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High to Low pellet cladding gap heat transfer modeling methodology in an uncertainty quantification framework for a PWR Rod Ejection Accident with best estimate coupling

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Abstract. High to Low modeling approaches can alleviate the computationally expensive fuel modeling in nuclear reactor's transient uncertainty quantification. This is especially the case for Rod Ejection Accident (REA) in Pressurized Water Reactors (PWR) where strong multi-physics interactions occur. In this work, we develop and propose a pellet cladding gap heat transfer (H_{gap}) High to Low modeling methodology for a PWR REA in an uncertainty quantification framework. The methodology involves the calibration of a simplified H_{gap} model based on high fidelity simulations with the fuel-thermomechanics code ALCYONE1. The calibrated model is then introduced into the CEA developed CORPUS Best Estimate (BE) multi-physics coupling between APOLLO3[®] and FLICA4. This creates an Improved Best Estimate (IBE) coupling that is then used for an uncertainty quantification study. The results indicate that with IBE the distance to boiling crisis uncertainty is decreased from 57% to 42%. This is reflected to the decrease of the sensitivity of H_{gap} . In the BE coupling H_{gap} was responsible for 50% of the output variance while in IBE it is close to 0. These results show the potential gain of High to Low approaches for H_{gap} modeling in REA uncertainty analyses.

1 Introduction

The improvement of nuclear reactors computational modeling together with the increasing requirements in safety analyses lead to the development of Best Estimate Plus Uncertainty (BEPU) approaches [1]. BEPU is a systematic approach where Best Estimate (BE) codes are used to calculate safety criteria with an estimation of their respective uncertainties. BEPU is a step forward from conservative approaches allowing for better quantification of the safety margins. BE codes are considered the codes that take into account the most important underlying physical phenomena, governing the different studied scenarios, with reasonable approximations. Different BE codes usually model different physics. The correct modeling of transient scenarios can require the coupling between different BE codes due to the multi-physics interactions. This creates many challenges for the uncertainty quantification (UQ). With the term UQ we mean the estimation of the statistical distributions of the outputs of interest (in particular, their means and standard deviations) and the global sensitivity analysis of the outputs (in particular,

their Shapley indices). Many code evaluations are required for the estimation of the statistical quantities and of the sensitivity indices rendering thus the computational expensive modeling the main limitation. A large scope of undergoing research, in both academia and industry, is the multifidelity High to Low modeling approaches that can reduce in an efficient way the computational cost while retaining a good predictive modeling.

The multifidelity approaches combine different sources of information coming from high fidelity models, low fidelity models and experiments. The fundamentals work of [2] and [3] created the theoretical framework that lead to papers such as [4] in structural dynamics, where a cheap surrogate model based on Polynomial Chaos was considered as a low fidelity model and corrected by a high fidelity code in order to accelerate the Bayesian calibration process using experimental data. In [5] a methodology for combining information from multifidelity codes and experiments in a Bayesian hierarchical model was developed using Gaussian processes. In [6] a novel machine learning based multifidelity approach was discussed in the context of Bayesian optimization. A comprehensive and detailed survey of multifidelity methods in uncertainty quantification, statistical inference and optimization can be found in

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[7]. In nuclear and more particularly in thermal-hydraulics the result of the PREMIUM project [8] indicated a strong user effect in the input uncertainty quantification. For this purpose in [9] a set of good practices is discussed regarding the input uncertainty quantification.

In this work we focus on the study of the Rod Ejection Accident (REA) in Pressurized Water Reactors (PWR) with a multi-physics coupling in an UQ framework. During the REA strong multi-physics coupling effects occur between neutronics, fuel-thermomechanics and thermal-hydraulics. This necessitates a multi-physics modeling to take into account the interdisciplinary interactions increasing significantly the computational cost. The uncertainty quantification for REA becomes thus very challenging. In this coupling the fuel-thermomechanics modeling is the most expensive since it solves at the fuel rod scale the thermal conduction equations coupled with the thermo-mechanical ones at a fine discretization. A High to Low modeling is necessary to introduce and use a simplified model for fuel-thermomechanics reducing the computational cost. The high fidelity modeling manages to model complex thermo-mechanical and physico-chemical phenomena occurring during a REA. Some examples are the high burn-up structure, fission gas releases in the pellet-cladding gap and the pellet cladding mechanical interaction (PCMI). All these phenomena impact the fuel rod behavior through the pellet cladding gap heat transfer (H_{gap}). For this reason the low fidelity fuel-thermomechanics modeling usually does not model explicitly these phenomena but directly use a pre-defined H_{gap} value. There is, therefore, a strong interest in developing High to Low models for H_{gap} in REA. In this work, we develop and propose a methodology to develop such High to Low models for H_{gap} . The high fidelity fuel-thermomechanics code ALCYONE1 [10] is used to calibrate a simplified H_{gap} model based on fuel thermal expansion. Compared to previous works such as [5], the low fidelity model is not a fitted surrogate but a physics based model that is calibrated in a preliminary way by minimizing the discrepancy with ALCYONE1 predictions. The model is then introduced into the CEA developed CORPUS [11] Best Estimate (BE) multi-physics tool, where core neutronics code APOLLO3[®] [12] is coupled with core thermal-hydraulics code FLICA4 [13]. This creates an Improved Best Estimate (IBE) modeling of REA that is used for UQ. To the knowledge of the authors this is one of the first attempts to address H_{gap} High to Low modeling in transients. Some considerations have been discussed in the context of the UAM (Uncertainty Analysis in Modelling) benchmark [14]. The benchmark consists of three phases starting from stand-alone neutronics uncertainty analysis for steady state and reaching up to full coupling at the system level for transient scenarios. In this benchmark the H_{gap} is treated through lookup tables for the steady state and evolution calculations. However, there is not a dedicated treatment for the transient scenarios and this work and its prospects could be potentially integrated in the benchmark. Additionally in [15] the pellet cladding modeling was optimized including experimental data. The model's uncertainty was estimated as well.

