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► To cite this version:

Lucille Carbillet, Michael J Heap, Patrick Baud, Fabian B Wadsworth, Thierry Reuschle. Mechanical compaction of crustal analogs made of sintered glass beads: the influence of porosity and grain size. *Journal of Geophysical Research: Solid Earth*, 2021, 10.1029/2020JB021321 . hal-03184394

HAL Id: hal-03184394

<https://hal.science/hal-03184394>

Submitted on 29 Mar 2021

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1 **Mechanical compaction of crustal analogs made of sintered glass beads: the influence**
2 **of porosity and grain size**

3

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11

12 **Key Points:**

13 The mechanical compaction behavior of monodisperse sintered glass bead samples is
14 similar to that of well-sorted monomineralic sandstones

15 During triaxial compression at high confining pressure, discrete compaction bands
16 developed in a synthetic sample with a porosity of 0.35

17 All else being equal, increasing grain diameter from 0.2 to 1.15 mm decreases the stress
18 to reach C^* by more than a factor of two

19 Abstract

20 The fundamentals of our understanding of the mechanical compaction of porous rocks stem from
21 experimental studies. Yet, many of these studies use natural materials for which microstructural
22 parameters are intrinsically coupled, hampering the diagnosis of relationships between
23 microstructure and bulk sample behavior. To probe the influence of porosity and grain size on
24 the mechanical compaction of granular rocks, we performed experiments on synthetic samples
25 prepared by sintering monodisperse populations of glass beads, which allowed us to
26 independently control porosity and grain diameter. We conducted hydrostatic and triaxial
27 compression tests on synthetic samples with grain diameters and porosities in the ranges 0.2-1.15
28 mm and 0.18-0.38, respectively. During hydrostatic compaction, sample porosity decreased
29 suddenly and substantially at the onset of inelastic compaction due to contemporaneous and
30 extensive grain crushing, a consequence of the monodisperse grain size. During triaxial tests at
31 high confining pressure, our synthetic samples failed by shear-enhanced compaction and showed
32 evidence for the development of compaction bands. Critical stresses at the onset of inelastic
33 compaction map out linear-shaped yield caps for the porosity-grain diameter combinations for
34 which the critical stress for inelastic hydrostatic compaction is known. Our yield caps reinforce
35 the first-order importance of porosity on the compactive yield strength and show, all else being
36 equal, that grain size also exerts a first-order control and should therefore be routinely measured.
37 Our study further reveals the suitability of sintered glass beads as analogs for crustal rocks,
38 which facilitate the study of the deconvolved influence of microstructural parameters on their
39 mechanical behavior.

40

41 Plain Language Summary

42 Porous rocks that form the shallow part of the Earth's crust are submitted to pressure conditions
43 under which they deform by compaction, i.e., their porosity is reduced. Our understanding of the
44 compaction stems primarily from laboratory experiments conducted on samples of natural rocks.
45 Yet, because the internal structure of natural materials is complex, studying of the influence of
46 structural parameters in isolation, such as porosity and grain size, on the way rock compacts is
47 limited. To tackle this issue, we conducted compression tests on synthetic samples made of fused
48 glass beads for which we could control porosity and grain size. When the pressure on the

49 synthetic rocks is increased uniformly in all directions, a threshold pressure, characteristic of the
50 rock strength, is reached beyond which they compact suddenly and substantially. When a
51 differential stress is imposed on the synthetic rocks, discrete bands of lower porosity are
52 observed. We show that porosity and grain size exert a first-order control on the ability of the
53 synthetic rocks to resist compaction. All else being equal, if the grain size is divided by five, the
54 pressure beyond which the sample will deform by irreversible compaction is multiplied by more
55 than two. Further, our synthetic samples are good analogs for natural rocks such as sandstones
56 and tuffs and our results therefore have broad applications, from reservoir compaction and
57 subsidence to the destabilization of volcanoes.

58

59 **1 Introduction**

60 The mechanical compaction of porous materials is an important process in the Earth's crust. It is
61 one of the main deformation mechanisms of lithification, diagenesis, fault growth, and/or sealing,
62 and plays a key role in many processes in sedimentary settings such as reservoirs, aquifers, and
63 basins (Bjørlykke, 2006; Guéguen & Boutéca, 2004; Taylor et al., 2008), and in volcanic settings
64 (Farquharson et al., 2017; Grunder & Russell, 2005; Quane et al., 2009). Understanding the
65 phenomenology and micromechanics of compaction rests upon the ability to characterize the
66 evolution of microstructure through compactant deformation. To predict the occurrence and
67 extent of mechanical compaction, knowledge of the relationship between rock microstructural
68 attributes and bulk mechanical properties is crucial. Indeed, the effective macroscopic properties
69 of heterogeneous materials such as crustal rocks intricately depend on the phases present, their
70 volume fraction, their spatial distribution, and their properties (e.g., Torquato, 2002). Therefore,
71 relating microstructural attributes of porous rock to bulk properties has been the focus of
72 numerous studies in the past decades, the majority of which relied on direct experimental
73 measurements or numerical simulations (Blair et al., 1993; Doyen, 1988; Eberhart-Phillips et al.,
74 1989; Ghazvinian et al., 2014; Schöpfer et al., 2009; Scott & Nielsen, 1991).

75 As early as 1990, it had already been suggested the two principle microstructural controls on the
76 mechanical and hydraulic properties of sedimentary rocks were (1) porosity and (2) grain size
77 (Bourbie & Zinszner, 1985; Paterson & Wong, 2005; Rutter & Glover, 2012; Zhang et al., 1990).
78 Broadly speaking, an increase in rock porosity causes a decrease in strength (e.g., Baud et al.,

79 2014; Chang et al., 2006) and an increase in permeability (Bernabé et al., 2003; Dardis &
80 McCloskey, 1998). In detail, porosity also exerts an influence on the type of failure that can result
81 from the application of crustal stresses (i.e., brittle or ductile). Low-porosity rock will remain
82 brittle even under a wide range of pressure conditions (analogous to depth), whereas high-
83 porosity rock will only behave in a brittle manner at relatively low-pressure and will transition to
84 ductile behavior at high-pressure (Wong et al., 1997; Wong & Baud, 2012). Alongside the
85 influence exerted by porosity, grain size has also been the target of an increasing number of
86 experimental studies which demonstrated its controlling influence on mechanical and hydraulic
87 properties (Atapour & Mortazavi, 2018; Schultz et al., 2010; Wasantha et al., 2015). However,
88 when considering porosity and grain size, one usually refers to average values for the bulk
89 volume of samples. As pores and grains are not always homogeneously distributed, a more
90 accurate way to describe microstructure is to use pore and grain size distributions. Grain size
91 distribution in lithified sedimentary rocks is also known to influence the mechanical behavior
92 and failure mode (Guéguen & Fortin, 2013; Weng & Li, 2012; Xu et al., 2020), notably the
93 possible development of compaction localization at high effective pressures (Baud et al., 2004).
94 Assuming that grain crushing initiates by Hertzian fracture at grain contacts, Zhang et al. (1990)
95 proposed a micromechanical model predicting the stress required to achieve grain crushing using
96 porosity and grain size. While the model by Zhang et al. (1990) is in basic agreement with the
97 existing data set, Rutter and Glover (2012) suggested that data for sandstones would be better
98 described by a different empirical law. Moreover, the scatter on compiled experimental data
99 remains large (Baud et al., 2014; Chang et al., 2006). Indeed, trends in plots of strength as a
100 function of porosity or grain size are complicated by the fact that other microstructural
101 parameters, such as pore size and shape, their distributions, or matrix composition, change
102 together with porosity and grain size. For example, a decrease in porosity is often associated with
103 an increase in the proportion of cement, that, if located along grain boundaries, can greatly
104 increase the strength of granular materials (Baud et al., 2017; David et al., 1998; de Bono et al.,
105 2015; Haeri et al., 2005; Yin & Dvorkin, 1994). These complexities arise from the fact that the
106 influence of porosity, grain size, and these other microstructural considerations are all inter-
107 connected and that ultimately a fruitful way forward would be to find a method by which they
108 can be deconvolved and studied in isolation.

109 The uncertainty ensuing from the strong coupling between microstructural parameters, the
110 inherent variability from sample to sample and the heterogeneity of natural materials limits the
111 extent to which experimental studies can draw definitive conclusions about the influence of
112 specific microstructural attributes on the mechanical properties of natural materials. To tackle
113 this issue, several strategies could be considered: experiments using particularly simple materials
114 occurring with a broad range of porosity such as Fontainebleau sandstone (Saadi et al., 2017;
115 Sulem & Ouffroukh, 2006) or Leitha limestone (Baud et al., 2017); simulations using numerical
116 samples (Schöpfer et al., 2009; Weng & Li, 2012); or experiments using synthetic samples
117 (Bouzidi & Schmitt, 2012; Castagna & Backus, 1993; Chapman et al., 2018; David et al., 1998;
118 Plona et al., 1980). In this study, we chose to follow the rationale of Berge et al. (1995), Guyon
119 et al. (1987), and Wadsworth et al. (2016) who proposed sintered soda-lime silica glass beads as
120 suitable analogs for granular crustal rocks, such as sandstones and tuffs. Silicate glass
121 compositions have been extensively studied and data pertaining to their properties have been
122 gathered in handbooks for various applications (e.g., Bansal & Doremus, 2013). The elastic
123 properties of soda-lime silica glass are comparable to those of granular sedimentary and volcanic
124 rocks (Berge et al., 1995; Vasseur et al., 2016). Additionally, in nature, grains that go through the
125 different steps of diagenesis and form variably porous upper crust material are well
126 approximated, to a first order, by sintering beads. Viscous sintering of glass beads then allows
127 for the reproduction of the granular to non-granular transition and the preparation of synthetic
128 rocks of pre-determined final porosity and grain size (Wadsworth et al., 2016).

129 In this paper, we present results of a suite of mechanical tests performed on synthetic samples
130 made of monodisperse distributions of glass beads. After describing the preparation technique
131 and the intact microstructure of our synthetic samples, we present the mechanical data and the
132 associated failure mode. These results are discussed, and we will focus on the following
133 questions. Mechanically speaking, how do the sintered glass beads samples compare with natural
134 sandstones? Quantitatively, what is the influence of grain size and porosity on mechanical
135 compaction? Considering the importance of compaction bands in the fields of rock mechanics,
136 hydrology, and geology, could this failure mode be reproduced in synthetic samples?

137

138 2 Preparation and characterization of the synthetic samples

139 2.1 Viscous sintering of monodisperse populations of glass beads

140 When heated above the glass transition temperature interval, glass beads become viscous
 141 droplets. If these glass beads are packed together when heated then, as they transition from glass
 142 beads to viscous droplets, they can interact and coalesce in a process referred to as viscous
 143 sintering (Frenkel, 1945; Mackenzie & Shuttleworth, 1949; Wadsworth et al., 2016). The
 144 dominant consequence of viscous sintering is that the porosity is reduced with time. Because it is
 145 temperature-activated, this process has advantages for producing idealized porous materials. A
 146 desired packing arrangement, or grain size distribution can be determined in the cold, room
 147 temperature state, and then via heating, viscous sintering processes can be used to evolve that
 148 state to lower porosities.

149 Viscous sintering is driven by interfacial tension between the glass beads and the interstitial gas
 150 between the beads (Kuczynski, 1949). During viscous sintering, an initial system of viscous
 151 droplets evolves with time through two main stages: (1) the growth of necks between droplet-
 152 droplet pairs that share a contact (Frenkel, 1945), and (2) the shrinkage and closure of the pores
 153 between the droplets (Mackenzie & Shuttleworth, 1949). The initial system of viscous spherical
 154 droplets and interstitial pores evolves into a system of isolated pores within a viscous liquid
 155 continuum. That is, the end-state (gas in a liquid) is the inverse of the starting state (liquid in a
 156 gas) (Wadsworth et al., 2017). In practice, in order to reach a desired porosity in a desired time
 157 for a given grain size of glass bead, we control the temperature of synthesis (Wadsworth et al.,
 158 2016). The effect of changing the grain size is to change the pore size between the grains;
 159 therefore the ability to tweak the grain size of the starting glass bead population allows us to
 160 control the pore size distribution independently from the porosity, effectively deconvolving these
 161 structural controls.

162 **Table 1.** Chemical composition of glass beads (provided by manufacturer) used in this study.
 163 N.b. All wt% are recalculated to 100% disregarding the minor effect of loss on ignition.

Oxide	SiLiBeads (wt%)	SpheriGlass (A-Glass) (wt%)
SiO ₂	72.95	72.5

Na₂O	13.08	13.7
CaO	9.06	9.8
MgO	4.25	3.3
Al₂O₃	0.58	0.4
FeO/Fe₂O₃	-	0.2
K₂O	-	0.1

164

165 We prepared three sets of samples using monodisperse populations of glass spheres of diameter
166 between 0.15 and 0.25 mm (Spheriglass A-glass 1922 from Potters Industries Inc.), 0.4 and 0.6
167 mm (SiLibeads Glass beads type S 5218-7), or 1 and 1.3 mm (SiLibeads Glass beads type S
168 4504) of similar chemical composition (Table 1). The corresponding grain diameter distributions
169 are presented in Figure 1(a). The synthetic rocks were prepared as blocks from which samples
170 were cored. For each block, a monodisperse distribution of beads was poured into a ceramic tray
171 of dimensions 205 × 125 × 50 mm. The tray was then manually shaken to flatten out the beak
172 pack surface and then placed inside an electric box furnace (L9/11/SKM by Nabertherm). The
173 box furnace was set to heat at a constant rate of 3 °C.min⁻¹ to 680 °C, which is above the glass
174 transition onset temperature of 549 °C provided by the manufacturer (similar for both bead type;
175 Table 1). The peak sintering temperature was maintained constant for 1 to 12 hours depending on
176 the target final porosity (longer times result in lower porosity). The tray was moved to 180° of its
177 initial position halfway through the dwell to reduce the heterogeneity of the sintered block that
178 may arise when the temperature distribution in a furnace is not even. After being held constant
179 for a fixed time, the temperature in the furnace was lowered to 500 °C at a cooling rate of
180 1 °C.min⁻¹ and finally decreased to ambient temperature at a cooling rate of 3 °C/min. This
181 cooling workflow was designed to minimize thermal microcracking. 20 mm-diameter cylindrical
182 samples were cored along the horizontal axis of the resulting sintered block to minimize gravity
183 induced porosity gradients along the axis of the samples. These samples were then cut and
184 precision-ground to a nominal length of 40 mm.

