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# 1 Effect of prestress on phononic band gaps induced by inertial amplification

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10 Phononic crystals and elastic metamaterials have recently received significant attention due to their  
11 potential for unconventional wave control. Despite this interest, one outstanding issue is that their  
12 band diagram is typically fixed, once the structure designed. To overcome this limitation, periodic  
13 structures with adaptive elastic properties have recently been proposed for Bragg- and local resonance-  
14 driven structures.

15 In this context, we report about the effect of an applied external mechanical load on a periodic struc-  
16 ture exhibiting band gaps induced by inertial amplification mechanism. If compared to the cases of  
17 Bragg scattering and ordinary local resonant metamaterials, we observe here a more remarkable curve  
18 shift, modulated through large but fully reversible compression(stretch) of the unit cell, eventually  
19 triggering significant (up to two times) enlargement(reduction) of the width of a specific band gap.  
20 An important up(down)-shift of some dispersion branches over specific wavenumber values is also ob-  
21 served, showing that this selective variation may lead to negative group velocities over larger(smaller)  
22 wavenumber ranges. In addition, the possibility for a non-monotone trend of the lower limit of the  
23 first BG under the same type of external applied prestrain is found and explained through an an-  
24 alytical model, which unequivocally proves that this behaviour derives from the different unit cell  
25 effective mass and stiffness variations as the prestrain level increases. These peculiarities derive from  
26 the hinge-like behaviour of some regions of the unit cell, which is typical of structures exhibiting the  
27 inertial amplification mechanism.

28 The effect of the prestress on the dispersion diagram is investigated through the development of a 2-step  
29 calculation method: first, an Updated Lagrangian scheme, including a static geometrically nonlinear  
30 analysis of a representative unit cell undergoing the action of an applied external load is derived, and  
31 then the Floquet-Bloch decomposition is applied to the linearized equations of the acousto-elasticity  
32 for the unit cell in the deformed configuration.

33 Finally, the most evident consequence on the dispersion curves of the application of an external  
34 prestress, i.e. the band gap shift with respect to the unloaded structure, is demonstrated through  
35 nonlinear transient numerical simulations, clearly proving the capability of the structure to switch  
36 from a pass- to a stop-band behaviour over the same frequency range.

37 The results presented herein provide insights in the behaviour of band gaps induced by inertial am-  
38 plification, and suggest new opportunities for real-time tunable wave manipulation.

## 39 I. INTRODUCTION

40 Phononic crystals and elastic metamaterials have proved to be powerful platforms to achieve a plethora of unconven-  
 41 tional vibrational behaviours deriving from their peculiar dispersion diagrams, characterized by frequency band gaps  
 42 (BGs) and pass-bands, i.e. frequency regions where the propagation of waves is inhibited or supported, respectively<sup>1</sup>.  
 43 This allowed to achieve frequency selective wave filtering<sup>2</sup>, guiding<sup>3-5</sup> and splitting<sup>6,7</sup>, stimulating the conception of  
 44 pioneering applications, such as ultra-sensitive devices<sup>8</sup>, large scale metamaterials for vibration shielding<sup>9-11</sup>, sub-  
 45 wavelength imaging<sup>12</sup>, elastic wave cloaking / lensing<sup>13-15</sup>, etc.

46 In this context, an important issue is that phononic crystal and elastic metamaterial operational frequencies are typi-  
 47 cally fixed once the structure has been designed and fabricated. In contrast, in the majority of practical applications,  
 48 including the ones previously mentioned, it may be desirable to dynamically or adaptively tune the BGs (or some  
 49 of the dispersion branches) in terms of frequency, also after the structure has been fabricated. To overcome this  
 50 limitation, periodic systems with adaptive elastic properties have recently been proposed. For instance, BG tuning  
 51 has been achieved by means of piezoelectric materials<sup>16-18</sup>, temperature variation<sup>19-22</sup>, magneto- and light-based ap-  
 52 proaches<sup>23-27</sup>, as well as by the application of external mechanical loads<sup>28</sup>. Among them, the latter approach can be  
 53 easily implemented by imposing controlled displacements into specific portions of the structure.

54 In this context, Bigoni et al.<sup>29</sup> proposed for the first time the prestress as a practical way to reversibly alter the  
 55 dispersion diagram of a periodic structure, including the possibility of shifting the BG position. The feasibility of  
 56 the approach was confirmed formulating a theoretical model for an orthotropic, prestressed (compressible) elastic  
 57 layer vibrating on an elastic half space and assuming long-wave asymptotics for the solution. Gei et al.<sup>30</sup> relaxed the  
 58 hypothesis of perfect periodicity and investigated the effect of the prestress in quasi-periodic structures in the case of  
 59 flexural vibrations. Amendola et al.<sup>31</sup> studied the band structure of tensegrity mass-spring chains, and the possibility  
 60 to tune the dispersion relation of such systems by suitably varying local and global prestress variables, given their  
 61 remarkable softening / stiffening response under axial or compressive loading<sup>32,33</sup>.

62 Periodic elastomeric structures, thanks to their capacity of repetitively undergoing large strain deformations in a  
 63 fully reversible manner, brought to BG nucleation / annihilation mechanisms triggered by the application of external  
 64 loads radically changing the unit cell geometry<sup>34</sup>. Deformations in the linear and nonlinear regimes, as well as diverse  
 65 geometrical topologies have been explored<sup>35-38</sup>.

66 Finally, it has been observed that also mechanical instabilities induced, for instance, by the application of external  
 67 loads, may alter the propagation of elastic waves. Slesarenko et al. induced instabilities in soft composite materials  
 68 achieving a significant decrease of the group velocity (up to going negative) of the transverse waves under specific  
 69 micropolar conditions<sup>39</sup>.

70 However, the majority of the aforementioned investigations are limited to the context of (i) Bragg- or (ii) ordinary  
 71 resonance-induced BGs, whereas in the present paper, we report about the effects of an applied prestress on (iii) peri-  
 72 odic structures exhibiting BGs induced by inertial amplification mechanisms. While in (i) the wave scattering derives  
 73 from assemblages of periodic unit cells, requiring thus the wavelength of the incoming wave to be comparable to the  
 74 structural periodicity<sup>40</sup>, and in (ii) the dynamic behaviour is mainly governed by the eigenfrequencies of resonators  
 75 included in the structure<sup>41</sup>, in (iii) large inertial forces are generated by amplifying the motion of a mass, which in  
 76 turn increases the inertia of the overall system and lowers its resonance frequency, allowing thus for sub-wavelength

77 and broadband BGs, while keeping the structure lightweight<sup>42,43</sup>.

78 If compared to the cases of Bragg scattering and ordinary local resonant metamaterials<sup>44</sup>, we show that the inertial am-  
 79 plification allows for a more remarkable curve shift, modulated through large but fully reversible compression(stretch)  
 80 of the unit cell, eventually triggering significant enlargement(reduction) of a specific band gap width. We also observe  
 81 a selective up(down)-shift of some dispersion branches, leading to negative group velocities over specific wavenumber  
 82 ranges. In addition, a non-monotone trend of the lower limit of the first BG under the same type of external applied  
 83 prestrain is found and explained through an analytical model, which shows that this behaviour derives from the differ-  
 84 ent unit cell effective mass and stiffness variations as the prestrain level increases. Examining the deformed geometries  
 85 consequent the application of the prestress highlights how the remarkable band shift is due to the hinge-like behaviour  
 86 of some regions of the unit cell, typical of the inertial amplification mechanism and responsible for a large deformation  
 87 state, i.e. change of the unit cell geometry. We consider the static deformation induced by the prestress to be in the  
 88 linear elastic regime so to have a complete reversibility of the phenomena (tunability). The analysis is performed in  
 89 terms of small amplitude motions superimposed on a deformed state once the desired load has been applied.

90 The paper is organized as follows: in section II, the 2-step Updated Lagrangian scheme, including (i) a static geo-  
 91 metrically nonlinear analysis of a representative unit cell undergoing the action of an applied external load and (ii)  
 92 the Floquet-Bloch decomposition applied to the linearized equations of the acousto-elasticity for the unit cell in the  
 93 deformed configuration, is presented. Section III provides evidence for the dispersion band alteration induced by  
 94 the application of the prestress in a periodic structure exhibiting BG induced by inertial amplification mechanism.  
 95 Parametric dispersion curves for different values of prestress are presented and compared to the original structure  
 96 (i.e., without the application of any prestress). Afterwards, a 2-step nonlinear transient numerical simulation confirms  
 97 the BG shift induced by the prestress in a finite structure, proving its ability to switch from a pass- to a stop-band  
 98 behaviour over the same frequency range. The prestress is easily implemented by applying prescribed displacement  
 99 at specific edges of the structure prior to the wave propagation. The full tunability of the structure is guaranteed by  
 100 the possibility of readily applying and removing the imposed deformations. Finally, section IV summarizes the main  
 101 results of the present research and provides future perspectives, shedding light on the possibility of investigating the  
 102 effect of an additional state of prestress, internal, cross-linking the fields of metamaterials and tensegrity structures.

## 103 II. FLOQUET-BLOCH ANALYSIS OF A PRESTRESSED PHONONIC CRYSTAL

104 In this work, the band structure diagrams are computed using a Floquet-Bloch finite element method formulated  
 105 within an Updated Lagrangian scheme. As schematically presented in Fig. 1, the procedure consists of two main  
 106 computational steps, namely (i) a nonlinear static analysis involving large strains and displacements, and (ii) a so  
 107 called small-on-large dynamic analysis, in which small vibrations are superimposed on the statically deformed unit  
 108 cell. The main computational aspects of the two steps are outlined in the following.