In Section 2 we detail the two available coupling frameworks at CEA for the modeling of REA. The computationally expensive Best Effort coupling and the cheaper BE coupling. In Section 3 the specifications of the case study are presented. The geometry of the studied PWR core and the selected nodalization are provided together with the REA characteristics and the inputs and outputs of interest. The High to Low H_{gap} modeling methodology is based on the results of an UQ analysis performed with the BE coupling (BE UQ). In Section 4 we present these results. In Section 5 we present the calibration of the High to Low H_{gap} model. The simplified H_{gap} model is detailed and the calibration results are presented. As mentioned above, the obtained H_{gap} model is introduced into the previous coupling creating the IBE. In Section 6 an UQ analysis is performed with the IBE coupling (IBE UQ) and the results are compared with the BE results of Section 4. Finally, we end this article with the main conclusions and perspectives of this work.

2 REA coupling framework

The REA is initiated by a control rod ejection due to mechanical malfunction inserting positive reactivity in the core. As a consequence power increases adiabatically until the fuel temperature starts increasing as well introducing a Doppler negative feedback that creates a power peak. The power then continues to decrease and when the heat flux reaches the moderator its density will start decreasing adding another negative feedback due to the negative moderator temperature effect. Depending on the core state at the moment of the ejection the power evolution and its damage on the first containment barrier (cladding) can vary significantly. During the transient strong multi-physics interaction effects occur between neutronics, fuel-thermomechanics and thermal-hydraulics necessitating a multi-physics coupling framework.

At CEA two different coupling schemes are established [16] for the modeling of REA based on CORPUS multi-physics tool as can be seen in Figure 1a. APOLLO3[®] code is used for core neutronics, FLICA4 code for core thermal-hydraulics and ALCYONE1 code for pin fuel-thermomechanics. The Best Effort scheme involves the full coupling between the codes. At each time step the codes exchange 3D fields. APOLLO3[®] uses the fuel Doppler temperature T_f from ALCYONE1 and moderator temperature T_m from FLICA4 to compute the power generated in the fuel P_f and the fluid P_l . FLICA4 uses P_l from APOLLO3[®] and the cladding wall heat flux Φ_w from ALCYONE1 to compute the T_m and the external cladding wall temperature T_c^{ext} . ALCYONE1 uses the P_f from APOLLO3[®] and the T_c^{ext} from FLICA4 to compute the T_f and Φ_w . The Best Effort scheme models each discipline accurately but it is computationally very expensive for a full core REA and thus its use for the uncertainty propagation and global sensitivity analysis in the UQ framework is prohibited. For this reason the BE scheme is used where the coupling is reduced between APOLLO3[®] and FLICA4. The complex fuel-thermomechanics phenomena

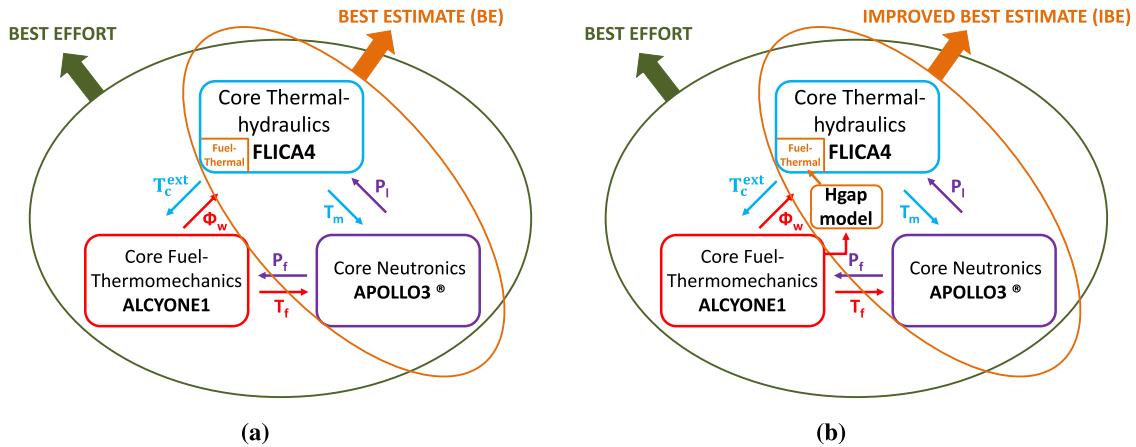


Fig. 1. CEA coupling framework used for REA (a) and the proposed improvement in the BE scheme (b).

