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Frequency-Tunable Slot-Loop Antenna based on KNN Ferroelectric Interdigitated Varactors

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Abstract— A miniature frequency-tunable slot-loop antenna ($0.128\lambda_0 \times 0.077\lambda_0$) based on ferroelectric $\text{K}_{0.5}\text{Na}_{0.5}\text{NbO}_3$ (KNN) interdigitated varactors is investigated at Ku-band. KNN material has been selected among the ferroelectric oxide family because of its competitive properties for microwave applications. Its high permittivity value ($\epsilon_r \approx 360$ at 10 GHz) and its wide frequency tunability under an external static electric field E_{bias} make it a promising candidate for frequency-agile antennas and circuits at microwaves. The antenna prototype has been designed and elaborated on MgO substrate ($\epsilon_r = 9.8$ and $\tan\delta \approx 10^{-4}$ at 10 GHz). Fabrication details including laser microetching process of the ferroelectric layer are also described. The center frequency of the slot-loop antenna can therefore be tuned monotonously from 15.22 to 15.97 GHz under $E_{bias} = 88$ kV/cm, leading to a frequency tunability rate equal to 4.6%. These results demonstrate for the first time the ability of the KNN material to be used for miniature tunable antennas, in comparison with $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$, currently considered as the most relevant material for such applications.

Index Terms— Ferroelectric films, Microwave devices, Slot Antennas, Tunable devices, Varactors.

I. INTRODUCTION

Nowadays, the intensive use of connected objects creates a growing demand for miniaturization in electronics. In this competitive environment, tunable antennas promote attractive solutions for multi-standard and/or adaptive wireless systems. Among the technical solutions available to achieve frequency tunability, ferroelectric thin films exhibit numerous advantages. Indeed, they exhibit low energy consumption, fast response times (lower than 1 μs), and enable a monotonous tuning of devices. Moreover, the films can be implemented fairly easily in tunable capacitors (varactors), based on microstrip interdigital capacitor (IDC) or metal-insulator-metal (MIM) technologies. Furthermore, their intrinsic high permittivity value is a key advantage for device miniaturization. Therefore, this technology is a promising solution for cost and size reductions of tunable microwave devices [1]–[3]. The

investigation of various ferroelectric materials, in particular among the lead-free oxides, is a key issue to identify the best candidates to lead to performant tunable antennas. Taking into account all the steps of the design, fabrication and measurements of the antenna is very important to achieve a relevant evaluation of the materials for further use.

Ferroelectric materials have been investigated at microwaves for tunable phase shifters (e.g. [4]), tunable filters (e.g. [5]) and tunable antennas (e.g. [6]). Most of these studies are based on $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$ (BST) materials due to its composition-dependent dielectric characteristics and its low loss tangent value ($\tan\delta$ lower than 0.03 at 20 GHz on thin films [7]). Among the examples, in 2012, H.-Y. Li *et al.* introduced a slot-loop miniature tunable antenna with BST-based interdigitated varactors and operating close to 15 GHz [8]; such antenna exhibited a 1%-frequency tunability rate under 195 kV/cm dc bias electric field. To increase the tunability rate, this group proposed slot-loop miniature tunable antennas based on MIM varactors operating at C- and X-bands [9], [10]. MIM capacitors have been often exploited [9]–[13] as this configuration helps to increase the applied external static electric field, thus leading to an increase of the tunability rate up to 27.3% and 30.6%, respectively (Table I). However, these antennas usually suffered from very low gain values and such MIM capacitors are really challenging to fabricate. Other details from miniature antenna structures using ferroelectric-based varactors are also reported in Table I.

Even though BST material is usually considered as one of the most relevant ferroelectric oxide for microwave applications, alternative materials are currently under investigation, such as $\text{AgTa}_{1-x}\text{Nb}_x\text{O}_3$ [14], $\text{Sr}_{1-x}\text{Bi}_x\text{TiO}_3$ [15], $\text{BaZr}_x\text{Ti}_{1-x}\text{O}_3$ [16], $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ [17] and $\text{KTa}_x\text{Nb}_{1-x}\text{O}_3$ [18]. A tunable antenna based on $\text{KTa}_x\text{Nb}_{1-x}\text{O}_3$ (KTN) films was proposed in [19], [20]. It exhibited a maximum gain value equal to 6.7 dBi and 1.7% frequency tunability rate under 85 kV/cm dc bias electric field.