185 2.2 Description of the sintered glass beads samples

186 A photograph of one of the synthetic samples is provided as Figure 1(b). Insights into the
187 microstructure of the synthetic samples were gained using polished thin sections observed under
188 a scanning electron microscope (SEM) (Figure 1(c)(d)). The SEM images were acquired on a
189 polished slice of a sample with a porosity of 0.35 and a mean grain diameter of 0.2 mm. As
190 predicted by the Frenkel model, adjacent beads are connected by a neck and pore space remains
191 between the bonded grains (Figure 1(d)). The lowest porosity obtained in this study is 0.22.
192 Therefore, all our samples are in the range between high porosity – close to the initial packing
193 porosity where incipient sintering has only formed necks – and intermediate porosity – where
194 sintering has progressed and begun to close the pore network. Our study does not encompass low
195 porosity synthetic rocks which would exhibit pore structures close to isolated pores in a glass
196 medium (the equilibrium porosity at the end of sintering is 0.03; Wadsworth et al., 2016) .
197 Thus, all our samples are in the upper range of porosity encompassed by natural granular rocks.
198 While a material is only truly granular when the individual grains can move relative to one
199 another (which is the case for the glass beads prior to sintering), our synthetic rocks are close to
200 that granular end member case. The microstructure of an assembly of soda-lime silica glass
201 spheres that underwent densification by sintering to a more advanced stage have been imaged in
202 2D by Vasseur et al. (2016) and continuously in 3D by Wadsworth et al. (2017), who performed
203 X-ray computed-tomography. These studies showed that the topological inversion of the viscous
204 system takes place continuously through sintering, hence allowing for the construction of a
205 unified physical description for the evolution of porosity and permeability during viscous
206 sintering.

207 Although statistically homogeneous, the granular materials prepared here by sintering glass
208 spheres present heterogeneities on the scale of 2-3 grains. Indeed, SEM images of intact samples
209 reveal small heterogeneities in the pore size distribution (Figure 1(c)). As our preparation
210 workflow allows for controlling the diameter of the grains and the degree of polydispersivity but
211 not for designing the exact nature and structure of the porous space, some porous patches, whose
212 width can reach 0.4 mm, can be observed in our intact samples (Figure 1(c)). Using square
213 windows of 0.8 mm of edge-length and of 2mm of edge-length, 2D porosity measurements were
214 performed on SEM images of intact samples (using ImageJ). The square window with an edge-
215 length of 2 mm ensures that the measured area contains at least 10 glass beads in any one

216 direction, to ensure a representative element volume (REV), and the square window with an
217 edge-length of 0.8 mm allows us to better understand whether there are variations in porosity on
218 a smaller scale. Figure 1(e) presents histograms of the distributions of 2D porosity measurements
219 obtained for the zoomed-out SEM image in Figure 1(c). While porosity measurements performed
220 in the larger window provide a monomodal distribution closely-clustered around 0.35, porosity
221 measurements performed in the smaller window yield local values up to 0.42 in a sample with an
222 average porosity of 0.35. We refer to these volumes as porosity clusters. In addition, the absence
223 of cement is accompanied by heterogeneities in the local grain contacts geometry, as previously
224 reported by den Brok et al. (1997). Sintered porous materials are random heterogeneous but
225 isotropic porous media in terms of their microstructure, where we use ‘heterogeneous’ to refer to
226 the lack of structural order. However, our samples are homogeneous in the sense that the random
227 variation in the microstructure occurs on length scales much less than the sample lengths.

228 **3 Experimental procedures**

229 To study mechanical compaction using synthetic samples, we conducted a suite of mechanical
230 tests on sintered glass bead samples. We performed hydrostatic and conventional triaxial
231 compression experiments. During hydrostatic experiments the principal stresses are equal in all
232 directions, i.e., the state of stress is $\sigma_1 = \sigma_2 = \sigma_3$. During triaxial experiments, an axial stress is
233 superimposed onto a hydrostatic pressure. The principal stress parallel to the axis of the sample
234 is higher than the principal stresses normal to this axis, i.e., the state of stress is $\sigma_1 > \sigma_2 = \sigma_3$.
235 Although we focus here on compaction, we performed a few triaxial tests at relatively low
236 pressure to identify the brittle-ductile transition. A summary of all our experiments is provided in
237 Table 2. The solid density of glass beads was determined using a helium pycnometer
238 (Micromeritics AccuPyc II 1340) prior to and after sintering at 680°C. We found that the solid
239 density of the glass beads, 2.49 g/cm³, was unchanged following exposure to 680°C. As we
240 know the solid density of the glass beads, porosity was derived from the dimensions and the
241 mass of the samples. The mean error associated with the porosity measurement is 0.005 (Table
242 2). The permeability of the samples was measured prior to deformation using a benchtop gaz
243 (nitrogen) permeameter. Permeability was measured under a confining pressure of 1 MPa using
244 the steady-state method (following the method detailed in Heap et al., 2017). All experiments
245 were conducted at the Ecole et Observatoire des Sciences de la Terre (EOST) in Strasbourg

246 (France) following the procedure detailed by Baud et al. (2015). All samples underwent the same
 247 preparation before the experiments. First, the samples were encased in very thin (< 1 mm-thick)
 248 copper foil jackets to preserve bulk sample cohesion following deformation (so that thin sections
 249 could be prepared) and to avoid disking. The samples were then dried in a vacuum oven at 40 °C
 250 for at least 48 hours and then vacuum-saturated with deionized water. Before each test, the
 251 sample to be deformed was positioned between two steel end-caps – the bottom one of which has
 252 a concentric hole at the center for fluid access to the pore pressure system. In addition, the
 253 bottom endcap was separated from the sample by a thin highly permeable filter, made from
 254 coffee filter paper, to prevent broken beads from infiltrating the pore pressure piping during the
 255 experiments. Viton® tubing was used to separate the sample from the confining pressure system.
 256 All experiments were performed at room temperature on water-saturated samples. Computer-
 257 controlled stepping motors were used to independently regulate the confining pressure, pore fluid
 258 pressure and axial stress. Data were acquired with a sampling period of 10s for hydrostatic
 259 experiments and 1s for triaxial compression experiments.

260 **Table 2.** Experimental conditions and mechanical data of the synthetic samples tested in this
 261 study. Triaxial tests were conducted at nominal strain rates of 10^{-5} s^{-1} .

Sample	Porosity	+/- (mean error = 0.005)	Confining pressure P_c (MPa)	Pore pressure P_p (MPa)	Effective pressure $P_{\text{eff}} = P_c - P_p$ (MPa)	Peak stress σ_v		Yield stress C^*	
						P (MPa)	Q (MPa)	P (MPa)	Q (MPa)
<i>mean grain diameter 1.15 mm</i>									
1814	0.181	0.004	-	-	0	10	30	-	-
1812	0.183	0.003	40	10	30	-	-	92	185
1816	0.189	0.004	60	10	50	-	-	115	194
1412	0.271	0.005	30	10	20	38	55	-	-
1414	0.265	0.005	70	10	60	-	-	80	59
1419	0.262	0.005	100	10	90	-	-	105	45
1413	0.269	0.005	130	10	120	-	-	132	35
1411	0.271	0.005	160	10	150	-	-	159	28
114012	0.294	0.006	-	-	0	1.4	4.3	-	-

114013	0.302	0.006	40	10	30	36	17	-	-
114011	0.308	0.006	70	10	60	74	43	-	-
1314	0.294	0.006	100	10	90	-	-	102	35
1313	0.303	0.006	130	10	120	-	-	128	23
114016	0.294	0.006	-	10	hydrostatic	-	-	<i>P*</i>	
								156	0

mean grain diameter 0.5 mm

2317	0.255	0.005	-	-	0	10	31	-	-
23111	0.249	0.005	40	10	30	74	132	-	-
2316	0.256	0.005	70	10	60	-	-	92	97
2318	0.258	0.005	110	10	100	-	-	133	100
2313	0.263	0.005	160	10	150	-	-	177	80
2314	0.256	0.005	190	10	180	-	-	200	60
22114	0.299	0.006	-	-	0	20	7	-	-
2218	0.302	0.006	30	10	20	-	-	40	59
27312	0.304	0.006	50	10	40	-	-	61	63
22111	0.292	0.006	70	10	60	-	-	83	70
27314	0.295	0.006	90	10	80	-	-	99	58
27315	0.294	0.006	110	10	100	-	-	117	52
22213	0.301	0.006	120	10	110	-	-	125	45
27313	0.299	0.006	130	10	120	-	-	133	39
2213	0.299	0.006	150	10	140	-	-	152	36
2217	0.296	0.006	170	10	160	-	-	168	23
27311	0.295	0.006	-	10	hydrostatic	-	-	<i>P*</i>	
								173	0

mean grain diameter 0.2 mm

31012	0.225	0.005	-	-	0	20	59	-	-
31713	0.220	0.004	40	10	30	-	-	87	172
31013	0.222	0.004	70	10	60	-	-	130	212
37	0.226	0.005	90	10	80	-	-	150	212
31113	0.256	0.005	70	10	60	-	-	109	147
31110	0.266	0.006	130	10	120	-	-	177	170
311	0.262	0.005	160	10	150	-	-	200	150
31114	0.255	0.005	190	10	180	-	-	225	135
3813	0.300	0.005	40	10	30	68	115	-	-
3814	0.307	0.006	70	10	60	-	-	92	95
3413	0.305	0.006	130	10	120	-	-	146	77
3411	0.299	0.006	190	10	180	-	-	200	61
3311	0.346	0.007	30	10	20	-	-	35	46
3612	0.353	0.008	50	10	40	-	-	58	55
339	0.351	0.008	70	10	60	-	-	74	42
3314	0.356	0.007	90	10	80	-	-	91	33
3312	0.357	0.008	-	10	hydrostatic	-	-	P^*	
								118	0
3710	0.385	0.009	40	10	30	-	-	37	22
379	0.387	0.009	50	10	40	-	-	46	19
3711	0.385	0.007	60	10	50	-	-	54	13
3712	0.382	0.007	-	10	hydrostatic	-	-	P^*	
								69	0

262

263 For both hydrostatic and triaxial compression tests, the confining pressure P_c (kerosene) and the
264 pore fluid pressure P_p (deionized water) were first slowly increased to their target values using
265 servo-controlled pumps (see Table 2 for values). A fixed pore fluid pressure P_p of 10 MPa was
266 used for all experiments and we assume a simple effective pressure law $P_{\text{eff}} = P_c - P_p$, operative

267 for rock failure under static conditions, as shown for sandstones by Baud et al. (2015) in the
268 brittle and ductile regimes. For the hydrostatic tests, the effective pressure P_{eff} was increased in
269 small steps from its initial value of 2 MPa until the critical stress state for the onset of grain
270 crushing P^* (Zhang et al., 1990), or the upper pressure limit of the press ($P_c = 200$ MPa), was
271 reached. We waited for microstructural equilibrium at each step before increasing the confining
272 pressure further. To do this, we assume that microstructural equilibrium was achieved when the
273 rate of the pore volume change (recorded by monitoring the displacement of the piston in the
274 pore pressure intensifier) was lower than 10^{-2} s^{-1} . The amount by which P_{eff} was increased at each
275 step varied from 1 to 10 MPa depending on the time necessary to reach microstructural
276 equilibrium at the previous step. For triaxial experiments, once the targeted effective pressure P_{eff}
277 was reached (i.e., hydrostatic pressurization, see Table 2 for values), the system was left to
278 equilibrate until the pore fluid change was lower than 10^{-2} s^{-1} . Then, at constant P_{eff} , the sample
279 was loaded as the upper piston was lowered at a fixed servo-controlled rate corresponding to a
280 nominal strain rate of 10^{-5} s^{-1} . Considering the range of permeabilities of the synthetics (from 10^{-13}
281 to 10^{-11} m^2 , measured at a P_c of 1 MPa), the strain rate applied during triaxial compression was
282 low enough to ensure drained conditions (i.e., the product of the strain rate and the Darcy
283 timescale $Da = t_D \dot{\epsilon} = \mu_f L^2 / (k \Delta P)$ is much less than unity (Heap & Wadsworth, 2016)).

284 During all tests, a linear variable differential transformer (LVDT) monitored the position of the
285 upper piston with an accuracy of $0.2 \text{ }\mu\text{m}$, thus giving access to displacement, and a pressure
286 probe in the axial pressure circuit provided a measurement of the applied axial force. Using the
287 initial dimensions of the sample, axial stress and strain were obtained. Porosity change was
288 provided by the conversion of the pore volume change given by the displacement of the piston in
289 the pore pressure intensifier (the system was calibrated to take into account the compressibility
290 of the pore fluid (water)). Finally, acoustic emission (AE) activity was recorded using a USB AE
291 Node from Physical Acoustics and a piezoelectric transducer (a micro80 sensor from Physical
292 Acoustic with a bandwidth of 200-900 kHz) attached to the lower piston. AE activity was
293 monitored using the software AEwin and we set the detection threshold for an AE hit at 28 dB.
294 The AE energy is determined by AEwin as the area under the received waveform. Experiments
295 were stopped after the samples were unloaded at the same servo-controlled rate as loading and
296 the pressures removed slowly so as not to damage the samples. For experiments conducted in the
297 brittle regime, samples were unloaded following macroscopic failure. In the ductile regime,

298 samples were deformed up to a 4% axial strain if mechanical data indicated strain localization
299 (i.e., if there were small stress drops in the mechanical data) and up to 6% if not. Based on
300 previous studies on natural rocks (Baud et al., 2004), these strains are considered suitable for
301 subsequent observation of microstructural deformation features. To gain insights into the
302 microstructure, polished thin sections were prepared using selected deformed samples and
303 micrographs of the thin sections were obtained using a SEM.