during REA are modeled by the fuel-thermal module in FLICA4. In this module only the thermal aspects are modeled and all the other phenomena are taken into account through a constant H_{gap} during the transient. This simplification is very limiting for the UQ because it leads to the use of large H_{gap} uncertainties in order to penalize for the poor thermomechanics modeling. In this work we develop and propose an offline High to Low H_{gap} modeling methodology that alleviates the poor H_{gap} modeling issue during REA. This creates the IBE coupling scheme illustrated in Figure 1b.

3 Case study

3.1 PWR geometry and modeling

The REA is studied in a large scale PWR core. The geometry has an 1/8 symmetry illustrated in Figure 2. It consists of 193 fuel assemblies with UO_2 and $UO_2 - GdO_3$ fuel compositions. Two different types of control rods are inserted at different depths. The black rods (B) with high neutrons absorption that are typically used for the shut-down of the reactor and the grey rods with less neutrons absorption that are used in the day to day reactivity control. The core is at Hot Zero Power (HZIP) conditions at the end of the cycle. Around the fuel assemblies there is one ring of water reflector assemblies. The total height of the core is 468.72 cm with a bottom and top reflector of 21 cm leading to a fuel active height of 426.72 cm. Each assembly is a 17×17 lattice of fuel pins with pitch 21.504 cm. The control rod that will be ejected initiating the REA is located on the periphery as highlighted in Figure 2. It is inserted 97 cm from the top into the fuel active region. Due to the extraction of the control rod there is 1/2 symmetry for the REA.

The REA in the PWR core geometry is modeled using the BE and IBE coupling scheme discussed in Section 2. For core neutronics, APOLLO3[®] code is used with a two group Diffusion approximation and void boundary conditions on the neutron current. The two group macroscopic cross-sections are parameterized in burn-up, boron

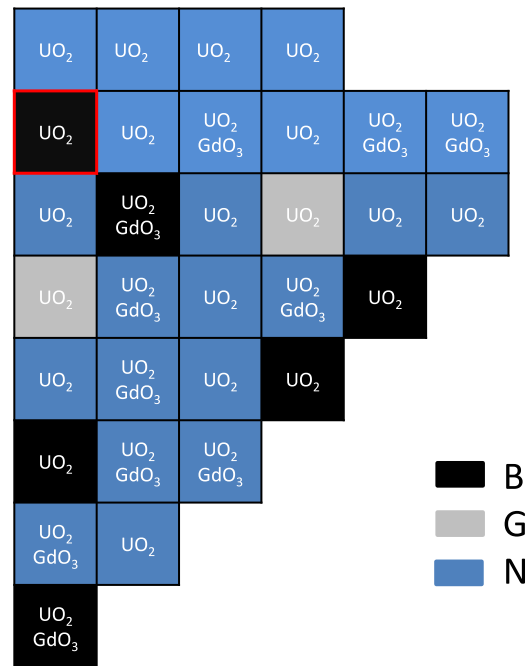
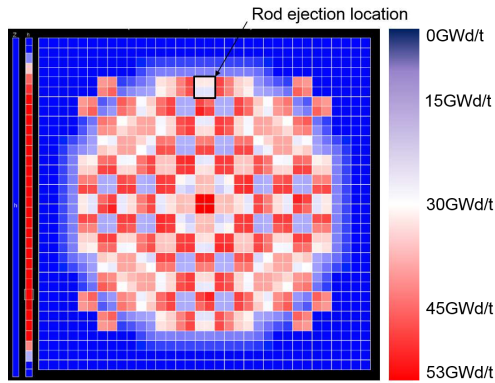


Fig. 2. PWR 1/8 core geometry and characteristic dimensions. B indicates assemblies with black control rods, G with grey control rods and N with no control rods. The ejected control rod location is highlighted with red borders.

concentration, moderator density and fuel temperature. The radial discretization is at the level of the quarter of assembly. For the axial discretization 34 meshes are used of which 30 are for the fuel active height and the rest for the top and bottom reflectors. For core thermal-hydraulics, FLICA4 is used with a 4 equations porous modeling and a multi-1D axial flow approximation. The system of 4 equations consists of: mixture mass balance, vapor mass balance, mixture momentum balance and mixture energy balance. The boundary conditions are the inlet mass flow and enthalpy and the outlet pressure. For the radial discretization one thermal-hydraulic channel is used for each assembly. For the axial discretization

Table 1. HZP initial conditions of the PWR core.