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TABLE I
MINIATURE AND TUNABLE ANTENNAS BASED ON PRINTED FERROELECTRIC VARACTORS

Reference	[12]	[13]	[11]	[8]	[9]	[10]	[19], [20]	<i>This work</i>
Substrate	Sapphire	Sapphire	Sapphire	Sapphire	Sapphire	Sapphire	Sapphire	MgO
Ferroelectric material	BST	BST	BST	BST	BST	BST	KTN	KNN
Film thickness (nm)	250	250	250	200	200	170	600	600
Radiating element size (mm²)	3.8×3.8	3.8×3.8	4.8×5.1	1.2×3.8	2.5×2.5	2.5×2.5	14.4×3.6	2.5×1.5
Varactor technology	MIM	MIM	MIM	IDC	MIM	MIM	CPW	IDC
$E_{bias,max}$ (kV/cm)*	120	280	400	195	350	880	85	88
Frequency range (GHz)**	5.8-6.1	5.28-5.77	7.42-7.9	15.18-15.36	5.57-7.33	6.71-9.14	17.0-17.3	15.22-15.97
Tunability rate (%)	5	8.9	6.3	1.2	27.3	30.6	1.7	4.6
Tunability performance η^*	0.04	0.03	0.02	0.01	0.08	0.03	0.02	0.05
Gain (dBi)	-3	-3	/	0.5	-10.8	-3.1	6.7	-2

* As mentioned or computed from the available paper data

** Measured frequencies at minimal $|S_{11}|$ without and under $E_{bias,max}$

Another alternative to BST material lies in the perovskite-type $K_{0.5}Na_{0.5}NbO_3$ (KNN) oxide. The KNN system is most famous for its piezoelectric properties, since Saito *et al.* reported high piezoelectric modulus values ($d_{33} \approx 300$ pC/N [21]) with a Curie temperature close to 400°C [22], making it a promising alternative to the widely used $PbZrTiO_3$ material. In addition, recent studies have also demonstrated interesting KNN thin films properties at microwaves with a high dielectric constant ($\epsilon_r \approx 360$ at 10 GHz and 22%-frequency tunability under 94 kV/cm dc bias electric field [23], [24]).

In the present work, a frequency-tunable slot-loop antenna was designed, fabricated and measured using KNN film-based microstrip IDC varactors. Although previous works have demonstrated the relevance of ferroelectric varactors for miniaturization and reconfigurability (e.g. [10], [13]), the present study reports, for the first time to the best of our knowledge, the use of KNN material for frequency-tunable antenna application. The paper is organized as follows. Design, fabrication and measurement procedures are described in Section II. Numerical and measured results are presented, compared and discussed in Section III. Conclusions are drawn in Section IV

II. ANTENNA DESIGN, FABRICATION, AND MEASUREMENT PROCEDURES

A. Antenna design

The proposed antenna is a 2.5 mm × 1.5 mm slot-loop antenna fabricated on a 600 nm-thick KNN thin film grown on 10 mm × 10 mm × 0.5 mm MgO substrate ($\epsilon_r = 9.8$ and $\tan\delta \approx 10^{-4}$ at 10 GHz and room temperature). The antenna was designed to operate at *Ku*-band. Its layout (inspired from [8], [9]) and cross-section view are reported in Fig. 1a and 1b respectively. The antenna dimensions are detailed in Table II. The slot loop (width $G = 50$ μm) is fed through a 50-Ω coplanar waveguide (CPW) transmission line ($w = 100$ μm, $g = 300$ μm). Interdigitated varactors are symmetrically placed in the upper and lower slots to tune the antenna operating frequency. The antenna is polarized through an external dc voltage from 0 V to

150 V. As the gap G_c between the capacitor fingers is 15 μm in width, the maximum applied dc voltage leads to a maximum external static electric field $E_{bias} = 100$ kV/cm, a significantly low value compared with those reported in Table I (except for [19], [20]). The main dielectric characteristics of the KNN film used for the antenna design are: $\epsilon_r = 355$ and $\tan\delta = 0.35$ without biasing; $\epsilon_r = 315$ and $\tan\delta = 0.30$ under $E_{bias} = 27$ kV/cm (the maximum E_{bias} value applied on the transmission lines used to retrieve the (ϵ_r ; $\tan\delta$) dielectric characteristics of the KNN film at 10 GHz [23], [24]). The antenna dimensions, the placement and numbers of varactors were optimized using Ansys HFSS v18.0; the fabrication constraints have also been taken into account, as explained below.