304 **4 Mechanical data**

305 In this study, compressive stress and compactive strain, i.e., shortening for axial strain and
306 decreasing volume for volumetric strain, will be conventionally taken as positive. The maximum
307 and minimum applied principal compressive stresses are referred to as σ_1 and σ_3 , respectively,
308 the differential stress as $Q = \sigma_1 - \sigma_3$ and the effective mean stress as $P = (\sigma_1 + 2\sigma_3)/3 - P_p$.

309 4.1 Results of the hydrostatic and triaxial tests

310 Representative data for the mechanical response of sintered glass bead samples to hydrostatic
311 loading are presented in Figure 2. The hydrostatic experiment was conducted on a synthetic
312 sample with a porosity and mean grain diameter of 0.38 and 0.2 mm (3714 in Table 2) and the
313 mechanical data are plotted alongside the corresponding AE activity (dashed purple). The gray
314 dashed curve in Figure 2 presents the mechanical data from an experiment performed on a
315 sample with a very similar porosity and the same grain diameter to show the reproducibility
316 (3712 in Table 2). The porosity reduction in percentage corresponds to the absolute loss of
317 porosity. In Figure 2, the hydrostats present the following characteristic phases. (1) The initial
318 evolution of porosity with increasing effective pressure is non-linear. The duration of this first
319 stage varies from sample to sample, as demonstrated by the difference between the black and the
320 gray curves, and is positively correlated to porosity. (2) The second phase consists of a linear
321 decrease of porosity as a function of increasing effective mean stress, which is characteristic of
322 poroelastic behavior. Almost no AEs are recorded during the initial non-linear and linear
323 portions of the hydrostatic experiment (Figure 2). However, a sudden increase in cumulative AE,
324 associated with a sharp breaking point in the mechanical data, indicated as P^* , marks the
325 transition to (3) a third phase characterized by a large decrease in porosity (of about 0.1) at
326 constant effective pressure. For siliciclastic rock, this inflection on the hydrostat followed by a

327 large porosity reduction is characteristic of inelastic compaction by delocalized grain crushing
328 (Zhang et al., 1990), P^* therefore represents the critical stress for the onset of grain crushing.
329 After equilibrium of the system has been reached for the critical state of stress P^* , further
330 increase of the effective stress is accompanied by hardening. Samples submitted to hydrostatic
331 loading (up to the maximum capability of the pressure cell; i.e., $P_c = 200$ MPa) presented
332 effective pressure-porosity reduction curves similar to the hydrostats presented in Figure 2.

333 Triaxial compression experiments were conducted at effective pressures P_{eff} ranging from 20 to
334 180 MPa and, depending on the effective pressure P_{eff} , led to either brittle or ductile failure. A
335 representative curve for the mechanical data and AE activity corresponding to failure by
336 dilatancy and shear fracture formation (i.e., brittle behavior) is presented in Figure 3. The stress-
337 strain curve can be divided into three parts. (1) First, the axial strain increases linearly with the
338 differential stress and very few AEs are recorded. (2) Second, a sudden increase in the AEs
339 accompanies a small decrease in the slope of the stress-strain curve, which corresponds to the
340 onset of dilatancy (Figure 3). (3) Finally, as the AE bursts, the differential stress reaches a peak
341 (marked as σ_v) and then drops to a residual value. Among the synthetic samples deformed under
342 triaxial conditions, samples of porosity below 0.26 demonstrated brittle behavior up to effective
343 pressures of 30 to 60 MPa, depending on their grain diameter. The peak stresses σ_v for samples
344 deformed in the brittle regime are compiled in Table 2.

345 Figure 4 shows the third type of mechanical data obtained in this study, i.e., mechanical data for
346 triaxial tests conducted on synthetic samples at relatively high confinement and which failed by
347 shear-enhanced compaction. On Figure 4, the stress-strain curve can be delimited into two main
348 portions. (1) As we first load the sample, axial strain increases linearly with differential stress
349 and no AEs are recorded. (2) Then, a subtle decrease in the slope of the stress-strain curve takes
350 place as the AEs start to increase at the onset of shear-enhanced compaction C^* (Wong et al.,
351 1997). Finally, the stress-strain curve reaches a plateau punctuated by stress drops that correlate
352 to spikes in the AEs. These stress drops are suggestive of the formation of compaction bands
353 (Baud et al., 2004). All samples deformed in the range of effective pressures corresponding to
354 shear-enhanced compaction demonstrated such stress drops, sometimes accompanied by strain
355 hardening. The critical stresses C^* for samples deformed in the ductile regime are compiled in
356 Table 2.

357 An overview of the mechanical data collected for this study is presented in Figure 5. Mechanical
358 data for triaxial experiments are compiled with their corresponding hydrostatic pressurization
359 curves, for samples of porosity ranging from 0.18 to 0.38 and for mean grain diameters of 1.15
360 (blue), 0.5 (green) and 0.2 (orange) mm. At low and high effective pressures, the mechanical
361 data present the phases described for Figure 3 and Figure 4, respectively. The mechanical data
362 for triaxial compression follow the hydrostat in the poroelastic domain. The deviation from the
363 hydrostat marks the transition to inelastic deformation, either by dilatancy (increase in porosity)
364 or by shear-enhanced compaction (porosity reduction). Some samples deformed in a mode that
365 cannot be easily defined as “brittle” or “ductile”. The mechanical data for the experiments
366 performed at effective pressures of 30, 60, and 90 MPa in Figure 5(c) are representative of this
367 hard-to-define failure mode, which we will refer to as transitional. For all the experiments, peak
368 stresses and critical stresses were identified to map out the failure envelopes of our synthetic
369 samples (Table 2).

370 4.2 Critical stress states: effect of porosity and grain size

371 For all experiments, critical stress values were identified in accordance with the failure mode
372 (Figures 2, 3 and 4). Regarding experiments conducted in the brittle and transitional regime,
373 critical stresses P and Q were respectively identified at the peak and at the first stress drop. For
374 experiments conducted in the ductile regime, the stresses P and Q were identified at the deviation
375 from the hydrostat, i.e., at the onset of shear-enhanced compaction C^* (Figure 5). Table 2
376 includes all experiments for which the critical stresses could be clearly identified using
377 mechanical data and AE measurements.

378 When plotted in the effective mean stress P - differential stress Q space, peak stresses map out
379 the brittle failure envelope (open symbols) and C^* values map out the compactive yield envelope
380 (solid symbols). When it could be measured, P^* anchors the yield envelope on the x-axis (P^*
381 could not be measured for all combinations of porosity and grain size due to the pressure
382 limitations of the triaxial press). The experiments that exhibited a transitional failure mode exist
383 where the brittle envelope meets the yield cap. Figure 6 presents a compilation of failure
384 envelopes for our synthetic samples. Overall, several common features of the envelopes should
385 be noted. First, brittle failure of these porous materials is restricted to a small area of the stress
386 space. Second, regarding compactive yield caps, P and Q are linearly correlated, which is

387 particularly clear for the caps on Figure 6(c). Third, shear-enhanced compaction occurs over a
388 wide range of stress states. For a given grain diameter, porosity is seen to influence compactive
389 yield behavior. Broadly speaking, the higher porosity, the lower the stress that required for
390 inelastic yield. For example, samples of mean grain diameter of 1.15 mm (Figure 6(a)) submitted
391 to triaxial compression under an effective pressure of 120 MPa yielded at 23 and 35 MPa of
392 differential stress for initial porosities of $\phi = 0.30$ and $\phi = 0.26$, respectively. For samples of
393 mean grain diameter of 0.5 mm (Figure 6(b)), triaxial compression under an effective pressure of
394 100 MPa resulted in critical differential stresses of 100 MPa for $\phi = 0.26$ compared to 52 MPa
395 for $\phi = 0.30$. Finally, for synthetic samples of mean grain diameter of 0.2 mm (Figure 6(c))
396 deformed at $P_{\text{eff}} = 60$ MPa, inelastic yielding took place at 223 MPa when $\phi = 0.22$, 147 MPa
397 when $\phi = 0.26$, 95 MPa when $\phi = 0.30$, and 42 MPa when $\phi = 0.35$. In summary, increasing the
398 porosity from 0.22 to 0.35 decreased the stress required for C^* by more than a factor of five
399 (Table 2).

400 All else being equal, grain diameter also exerts an important influence on the compactive
401 behavior. Figure 7(a) and Figure 7(b) presents a compilation of caps for $\phi = 0.30$ and 0.25-0.26,
402 respectively, for three different mean grain diameters (1.15 mm in blue, 0.5 mm in green, and 0.2
403 mm in orange). For $\phi = 0.25-0.26$ and $P_{\text{eff}} = 60$ MPa, shear-enhanced compaction started at 59,
404 97 and 147 MPa for monodisperse samples of 1.15, 0.5 and 0.2 mm of mean grain diameter
405 respectively. For $\phi = 0.30$ and $P_{\text{eff}} = 120$ MPa, C^* was reached at 23, 39 and 77 MPa for samples
406 of 1.15, 0.5 and 0.2 mm of mean grain diameter respectively. In summary, increasing the mean
407 grain diameter from 0.2 to 1.15 mm decreased the stress required for C^* by more than a factor of
408 two (Table 2).

409 **5 Microstructural observations**

410 Representative SEM micrographs for the microstructure of a synthetic sample after hydrostatic
411 compression to beyond P^* are presented in Figure 8. The images correspond to a sample with an
412 initial porosity and mean grain diameter of 0.357 and 0.2 mm (sample 3312; see Table 2),
413 respectively, deformed up to a porosity reduction of 0.16. The corresponding mechanical data are
414 presented in Figure 5(i). At the lowest magnification, the thin section shows extensive
415 delocalized grain crushing. Zooms into the microstructure confirm that most grains were entirely
416 crushed and that the resulting shards progressively filled the porosity as the sample compacted.

417 Uncrushed glass beads allow for the observation of cross-cutting microfractures propagating
418 from grain to grain. On the basis of 2D image analysis (using ImageJ), the local final porosity
419 was estimated. The least and most damaged areas yielded porosity values around 0.30 and 0.11,
420 respectively.

421 Representative SEM for the microstructure of a synthetic sample triaxially deformed to beyond
422 C^* are presented in Figure 9. The images correspond to a sample with an initial porosity and
423 mean grain diameter of 0.35 and 0.2 mm (sample 3314; see Table 2), respectively, triaxially
424 deformed at an effective pressure of 80 MPa up to an axial strain of 3.5%. The corresponding
425 mechanical data are presented in Figure 5(i). As suggested by the small stress drops punctuating
426 the stress-strain curve beyond C^* and the corresponding bursts of AE activity (Figure 5(i)), the
427 sample contains evidence of compaction localization. Several discrete bands were observed in
428 the upper and lower parts of the thin section, i.e., at the extremities of the sample, and one cross-
429 cutting discrete band was observed in the middle (Figure 9). The compaction band in the middle
430 is 2-5 grains wide – i.e., thickness of 0.4 to 1 mm – and is oriented normal to the direction to the
431 maximum principal stress σ_1 . Note that the band appears to avoid the porosity patches, and thus
432 slaloms between them. A zoom on the band shows extensively fractured and compacted glass
433 beads (Figure 9). Shards resulting from the fracturing and crushing fill the porosity within the
434 band, reducing the porosity from 0.35 to approximately 0.27 (estimation based on 2D
435 measurements on the SEM images using ImageJ). The grains are unaffected outside the
436 compaction band, and the porosity was estimated using ImageJ to be similar to that measured in
437 the laboratory (0.36).

438 **6 Discussion**

439 6.1 Suitability of sintered glass beads as crustal analogues

440 Synthetic granular rocks such as our sintered soda-lime silica glass beads provide a well-
441 characterized two-phase medium for investigating mechanical processes in siliciclastic rock. Our
442 motivation for using synthetic samples was to quantify the influence of individual
443 microstructural parameters (e.g., porosity and grain diameter) on the mechanical behavior of
444 granular rock by keeping all other parameters constant. In natural sandstones, for example,
445 samples with different porosities may also be characterized by different grain and pore sizes and

446 distributions. However, understanding the mechanical behavior of sandstones using fused glass
447 bead synthetics hinges on the comparability of natural and synthetic sandstones. Before
448 discussing the suitability of sintered glass beads as analogs for crustal rocks, we will briefly
449 mention the differences between the microstructure of our synthetic samples and natural crustal
450 rocks. First, the grain size distribution of all the synthetic samples is monomodal and closely-
451 clustered (Figure 1a). Natural sandstones, for example, can be characterized by polydisperse
452 grain size distributions. Second, the grains in our synthetic samples are spherical and have
453 identical physical and mechanical properties, while natural sandstones often contain non-
454 spherical grains and different types of grains (e.g., quartz and feldspar). Finally, natural
455 sandstones can contain cement (e.g., clay cement between grains). Our synthetic samples do not
456 contain cement (Figure 1c and 1d). To compare our synthetic samples to natural sandstones, we
457 selected sandstones whose porosity and grain diameter lie in the range covered by our synthetic
458 samples (our porosity range is 0.18-0.38 and our grain diameter range is 0.2-1.2 mm). We chose
459 Boise sandstone (porosity of 0.35 and average grain radius 0.46 mm; Bedford et al., 2019; Zhang
460 et al., 1990), Idaho Gray sandstone (porosity of 0.36 and average grain radius 0.7 +/- 0.2 mm;
461 Bedford et al., 2019) and Bentheim sandstone (porosity of 0.23 and average grain radius 0.3 mm;
462 Klein et al., 2001). Bentheim sandstone is a monomineralic sandstone with a narrow grain size
463 distribution. Due to its homogeneous mineralogy and well sorted grain size, it has been used in
464 many rock deformation studies, notably on strain localization (Baud et al., 2004; Tembe et al.,
465 2006, 2008; Wong et al., 2001). It is therefore an ideal sandstone to compare with our synthetic
466 samples. We compiled mechanical data from hydrostatic and triaxial experiments conducted in
467 conditions similar to those imposed during experiments on the synthetic samples, i.e., at room
468 temperature on water-saturated samples at a fixed pore pressure of 10 MPa. In Figure 10, we plot
469 selected mechanical data from our database alongside mechanical data from hydrostatic
470 experiments (a) and triaxial experiments (b) conducted on Boise, Idaho Gray and Bentheim
471 sandstones.