### 109 A. Static analysis

110 Following the application of a static volume load  $\mathbf{f}_{V0}$ , or surface load  $\mathbf{f}_{S0}$ , the unit cell  $\Omega_0$  identified by the position  
 111 vector  $\mathbf{x}$  and represented by the lattice vector  $\mathbf{r}_0 = \{r_{01}, 0\}^T$  and its reciprocal vector  $\mathbf{g}_0 = \{g_{01}, 0\}^T = \{r_{01}/2\pi, 0\}^T$ ,

112 undergoes a displacement  $\mathbf{u}_0$  that results in a change of configuration from the undeformed state  $C_0$  to the static  
 113 deformed state  $C$  (see Fig. 1). The deformed domain and matrix of the lattice vectors in the (deformed) configuration  
 114  $C$  are identified by  $\Omega$  and  $\mathbf{r} = \{r_1, 0\}^T$ , respectively. The relation between  $\mathbf{r}_0$  and  $\mathbf{r}$  can be expressed as  $\mathbf{r} = \mathbf{F}_L \mathbf{r}_0$ ,  
 115 where  $\mathbf{F}_L$  defines the affine component of the deformation gradient such that  $\mathbf{F}_L = \mathbf{F}^{-1} \mathbf{F}_P$ , being  $\mathbf{F} = \nabla_{\mathbf{x}} \mathbf{u}_0 + \mathbf{I}$  the  
 116 deformation gradient,  $\mathbf{F}_P$  a periodic non-affine deformation<sup>45</sup> and  $\nabla_{\mathbf{x}} = \{\partial/\partial x_1, \partial/\partial x_2\}^T$ . The equilibrium equations  
 117 with respect to the undeformed configuration  $C_0$  can be derived from the variational statement:

$$\int_{\Omega} (\mathbf{S}(\mathbf{x}) : \delta \mathbf{E}(\mathbf{x}) - \mathbf{f}_{V_0} \cdot \delta \mathbf{u}_0) da = \int_{\partial \Omega} \mathbf{f}_{s_0} \cdot \delta \mathbf{u}_0 ds, \quad (1)$$

118 subjected to the Dirichlet boundary conditions:

$$\mathbf{u}_0(\mathbf{x} + \mathbf{r}_0) = \mathbf{u}_0(\mathbf{x}), \quad (2)$$

119 in which  $\mathbf{E} = \frac{1}{2}(\mathbf{F}^T) \mathbf{F} - \mathbf{I}$  is the Green-Lagrange strain tensor and  $\mathbf{S} = \mathbf{D}_0 : \mathbf{E}$  the second Piola-Kirchhoff stress  
 120 tensor. The tensor of tangential elastic moduli,  $\mathbf{D}_0$ , is expressed by  $\mathbf{D}_0 = 4\partial^2 \psi / (\partial \mathbf{C} \partial \mathbf{C})$ , being  $\mathbf{C} = \mathbf{F}^T \mathbf{F}$  the right  
 121 Cauchy-Green deformation tensor and  $\psi$  the elastic energy density. The material of the unit cell in  $C_0$  is specified by  
 122 the density  $\rho_0$  while, assuming a hyperelastic material behavior described by the Murnaghan's model<sup>46-49</sup>, the elastic  
 123 energy density can be defined as:

$$\begin{aligned} \psi = & \frac{1}{2} (\lambda + 2\mu) I_1^2(\mathbf{E}) - 2\mu I_2(\mathbf{E}) + \frac{1}{3} (l + 2m) I_1^3(\mathbf{E}) \\ & - 2m I_1(\mathbf{E}) I_2(\mathbf{E}) + n I_3(\mathbf{E}), \end{aligned} \quad (3)$$

124 in which  $\lambda$  and  $\mu$  denote the first and second Lamé parameters, respectively,  $(l, m, n)$  the third order Murnaghan  
 125 parameters, and  $I_1(\mathbf{E})$ ,  $I_2(\mathbf{E})$  and  $I_3(\mathbf{E})$  the first, second and third invariants of the Green-Lagrange strain tensor,  
 126 respectively.

127 The application of a standard Galerkin approach to Eq. (1) results in the generalized system of equations:

$$[\mathbf{\Gamma}_0^T \mathbf{K}(\mathbf{Q}_0) \mathbf{\Gamma}_0] \mathbf{Q}_0(\mathbf{X}) = \mathbf{P}_0(\mathbf{X}), \quad (4)$$

128 where  $\mathbf{K}(\mathbf{Q}_0)$  is the static stiffness matrix,  $\mathbf{P}_0$  the global vector of nodal forces,  $\mathbf{Q}_0$  the global vector of independent  
 129 nodal displacements and  $\mathbf{\Gamma}_0$  the mapping operator resulting from Eq. (2) and realizing the condition  $\mathbf{U}_0 = \mathbf{\Gamma}_0 \mathbf{Q}_0$ .  
 130  $\mathbf{U}_0$  indicates the full vector of nodal displacements. In this work, the solution of Eq. (4) is carried out using Comsol  
 131 Multiphysics 5.3<sup>50</sup>.

132 Following the Updated Lagrangian scheme, once the displacements  $\mathbf{Q}_0$  are obtained, the reference configuration is  
 133 updated from  $C_0$  to  $C$  by calculating the corresponding nodal coordinates  $\mathbf{x} = \mathbf{x}_0 + \mathbf{\Gamma}_0 \mathbf{Q}_0(\mathbf{x}_0)$ . The updated material  
 134 properties in  $C$  are given by  $\rho = \rho_0 (\det \mathbf{F})^{-1}$  and  $D_{ijkl} = (\det \mathbf{F})^{-1} F_{iI} F_{jJ} F_{kK} F_{lL} (D_0)_{IJKL}$ , while the Cauchy stress  
 135 tensor is obtained from the relation  $\boldsymbol{\sigma} = (\det \mathbf{F})^{-1} \mathbf{F} \mathbf{S} \mathbf{F}^T$ . The geometry of the unit cell in the configuration  $C$  is then  
 136 re-meshed and used as the basis for the linear dynamic analysis described in the next section.

## 137 B. Dynamic Analysis Using the Floquet-Bloch Decomposition

138 Following the small-on-large analysis approach<sup>47,51-54</sup>, in which  $C$  is the new reference configuration, the position  
 139 vector for the unit cell in the dynamic deformed configuration  $C'$  (Fig. 1) is approximated as  $\mathbf{x}' \approx \mathbf{x}$  while, from the

140 application of the Floquet-Bloch theorem, any small harmonic perturbation  $\mathbf{u}(\mathbf{x})$  can be expressed as<sup>55</sup>:

$$\mathbf{u}(\mathbf{x}) = \tilde{\mathbf{u}}(\mathbf{x})\exp(ikx)\exp(-i\omega t), \quad (5)$$

141 in which  $\tilde{\mathbf{u}}(\mathbf{x})$  is a  $\Omega$ -periodic displacement amplitude,  $t$  denotes the time,  $\omega$  the angular frequency, and  $k \in \Lambda$  the  
142 Bloch wavenumber, being  $\Lambda$  the reciprocal unit cell defined in  $C$  by the reciprocal lattice vector  $\mathbf{g} = \mathbf{F}_L^{-T} \mathbf{g}_0$ .

143 By defining the  $k$ -shifted gradient of a generic  $\Omega$ -periodic vector field  $\tilde{\phi}(\mathbf{x})$  as:

$$\nabla_k \tilde{\phi}(\mathbf{x}) = \nabla_{\mathbf{x}} \tilde{\phi}(\mathbf{x}) + ik \tilde{\phi}(\mathbf{x}) \otimes (\mathbf{r} \|\mathbf{r}\|^{-1}), \quad (6)$$

144 the solution of the elastodynamic problem for free vibrations of the unit cell in  $C$  subjected to an initial stress  $\boldsymbol{\sigma}_0$  can  
145 be obtained from the variational statement:

$$\begin{aligned} & -\omega^2 \int_{\Omega} \rho(\mathbf{x}) \delta \tilde{\mathbf{u}}^*(\mathbf{x}) \cdot \tilde{\mathbf{u}}(\mathbf{x}) d\Omega \\ & + \int_{\Omega} \delta \tilde{\mathbf{e}}_k^*(\mathbf{x}, \vartheta) : \mathbf{D}(\mathbf{x}) : \tilde{\mathbf{e}}_k(\mathbf{x}) d\Omega \\ & + \int_{\Omega} \boldsymbol{\sigma}_0(\mathbf{x}) : [(\nabla_k \delta \tilde{\mathbf{u}}^*(\mathbf{x}))^T \nabla_k \tilde{\mathbf{u}}(\mathbf{x})] d\Omega = 0, \end{aligned} \quad (7)$$

146 subjected to the Dirichlet boundary condition:

$$\tilde{\mathbf{u}}(\mathbf{x} + \mathbf{r}) = \tilde{\mathbf{u}}(\mathbf{x}) \quad \text{on } \partial\Omega, \quad (8)$$

147 in which  $(\cdot)^*$  stands for the conjugate of a complex vector or tensor field,  $\tilde{\mathbf{e}}_k(\mathbf{x}) = \frac{1}{2}[\nabla_k \tilde{\mathbf{u}}(\mathbf{x}) + (\nabla_k \tilde{\mathbf{u}}(\mathbf{x}))^T]$  follows  
148 from Eq. (6) and denotes the linearized Green-Lagrange strain tensor.

149 The finite element discretization of Eqs. (7) and (8) proceeds by first generating a new mesh for the deformed geometry  
150 of the unit cell in  $C$  and then applying a Galerkin approach<sup>56</sup>. As a results, the following generalized linear eigenvalue  
151 problem is obtained:

$$\{\boldsymbol{\Gamma}^T [k^2 \mathbf{K}_3 + ik(\mathbf{K}_2 - \mathbf{K}_2^T) + \mathbf{K}_1 - \omega^2 \mathbf{M}] \boldsymbol{\Gamma}\} \tilde{\mathbf{Q}}(\omega) = \mathbf{0}, \quad (9)$$

152 in which  $\boldsymbol{\Gamma}$  is a mapping operator implementing the Dirichlet boundary condition in Eq. (8), such that  $\tilde{\mathbf{U}} = \boldsymbol{\Gamma} \tilde{\mathbf{Q}}$ ,  
153 where  $\tilde{\mathbf{U}}$  is the global vector of nodal displacement amplitudes and  $\tilde{\mathbf{Q}}$  a subvector of  $\tilde{\mathbf{U}}$  collecting only its independent  
154 components. The expressions of  $\mathbf{K}_3$ ,  $\mathbf{K}_2$ ,  $\mathbf{K}_1$  and  $\mathbf{M}$  are given in the Appendix A, for the sake of brevity.