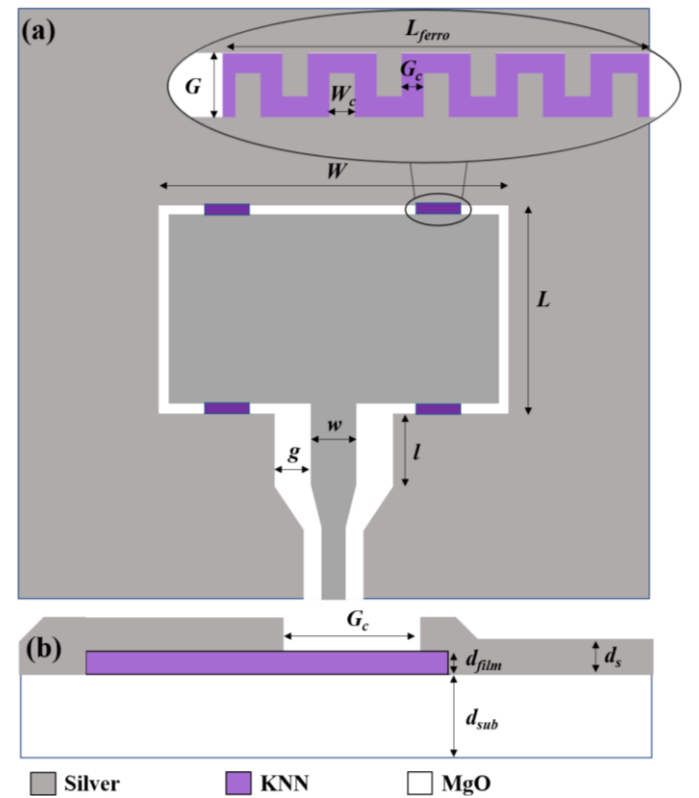


Fig. 1. (a) Layout (top view) and (b) cross-section of the frequency-tunable IDC varactor (not-to-scale).

TABLE II
DIMENSIONS OF THE FREQUENCY-TUNABLE SLOT-LOOP ANTENNA

Symbol	L	W	G	l	w	g	L_{ferro}	W_c	G_c	d_{sub}	d_s	d_{film}
Length (μm)	1500	2500	50	2500	100	300	320	20	15	500	2	0.6

B. Antenna fabrication

The manufacturing process of the antenna prototype is the following. First a 600 nm-thick ferroelectric film was grown by pulsed laser deposition on a (100) MgO substrate, using a KrF excimer laser (Coherent company, pulse duration: 20 ns, $\lambda = 248$ nm) with an energy of 210 mJ, a fluence of 2-3 J.cm⁻² and a working frequency of 4 Hz to ablate the ceramic KNN target. The film was deposited at 650°C under 0.3-mbar oxygen pressure. (100) MgO substrate was selected here because of (i) its suitable dielectric characteristics at microwaves, and (ii) the low mismatch between its crystalline parameters and those of the KNN film, promoting a high structural ferroelectric layer quality enhancing the frequency tunability [24]. X-ray diffraction showed a (100)-oriented single phase KNN perovskite film. As expected, the KNN films exhibited epitaxial relationships with the (100) MgO single crystal substrate [24]. Further details on the laser deposition process and the structural properties of the ferroelectric thin film are reported in [23], [24].