472 Regarding the hydrostatic behavior. (Figure 10(a)), we first note that, during the initial loading
473 and increase of the effective pressure up to P^* , Boise, Idaho Gray, and the synthetic sample with
474 a porosity of 0.35 present porosity reduction curves that are almost identical. The characteristic
475 “tail” at the beginning of the hydrostat is typically attributed to the closure of microcracks
476 (Walsh, 1965). Assuming our sintered glass beads do not contain microfractures at the beginning

477 of the hydrostatic pressurization, as indicated from our microstructural analysis of the intact
478 material, we attribute the non-linear initial portion of the hydrostat to grain rotations and
479 rearrangements, which is corroborated by the positive correlation between the size of the tail (i.e.,
480 the amount of compaction) and the porosity of the sample. Qualitatively speaking, the
481 compaction curves evolve differently beyond P^* . While a progressive inflection and strain
482 hardening is observed for both Boise and Idaho Gray sandstones, P^* manifests as a sharp
483 breaking point beyond which the synthetic sample undergoes a porosity reduction of about 0.1
484 without hardening. Zhang et al. (1990) demonstrated that the first inflection in the hydrostat
485 corresponds to the inception of grain crushing and that increasing the effective pressure beyond
486 this point exacerbates the deformation. This gradual behavior is absent for the synthetic sample,
487 which experiences extensive grain crushing and porosity loss at the state of stress just higher
488 than P^* . The observation of extensive grain crushing at a stress just above P^* is similar to that
489 reported for Bentheim sandstone, a rock that also contains a closely-clustered monomodal grain
490 size distribution (Baud et al., 2006)(Figure 10(a)(c)). Examination of the microstructure showed
491 that very few areas in the sample remained uncrushed (Figure 8). Contrary to most natural
492 sandstones (e.g., Caruso et al., 1985), our synthetic rocks are composed of monomodal
493 distributions of uniform grains of identical elastic properties. Thus, the force chains induced in
494 the granular framework during loading are expected to be more homogeneously distributed in
495 our monodisperse synthetic samples (Guéguen & Boutéca, 2004; Papadopoulos et al., 2018). As
496 a result of this homogeneity, when the externally applied effective pressure reaches the critical
497 value P^* , the normal forces induced at the grain contacts must reach the critical value at the same
498 time, and most grains are thus crushed at the same state of stress. Quantitatively, the effective
499 stress at which the onset of grain crushing (P^*) occurs is higher in our synthetic rock (120 MPa)
500 than it is in Boise (75 MPa) and Idaho Gray (55 MPa) sandstones. Several differences between
501 the synthetic and natural samples could be considered to explain the higher P^* in the synthetic
502 samples. First, Boise and Idaho Gray sandstone have a larger average grain diameter. Second,
503 Boise and Idaho Gray sandstone contain minerals other than quartz that are characterized by
504 lower values of fracture toughness, such as feldspar (Atkinson & Meredith, 1987). However,
505 although the mineral composition of the two sandstones is very close, the P^* of Boise sandstone
506 is about 25 MPa higher than that of Idaho Gray sandstone (Figure 10(a)). Therefore, we

507 speculate that the much higher P^* for the synthetic samples could arise from the difference in
508 grain diameter (the smaller the grains, the stronger the sample).

509 We will now compare the behavior of natural sandstones with the one of our synthetic samples
510 when subject to triaxial compression. Figure 10(b) presents mechanical data from triaxial tests
511 conducted on a synthetic sample with a porosity of 0.3 (orange line) and on Bentheim sandstone
512 (Baud et al., 2004) (black line) under an effective pressure of 120 MPa. Qualitatively, the stress-
513 strain curves are very similar. Quantitatively, C^* is about 50 MPa higher in Bentheim sandstone
514 than in the synthetic sample and is likely the result of the difference in porosity and grain size
515 (both higher for the synthetic sample). Beyond C^* , the mechanical data for both samples show
516 small stress drops, suggesting that the samples failed by development of compaction localization,
517 as shown by Baud et al. (2004).

518 Although studies on the mechanical behavior of tuffs under hydrostatic and triaxial compression
519 are comparatively rare (e.g., Heap et al., 2015a; Zhu et al., 2011), our new data for sintered
520 synthetic samples are also relevant to welded granular materials. Indeed, in the case of welded
521 tuffs – the product of the deposition of hot volcanic ash and lapilli – our samples are an exact
522 analog, where volcanic welding and glass sintering are fundamentally the same dynamic process
523 (Wadsworth et al., 2019). We note that in nature, welding of tuff can be associated with
524 internally porous clasts, vesiculation or resorption, viscosity or temperature gradients, and shear,
525 all of which can conspire to complicate microstructure relative to sintered glass beads, but that
526 nevertheless, the broad theme of mechanical results given here are relevant in volcanic
527 environments as well as other crustal scenarios.

528 6.2 Deconvolution of microstructural parameters

529 In nature, porosity is often related to grain diameter. However, numerous other parameters such
530 as grain sorting, shape, orientation, location of cements, and the extent of compaction, can
531 influence the bulk porosity of a porous rock (Rogers & Head, 1961; Scherer, 1987). One of the
532 results of this multi-component control on porosity is that crustal rocks that show a low porosity
533 are not necessarily composed of small grains and vice versa. In fact, crustal rocks span a wide
534 range of porosity-grain size combinations and can demonstrate complex porosity-grain size
535 relationships. For illustration, we have compiled the porosity and the mean grain diameter of 19
536 natural sandstones that have repeatedly been used in laboratory studies (Figure 11). Porosity

537 values are in the range 0.03-0.38 and mean grain diameter values are in the range 0.075-0.92 mm.
538 If we consider only this subset of natural sandstones, several observations can be made: (1) for
539 the few sandstones with a porosity higher than 0.25, the mean grain diameter varies over a range
540 twice as large as sandstones of lower porosity (0.2-0.9) and (2) for sandstones of porosity lower
541 or equal to 0.25, mean grain diameter is lower than 0.5 mm and clusters around 0.28 mm; such
542 that the grain size effect on porosity becomes attenuated as diagenesis progresses as pore and
543 pore throats are compacted. By compiling these data, we can conclude that (3) sandstones that
544 come from a single formation (see for example Buntsandstein, Fontainebleau or Boise
545 sandstones) can cover a large range in grain diameter and porosity, within which variations in
546 grain diameter appear to occur independently from variations in porosity and vice versa. For
547 example, the porosity of Fontainebleau sandstone can vary greatly (0.03-0.28), while the mean
548 grain diameter (0.250 mm) remains constant (Bourbie & Zinszner, 1985; Lindquist et al., 2000;
549 Louis et al., 2007). It is important to note that there is some bias in sample selection for
550 laboratory studies, such that crustal rocks with a low variability within a unit are favored so that
551 repeat measurements can be made (e.g., Menéndez et al., 1996). We can find that field studies
552 reported a much wider range of average grain size and porosity for sandstones, which can be
553 encountered as very fine-grained (0.0625 mm; Selley, 2004) and can grade up to very coarse-
554 grained and pebbly (2 mm; Selley, 2004), with well to poorly-sorted distributions and porosity
555 ranging over more than one order of magnitude 0.02-0.30 (e.g., Morrow, Nugget, Bartlesville,
556 and Grimsby sandstone; Nelson & Kibler, 2003). For instance, anomalously high porosities were
557 reported in a significant number of deeply-buried (> 4 km) reservoir sandstones worldwide (e.g.,
558 porosity in the range 0.24-0.40 in the Tertiary channel-fill sandstone, offshore west Africa; Bloch
559 et al., 2002).

560 Deconvolving structural parameters such as porosity and grain size is necessary to derive
561 definitive constraints on the micromechanics of compaction from experimental studies. Indeed,
562 while the importance of porosity in controlling yield strength is well-established for crustal rocks
563 (e.g., Wong & Baud, 2012), the independent effect of a change of grain or pore size is only
564 poorly investigated (Atapour & Mortazavi, 2018). As revealed when compiling grain diameter
565 and porosity for laboratory sandstones (Figure 11), it is possible that the approximate consistency
566 in the grain diameter has meant that its influence on compactive yield strength has been masked
567 in rock mechanics study thus far. Sintering glass beads has allowed us to effectively deconvolve

568 the effect of porosity and grain diameter and other microstructural factors, to parameterize
569 specifically for their importance.

570 6.3 Influence of porosity and grain size on compactive yield

571 Our synthetic samples were designed and prepared to maximize microstructural homogeneity.
572 Yet, they present heterogeneities in the porosity distribution and in the geometry of grain-to-
573 grain contacts (Figure 1). Similar porosity clusters have been reported in Bleurswiller sandstone,
574 the mechanical compaction of which has been investigated in several studies (Baud et al., 2015;
575 Fortin et al., 2005, 2006; Tembe et al., 2008). These published works have demonstrated the
576 importance of porosity clusters on the micromechanical processes leading to inelastic
577 compaction. Indeed, while yield envelopes reported for natural sandstones are typically elliptical
578 in shape (Baud et al., 2006; Guéguen & Fortin, 2013; Wong et al., 1997), Bleurswiller sandstone
579 presents an approximately linear yield cap (Baud et al., 2015). The linear yield envelope of
580 Bleurswiller was fitted by Baud et al. (2015) using a dual-porosity micromechanical model for
581 cataclastic pore collapse. The pore collapse model, initially developed for dual-porosity
582 carbonates, treats the pore size distribution as bimodal with the pore space divided into
583 microporosity and macroporosity (i.e., a porosity cluster) (Zhu et al., 2010). Assuming the matrix
584 into which porosity clusters are embedded fails according to the Coulomb criterion, the pore
585 collapse model predicts that a porosity cluster collapses when the stress field in its vicinity
586 attains the critical state according to the Coulomb criterion, which results into a linear
587 dependence of the differential stress Q at the yield point C^* with the effective stress P (Baud et
588 al., 2015). Although our yield caps that include P^* appear linear, further microstructural analysis
589 need to be done to identify the micromechanical process and clarify the role of pore collapse in
590 the failure of our synthetic samples.

591 The pore space heterogeneities of our synthetic samples appear to influence the micromechanics
592 of failure. Yet, we believe they do not prevent us from discussing the relative influence of bulk
593 porosity on the compactive yield behavior. A compilation of six yield envelopes for synthetic
594 samples of porosity of 0.25 and 0.30 and of mean grain diameter of 0.2, 0.5 and 1.15 mm is
595 presented in Figure 12. All of the compactive yield caps are linearly shaped with a negative slope.
596 Overall, we observed that, for a given grain diameter, increasing porosity decreases the stress at
597 which C^* occurs and that a difference in porosity of 0.01 results in a difference in C^* of

598 approximately 8% +/- 5%. This appears to apply whatever the grain diameter is in the range
599 0.15-1.3 mm. Indeed, at an effective pressure of 60 MPa, an increase of porosity from 0.26 to
600 0.30 (+0.04), decreases the stress at which C^* occurs from 59 to 43 MPa (-28%), 97 to 70 MPa (-
601 28%) and from 147 to 95 MPa (-35%) for mean grain diameter of 1.15, 0.5 and 0.2 mm,
602 respectively.

603 As for porosity, grain size was experimentally identified to have a first-order control on
604 compactive yield of porous siliciclastic rock (Wong, 1990; Wong et al., 1992, 1997; Zhang et al.,
605 1990) and has been included as a parameter in micromechanical models (e.g., Sammis & Ashby,
606 1986; Zhang et al., 1990). In the Hertzian fracture model of Zhang et al. (1990), average grain
607 radius acts as a scaling parameter for the critical pressure P^* with an equal weight than porosity.
608 This model was successfully applied to a number of natural and synthetic sandstones and
609 unconsolidated materials (David et al., 1998; Wong et al., 1997) with some scatter. However,
610 although a consensus on the key influence of grain size has been reached, compactive yield caps
611 compilations for sandstones often only discuss the influence of porosity. Figure 13 shows a
612 compilation of compactant failure caps for Boise and Bleurswiller sandstones (data from Cheung
613 et al., 2012) and sintered samples that only differ from one another in terms of their average
614 grain diameter. If we consider only the yield caps of the synthetic samples, we observe that, all
615 else being equal, an increase in average grain diameter from 0.2 to 0.5 mm (+130%) or from 0.5
616 to 1.15 mm (+150%) shifts the stress at which C^* occurs to values approximately 2 times lower
617 (-50%) (Figure 13). Moreover, the difference in C^* that results from a change in grain diameter
618 remains approximately the same whatever the porosity. Thus, our data show that an increase in
619 average grain diameter by a factor of 2 results in a decrease in the stress to reach C^* of
620 approximately 50 +/- 5%. As for Boise and Bleurswiller sandstone, they are similar in
621 mineralogy and porosity but, although both their grain diameter distributions present a peak at
622 125 μm , the former has a wider sorting that extends up to 725 μm . Despite significantly different
623 grain sorting, their compactive yield caps for the onset of shear-enhanced compaction are very
624 similar, albeit slightly different in shape with a more linear cap for Bleurswiller sandstone. The
625 caps of our synthetics are similar in shape to those of the natural sandstones but are mapped out
626 at very different stress states (Figure 11). Tembe et al. (2008) reported that Bentheim sandstone,
627 although similar to Boise and Bleurswiller sandstones in terms of porosity, presents a compactive
628 yield cap characterized by higher stresses. Indeed, the abundance of secondary minerals (feldspar,

629 oxide and mica) in Boise and Bleurswiller compared to Bentheim (>99% quartz) likely causes
630 the decrease in the compactive yield stresses for Boise and Bleurswiller sandstones. Similarly,
631 since Bleurswiller and Boise sandstones present a grain diameter distribution with a peak at 125
632 μm , we would expect their compactive yield caps to be mapped out at higher stresses than the
633 caps for the synthetic samples that have grain diameter distributions with peaks at 200, 500 and
634 1150 μm (Figure 13). The discrepancy in compactive yield stresses between Boise and
635 Bleurswiller sandstones and the synthetic samples can be attributed neither to porosity nor to
636 grain size, but possibly to the presence of cement and of secondary minerals other than quartz
637 (feldspar, oxide and mica).