155 The band diagrams of the phononic structure can be computed from the eigenvalue problem in Eq. (9) (i) by extracting  
156 the Bloch wavenumbers  $k(\omega)$  for any fixed frequency  $\omega$ , or (ii) by computing the natural frequencies  $\omega(k)$  of the system  
157 for any fixed Bloch wavenumber  $k$ . Since the focus of the present research does not require the knowledge of the  
158 spatial attenuation, the latter approach has been used, resulting computationally more convenient, as it does not  
159 require the transformation of the system into the state space.

### 160 III. RESULTS

161 To study the effect of an external mechanical load on a periodic structure exhibiting BGs induced by inertial  
162 amplification, the numerical method presented in the previous section is here applied to the representative unit cell  
163 reported in Fig. 2A. The unit cell consists of an epoxy matrix exhibiting elongated cross-like holes, and it was proposed  
164 for the first time by Acar and Yilmaz<sup>43</sup>. Its geometrical and material parameters are reported in Tables I, II.

TABLE I. Material constants for the epoxy<sup>44</sup>.

	$\rho_0$ [kg/m <sup>3</sup> ]	$\lambda$ [GPa]	$\mu$ [GPa]	$l$ [GPa]	$m$ [GPa]	$n$ [GPa]
Epoxy	1540	2.59	1.34	-18.94	-13.36	-9.81

TABLE II. Geometrical parameters of the unit cell presented in Fig. 2A. All the given parameters are in [mm].

$t_1$	$t_2$	$t_3$	$t_4$	$d_1$	$d_2$	$d_3$	$d_4$
3.2	0.4	3.2	0.4	5.2	2.0	20.0	4.0

## 167 A. Band structure analysis

168 As discussed in Section II, the first step for the band structure calculation is to extract the deformation induced in the  
169 unit cell by an initial state of stress / strain applied to the structure. To do this, two different sets of loading conditions  
170 are applied to the structure in the form of a normal displacement  $\mathbf{u}_0(\mathbf{x}_0) \cdot \mathbf{n}_0(\mathbf{x}_0)$  prescribed to the  $x_{02}$ -parallel faces  
171 of the unit cell (highlighted in purple in Fig. 2A). The out-of-plane degrees of freedom of the unit cell are blocked,  
172 so to prevent any possible bending deformation during the application of the loading conditions. The first loading  
173 set induces a state of compression and varies from 0 (no prestrained condition) to  $-360 \mu\text{m}$  (maximum compression  
174 condition) with a step of  $\Delta \mathbf{u}_0(\mathbf{x}_0) \cdot \mathbf{n}_0(\mathbf{x}_0) = -20 \mu\text{m}$ , while the second set induces a tensile state and varies from  
175 0 (no prestrained condition) to  $+130 \mu\text{m}$  (maximum traction condition) with a step of  $\Delta \mathbf{u}_0(\mathbf{x}_0) \cdot \mathbf{n}_0(\mathbf{x}_0) = +10 \mu\text{m}$ .  
176 For the sake of brevity, only the deformation of the unit cell under the conditions of maximum compression / traction  
177 are reported in Figs. 2B,C, respectively. Examining the induced deformation, it is possible to infer that the stress,  
178 and thus the deformation, is mainly localized into the hinge-like regions, responsible for the activation of the inertial  
179 amplification mechanism<sup>43</sup>. The analysis also shows that the maximum Von Mises stress level reached in the structure  
180 is of 33.1 and 21.2 MPa, for the two types of loading condition, respectively. Given these values of maximum stress,  
181 and applying the von Mises yield criterion<sup>57</sup>, the minimum mono-axial tensile strength required for our material to  
182 have a safety factor  $\geq 1$  is  $\sigma_{min} = 33.1 \cdot \sqrt{3} = 56 \text{ MPa}$  (if we consider a state of pure shear solicitation), which is  
183 an acceptable value for epoxy<sup>58</sup>. Considering that the aforementioned value is obtained in the most strict condition  
184 of pure shear (which is not the case in the system under consideration), an elastic behaviour of the material, and  
185 thus of the band diagram, over the full range  $[-360, +130] \mu\text{m}$ , modulated by the intensity of the applied prestrain,  
186 is guaranteed, allowing for a full reversibility of the undeformed configuration (original dispersion diagram), once  
187 the load is removed. For the sake of completeness, since the small on large theory is considered here, the dynamic  
188 component of the stress is negligible with respect to the static prestress. For this reason it can be assumed that the  
189 safety factor does not change between the static and dynamic configuration.

190 Once the static analysis performed for the aforementioned sets of prestrain, the deformed geometries are assigned  
191 as the input unit cells to calculate the dispersion diagrams exploiting the Floquet-Bloch theory (see section II). The  
192 out-of-plane displacement of the structure is kept blocked also in this phase, in order to limit the dispersion analysis  
193 to waves belonging to the  $x_1 - x_2$  plane. The band structures are computed considering the unit cell to infinitely  
194 duplicate in a periodic linear array, and assuming the epoxy in its linear elastic regime (the hypothesis of small  
195 displacements is now applied). The unit cell domain is meshed by means of 8-node hexagonal elements of maximum

size  $L_{FE} = 0.2$  mm, which is found to provide accurate eigensolutions up to the frequency of interest<sup>59</sup>. It should be noted that, since the applied prestrain applied to each face of the cell induces isotropic deformation in the  $x_1 - x_2$  plane in both compression and traction cases, the deformation gradient  $\mathbf{F}$  and its affine component  $\mathbf{F}_L$  are diagonal and, as a consequence, the orientation of the reciprocal lattice vectors  $\mathbf{g}_1$  in the deformed configurations does not change with respect to that in the undeformed configuration. This implies that the orientation of the Bloch wavevector also remains unchanged between the undeformed and deformed configurations (see Fig. 1D). Therefore, the resulting eigenvalue problem  $(\mathbf{K} - \omega^2\mathbf{M})\mathbf{u} = \mathbf{0}$  is solved by varying the non-dimensional wavevector  $\mathbf{k}^*$  along the irreducible path  $[\Gamma - X]$ , with  $\Gamma \equiv (0, 0)$  and  $X \equiv (\pi/a, 0)$ , being  $a = \left(2 \cdot \sum_{i=1}^3 d_i + d_4\right)$  the lattice parameter.

Figure 3 reports parametric plots of the dispersion diagrams of the unit cell as a function of the external prestrain intensity inducing compression (Fig. 3A) or traction (Fig. 3B) states in the structure. The dispersion curves are color-coded on the base of the level of prestrain applied at the boundaries of the unit cell in the pre-loading phase. Specifically, the color bar of Fig. 3A varies gradually from  $-360 \mu\text{m}$  (blue: maximum compression state) to  $0$  (green: unprestrained condition), respectively. Analysing the band diagrams, it is possible to observe that increasing the compressive state in the unit cell induces (i) a general up-shift (curves shading into dark blue) of the dispersion branches, as well as (ii) group velocity inversion in the third band when  $k^*$  gets close to the high symmetry point  $X$ , as indicated by the black arrow. The band inversion is more evident comparing the dispersion curves singularly plotted for the  $-360 \mu\text{m}$  and  $0 \mu\text{m}$  prestrain cases, as reported in Fig. S1A and Fig. S1B. Further inspection of the dispersion diagram allows to infer that the unprestrained unit cell (green curves) allows for the opening of two BGs in the  $[0 - 3000]$  Hz frequency range, going from 170 to 470 Hz and 703 to 1180 Hz, respectively (see Fig. 4A at  $0 \mu\text{m}$  imposed displacement). The upper and lower bounds for both the first and second BGs shift in frequency for increasing values of the prestrain (see Fig. 4A). However, although the global width of the first BG experiences a limited variation, both its upper and lower bounds undergo a remarkable frequency shift (they both almost triple their frequency). On the contrary, the lower bound of the second BG is rather stable in frequency for increasing values of the prestrain, while its upper limit experiences a considerable frequency up-shift. This is responsible for an overall enlargement of the BG width (almost doubling with respect to the unstressed case). Finally, it is possible to notice that the lower bound of the second BG experiences a sort of inflection point when no displacement is imposed. The different behaviours of the two BGs highlights a selective nature of the prestress in altering the dispersion diagram. The aforementioned effects partially apply also for the case of unit cell subjected to an external traction pre-loading, i.e. both curve shifting and group velocity inversion are observed (Fig. 3B). However, in this case, group velocity inversion involves more bands (the third and fourth ones) and occurs at lower reduced wavenumber values ( $k^* \simeq \frac{\pi}{2a}$ ), as highlighted by the black arrows in Fig. 3B (refer to Fig. S1B and Fig. S1C for a direct comparison of the dispersion curves singularly plotted for the  $0 \mu\text{m}$  and  $+130 \mu\text{m}$  prestrain cases). This implies that, differently from the compression case, when an external state of traction is induced in the pre-loading phase, only few dispersion curves clearly shift towards higher frequencies (the first, the second, the fifth and sixth bands) over the full range of  $k^*$  (from  $0$  to  $\pi/a$ ), whereas some others (the third and the fourth ones) exhibit both a down- and an up-shift over a wide range of  $k^*$ . As a consequence, while the first BG is almost kept unaltered in terms of frequency width and slightly shifts towards higher frequencies (see Fig. 4B), the second BG experiences a remarkable width decrease (up to 3 times less the original BG).

At this point, it is worth to point out here the different dynamic behaviour of inertially amplified elastic metamaterials



with respect to the ordinary ones when subjected to an external state of prestress that emerges from the present research. Focusing the attention on the case of prestrain inducing tensile deformation in the structure, in ordinary PCs the BGs tend to decrease its frequency regime, being this effect mainly driven by the geometrical changes of the unit cell rather than by the effective stiffness and mass alteration introduced by the prestress (see for instance Fig. 3A of ref.<sup>44</sup> and relevant literature on ordinary PCs presented in section I). On the contrary, in the case of inertially amplified elastic metamaterials, where the displacement mechanism is used to amplify the effective inertia of small masses<sup>60</sup>, the state of external solicitation represents an important means to control the effective stiffness / effective mass ratio of the structure. This additional degree of freedom may lead to both an increase or decrease of the lower limit of the first BG frequency regime, under the same type of applied prestrain (see for instance Figs. 3B and 4B, where the lower limit of the first BG increases although a prestress condition inducing tensile solicitation in the structure is applied).