Initial core power	3.8 W
Moderator density	0.745 g/cm ³
Pressure	155 bar
Volumetric flow rate	90954 m ³ /h
Fuel temperature	290 deg C
Moderator temperature	290 deg C
Boron concentration	95.5 ppm

**Fig. 3.** PWR core burn-up radial distribution in the core.

only the fuel active part is modeled using 30 meshes in accordance to APOLLO3[®] modeling. One average fuel pin per thermal-hydraulic channel with 1D radial modeling is used in FLICA4 with a discretization of 25 radial regions for the fuel and 3 for the cladding. For the time discretization of the REA an adaptive end time is adopted based on the integral power evolution. For each transient in the UQ when the power surpasses half its nominal value then a SCRAM signal is sent. It is considered that from this time on 0.6 s are needed in order for the SCRAM to take place and end the modeling of the transient. The incremental time step is constant and equal to 0.001 s. The control rod is ejected in 0.1 s.

3.2 Initial state and reference transient

The PWR core is critical at the end of the cycle with HZP condition, meaning that the temperature is around 290 deg C and the power negligible (3.8W). Since the core is at the end of the cycle the boron concentration is quite low at 95.5 ppm. Other characteristic conditions of the core are provided in Table 1. There is a burn-up distribution resulting from core evolution calculation performed in a previous internal CEA study. The obtained radial burn-up distribution at the end of cycle is illustrated in Figure 3. The burn-up radially averaged at the level of the assembly ranges from 10 to 52 GWd/t. The location of the ejected control rod is close to the periphery. In the core there is a radial and axial Xenon distribution that increases the control rod worth leading to an increased reactivity insertion and thus a violent prompt driven transient.

The reference (without uncertainties) REA characteristics obtained with the BE coupling are presented in

Table 2. Reference REA characteristic quantities.

Effective delayed neutron fraction	569 pcm
Control rod worth	1.2 \$
Maximum core power	2.54P _{nom}
Final core power	0.09P _{nom}
Power pulse width	38 ms
Time of maximum core power	292 ms
Maximum 3D deformation factor	25

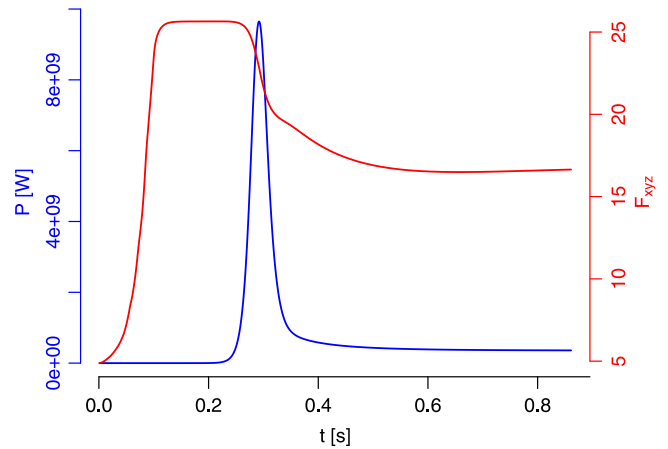
**Fig. 4.** Integral power and F_{xyz} deformation factor evolution for the reference REA.

Table 2 and Figure 4. The control rod worth is $\rho_{\text{worth}} = 1.2 \$$ indicating a prompt driven transient. In the Figure we can observe the created power pulse of width $\Gamma = 38$ ms with a maximum power of $P_{\text{core}}^{\text{max}} = 2.54P_{\text{nom}}$ at instant $t^{\text{max}} = 292$ ms. The nominal power is $P_{\text{nom}} = 3800$ MWth. Additionally, the F_{xyz} deformation factor evolution in time is plotted. It starts from a value of 5 and reaches up to 25 when the control rod is fully ejected (0.1 s).

3.3 Input and outputs identification

Before presenting the BE UQ results we define the uncertain inputs that will be considered together with the outputs of interest. The inputs and outputs for the three disciplines are defined in Table 3. The statistical distributions of the inputs are presented in [17] and are included in Appendix A. In neutronics the two-group macroscopic cross-sections and the kinetic parameters are considered with a multivariate normal distribution. The rest of the inputs are considered independent of the neutronic inputs and between them. The thermal-hydraulic input distributions are mainly based on CEA experts opinions and are applied as random multiplicative factors with mean 1 on the different models. The UAM recommendations are used for the fuel-thermal inputs, i.e. for the thermal conductivities and specific heat capacities. The H_{gap} is the quantity of focus in this work. In the BE coupling scheme H_{gap} is an uncertain constant with a uniform distribution between the value for a complete open gap ($2e^3 \text{ Wm}^{-2} \text{ K}^{-1}$) and the one for a pellet-cladding contact ($5e^4 \text{ Wm}^{-2} \text{ K}^{-1}$). In

Table 3. Inputs and outputs identification by discipline: **neutronics**, **fuel-thermal** and **thermal-hydraulics**.