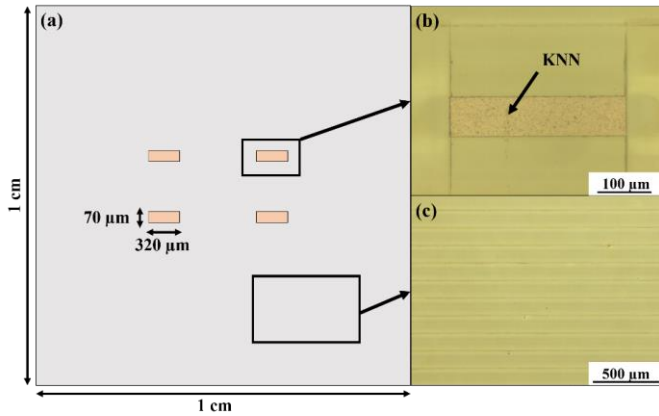


Fig. 2. (a) Schematic representation (not-to-scale) and (b), (c) pictures (optical microscopy) of a KNN strip and of a KNN-free substrate after laser microetching, respectively.

Afterwards, the KNN film was locally ablated by laser microetching process to keep only four 320 μm × 70 μm KNN areas on which the interdigital capacitors were printed (Fig. 2). This route allows reducing the global loss of antenna because the ferroelectric materials usually exhibit relatively high dielectric loss (their loss tangent $\tan\delta$ is typically higher than 1%). As previously demonstrated, the global loss was reduced by a factor four by confining the ferroelectric layer into the active areas [25]. To this end, a KrF excimer laser (*MLI-200, MLaser*, $\lambda = 248$ nm) was used to etch the 600 nm-thick KNN layer with a 150 μm × 150 μm laser spot size and an energy of 3 mJ reduced of 45% through an optical filter. The parameters and etching pattern were set by *OptecCAD* and *Process Power* software tools. The slot-loop antenna was then printed on such layer from a 2 μm-thick silver overlayer / 5 nm-thick titanium underlayer deposited by RF magnetron sputtering. Therefore, the silver thickness is three times larger than the skin depth value ($\delta = 0.53$ μm) at 15 GHz. Standard photolithography was used to pattern the antenna (Fig. 3) followed by a standard wet etching process to finally fabricate the miniature antenna.

The antenna prototype was fed by a home-made SMA-type connector (V glass bead connector, diameter $\varnothing = 300$ μm)

plugged into a 20 mm × 10 mm × 5.5 mm mechanical holder. The antenna was then measured between 12 GHz and 18 GHz at room temperature using a *StarLab* near-field spherical anechoic chamber. An external dc bias electric field ranging from $E_{bias} = 0$ kV/cm to $E_{bias} = 88$ kV/cm was applied on the varactors. Note that the maximum $E_{bias} = 100$ kV/cm could not be achieved because of the slight over-etching of the gaps G_c attached to the wet etching process (17 μm against 15 μm). The use of SHF BT 45D HV200 (SHF Communication technologies AG) broad band bias tees resulted in a measured gain lowered by 0.4 dB.

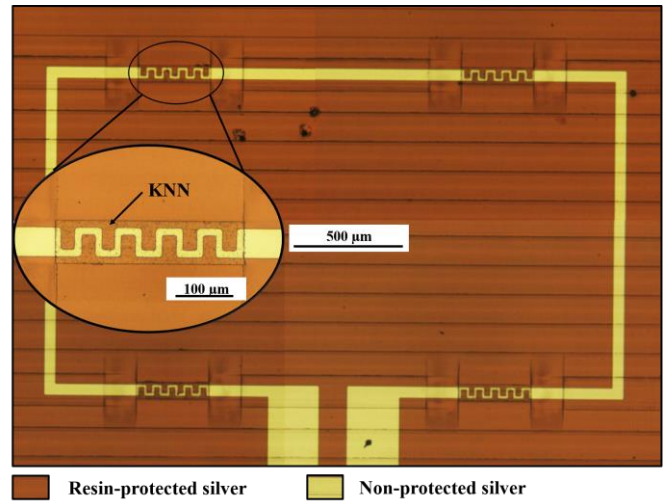


Fig. 3. Picture by optical microscopy of the patterned antenna after the standard photolithography step.