638 Overall, we varied grain diameter by one order of magnitude (Figure 11) and we see a large
639 effect of that variation on the yield compactive strength of our synthetic samples. Grain
640 diameters of natural sandstones can also vary by more than one order magnitude (Nelson &
641 Kibler, 2003), but the effect of that variation has not hitherto been deconvolved from other
642 microstructural factors. We thus conclude that, if grain size were to be accounted for
643 quantitatively, its effect would be similar to that of porosity. However, we observe, for the range
644 of porosity and grain diameter used herein, that the influence of porosity on compactive yield is
645 higher than the influence of grain diameter. Indeed, to cover a similar range in the stress space,
646 the average grain diameter of our synthetic samples was increased by up to 600 % (relative to the
647 lowest range we used, 0.15-0.25 mm) while bulk porosity was only increased by up to 120%
648 (relative to the lowest porosity we used, 0.18).

649 6.4 Compaction localization

650 For all of our synthetic samples deformed in the regime of shear-enhanced compaction,
651 mechanical data show stress drops of variable amplitude (Figure 5), suggesting that compaction
652 localization took place (Baud et al., 2004; Heap et al., 2015b; Louis et al., 2006). This
653 observation concurs with the general consensus that microstructural homogeneity promote strain
654 localization in granular materials (Katsman et al., 2005; Louis et al., 2009; Wang et al., 2005).
655 Indeed, Cheung et al. (2012) demonstrated that uniform grain size distribution promotes the
656 development of discrete compaction bands. As our synthetic samples are characterized by a
657 monodisperse distribution of grain size, we expected compactant deformation to localize in the
658 form of compaction bands. In Figure 10(c) and Figure 10(d), we juxtaposed a SEM micrograph

659 of a discrete compaction band in a synthetic sample and a micrograph of a discrete compaction
660 band in Bentheim (from Baud et al., 2004), respectively. The compaction bands present very
661 similar microstructural attributes (Figure 10(c)(d)). An important difference is that our
662 micrograph has been obtained on a sample of porosity of 0.35. To our knowledge, the range of
663 porosity over which compaction bands were reported in sandstones is approximately 0.13; 0.29
664 (Fossen et al., 2011; Schultz et al., 2010; Tembe et al., 2008). The mechanical behavior of
665 sandstones with a porosity higher than 0.29 at or near the brittle-ductile transition has been
666 studied (e.g., Bedford et al., 2019; Cheung et al., 2012; Wong et al., 1997) but high-porosity
667 sandstones typically used in laboratory often have polydisperse distributions of grain size (see
668 for example, Boise sandstone), which has been recognized to inhibit strain localization.
669 Therefore, the effect of porosity on the propensity for compaction localization may have been
670 masked by the influence of other structural parameters. Our new data therefore extend the upper
671 limit of porosity for which compaction localization has been observed to 0.35 and suggest that
672 compaction localization can occur in samples with a porosity up to 0.38 (the highest porosity of
673 our set of samples).

674 However, although numerical simulations suggested compaction localization could occur in sand
675 packs (Marketos & Bolton, 2009), experimental validation for the formation of compaction
676 bands in high-porosity granular aggregates such as unconsolidated sands has not been reported.
677 For example, Hangx and Brantut (2019) performed triaxial experiments on Ottawa quartz sand
678 with a porosity of 0.36 and did not observe strain localization in the compactant regime of
679 deformation. These authors proposed that the possibility for grain rotation and rearrangement –
680 permitted by the lack of cementation – allows grain failure to be accommodated and prevents
681 stress concentration to occur. Although our high-porosity synthetic samples do not have cement,
682 we show that they can develop compaction bands in the regime of shear-enhanced compaction.
683 Therefore, we speculate that the necks formed at grain contacts during sintering in our synthetic
684 samples act as the cement in consolidated sandstones and play a key role in controlling
685 compaction localization. To a first-order, the potential for compaction localization appears to be
686 controlled not by porosity, but by the granular/non-granular and/or unconsolidated/consolidated
687 nature of rock, which is intimately related to the degree of cementation at grain contacts and by
688 extension, in some cases, to porosity (Lemée & Guéguen, 1996). Additionally, if we consider
689 that the porosity of a loose packing of grains is approximately 0.38 +/- 0.01 (Johnson & Plona,

690 1982), the observation of discrete compaction bands in a synthetic sample of porosity of 0.35
691 suggests that even a small proportion of consolidated/cemented grain contacts could be sufficient
692 to trigger stress concentrations within aggregates and the formation of compaction bands.

693 **7 Crustal implications and concluding remarks**

694 Crustal rocks such as sandstones and tuffs, the primary microstructural elements of which are
695 comparable with our synthetic samples, occur as geological units in reservoirs, aquifers, fault
696 zones and in volcanic environments; settings where they typically undergo structural changes
697 due to geologic processes. Therefore, implications – and applications – of our results for natural
698 systems are broad. For example, in the context of hydrocarbon and/or geothermal reservoirs,
699 depletion-induced reservoir compaction is an ubiquitous phenomenon that eventually leads to
700 surface subsidence (Gambolati et al., 2006; Nagel, 2001). On assessing which sedimentary layer
701 compacts first and/or to the highest extent, unconsolidated upper formations and clay-rich
702 formations are usually considered as the best candidates. However, reservoir formations are often
703 only vaguely described as coarse- or fine-grained and grain size is rarely considered in numerical
704 terms (Sun et al., 2018b), even in geotechnical models predicting the extent of irreversible
705 compaction for the bulk reservoir (Buscarnera et al., 2020; Hol et al., 2018). Our new data
706 suggest that formations with large grain diameters, alongside those with a high porosity, could be
707 prime candidates for mechanical compaction and should therefore be considered when assessing
708 reservoir subsidence.

709 In volcanic contexts, inelastic compaction of edifice-forming rock (including non-volcanic
710 basement rocks) presumably acts as a driving force in the growth and destruction life-cycle of
711 large volcanoes (Bakker et al., 2015; Concha-Dimas et al., 2005; Heap et al., 2015c; Van Wyk
712 De Vries & Borgia, 1996), which involves episodes of spreading that eventually leads to
713 catastrophic collapses (Van Wyk De Vries & Francis, 1997). Since flank and/or edifice collapse
714 models often invoke a weak/ductile internal or basal unit to explain instability and collapse
715 (Ablay & Hürlimann, 2000; Morgan & McGovern, 2005; Voight, 2000), it is important to
716 understand what controls the mechanical behavior of porous rocks, especially considering that
717 porous volcanic rocks can also develop compaction bands (Heap et al., 2015b, 2020). Our
718 synthetic materials could help understand whether simple empirical or theoretical models can
719 effectively describe the relationship between grain size, porosity and compactive yield strength,

720 and thus give accurate predictions for the evolution of inelastic compaction and subsequent
721 subsidence and/or edifice spreading. Moreover, since our synthetic samples consist of a very
722 simplified two-phase medium, such laws can be easily tested against discrete element method
723 simulations of reservoir compaction (Alassi et al., 2006; Sun et al., 2018a) or volcanic collapses
724 (Harnett et al., 2018) for example.

725 Our approach has allowed us to study the influence of deconvolved microstructural attributes on
726 mechanical compaction. The set of mechanical and microstructural data we present show that the
727 failure mode of analog samples made of sintered glass beads transit from brittle at low
728 confinement to ductile with shear-enhanced compaction at high confinement. Compactive yield
729 caps are mapped out on a range of stress states comparable to those for natural crustal rocks (the
730 porosity and grain diameter of which are similar to those of our synthetic samples, i.e., 0.18-0.38
731 and 0.2-1.15 mm, respectively) and are linearly shaped when P^* is known and are likely linearly
732 shaped for the porosity-grain diameter combinations for which P^* could not be measured (due to
733 the pressure limit of the triaxial apparatus). Qualitatively speaking, mechanical and
734 microstructural data are very similar between the natural and synthetic samples. Regarding the
735 influence of porosity and grain size, we arrived at the following main conclusions. First,
736 increasing only porosity or only grain diameter decreases the stress at which the onset of shear-
737 enhanced compaction C^* occurs. Second, to increase the stress at C^* by 50%, porosity has to be
738 decreased – in isolation – by 0.06 (30% relative to the range 0.18-0.38) whereas average grain
739 diameter has to be decreased – in isolation – by 0.50 mm (53% relative to the 0.2-1.15 mm).
740 Although the influence of porosity can be regarded as higher than the influence of grain size, our
741 study demonstrates that, over the investigated range of porosity and grain diameter, they both
742 exert a first-order control on the mechanical compaction of natural crustal rocks, which can span
743 over a much broader range of porosity and grain diameters. Therefore, alongside porosity, grain
744 diameter should become a routinely measured structural parameter when dealing with the
745 mechanical compaction of natural crustal rocks.

746 Overall, we believe our study demonstrates the great suitability of sintered glass beads as crustal
747 rock analogs and the great opportunity they embody for studying microstructural parameters
748 such as porosity and average grain diameter in isolation. Since mixtures of glass beads of
749 different diameters can be prepared, variably polydisperse sintered samples can be synthesized
750 and used to investigate the influence of grain size distribution and polydispersivity on

751 mechanical and hydraulic behavior. Further, the addition of cement and/or other materials to the
752 glass bead mixtures could also be considered in order to sharpen our understanding of the
753 deconvolved influence of microstructural parameters on the mechanical and hydraulic properties
754 of crustal rocks.

755 **Acknowledgments and Data**

756 This paper has benefitted from constructive reviews by Douglas Schmitt, Sergey Stanchits and
757 one anonymous reviewer. Jérôme Fortin, Mai-linh Doan, Jérémie Vasseur and Dominique de
758 Ligny are thanked for the discussions. The authors thank Bertrand Renaudié for the preparation
759 of the samples and Gilles Morvan for his assistance using the SEM. The first author
760 acknowledges funding from the Doctoral School at the University of Strasbourg. The data
761 supporting the manuscript's analysis and conclusions is available at
762 <https://doi.org/10.6084/m9.figshare.13208192> .

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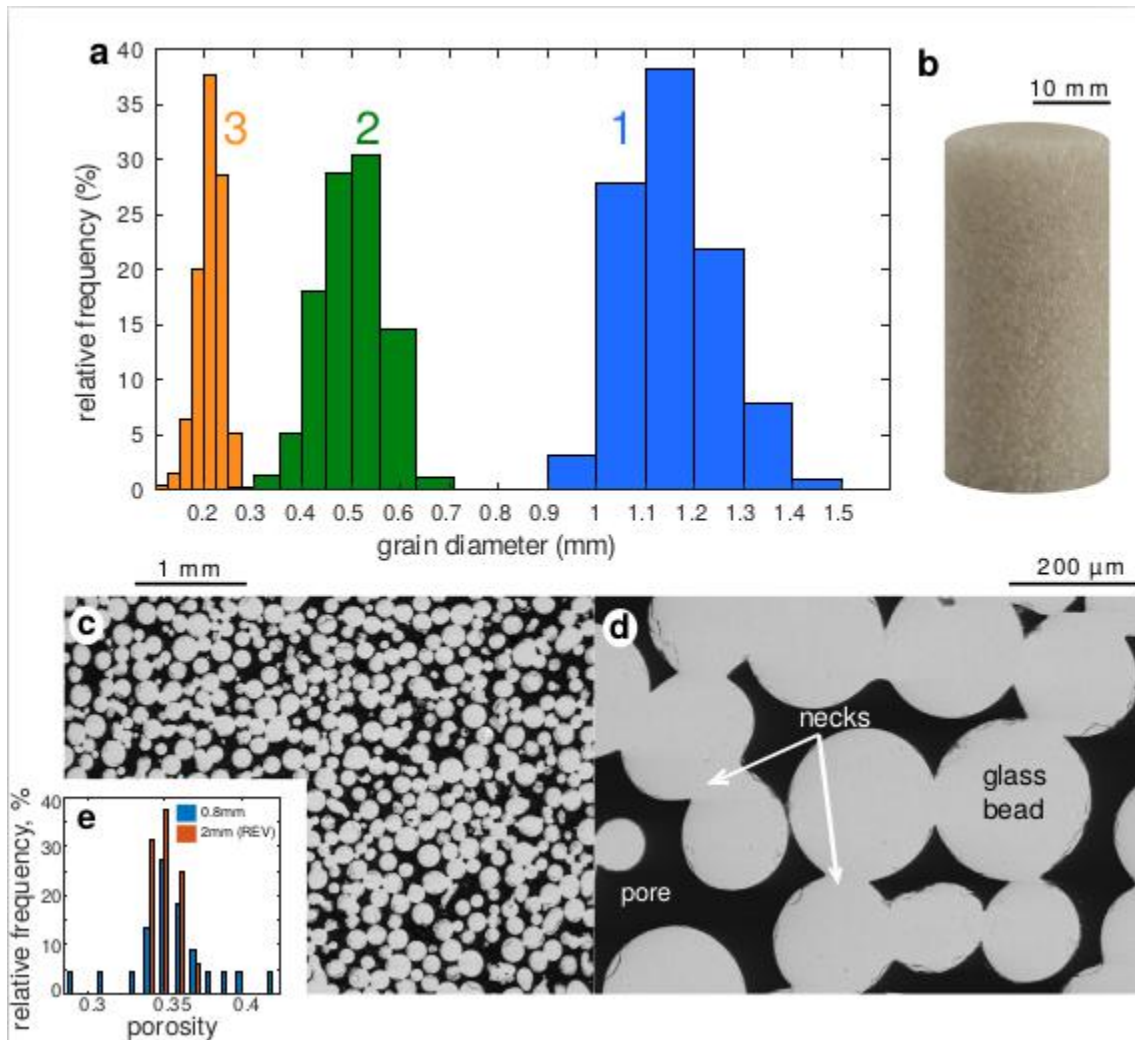
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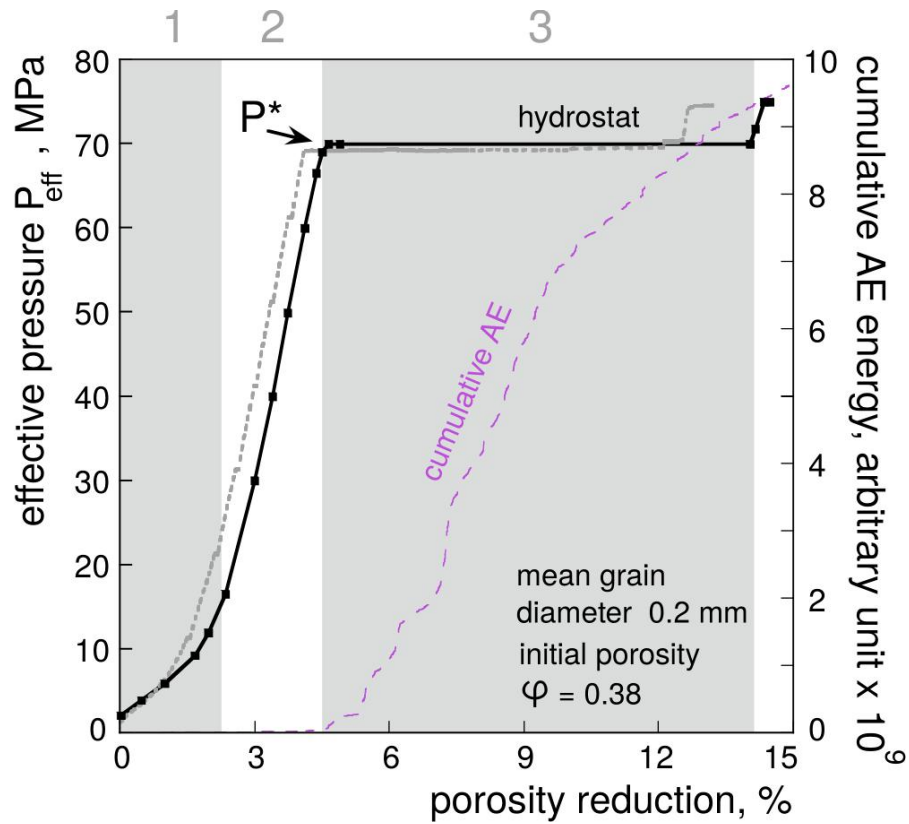
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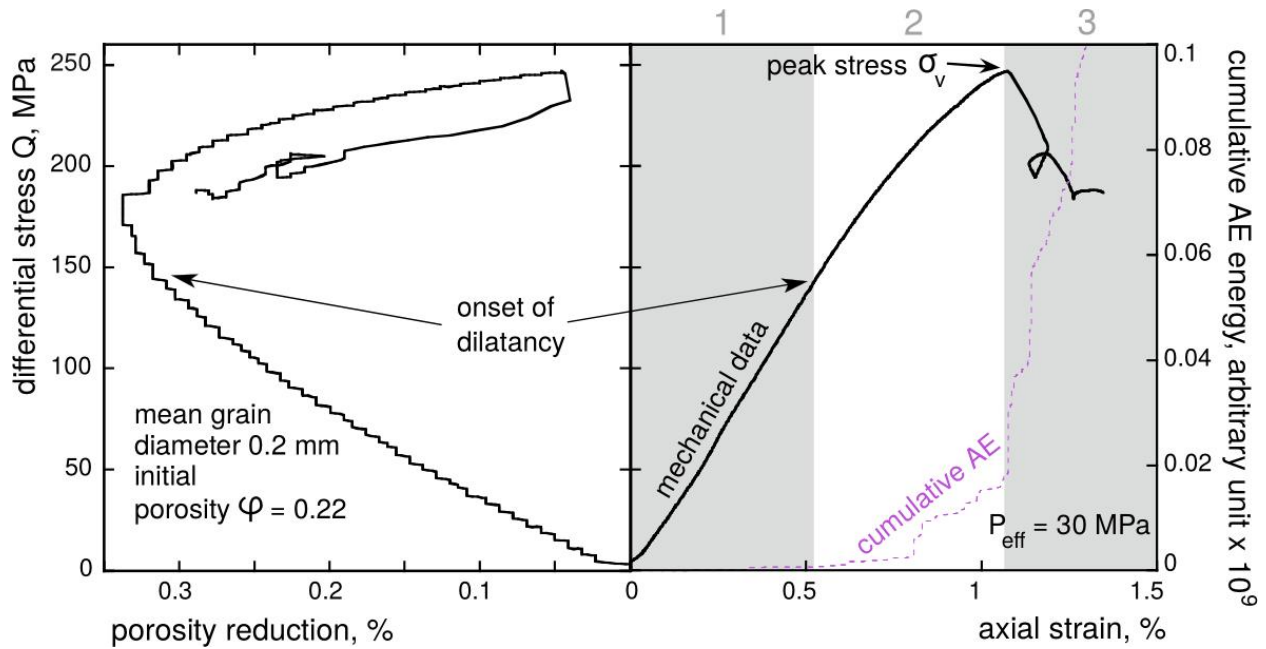
1114