Inputs (22)			
$TD_g(\mathbf{2})$	Disappearance cross-section of group g	$NF_g(\mathbf{2})$	ν xfission cross-section of group g
$D_g(\mathbf{2})$	Diffusion coefficient of group g	$S_{1 \rightarrow 2}$	Scattering cross-section of group 1 to 2
$IV_g(\mathbf{2})$	Inverse velocity of group g	β_{eff}	Effective delayed neutrons
λ_{eff}	Effective decay constant		
λ_f	Fuel thermal conductivity	λ_c	Cladding thermal conductivity
C_{Pf}	Fuel specific heat capacity	C_{Pc}	Cladding specific heat capacity
H_{gap}	Fuel-cladding gap heat transfer	T_R	Rowland temperature
P_r	Power radial profile		
H_c	Convective heat transfer	R_{crit}	Criterion for post-DNB heat transfer
R_{v0}	Recondensation	H_{dnb}	Post-DNB heat transfer
Outputs (3 scalars + 1 functional)			
P_{lin}^{max}	Local linear power (max in time)	$P_{lin}^{2D}(x, y)$	Radial distribution of linear power at the time and axial position of P_{lin}^{max}
H_f^{max}	Fuel stored enthalpy (max in time)		
DNB^{min}	Distance from R_{crit} (min in time)		

the IBE H_{gap} is calculated by a model and thus the uncertainty will be carried by the model parameters. For the outputs 3 scalars and 1 functional output are considered. In neutronics we consider the maximum in time and space of the local linear power during the REA P_{lin}^{max} and the radial linear power distribution P_{lin}^{2D} at the time instance and axial plane of P_{lin}^{max} . In fuel-thermomechanics we selected the maximum in time and space of the local stored enthalpy H_f^{max} while in thermal-hydraulics the minimum in time of the distance to Departure from Nucleate Boiling (DNB) DNB^{min} . The latter output is defined as the difference between the Departure from Nucleate Boiling Ratio (DNBR) and the DNB threshold R_{crit} . The UQ methodology is detailed and tested in [17] and [18]. The methodology consists of an initial screening of the inputs and the use of kriging models [19] to perform uncertainty propagation and global sensitivity analysis using Shapley indices [20,21]. More details about the methodology are discussed in Appendix B. The obtained results for the uncertainty propagation and global sensitivity analysis will be presented directly for both BE and IBE coupling schemes.

4 Best estimate uncertainty quantification

In this section we present the results of the BE UQ for the REA. The uncertainty propagation is performed by training kriging models between each scalar output and a reduced number of screened inputs. The screening is performed with a method based on HSIC statistical significance tests [22,23] presented in [17]. The kriging models are trained on a Latin Hypercube Sampling (LHS) of size 250. For the functional output Principal Component Analysis (PCA) [24] is used and kriging models are trained for two principal components that represent 95% of the outputs variances. For all the quantities of interest the obtained Q^2 of the kriging models, evaluated on a separate LHS of size 125, is close to 1 with smallest value 0.98 for DNB^{min} and 0.945 for the second principal component of P_{lin}^{2D} . More detailed results are provided in Appendix B.

The kriging models are used for brute force Monte Carlo uncertainty propagation with 10^5 samples and the results are presented in Figure 5. In each histogram we plot also the pdf of a normal distribution with the estimated mean and standard deviation (blue line) for a visual comparison of the normality. In Appendix B we present also the estimated relative standard deviations for the scalar quantities directly using the training LHS. It is important to notice that it is not recommended to use surrogate models for accurate estimation of the tails of the output pdf since they consist of rare events that the surrogate model has not been trained for.

We observe a quite large relative standard deviation for P_{lin}^{max} of around 57%. The result for P_{lin}^{2D} shows that the spatial distribution of the relative standard deviation does not vary significantly radially. For H_f^{max} a 20% relative standard deviation is obtained and the distribution is approximately normal. For DNB^{min} a large mean value is obtained with large relative standard deviation of 57% resulting in a very small probability of reaching boiling crisis.

For the global sensitivity analysis, Shapley indices are estimated for the scalar outputs and aggregate Shapley indices for the functional ones as discussed in [17]. All the Shapley indices are estimated using the kriging models. For a more detailed focus on the Shapley indices estimation with surrogate models we refer to [25]. The R language [26] package “sensitivity” [27] (function “shapleyPermRand”) was used for the estimation of the Shapley indices and their confidence intervals, that quantify the uncertainty of the estimation method. The results are presented in Figure 6. The inputs in this Figure are the selected ones by the screening process of the UQ methodology. For the outputs P_{lin}^{max} , P_{lin}^{2D} and H_f^{max} the β_{eff} is responsible for 50% of the output variance with the other 50% attributed to the cross-sections TD_1 , D_1 , $S_{1 \rightarrow 2}$ and IV_1 . All these cross-sections are highly correlated to each other and thus it is difficult to distinguish their separate contributions. For the output DNB^{min} the H_{gap} is the dominant input responsible for 50% of the output variance while the remaining 50% is attributed to the