To gain further mechanical insights about this peculiar behaviour, a thorough explanation on the change of the effective stiffness / effective mass ratio of the structure as a function of the applied prestrain is provided with the help of the model reported in Fig. 5, and proposed for the first time by the research group of Yilmaz<sup>61–64</sup>. Figure 5A shows the rigid link equivalent model, which assumes pin joints at the middle points of the flexural hinges. Lumped parameters  $m$ ,  $m_a$  and  $k_{eff}$  are reported along with the principal geometrical parameters  $\vartheta$  (initial link angle) and displacements ( $\delta_x$  and  $\delta_y$ ) consequent the application of a prestrain inducing tensile solicitation in the system. Already in the undeformed configuration, an angle  $\vartheta$  exists between the equivalent rigid links (lines in red) and the ground.

$$f_p = \left( \sqrt{\frac{k_{eff}}{m_{eff} + m}} \right) / (2\pi) = \left( \sqrt{\frac{k_{eff}}{m_a(\cot^2(\vartheta) + 1)/4 + m}} \right) / (2\pi) \quad (10)$$

where  $m_a(\cot^2(\vartheta) + 1)/4$  defines the effective mass of the system.

When a tensile prestress is applied,  $\vartheta$  decreases to  $\vartheta_u$ , and the effective mass increases. If the stiffness  $k_{eff}$  is left unaltered, from Eq. (10) it clearly emerges that the lower limit of the first BG would decrease due to increase of the effective mass. However, if the effective stiffness  $k_{eff}$  increases more than the effective mass  $m_{eff}$  (the edge mass  $m$  does not depend on  $\vartheta$ ), then the lower limit of the first BG may also increase (this reasoning also applies to the case of prestrain inducing a compression state of solicitation and it may lead to analogous considerations).

To verify the correctness of the numerical approach proposed in this paper, a comparison of the analytical values of  $f_p$  deriving from Eq. (10) and the numerical solutions is performed and reported in Figs. 5B-D. Figure 5B reports the parametric plot of the dispersion curves of the unit cell when an external prestrain ( $[0 - 40] \mu\text{m}$  range) is applied inducing a tensile state in the structure. The  $[100 - 220]$  Hz frequency range is considered. The same polarization reported in Fig. 3 applies. The values of the frequency of the longitudinal branch responsible for the lower limit of the first BG are reported at the  $X$  high symmetry point in correspondence of the black arrows. Left panel of Fig. 5C reports the direct comparison of the analytical solution (triangular markers connected by the black line) deriving from Eq. (10) and the numerical results (magenta square markers). The values of  $k_{eff}$  introduced in the analytical model are directly calculated from the deformed numerical configuration according to standard homogenization procedures<sup>65,66</sup>. Right panel of Fig. 5C shows the variation of the effective stiffness  $\Delta k_{eff}$  and of the effective mass  $\Delta m_{eff}$ . This explains why the lower limit of the first BG increases, as shown in Figs. 3B and 4B, even if a tensile prestress is applied to the structure. Indeed, the effective mass increase  $\Delta m_{eff}$  (Fig. 5D) is far lower than the stiffness increase  $\Delta k_{eff}$  (this is due to the chosen geometrical characteristics of the unit cell, including the out-of-plane dimension

272  $h = t_2$  limiting the value of  $m_a$ ). As a consequence, it is possible to conclude that in this case the BG alteration is  
 273 mainly stiffness driven.

274 Finally, to clearly show the enhanced potential of inertial amplification PCs with respect to the ordinary ones when  
 275 an external prestrain condition is applied, additional calculations by changing some of the geometrical and mechanical  
 276 parameters of the unit cell are performed. Inspired by the analytical model reported in Fig. 5A, a configuration of  
 277 the unit cell allowing for the lower limit of the first BG to exhibit a non-monotone trend has been found and reported  
 278 in Fig. 6. It is possible to observe that the lower limit of the first BG now first decreases, i.e., the increase of the  
 279 effective mass is dominant - the red curve is above the blue one at low values of prestrain (yellow rectangle) and then  
 280 increases, i.e., the increase in effective stiffness is dominant - the red curve is below the blue one at higher values of  
 281 prestrain (green rectangle). This has been obtained by changing some of the model parameters as follows:  $d_3 = 18.5$   
 282 mm,  $t_3 = 18.5$  mm,  $m_a = 1$  kg/m<sup>3</sup> and multiplying by a factor of 10 the Lamè and Murnaghan material parameters.  
 283 These results suggest that a deformation of the unit cell geometry induced by a compressive / tensile prestress state,  
 284 already in the elastic regime, can lead to significant changes in the passband and BG behaviours of a periodic structure,  
 285 especially if the BG nucleation mechanism is lead by IA.

## 286 B. Transient Calculation

287 The confirmation of the above mentioned BG tunability is here verified through a nonlinear transient numerical  
 288 simulation of wave propagation conducted on a finite waveguide comprising 50 unit cells disposed in the  $x_1$ -direction,  
 289 as shown in Fig. 7A. The idea, here, is to pre-load some unit cells of the waveguide before exciting elastic waves at one  
 290 of its edge, in order to locally and reversibly change the dispersion diagram and confirm the ability of the waveguide  
 291 to switch from a pass- to a stop-band behaviour over a specific frequency range.

292 After having pre-loaded the array, so to uniformly reach the prestrain condition of  $-360$   $\mu\text{m}$  in 6 unit cells (Fig. 7B),  
 293 elastic waves are excited at the left edge of the waveguide by means of an imposed displacement of  $1$   $\mu\text{m}$  in the  
 294  $x_1$ -direction (red arrow in Fig. 7A). Two input signals are considered: (i) a triangular-like excitation (top-left panel  
 295 of Fig. 7C) and (ii) a Hanning modulated 11 sine cycles centered at 1400 Hz (top-right panel of Fig. 7C), exhibiting  
 296 a rather broadband and narrowband frequency content, respectively (bottom panels of Fig. 7C). Such pulses have  
 297 been chosen according to the band structure shifts reported in Fig. 3 and to highlight the tunable filtering capabilities  
 298 of the designed waveguide under prestressed conditions. In both excitation cases, 20 ms long time transient explicit  
 299 simulations have been performed in order to allow multiple wave reflections to take place at both the edge of the  
 300 waveguide and of the prestressed unit cells.

301 In the case of excitation (i), time transient displacements in the  $x_1$ -direction are recorded at the two acquisition  
 302 points R1 and R2 (Fig. 7B), taken equidistant from the prestressed regions and chosen respectively before (B/f) and  
 303 after (A/t) the prestressed portion of the waveguide. After acquisition, signals are Fourier transformed and compared  
 304 to highlight the differences of the two responses in terms of frequency content. Figure 7D reports the displacement  
 305 along the  $x_1$ -direction at points R1 and R2 (top panel), as well as their energy content in the frequency domain  
 306 (lower panel). The frequencies of the computed BGs as a function of the applied prestrain are also highlighted as a  
 307 shaded region, where the color scale refers to the level of imposed displacement in the pre-loading phase. Examining  
 308 the energy content it emerges that the Fourier transform of the signal acquired before the prestrained region (B/f

309 - red line), where the diagram reported in Fig. S1B applies, presents component in the 1000 – 1600 Hz frequency  
 310 range, whereas the signal registered after the prestrained region (A/t - black line) has no frequency components in  
 311 this frequency range. On the contrary, for frequencies above  $\simeq 1600$  Hz, the amplitudes of the frequency contents are  
 312 comparable. This is in agreement with the two different dispersion diagrams and clearly confirms the possibility of  
 313 the waveguide to switch from a pass- to a stop-band behaviour over the 1000 – 1600 Hz frequency range by readily  
 314 applying and removing the imposed deformations, respectively.

315 When the second type of excitation (i.e., the Hanning modulated 11 sine cycles centered at 1400 Hz) is applied to  
 316 the left edge of the waveguide, the switch potential is even more evident. Indeed, reconstructing the full wave field  
 317 displacements at specific time instants, it is clearly visible that the pulse is fully supported in the first portion of the  
 318 waveguide (where no prestress is applied), whereas when the prestrained region begins the wave is strongly reflected  
 319 back.

#### 320 IV. CONCLUSIONS AND FUTURE PERSPECTIVES

321 In conclusion, in this work the effect of the application of an external prestress on the dispersion diagram has been  
 322 investigated. The geometrical deformation of the unit cell consequent the action of an applied external load has been  
 323 determined through a static geometrically nonlinear analysis, representing the first step of a so called Updated La-  
 324 grangian scheme of calculation. A Floquet-Bloch decomposition has then been applied (second step) to the linearized  
 325 equations of the acousto-elasticity for the unit cell in the deformed configuration.

326 The effect of the prestress on the the original band structure (i.e., unit cell without any pre-loading phase) has been  
 327 demonstrated through parametric Floquet-Bloch analysis and further confirmed by nonlinear transient numerical sim-  
 328 ulations, proving the capability of the structure to switch from a pass- to a stop-band behaviour in the same frequency  
 329 range ([1000 – 1600] Hz).

330 The results presented herein provide insights in the behaviour of band gaps induced by inertial amplification, and  
 331 suggest new opportunities for real-time tunable wave manipulation.

332 Future investigations will concern the extension of the present study in the direction of a tensegrity-inspired re-  
 333 design<sup>67,68</sup> of the unit cell reported in Fig. 1. A self-similar<sup>69</sup> reorganization of the structural elements will allow  
 334 the construction of a tensegrity architecture. The design will derive from the D-bar tensegrity systems<sup>67,68</sup>, equipped  
 335 with longitudinal and transverse cables. The idea will be to recursively divide the longitudinal span of the cell into  
 336 segments of equal length and replace each new segment with a smaller scale unit with equal shape<sup>67</sup>. Self-equilibrated  
 337 tensile forces in the cables and compressive forces in the struts will give rise to an internal state of prestress. Cables  
 338 and struts will present an offset in the transverse direction in order to prevent material overlapping. The application  
 339 of a self-equilibrated system of forces composed of tensile forces in the cables and compressive forces in the struts  
 340 will give rise to an *internal* state of prestress, which can superimpose to the external state of prestress, analysed in  
 341 the present work. Such initial states of stress will contribute to the geometric term of the stiffness matrix of the  
 342 structure<sup>67</sup>, and allow for an extra degree of freedom for the optimal tuning of the dispersion relation of the system<sup>31</sup>.