1115 **Figure 1.** Microstructural description of the synthetic samples. (a) Grain diameter distributions
 1116 corresponding to the different mean grain diameter considered, 3: 0.15-0.25 mm (orange), 2: 0.4
 1117 0.6 mm (green), 1: 1.0-1.3 mm (blue). Although these distributions are not technically
 1118 monodisperse but monomodal, we herein use the term monodisperse to describe our samples. (b)
 1119 Photograph of a synthetic sample with a porosity of 0.35 and a mean grain diameter of 0.2 mm
 1120 and (c) corresponding scanning electron micrograph of its microstructure (black: porosity, gray:
 1121 glass). (d) Scanning electron micrograph showing the necks that have grown between initially
 1122 adjacent beads during sintering. (e) 2D porosity distributions measured for the same sample
 1123 using a window with a 0.8 mm edge-length (blue) or with a 2 mm edge-length (representative
 1124 elementary volume, red) using image processing program ImageJ. Frequencies cluster around
 1125 0.35, which corresponds to the porosity measured in laboratory.



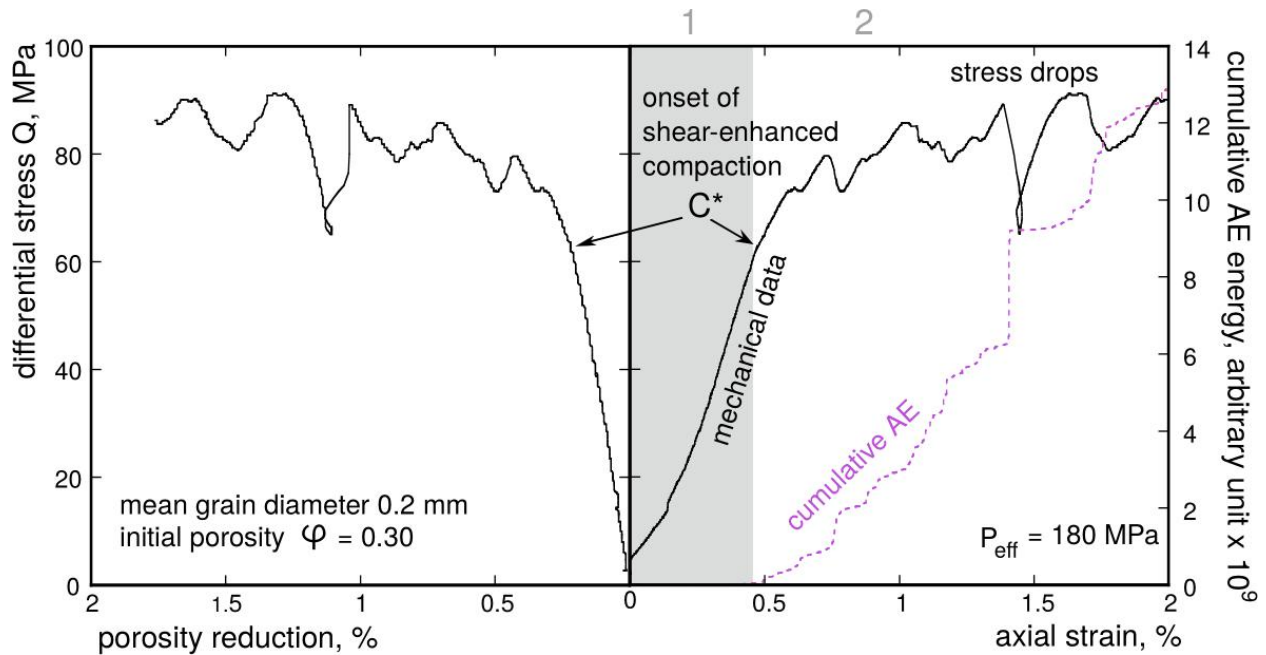
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1127 **Figure 2.** Representative mechanical data (black line) and cumulative acoustic emission energy
 1128 (purple dashed line) for hydrostatic tests performed on the synthetic samples. These data were
 1129 obtained on synthetic samples of mean grain diameter of 0.2 mm and initial porosity of 0.38. The
 1130 critical stress for the onset of grain crushing P^* is indicated by an arrow. The porosity reduction
 1131 in percentage corresponds to the absolute loss of porosity, i.e., a porosity reduction of 14% refers
 1132 to a drop from 0.38 to 0.24. (1) When P_{eff} is first increased, porosity decreases non-linearly as a
 1133 result of grains rearrangements. (2) As P_{eff} is increased further, the sample undergoes elastic
 1134 deformation until P_{eff} reaches the critical value P^* beyond which (3) the sample porosity
 1135 decreases suddenly and significantly by grain crushing (inelastic deformation).



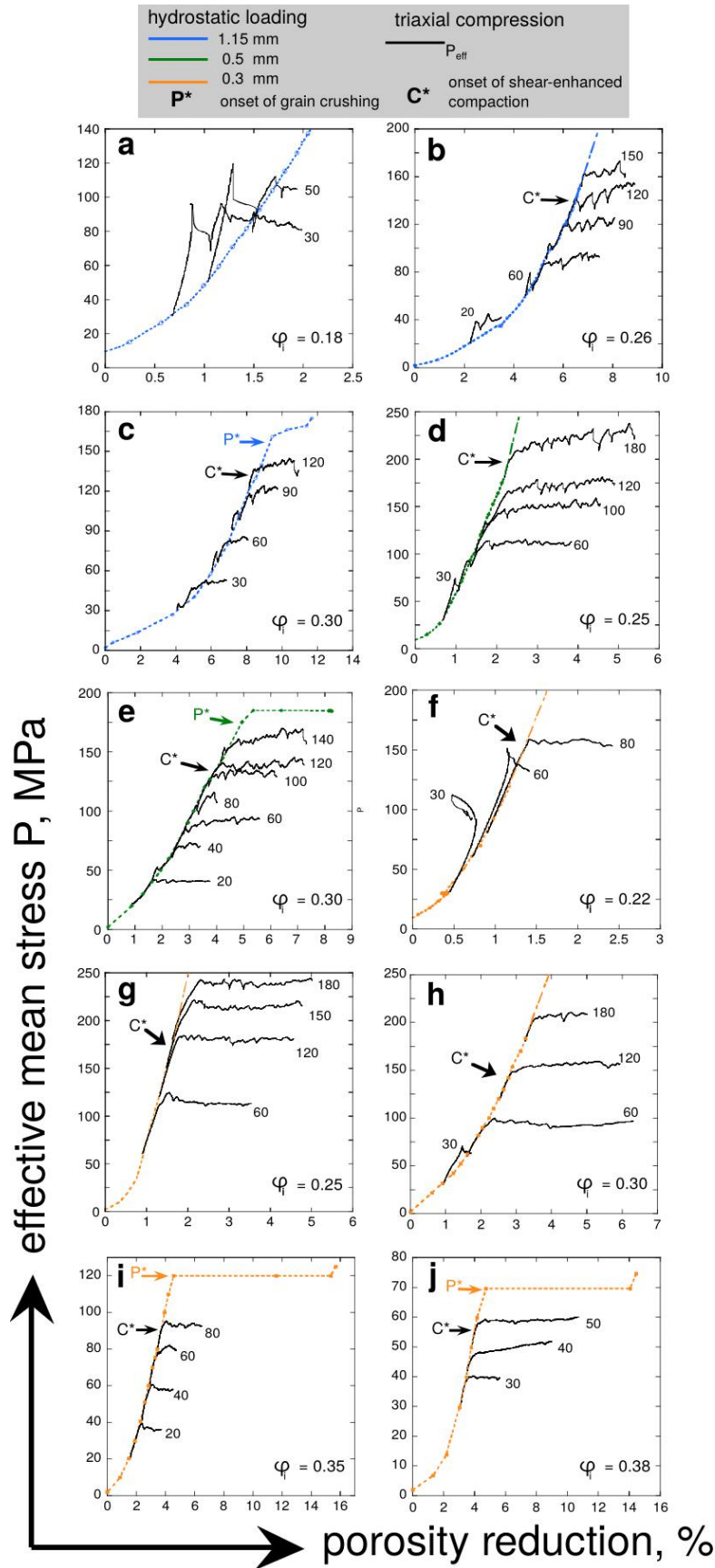
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1137 **Figure 3.** Representative mechanical data (black lines) and cumulative acoustic emission energy
 1138 (purple dashed line) for triaxial tests performed in the brittle regime. The triaxial test presented
 1139 was performed at $P_{\text{eff}} = 30$ MPa on a synthetic sample of mean grain diameter of 0.2 mm and
 1140 initial porosity of 0.22. The peak stress σ_v is indicated by an arrow. The porosity reduction in
 1141 percentage corresponds to the absolute loss of porosity, i.e., a porosity reduction of 0.4% refers
 1142 to a drop from 0.22 to 0.216. (1) When loading is first applied, the sample undergoes elastic axial
 1143 strain and porosity decreases linearly. (2) The transition to the inelastic stage of deformation
 1144 takes place at the onset of dilatancy and, as Q is increased further, it eventually reaches (3) a
 1145 critical peak stress σ_v at which point brittle failure takes place and the stress drops to a residual
 1146 value.