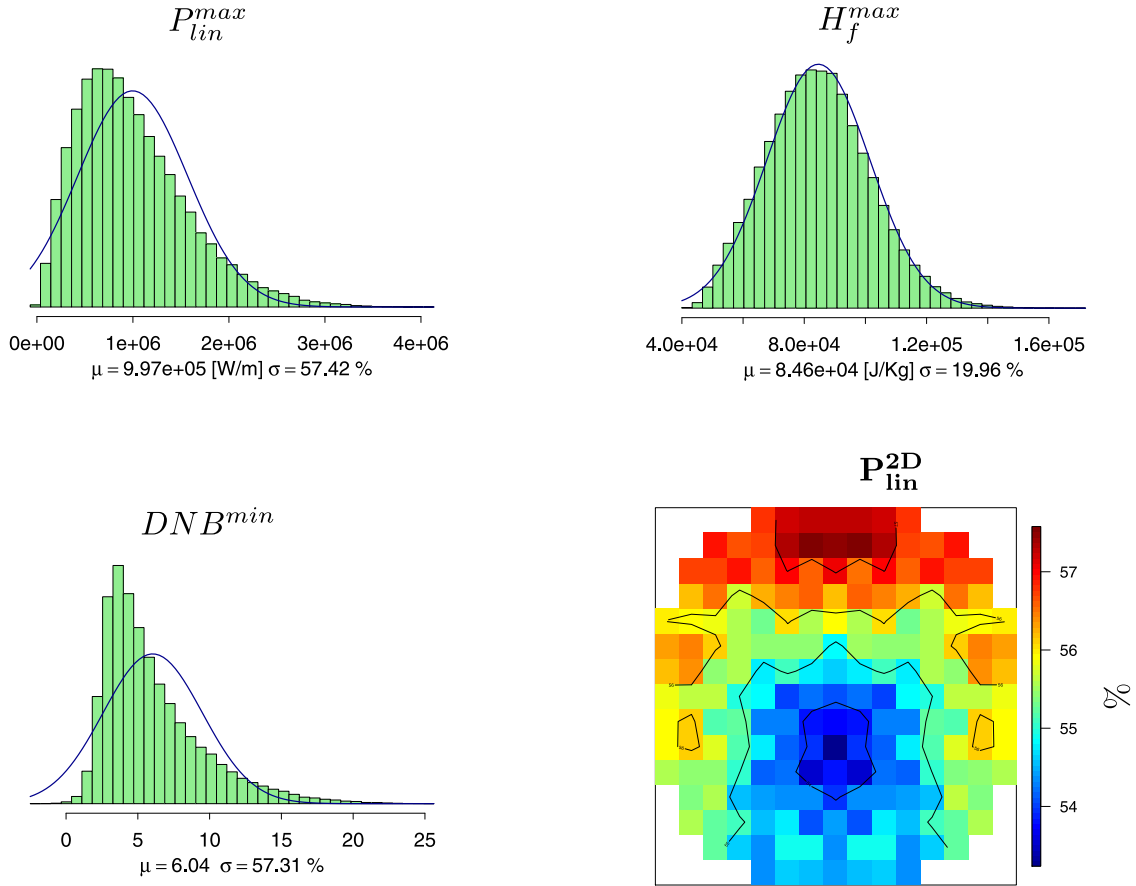


Fig. 5. P_{lin}^{max} , H_f^{max} and DNB^{min} histograms and P_{lin}^{2D} relative standard deviation distribution for BE UQ analysis.

cross-sections and the β_{eff} . This is due to the large H_{gap} uncertainty ranges and thus gives the incentive to improve its modeling.

5 High to low pellet cladding gap heat transfer modeling methodology

5.1 Introduction

The gap heat transfer (H_{gap}) modeling in the BE coupling is performed through a constant value during the REA with a uniform distribution over a large interval. This is one of the most important modeling differences between Best Effort and BE coupling. There is a strong interest thus to improve the H_{gap} modeling and to introduce it into a refined coupling that we will call Improved Best Estimate (IBE). In this subsection we address this challenge by developing a High to Low H_{gap} modeling methodology. The methodology involves the calibration of a simplified H_{gap} model that is based on fuel thermal expansion. We consider that this model is adequate for the REA and especially for the gap closing phase. The calibration is performed through decoupled ALCYONE V1.4 calculations with imposed power evolution. In this Section we first detail the model with its calibration parameters.

Afterwards, we present the methodology where we discuss issues such as how the power pulses are selected, how many H_{gap} models will be created for the different fuel assemblies etc. Finally, we present the calibration results for the PWR core.