III. RESULTS AND DISCUSSION

The S_{11} magnitudes were measured using Ground-Signal-Ground (GSG) probes (*Picoprobe*) under E_{bias} ranging from 0 to 88 kV/cm. The results are plotted in Fig. 4(a). Under such experimental conditions, the antenna center frequency is tuned monotonously from 15.22 to 15.97 GHz, leading to a frequency tunability rate TR equal to 4.6%, computed as follows:

$$TR = \left| \frac{Freq_{E_{bias}=0} - Freq_{E_{bias,max}}}{(Freq_{E_{bias}=0} + Freq_{E_{bias,max}})/2} \right| \times 100, \quad (1)$$

where $Freq_{E_{bias}=0}$ and $Freq_{E_{bias,max}}$ are the operating frequency values of the antenna without E_{bias} and under the maximum E_{bias} value, respectively. Under the various E_{bias} applied on the ferroelectric varactors, the antenna remains well matched with a -10 dB reflection bandwidth equal to 0.9 GHz and 1.0 GHz without and under $E_{bias} = 88$ kV/cm, respectively. Comparison between the simulated and measured reflection coefficients shows a similar response at 15.2 GHz without biasing. The slight tunability deviation between simulation (650 MHz) and measurements (750 MHz) is mostly attributed to the KNN dielectric values used in the numerical model.

Moreover the computed TR value is almost four times larger than that reported by Li *et al.* ($TR = 1.2\%$) using a similar topology of BST-based varactors and despite a larger biasing value used ($E_{bias} = 195$ kV/cm) [8]. Our result demonstrates once more the relevance of the KNN ferroelectric films for tunable devices at microwaves. The KTN-based tunable

antenna reported by Cissé *et al.* exhibited a lower frequency-tunability rate ($TR = 1.7\%$) under a similar E_{bias} value ($E_{bias} = 85$ kV/cm) [19], [20]. However, higher frequency tunability rates ($TR = 27.3\%$ and 30.6%) have been measured by Li *et al.* on antennas based on MIM BST varactors [9], [10]. In these studies, the maximum dc bias electric field equaled 880 kV/cm, thus about 10 times the value of the one used in the present work. It is worth noting that an accurate comparison of the tunability values required similar external static electric field. The high increase of tunability achieved through such MIM BST-based tunable antennas offers promising opportunities for the forthcoming tunable antennas based on MIM KNN varactors. Table I gives a more detailed overview of the various miniature and frequency-tunable antennas based on printed ferroelectric varactors.

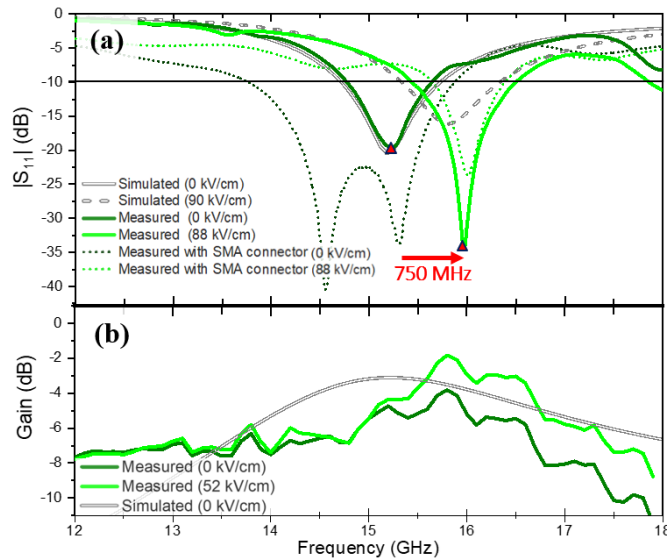


Fig. 4. Simulated and measured (a) reflection coefficient magnitudes vs. frequency under E_{bias} ranging from 0 kV/cm to 88 kV/cm; (b) simulated and measured gains vs. frequency without and under $E_{bias} = 52$ kV/cm.

The tunability performance η , as defined in (2), can be used advantageously to compare the antenna prototypes of the literature [13], [26], as follows:

$$\eta = \frac{TR}{E_{bias_max} - E_{bias_min}}, \quad (2)$$

where E_{bias_max} and E_{bias_min} are the maximum and minimum dc bias electric field values (kV/cm); and TR the antenna tunability rate (%) as defined in (1). Here the tunability performance of the antenna prototype equals $\eta = 0.05$ under $E_{max} = 88$ kV/cm. This value is among the highest one reported in the open literature for such antennas based on ferroelectric films (see Table I). For example, BST-based varactor tunable antennas exhibit $\eta = 0.03$ [13] and $\eta = 0.04$ [26].