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478 **Data availability.** The data that support the plots within this paper and other findings of this study are available  
479 from the corresponding author upon request.

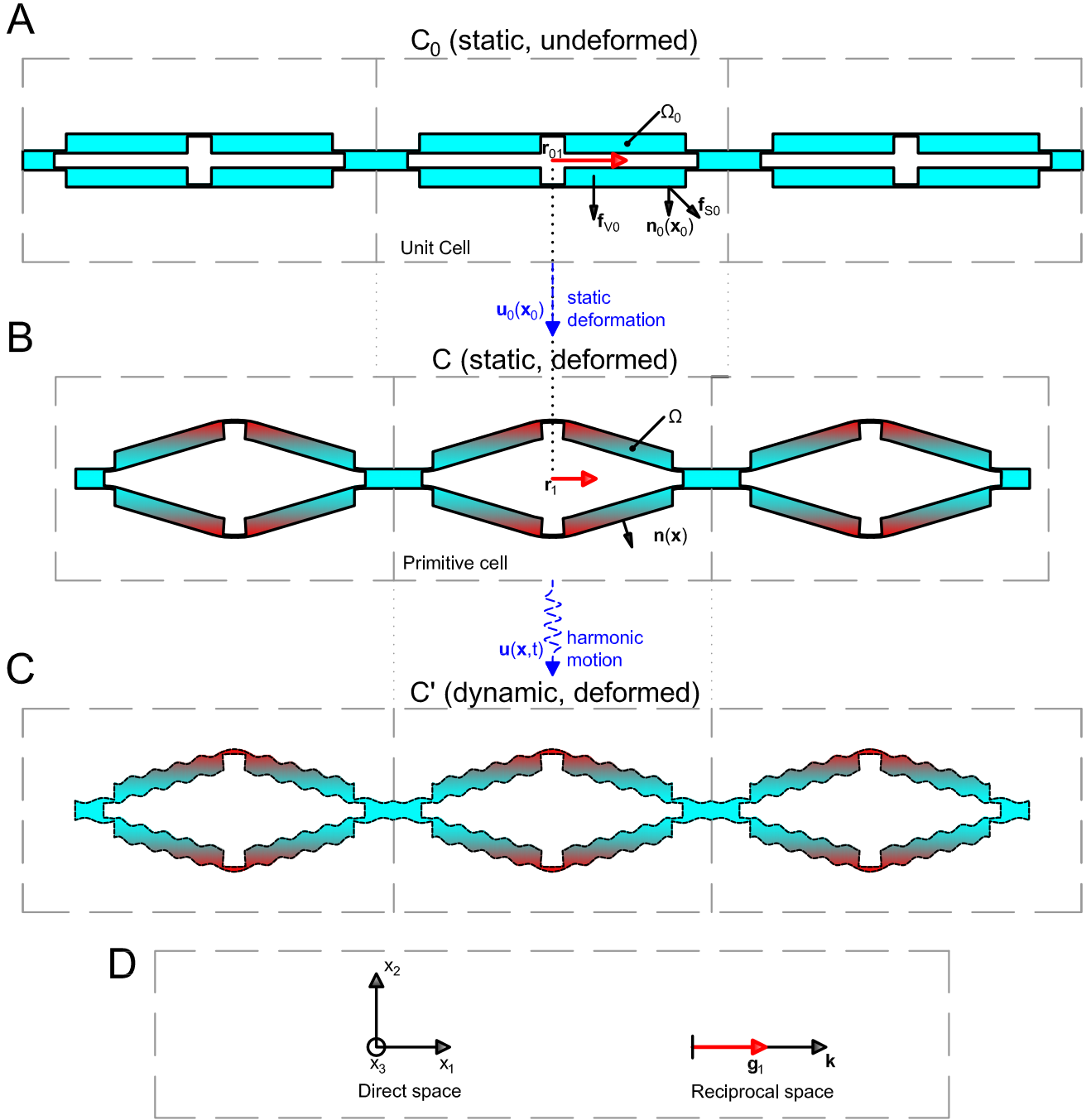


FIG. 1. **Graphic representation of the Updated Lagrangian scheme.** (A) The undeformed configuration  $C_0$ , i.e. the initial unit cell (delimited by dashed lines) used to calculate the displacement and stress fields introduced by the external mechanical load. (B) The static deformed configuration  $C$ , resulting from the application of the external mechanical load. (C) The dynamic configuration  $C'$  undergoing a harmonic motion. (D) The reference systems in the direct and reciprocal spaces.

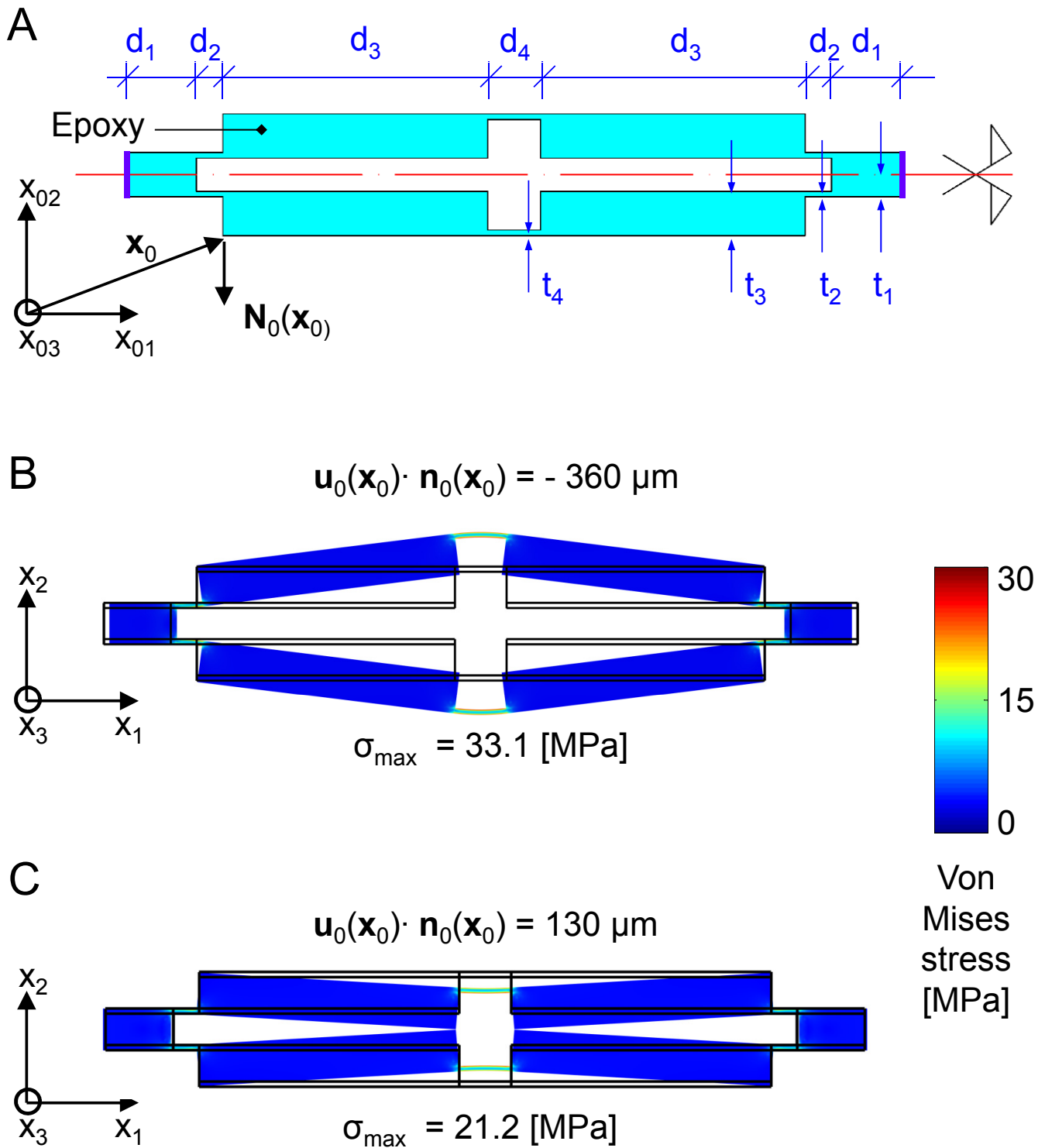


FIG. 2. Schematic representation of the undeformed unit cell and its deformed conditions under isotropic compression / traction. (A) Schematic representation of the unit cell exhibiting inertial amplification mechanism, positioned at  $\mathbf{x}_0$  with respect to the original reference systems  $x_{0i}$ , with  $i = 1, 2, 3$ . The structure is made of epoxy and it was proposed for the first time by Yilmaz et al. in ref.<sup>43</sup>. (B, C) Deformed configuration of the unit cell under isotropic  $\mathbf{u}_0(\mathbf{x}_0) \cdot \mathbf{n}_0(\mathbf{n}_0) = 130 \mu\text{m}$  traction ( $-360 \mu\text{m}$  compression). The colors denote the Von Mises stress in MPa. A maximum stress of 21.2 (28.6 33.1) MPa is observed. Deformations are in 1:1 scale.