5.2 Pellet cladding gap heat transfer simplified model

The sharp power increase in the REA leads to a corresponding sharp fuel temperature increase. We assume that the H_{gap} evolution is driven by the gap closing due to fuel thermal expansion and by the gas conductivity evolution in the gap. This is used to derive the simplified formulation for H_{gap} defined by equations (1a)–(1c).

$$H_{gap} = \frac{\lambda_g(T_g, E_f)}{e(T_f)}, \quad (1a)$$

$$\lambda_g = \lambda_{g,init} \left(1 + \theta_1 \frac{T_g - T_{g,init}}{T_{g,init}} + \theta_2 E_f \right) \quad (1b)$$

$$e(T_f) = r_{c,init} - r_f(T_f) \quad (1c)$$

where:

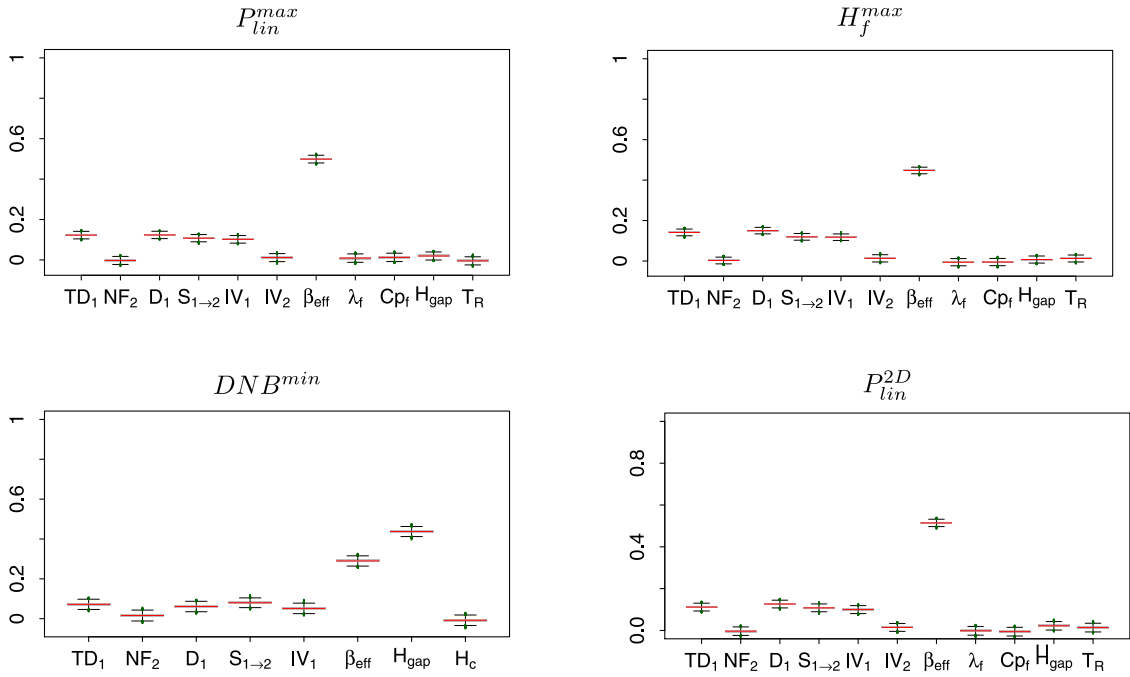


Fig. 6. P_{lin}^{max} , H_f^{max} and DNB^{min} Shapley indices and P_{lin}^{2D} aggregate Shapley indices for BE UQ analysis.

- λ_g is the gas conductivity in the gap and $\lambda_{g,init} = \frac{H_{gap}^{init}}{e_{init}}$ its initial value prior to the REA. The latter is calculated by the initial gap heat transfer H_{gap}^{init} and initial gap width e_{init} .
- T_g is the gas temperature and $T_{g,init}$ the initial gas temperature prior to the REA.
- E_f is the energy stored in the fuel during the REA.
- θ_1 and θ_2 are two calibration parameters that have to be estimated.
- e is the pellet-cladding gap width. It is assumed that only the fuel expansion is responsible for the gap evolution.
- $r_{c,init}$ is the initial internal cladding radius prior to the REA.
- $r_f = r_{f,init}\alpha_f(T_f)$ is the fuel external radius. The fuel expansion is modeled using the fuel expansion coefficient $\alpha_f(T_f)$ in ALCYONE1 which is a cubic function of the fuel temperature T_f .

The H_{gap} predicted by the proposed simplified model is based on fuel thermal expansion and depends on the evolution of the λ_g and e . The λ_g is considered a linear function of T_g and E_f . The latter allows to include a historical effect on the H_{gap} . The two calibration parameters to be determined θ_1 and θ_2 are the coefficients of T_g and E_f respectively. The e evolution is assumed to depend only on the fuel thermal expansion while the cladding radius remains constant. For the modeling of the gas temperature T_g the average between the external fuel temperature and the internal cladding temperature is used.

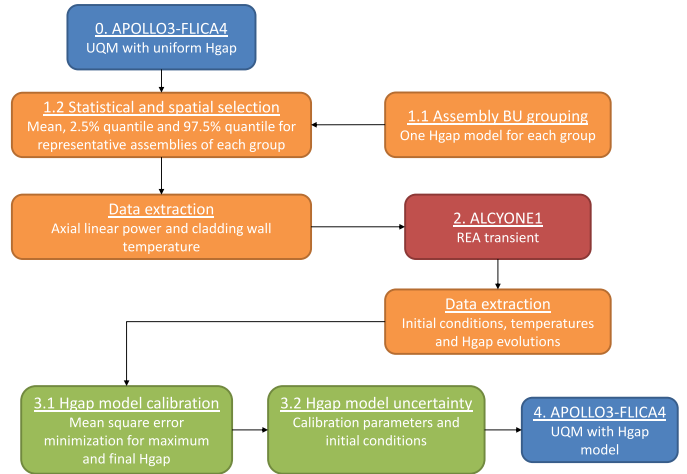


Fig. 7. High to Low H_{gap} modeling methodology scheme.

