 1984, DOI:10.1109/T-ED.1984.21687.
- [2] K. K. Hung, P. K. Ko, C. Hu, and Y. C. Cheng, "Random telegraph noise of deep-submicrometer MOSFETs," *IEEE Electron Device Lett.*, vol. 11, no. 2, pp. 90–92, 1990, DOI:10.1109/55.46938.
- [3] B. Kaczer *et al.*, "The defect-centric perspective of device and circuit reliability - From individual defects to circuits," *Eur. Solid-State Device Res. Conf.*, vol. 2015-Novem, pp. 218–225, 2015, DOI:10.1109/ESSDERC.2015.7324754.
- [4] K. Takeuchi *et al.*, "Direct observation of RTN-induced SRAM failure by accelerated testing and its application to product reliability assessment," *Dig. Tech. Pap. - Symp. VLSI Technol.*, pp. 189–190, 2010, DOI:10.1109/VLSIT.2010.5556222.
- [5] G. Ghibaudo, O. Roux, C. Nguyen-Duc, F. Balestra, and J. Brini, "Improved Analysis of Low Frequency Noise in Field-Effect MOS Transistors," *Phys. Status Solidi*, vol. 124, no. 2, pp. 571–581, 1991, DOI:10.1002/pssa.2211240225.
- [6] E. G. Ioannidis, C. A. Dimitriadis, S. Haendler, R. A. Bianchi, J. Jomaah, and G. Ghibaudo, "Improved analysis and modeling of low-frequency noise in nanoscale MOSFETs," *Solid. State. Electron.*, vol. 76, pp. 54–59, 2012, DOI:10.1016/j.sse.2012.05.035.
- [7] A. Tataridou, G. Ghibaudo, and C. Theodorou, "Influence of series resistance on the experimental extraction of FinFET noise parameters," in *International Conference on Microelectronic Test Structures*, 2020.
- [8] G. Ghibaudo, "New method for the extraction of MOSFET parameters," *Electron. Lett.*, 1988, DOI:10.1049/el:19880369.
- [9] G. Ghibaudo, "Analytical modelling of the MOS transistor," *Phys. status solidi*, 1989, DOI:10.1002/pssa.2211130127.
- [10] T. A. Karatsori *et al.*, "Full gate voltage range Lambert-function based methodology for FDSOI MOSFET parameter extraction," *Solid. State. Electron.*, vol. 111, 2015, DOI:10.1016/j.sse.2015.06.002.
- [11] J. B. Henry, A. Cros, J. Rosa, Q. Rafhay, and G. Ghibaudo, "Impact of access resistance on New-Y function methodology for MOSFET parameter extraction in advanced FD-SOI technology," *IEEE Int. Conf. Microelectron. Test Struct.*, vol. 0, pp. 0–4, 2017, DOI:10.1109/ICMTS.2017.7954269.
- [12] C. Mourrain, B. Cretu, G. Ghibaudo, and P. Cottin, "New method for parameter extraction in deep submicrometer MOSFETs," in *IEEE International Conference on Microelectronic Test Structures*, 2000.
- [13] J. A. Chroboczek, A. Szewczyk, and G. Piantino, "Low frequency noise point probe measurements on a wafer level using a novel programmable current amplifier," in *Noise in Physical Systems and 1/f Fluctuations*, 2001, pp. 701–704.
- [14] J. P. Colinge, R. W. Bower, and G. Editors, "Silicon-on-Insulator Technology," *MRS Bull.*, 1998, DOI:10.1557/S0883769400029766.
- [15] C. G. Theodorou *et al.*, "Low frequency noise variability in ultra scaled FD-SOI n-MOSFETs: Dependence on gate bias, frequency and temperature," *Solid.State.Electron.*, vol.117, pp.88–93, 2016, DOI:10.1016/j.sse.2015.11.011