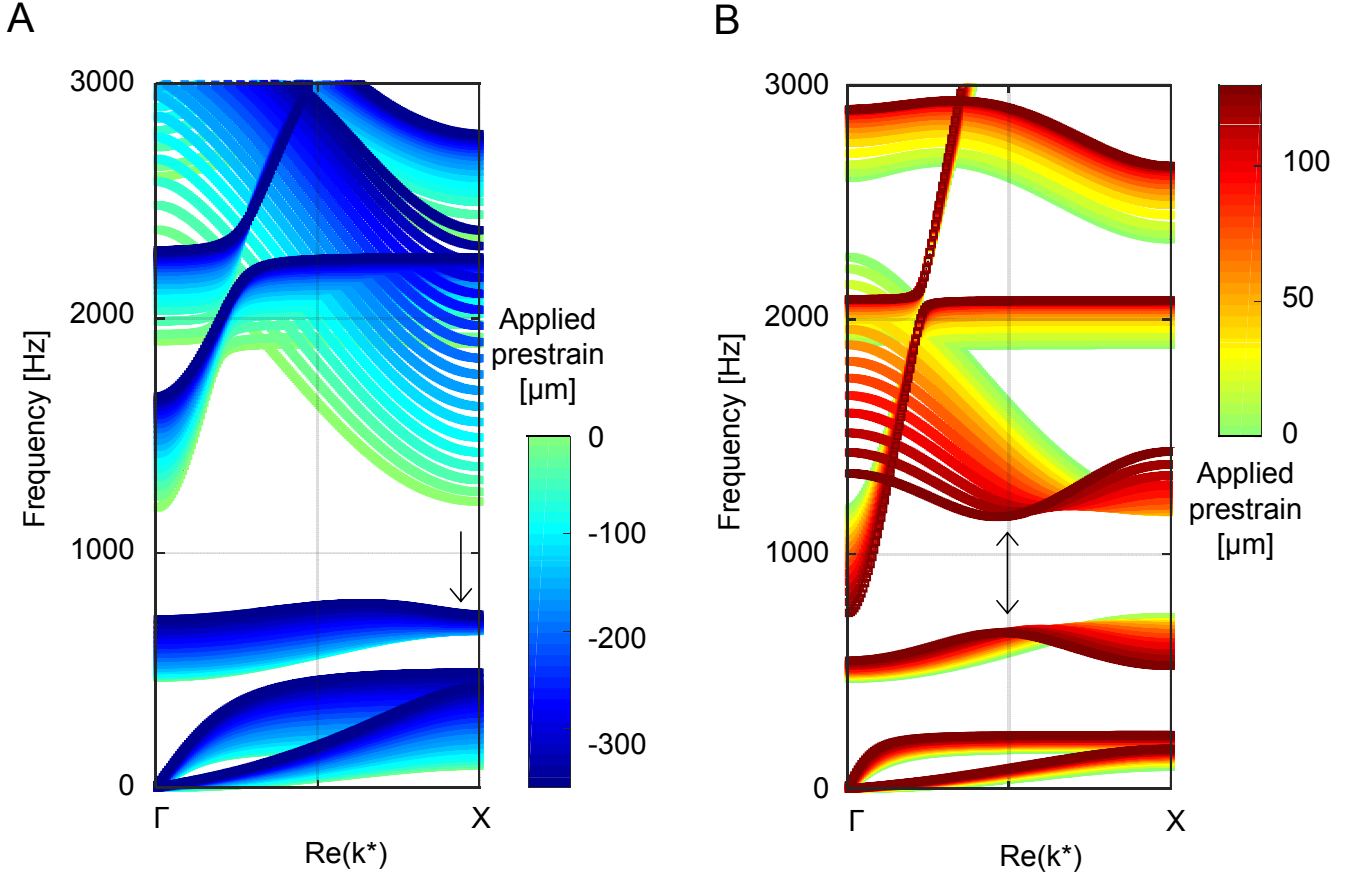


FIG. 3. **Band diagrams of the unit cell under different values of applied compression / traction.** (A) Parametric plot of the the real part of the reduced wavenumber  $k^*$  along the  $\Gamma - X$  irreducible path as a function of the applied prestrain inducing a compressive state in the structure. The dispersion curves are color-coded on the basis of the applied prestrain level at the boundaries of the unit cell in the pre-loading phase. The polarization factor color bar varies gradually from  $-360 \mu\text{m}$  (dark blue: maximum compression) to 0 (green: unprestrained structure). A general up-shift trend of the dispersion curves is observable (curves fading into dark blue) and a group velocity inversion (highlighted by the black arrow) occurs for the third band in proximity of the high-symmetry point  $X$ . (B) Parametric plot of the the real part of the reduced wavenumber  $k^*$  along the  $\Gamma - X$  irreducible path as a function of the applied prestrain inducing a tensile state in the structure. The dispersion curves are color-coded on the basis of the applied prestrain level at the boundaries of the unit cell in the pre-loading phase. The polarization factor color bar varies gradually from  $130 \mu\text{m}$  (dark red) to 0 (green: unprestrain structure). A general down-shift trend of the dispersion curves could be observed (curves fading into dark red). Group velocity inversions occur, in this case, in more bands (highlighted by the black arrows) and extend over a larger region of  $k^*$ .

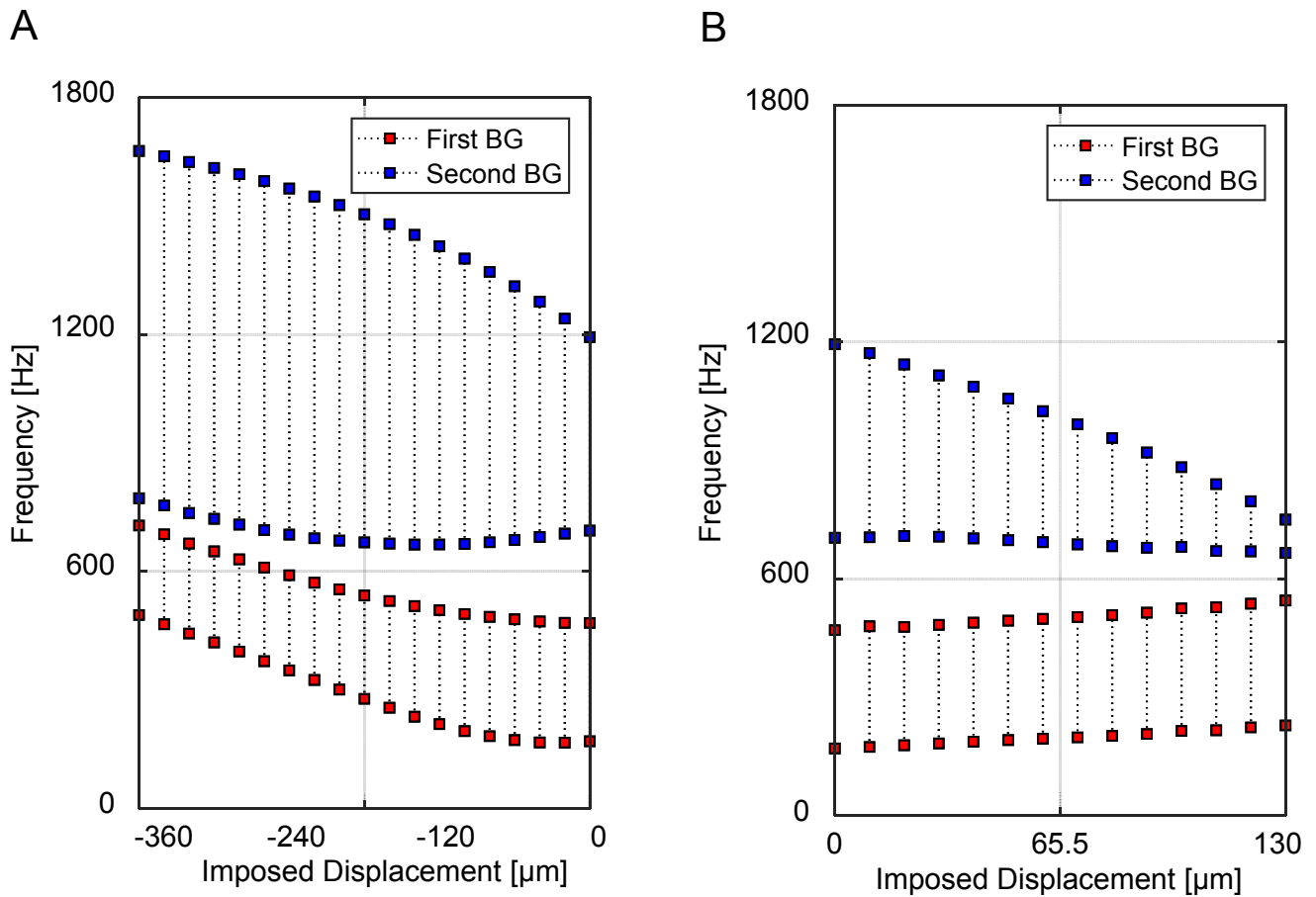


FIG. 4. Upper and lower bounds for the first and second BGs as a function of the applied prestrain inducing a compressive or tensile state in the structure. (A) In the case of increasing compressive prestrain, the first BG (black dashed lines delimited by red square markers) experiences a limited width variation, although both its upper and lower bounds are subjected to a remarkable frequency shift (towards higher frequencies). On the contrary, the lower bound of the second BG (black dashed lines delimited by blue square markers) is rather stable in frequency, while its upper bound still experiences a strong shift towards higher frequencies. This is responsible for an important global BG width enlargement (twice the initial value). (B) In the case of prestrain inducing a state of traction in the unit cell, a similar behaviour is observed for the first BG, whereas an important width reduction can be deduced for the second BG (up to three times the initial value), as the initial imposed solicitation is increased to  $130 \mu\text{m}$ .