S_{11} measurements performed using the SMA-type connector are also represented in Fig. 4(a) as this is the measurement set-up used for the radiation patterns. It is worth noting that the response at 14.5 GHz, not appearing in the numerical simulations and in the under probes measurement, is attributed to the home-made SMA connector, much larger than the antenna itself.

The antenna gains are presented in Fig. 4(b). A maximum gain of -2 dB was measured. This low value originates from the miniature size of the antenna (the dimensions of the radiating element equal $0.128\lambda_0 \times 0.077\lambda_0$ at 15.3 GHz). It is worth noting that this gain value remains in the range of those reported in the literature (-10.8 dB, -3.1 dB and 0.5 dB in [8]–[10], and -3 dB in [12–13] – see Table I).

The antenna radiation patterns are represented in Fig. 5. As expected, the measured radiation patterns are nearly omnidirectional [21], [22]. No significant variation is observed when the dc bias electric field is applied. The reflection coefficients and the radiation patterns were measured separately. A maximum E_{bias} equal to 52 kV/cm (lower than $E_{bias} = 88$ kV/cm for S_{11} measurements) was selected here to protect the equipments during measurements. It is worth noting that the antenna gain could be further enhanced by developing an antenna array based on the same design (e.g. [19], [20]).

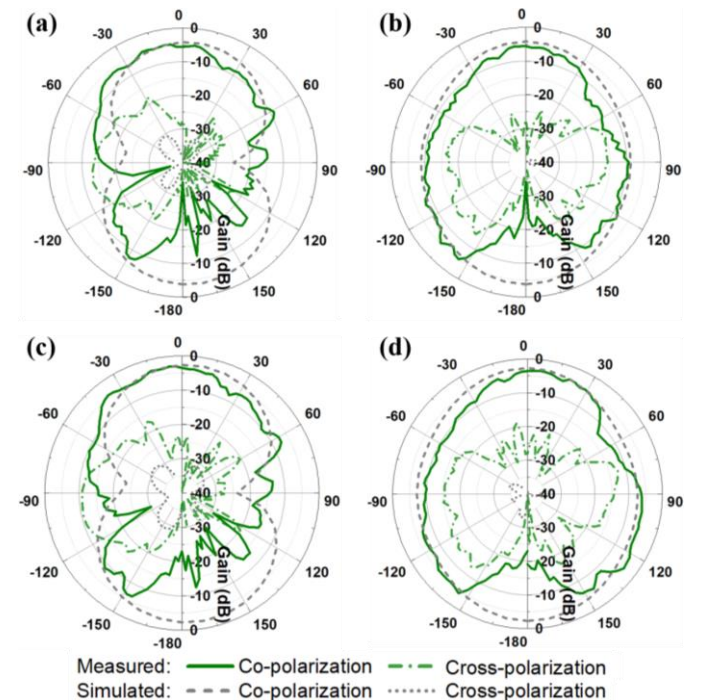


Fig. 5. Simulated and measured radiation patterns at 15.3 GHz without biasing: (a) E-plane and (b) H-plane; at 15.8 GHz under $E_{bias} = 52$ kV/cm: (c) E-plane and (d) H-plane.

IV. CONCLUSION

A miniature frequency-tunable slot-loop antenna loaded with KNN-based varactors was investigated at Ku -band. The design, fabrication and experimental results were presented, discussed and compared in detail. The antenna operating frequency was tuned from 15.22 to 15.97 GHz through a dc bias electric field applied up to $E_{bias} = 88$ kV/cm. Its frequency tunability rate ($TR = 4.6\%$) is among the highest value reported in the literature for such biasing conditions, demonstrating thereby that KNN is a competitive ferroelectric material for future tunable microwave device applications. Further improvements can be expected by increasing the biasing value and/or by changing IDC varactors by MIM varactors on such miniature and tunable microwave antennas.

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