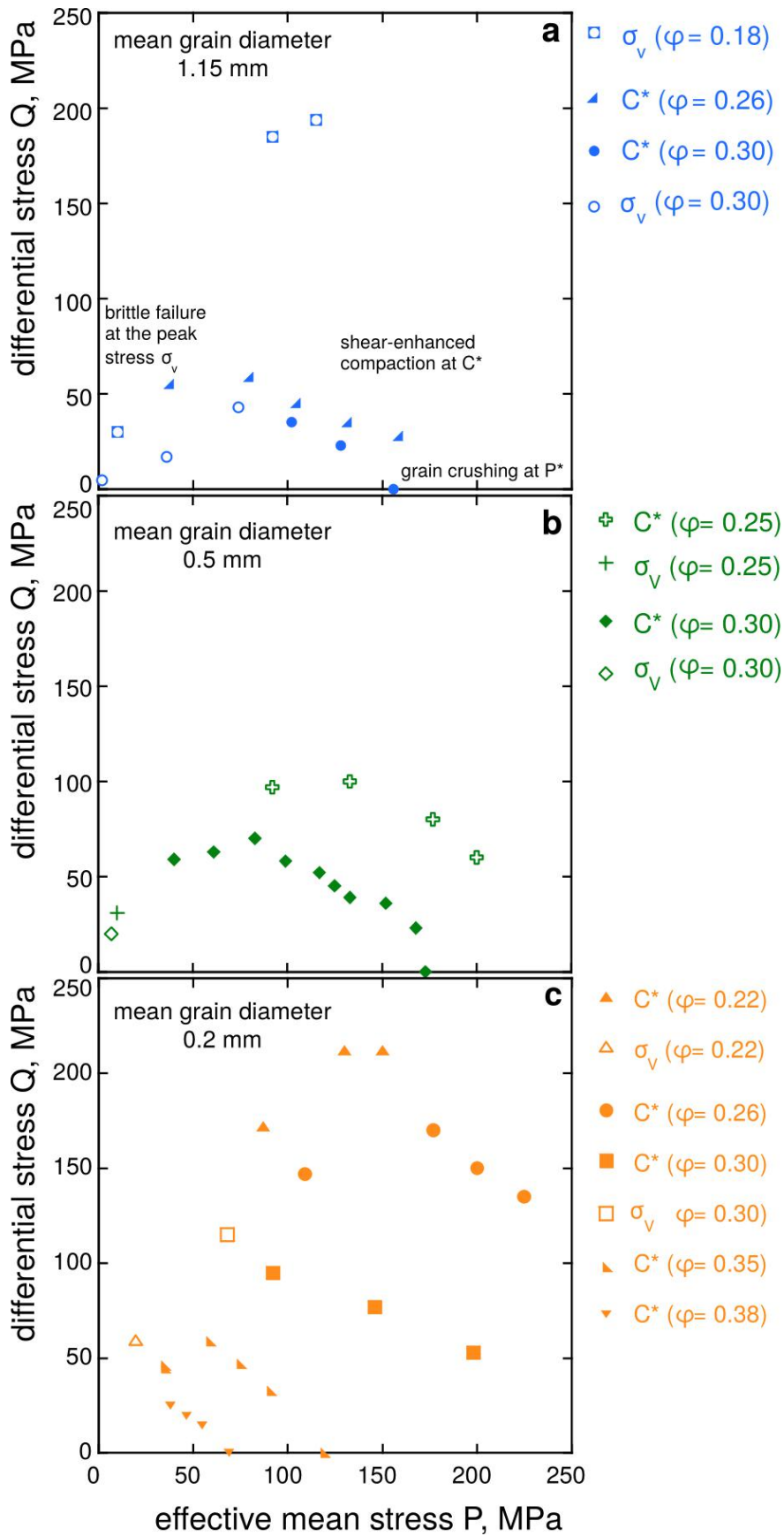


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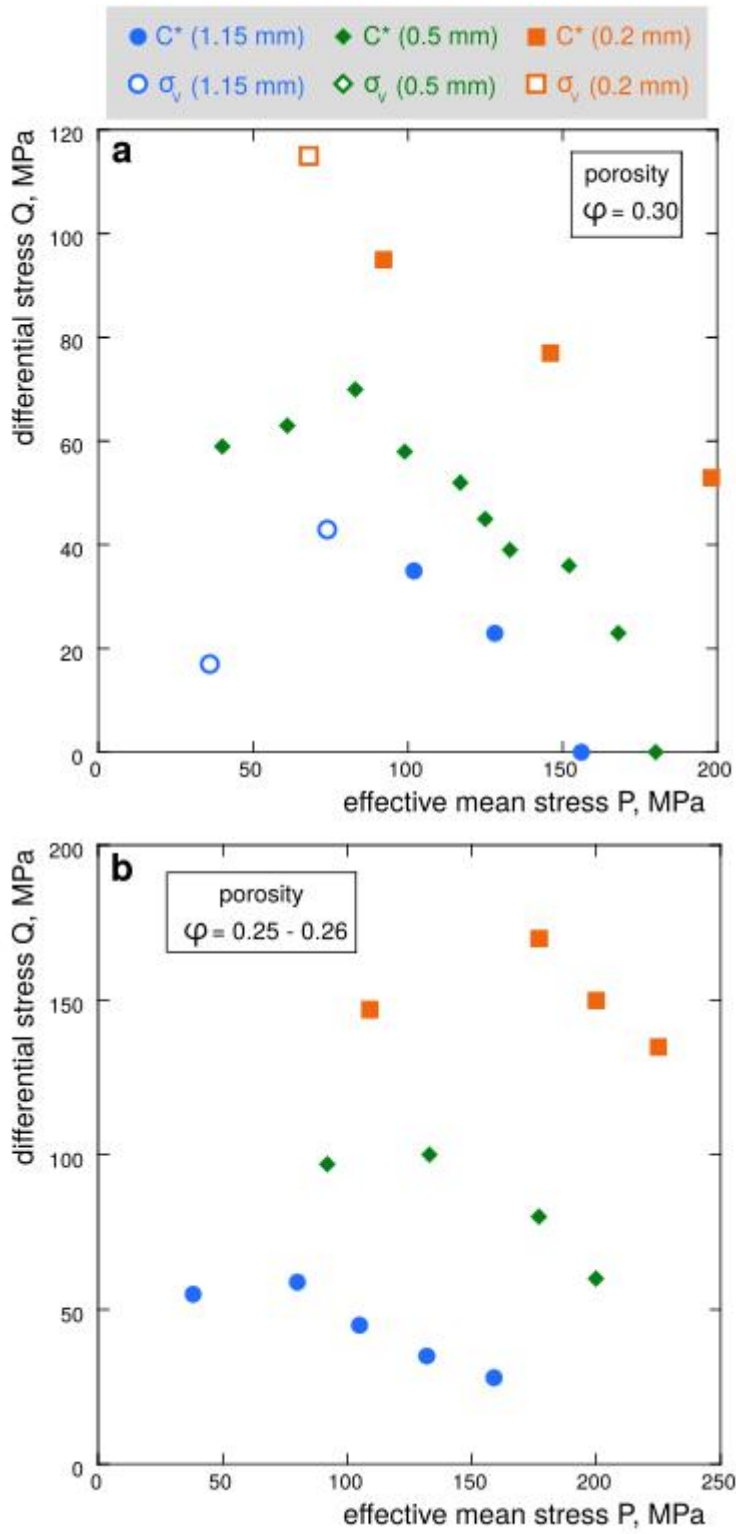
1148 **Figure 4.** Representative mechanical data (black lines) and cumulative acoustic emission energy
 1149 (purple dashed line) for triaxial tests performed in the regime of shear-enhanced compaction. The
 1150 triaxial test presented was performed at $P_{\text{eff}} = 180$ MPa on a synthetic sample of mean grain
 1151 diameter of 0.2 mm and initial porosity of 0.30. The critical stress for the onset of shear-
 1152 enhanced compaction C^* is indicated by an arrow. The porosity reduction in percentage
 1153 corresponds to the absolute loss of porosity, i.e., a porosity reduction of 2% refers to a drop from
 1154 0.30 to 0.28. (1) Axial strain increases and porosity decreases linearly as loading is first applied.
 1155 (2) The transition to the inelastic stage of deformation takes place as Q reaches the critical value
 1156 C^* for the onset of shear-enhanced compaction.



1158 **Figure 5.** Compilations of mechanical data from hydrostatic loading (dashed colored) and
1159 triaxial tests (black) for samples with a mean grain diameter of 1.15 mm (blue) and an initial
1160 porosity of (a) 0.18, (b) 0.26 and (c) 0.30; a mean grain diameter of 0.5 mm (green) and an initial
1161 porosity of (d) 0.25 and (e) 0.30; and a mean grain diameter of 0.2 mm (orange) and an initial
1162 porosity of (f) 0.22, (g) 0.25, (h) 0.30, (i) 0.35 and (j) 0.38. Effective pressures at which triaxial
1163 tests were conducted are indicated at the end of the corresponding curves. The onset for inelastic
1164 deformation corresponds to the departure of the effective mean stress – porosity reduction curve
1165 from the hydrostat. For illustration, the onset of shear-enhanced compaction is indicated as C* by
1166 black arrows. The critical stresses P* for the onset of grain crushing are indicated by colored
1167 arrows on the hydrostats.

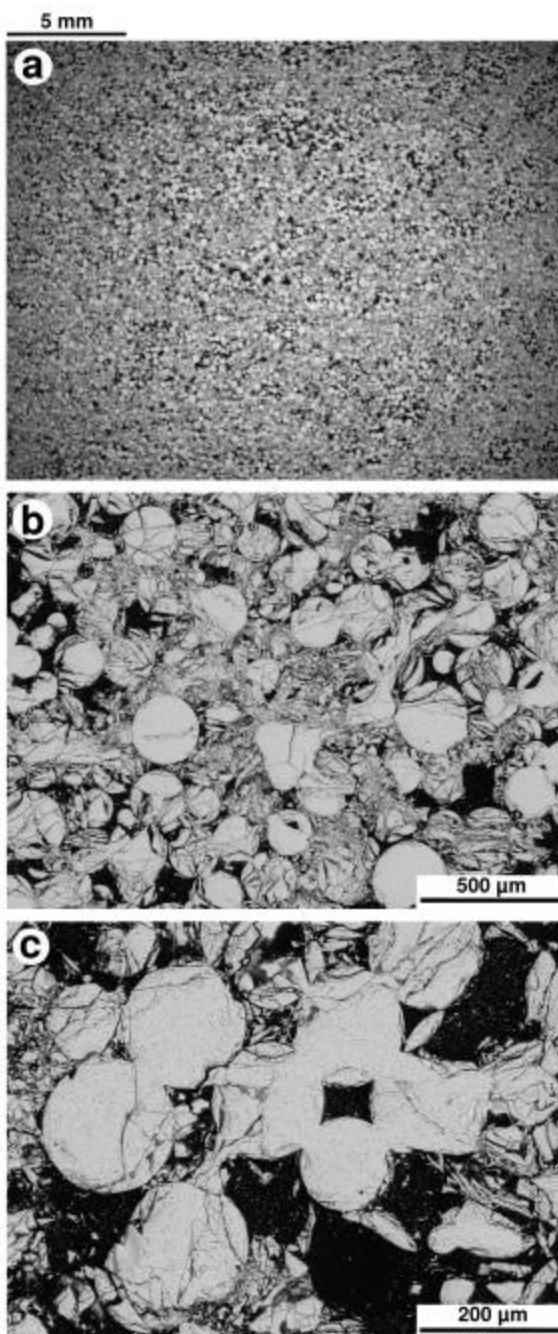


1169 **Figure 6.** Compilations of failure envelopes for synthetic samples of mean grain diameter of **(a)**
1170 1.15 mm, **(b)** 0.5 mm and **(c)** 0.2 mm. Initial porosity of the synthetic samples is indicated in the
1171 legend. Failure envelopes are mapped out by critical stresses σ_v (brittle triaxial test), C^* (ductile
1172 triaxial test) and P^* (hydrostatic test). Open symbols correspond to peak stress values and solid
1173 symbols to C^* values. P^* (also a solid symbol) anchors the envelope to the x-axis.



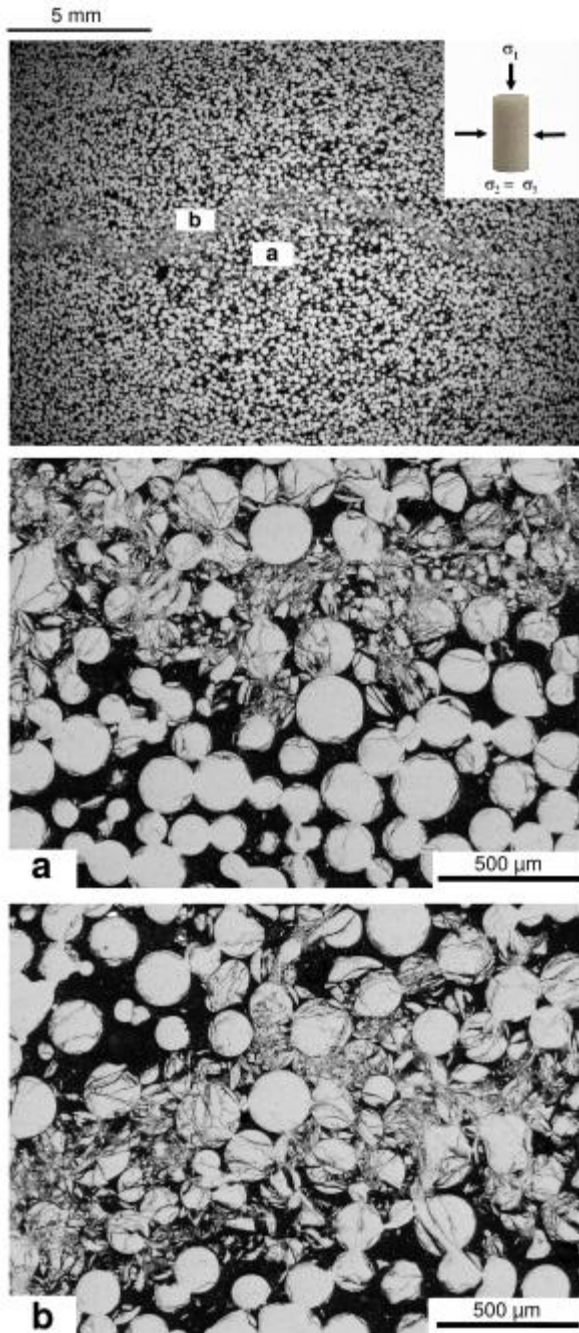
1175 **Figure 7.** Compilations of failure envelopes for synthetic samples with a porosity of **(a)** 0.30 and
1176 **(b)** 0.25. Mean grain diameter of the synthetic samples is indicated in the legend. Failure
1177 envelopes are mapped out by critical stresses σ_v (brittle triaxial test), C^* (ductile triaxial test) and
1178 P^* (hydrostatic test). Open symbols correspond to peak stress values and solid symbols to C^*
1179 values. P^* (also a solid symbol) anchors the envelope to the x-axis.
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1183 **Figure 8.** Representative scanning electron micrograph of the (a) microstructure of a synthetic
1184 sample deformed under hydrostatic loading up to an effective stress beyond P^* . (b)(c) Zooms in
1185 showing extensive grain crushing. Black: porosity, gray: glass.