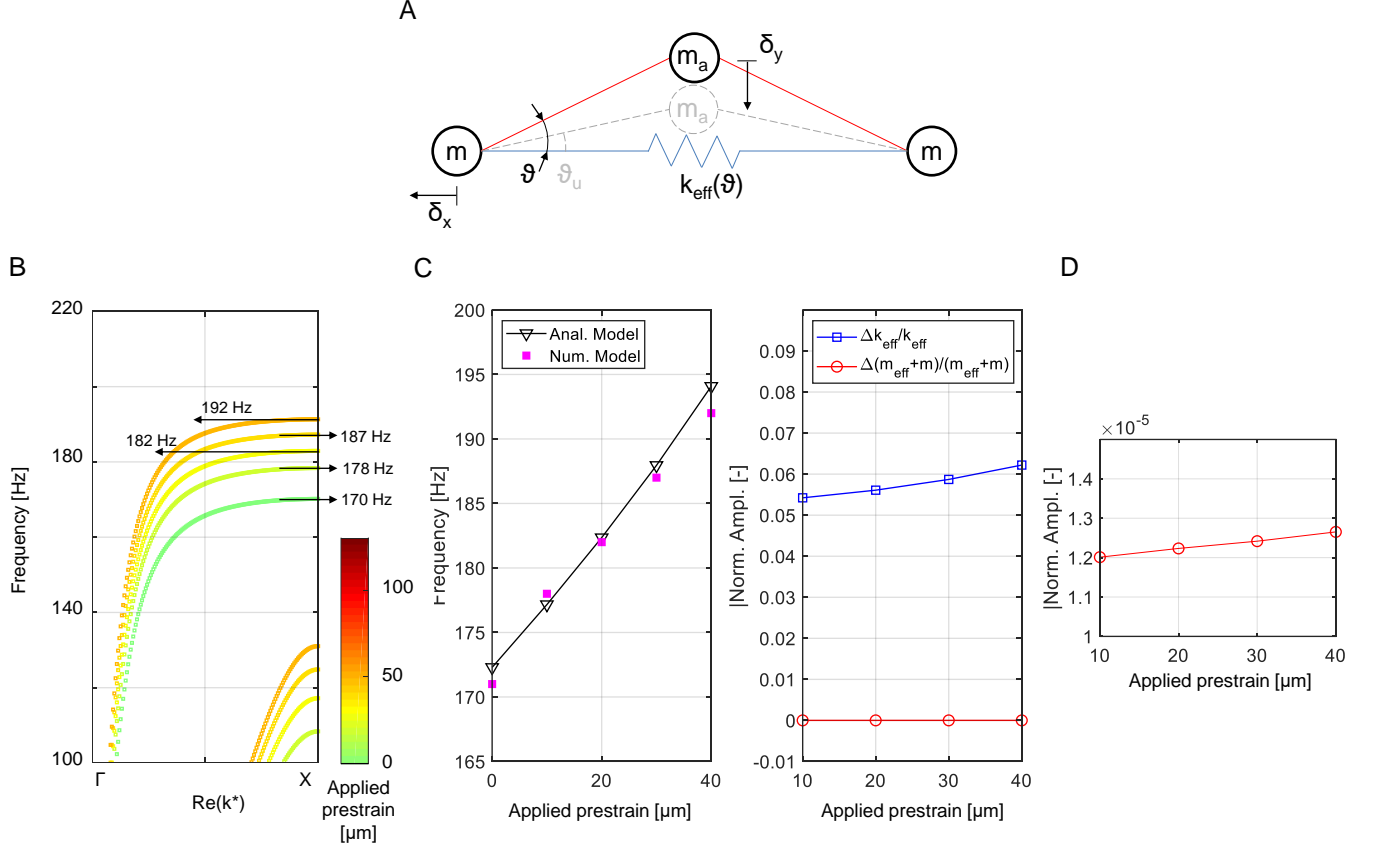


FIG. 5. **Change of the effective stiffness / effective mass ratio of the structure as a function of the applied prestrain: numerical - analytical comparison.** (A) Schematic representation of the rigid link equivalent model of the examined PC with inertial amplification mechanism<sup>62</sup>. Lumped parameters  $m$ ,  $m_a$  and  $k_{eff}$  are reported along with the principal geometrical parameters  $\vartheta$  (initial link angle) and displacements ( $\delta_x$  and  $\delta_y$ ) consequent the application of a prestrain inducing tensile sollicitation. (B) Parametric plot of the the real part of the reduced wavenumber  $k^*$  along the  $\Gamma - X$  irreducible path as a function of the applied prestrain inducing a tensile state in the structure in the [100 – 220] Hz frequency range. The same polarization reported in Fig. 3 applies. The values of the frequency of the longitudinal branch responsible for the lower limit of the first BG are reported at the  $X$  high symmetry point in correspondence of the black arrows. (C) Comparison of the analytical solution (triangular markers connected by the black line) deriving from Eq. 1 and the numerical values (magenta square markers) is reported in the left panel. On the right panel, the variation of the effective stiffness  $\Delta k_{eff}$  and of the effective mass  $\Delta m_{eff}$  explaining the reason of the lower frequency increase of the BG even if a tensile prestress is applied to the structure. Indeed, the effective mass increase is far lower than the stiffness increase. (D) Magnification of the change of the effective mass showing its increase.

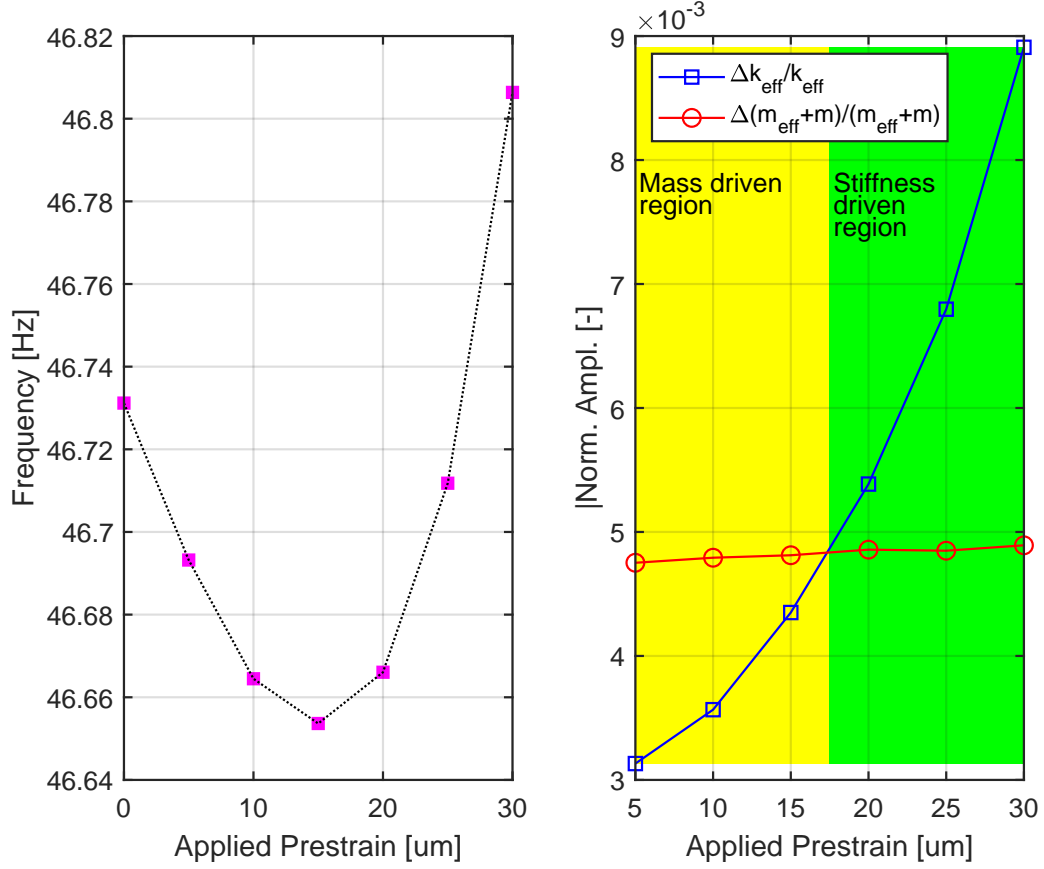
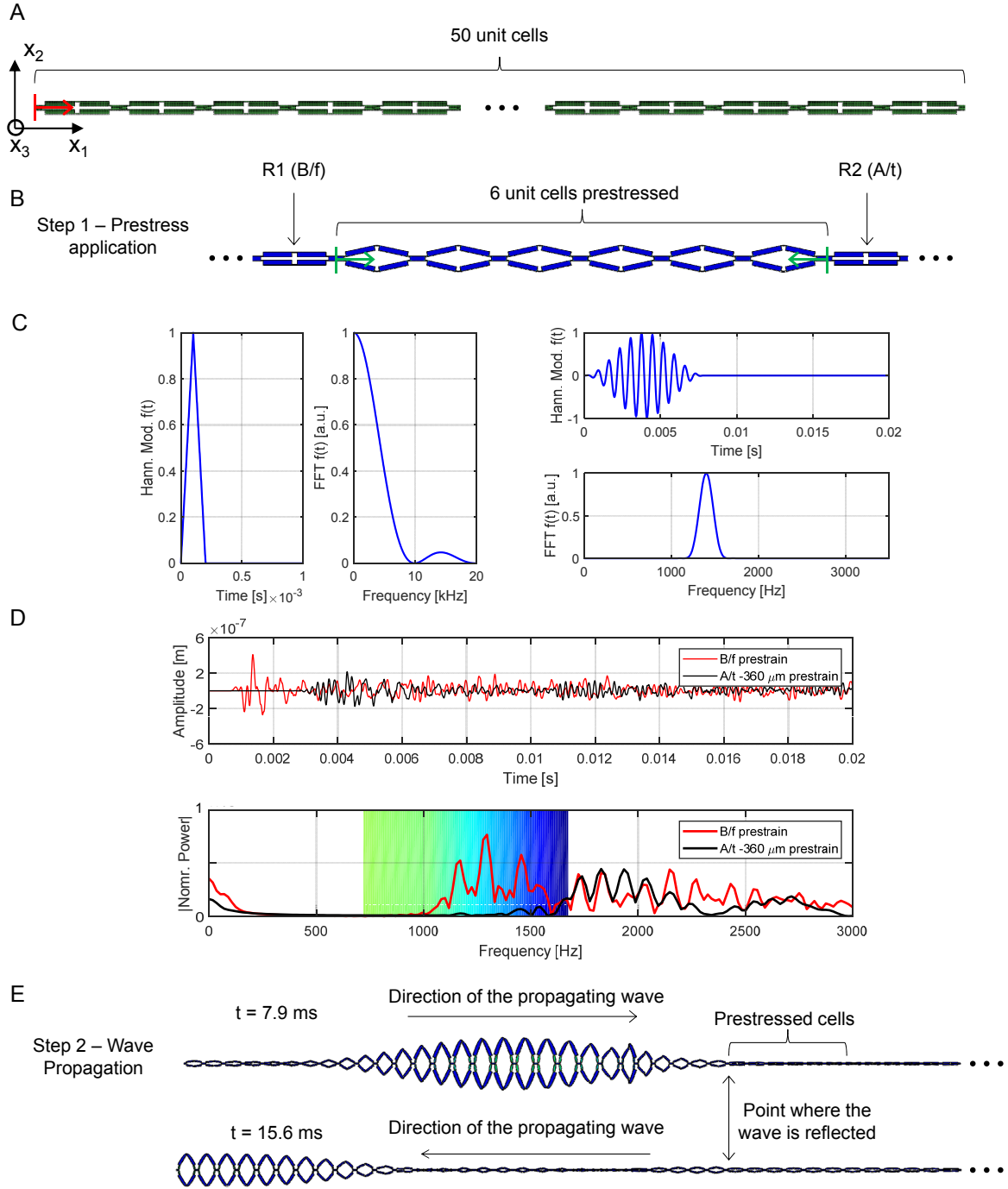


FIG. 6. **Additional degree of tunability of inertially amplified elastic metamaterials under external prestrain solicitation state.** (Left panel) Lower limit frequency of the first BG as a function of the applied prestrain. (Right panel) The variation of the normalized effective stiffness and of the normalized effective mass explaining the reason of the decrease / increase of the lower limit frequency of the first BG even if the same type of prestress (tension) is applied to the structure. Yellow and green rectangles determine the mass and stiffness driven regions, respectively.



**FIG. 7. Switch from a pass- to a stop-band behaviour of the waveguide.** (A) Schematic representation of the finite structure implemented for the nonlinear transient simulation. The model comprises 50 unit cells arranged in the  $x_{01}$ -direction. (B) Before exciting the propagation of elastic waves, an external load is applied over 6 internal unit cells of the array, so to locally induce the uniform prestrained condition of  $-360 \mu\text{m}$ . (C) Triangular-like (left panel) and 11 sine cycles centered at 1400 Hz Hanning modulated (right panel) excitations. (D) Signals recorded before (B/f) and after (A/t) the 6 prestressed unit cells (top panel) and their Fourier Transform (low panel), for the triangular-like excitation signal. The Fourier content clearly shows how the introduction of the prestress alters the frequency response function of the structure. The tunable BG is reported as a color-coded rectangle. The green region of the rectangle is the BG corresponding to the unprestrained unit cells (up to 1180 Hz), whereas the one fading to dark blue corresponds to the BG extension (up to 1680 Hz) induced by the introduction of the external compressive prestrain (up to  $-360 \mu\text{m}$ : dark blue). The comparison of the two signals proves that the same waveguide is capable to support or to inhibit waves having the same frequency content. (E) Snapshots at different time steps, for the narrowband excitation signal, showing how the unprestrained waveguide is capable of supporting the propagation of the wave, whereas the stressed region reflect back the majority of the waveform.

480 **APPENDIX A**

The different operators in Eq. (9) are expressed by:

$$\mathbf{M} = \bigcup_e \int_{\Omega_e} \mathbf{N}^T(\mathbf{x}) \rho(\mathbf{x}) \mathbf{N}(\mathbf{x}) da, \quad (11)$$

$$\mathbf{K}_1 = \bigcup_e \int_{\Omega_e} \mathbf{N}^T(\mathbf{x}) [\mathbf{B}^T \mathbf{D}(\mathbf{x}) \mathbf{B} + \mathbf{B}_0^T \boldsymbol{\Sigma}_0(\mathbf{x}) \mathbf{B}_0] \mathbf{N}(\mathbf{x}) da \quad (12)$$

$$\mathbf{K}_2 = \bigcup_e \int_{\Omega_e} \mathbf{N}^T(\mathbf{x}) [\mathbf{B}^T \mathbf{D}(\mathbf{x}) \mathbf{H} + \mathbf{B}_0^T \boldsymbol{\Sigma}_0(\mathbf{x}) \mathbf{H}_0] \mathbf{N}(\mathbf{x}) da, \quad (13)$$

$$\mathbf{K}_3 = \bigcup_e \int_{\Omega_e} \mathbf{N}^T(\mathbf{x}) [\mathbf{H}^T \mathbf{D}(\mathbf{x}) \mathbf{H} + \mathbf{H}_0^T \boldsymbol{\Sigma}_0(\mathbf{x}) \mathbf{H}_0] \mathbf{N}(\mathbf{x}) da, \quad (14)$$

481 where  $\Omega_e$  denotes the domain of the  $e$ -th finite element of the mesh,  $\bigcup_e(\cdot)$  the standard direct stiffness assembling  
482 procedure,  $\mathbf{N}(\mathbf{x})$  the matrix of shape functions for the  $e$ -th element, and  $\boldsymbol{\Sigma}_0(\mathbf{x})$  is a block-diagonal matrix of the form:

$$\boldsymbol{\Sigma}_0(\mathbf{x}) = \begin{bmatrix} \boldsymbol{\sigma}_0(\mathbf{x}) & \mathbf{0} \\ \mathbf{0} & \boldsymbol{\sigma}_0(\mathbf{x}) \end{bmatrix}, \quad (15)$$

while the different compatibility operators are expressed as:

$$\mathbf{B} = \frac{\partial}{\partial x_1} \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix} + \frac{\partial}{\partial x_2} \begin{bmatrix} 0 & 0 \\ 0 & 1 \\ 1 & 0 \end{bmatrix}, \quad (16)$$

$$\mathbf{B}_0 = \frac{\partial}{\partial x_1} \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix} + \frac{\partial}{\partial x_2} \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix} \quad (17)$$

$$\mathbf{H} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}, \quad \mathbf{H}_0 = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix}. \quad (18)$$

483 **APPENDIX B**

484 In this Appendix a direct comparison of the dispersion curves plotted for the specific cases of  $-360 \mu\text{m}$ ,  $0 \mu\text{m}$  and  
485  $+130 \mu\text{m}$  prestrain loads are reported as singular diagrams in Fig. S1.

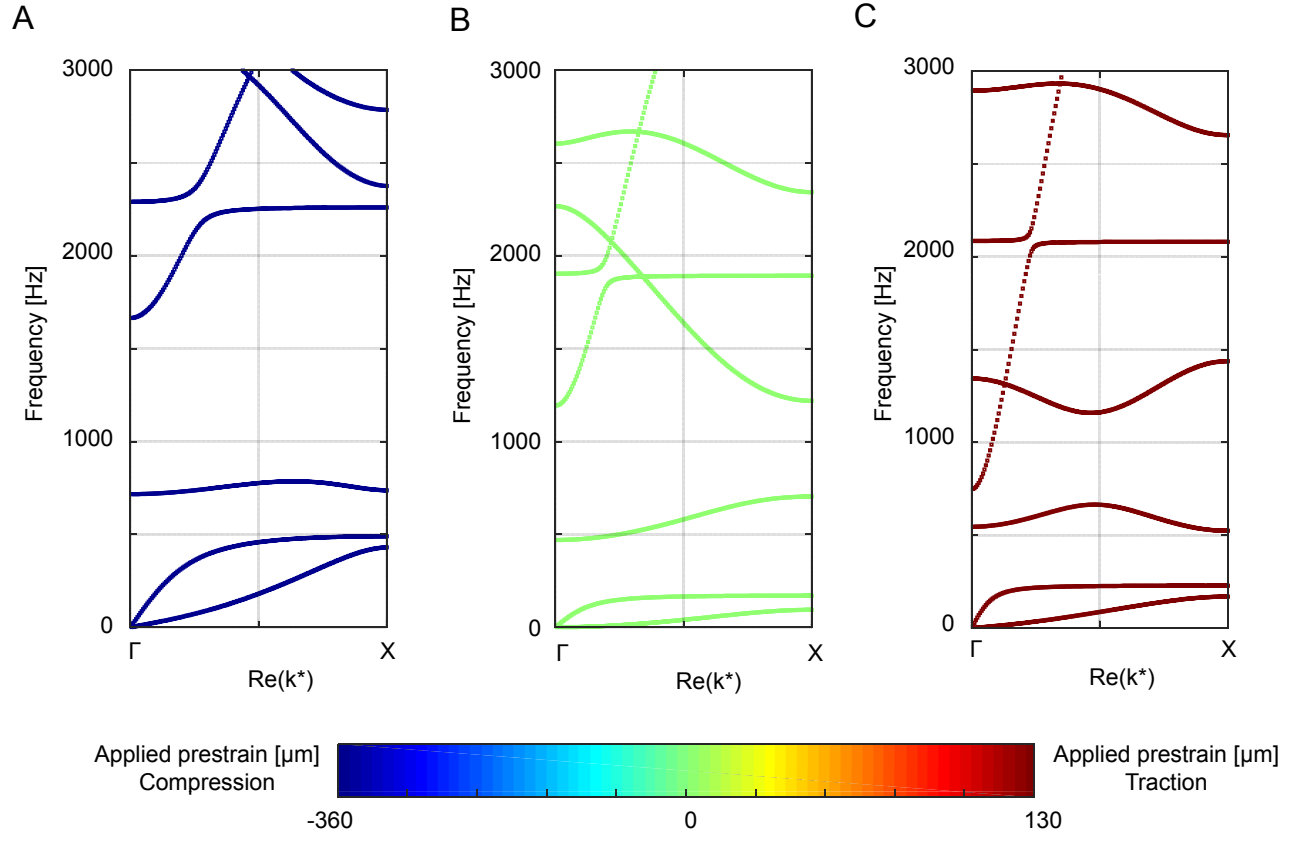


FIG. S1. **Plots of dispersion curves for single states of prestress.** Comparison of the dispersion curves plotted singularly for the (A)  $-360 \mu\text{m}$ , (B)  $0 \mu\text{m}$  and (C)  $+130 \mu\text{m}$  prestrain cases.