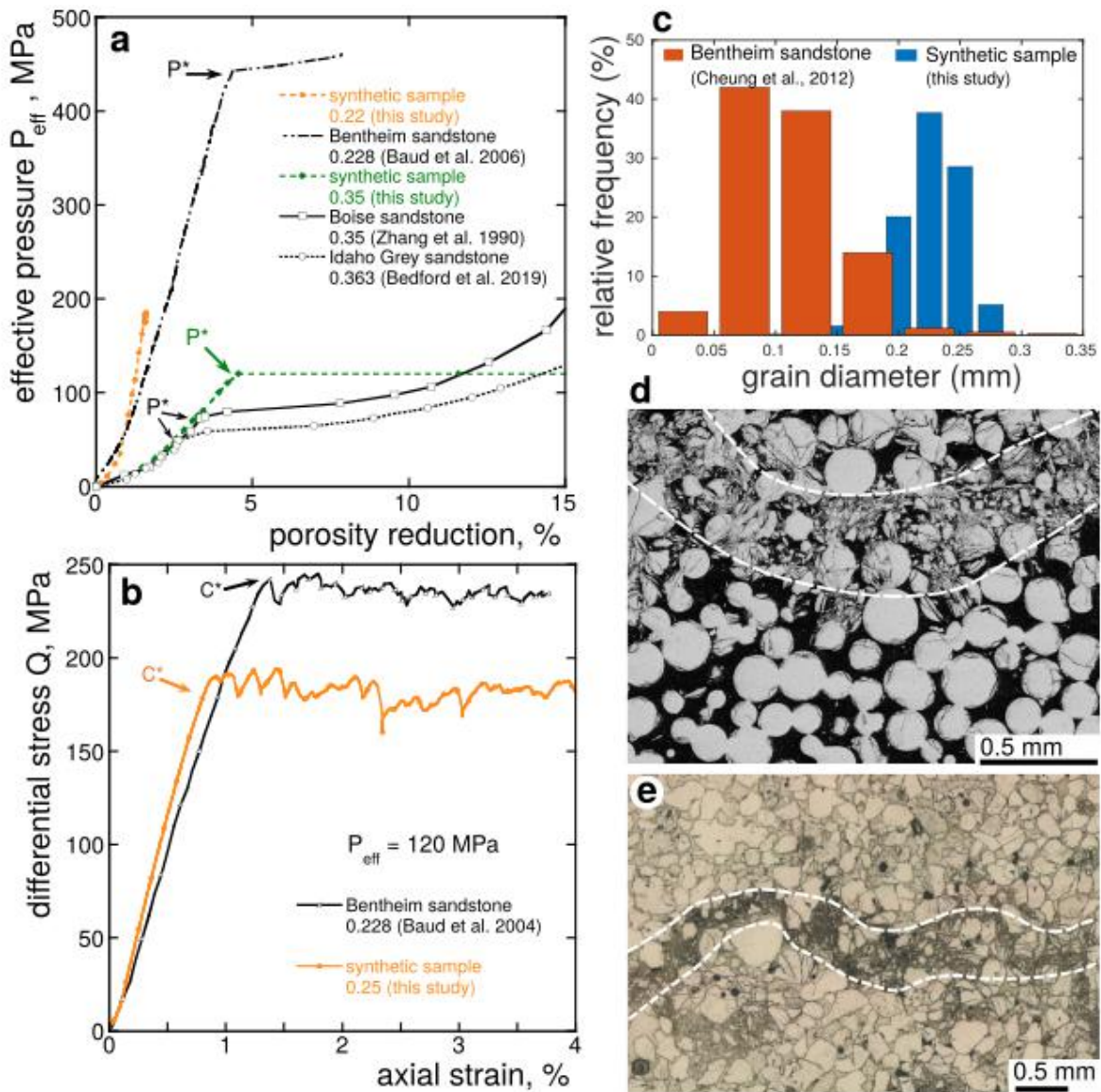


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1187 **Figure 9.** Scanning electron micrograph of the microstructure of a synthetic sample that failed
 1188 by development of discrete compaction bands. Sample 3314, with a porosity of 0.35 and a mean
 1189 grain diameter of 0.2 mm, was deformed under 80 MPa (Table 2). Overview of the thin section
 1190 allows for the observation of a discrete compaction band in the middle, formed in a direction
 1191 normal to the maximum principal stress σ_1 . (a) and (b) show micrographs of a discrete 2-5

1192 grain-thick band within which most grains are crushed. The microstructure outside of the band is
1193 almost intact. Black: porosity, gray: glass.
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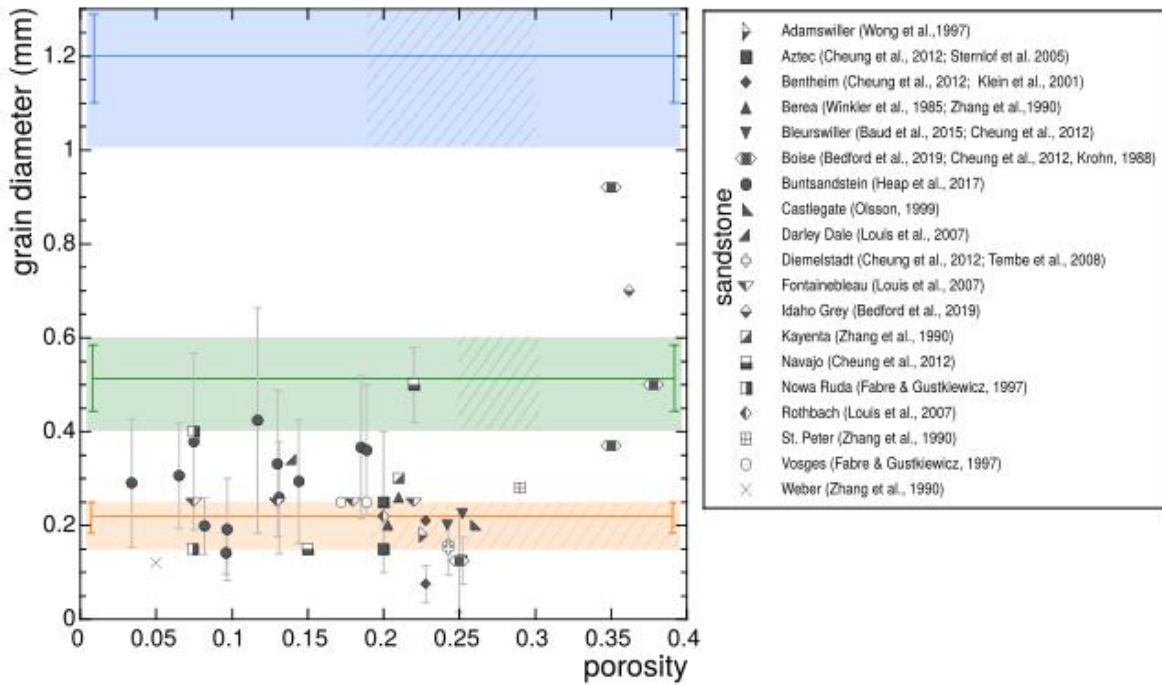


1196

1197 **Figure 10.** Data from tests performed on synthetic samples compared to data for sandstones
 1198 from the literature. (a) Comparison of the hydrostatic loading curve of a synthetic sample (green
 1199 dashed) with a porosity of 0.35 and a mean grain diameter of 0.5 mm and of the hydrostatic
 1200 loading curve of a synthetic sample (orange curve) with a porosity of 0.22 and a mean grain size
 1201 of 0.2 mm, with the hydrostat of Boise sandstone (black line), with a porosity of 0.35 and a mean
 1202 grain diameter of 0.92 mm (Zhang et al., 1990), the hydrostat of Idaho Gray sandstone (dashed
 1203 black) with a porosity of 0.363 and a mean grain diameter of 0.7 mm (Bedford et al. 2019) and

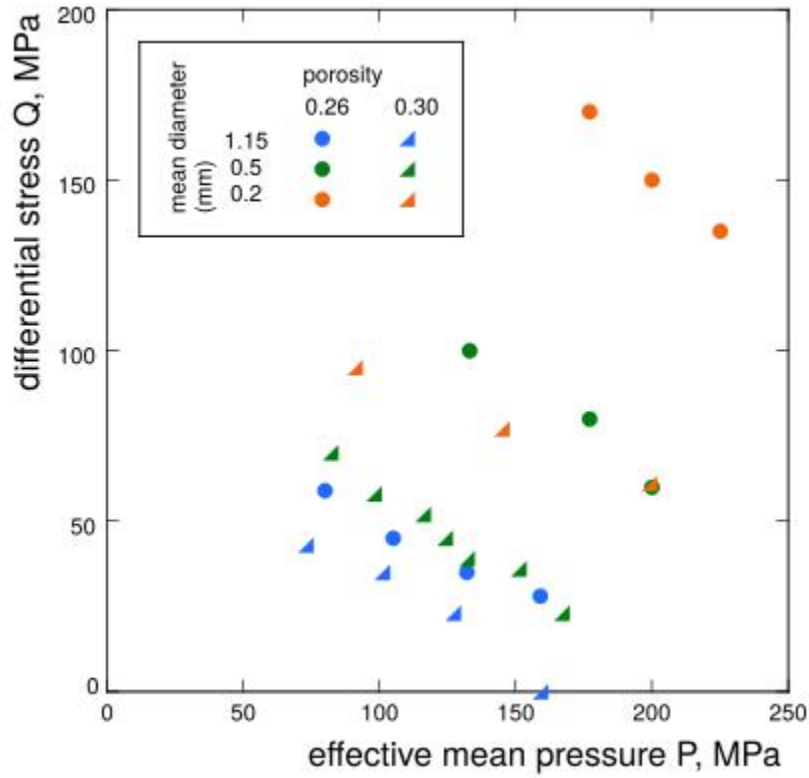
1204 the hydrostat of Bentheim sandstone with a porosity of 0.228 and a grain diameter of 0.3 mm
1205 (Baud et al., 2006). The onset of grain crushing is indicated as P^* . **(b)** Comparison of stress-
1206 strain curves obtained during a triaxial test at an effective pressure of 120 MPa performed on a
1207 synthetic sample (orange line) with a porosity of 0.25 and a mean grain diameter of 0.2 mm and
1208 on Bentheim sandstone (black line)(Baud et al., 2004). The onset of shear-enhanced compaction
1209 is indicated as C^* . **(c)** For reference, the smallest grain size distribution used in this study is
1210 presented along the grain size distribution of Bentheim sandstone (data from Cheung et al. 2012).
1211 **(d)** Comparison of a scanning electron micrograph of a discrete compaction band observed in a
1212 synthetic sample ($\phi = 0.35$) and **(e)** an optical microscope image of a discrete compaction band
1213 in Bentheim sandstone ($\phi = 0.23$; Baud et al., 2004).
1214

1215



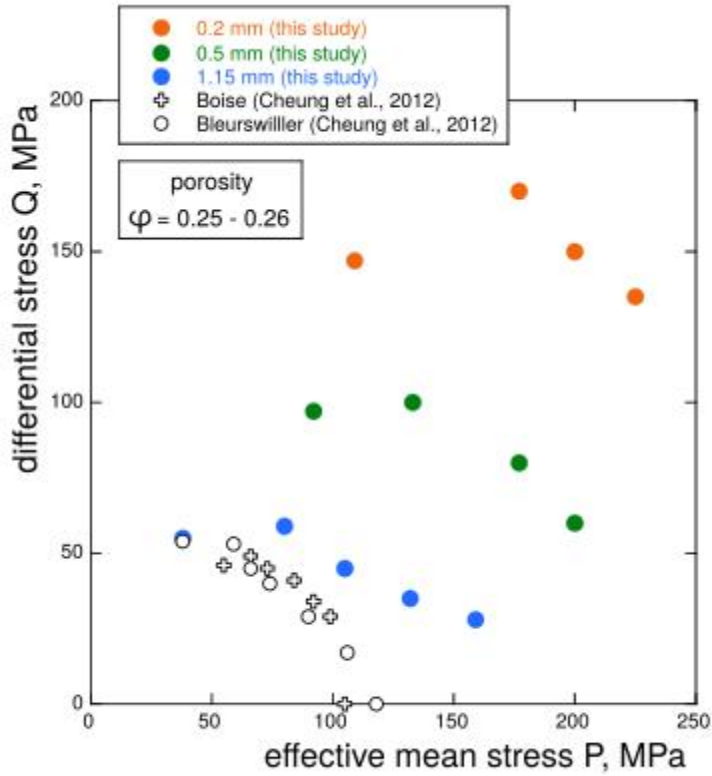
1216

1217 **Figure 11.** Compilation of porosity and grain diameter for laboratory sandstones. All data are
 1218 from the literature, references are given in the legend. Colored areas correspond to the range of
 1219 porosity-grain diameter accessible by sintering glass beads. The dashed areas correspond to the
 1220 range we specifically investigated in this study. The error bars give the standard deviation of the
 1221 grain diameter distribution, when it has been reported.



1222

1223 **Figure 12.** Influence of porosity on the compactive yield strength. Compactive yield envelopes
 1224 for synthetic samples with a porosity of 0.26 (round solid symbol) or 0.30 (triangle solid symbol)
 1225 and a mean grain diameter of 1.15 mm (blue), 0.5 mm (green) or 0.2 mm (orange) are compiled.



1226

1227 **Figure 13.** Influence of grain diameter on the compactive yield
 1228 envelopes for synthetic samples with a porosity of 0.25 and a mean grain diameter of 0.2 mm
 1229 (orange), 0.5 mm (green) and 1.15 mm (blue) are compiled with yield envelopes for Boise (open
 1230 cross) and Bleurswiller (open circle) sandstones (data from Cheung et al., 2012).