5.3 Methodology

Having defined the simplified H_{gap} model the next step is to calibrate it. To this purpose we developed the High to Low methodology illustrated in Figure 7.

The starting point is the application of the UQ methodology in the BE coupling of Section 4. The temperature evolution in the fuel depends on the fuel assembly burn-up and the power seen by this assembly at its position in the core. Since we need to build a H_{gap} model for every fuel spatial mesh (1080 meshes) a clustering is necessary. In step 1.1, we cluster the assemblies by similar radial average burn-up. This means that we will construct one H_{gap} model for every identified cluster. While each cluster will have the same model, their different fuel initial conditions

and the different power seen during the REA will lead to a 3D H_{gap} .

The next step 1.2 consists in selecting representative pulses from the BE UQ presented in Section 4. The pulses must cover most of the possible H_{gap} variations inside the cluster due to both statistical and spatial aspects. For the statistical aspect three pulses are extracted: namely the ones which have produced the mean, the 97.5% upper quantile, and the 2.5% lower quantile of P_{lin}^{max} . For the spatial aspects, one selects the assembly that achieves the maximal power for the pulses corresponding to the mean and upper 97.5% quantile and one selects the assembly that achieves the minimal power for the pulse corresponding to the lower 2.5% quantile. For the spatial aspects, when the mean and the upper 97.5% quantile are imposed then the assembly seeing the maximum power is selected. Correspondingly, when the lower quantile is imposed the assembly seeing the lowest power is selected. This creates for each H_{gap} model different representative axial and temporal profiles of linear power and external cladding temperature.

In step 2, the selected profiles are extracted and imposed in a decoupled ALCYONE1 REA transient calculation. One representative fuel pin is modeled. The resulting temperature and gap heat transfer profiles from ALCYONE1 are extracted and used for the H_{gap} model calibration. In step 3.1 the calibration is carried out by minimizing an objective function using the BFGS optimization method. The mean square error on the H_{gap} maximal and final values during the REA for each axial slice is considered as the objective function. Once the parameters that minimize this function are estimated the final step 3.2 is to quantify the calibrated model's uncertainty. The two main sources of uncertainties are the initial conditions and the calibrated parameters. The former one is quantified as two multiplicative factors on the initial gap width and the initial H_{gap} with normal distribution with mean one and standard deviation 0.1. This is a result of a previous uncertainty propagation for fuel evolution calculations with ALCYONE1. The results also showed that the initial gap width and H_{gap} are almost fully negatively correlated. This leads to make the assumption that the two coefficients are fully negatively correlated ($\rho = -1$) rendering thus one effective uncertain quantity for the initial conditions $H_{g,i}$. The latter uncertainty source is the calibrated parameters. For simplifying their uncertainty quantification, they are considered as fully positively correlated ($\rho = 1$) with uniform distributions. The bounds of the distributions are calculated in order to account for the calibration error. The effective uncertain input representing the calibration uncertainty is $H_{g,m}$. Finally, the model of equations (1a)–(1c), including its two effective uncertain parameters, is introduced into the multi-physics coupling creating the IBE modeling of Figure 1b. It can be seen as an intermediate modeling between the BE and Best Effort modelings. Since the H_{gap} model is a simple analytic function the computational cost of IBE is similar to BE amounting to a significant gain compared to Best Effort coupling. The average Best Effort computational time for one REA is 3 h while the average BE and IBE is 6 min.

5.4 Results

The first step 1.1 consists in clustering assemblies with similar burn-ups. For each cluster one H_{gap} model will be considered. In the PWR core there is a 3D burn-up distribution. This leads to a total of $193 \times 4 \times 30/2 = 11580$ meshes (due to symmetry) with different H_{gap} evolutions due to different burn-ups and power histories. In order to avoid constructing one H_{gap} model for each mesh, the clustering of the assemblies of different burn-ups is carried out. At first we consider only radial burn-ups, by averaging the axial variations. Secondly, we observe that the burn-ups have radially small variations around three main values 15 GWd/t, 30 GWd/t and 45 GWd/t due to the PWR fuel loading pattern. We, therefore, choose to cluster the assemblies based on these three values and we add one cluster for the minimum 10 GWd/t and one cluster for the maximum burn-up 52 GWd/t. This is done in order to have models covering all the burn-up variations. Additionally, it could be potentially used in the future for an application of a full 3D burn-up dependent H_{gap} model by constructing models that interpolate the calibration parameters.

To summarize we consider a total of 5 fuel assembly clusters and for each cluster one H_{gap} model will be constructed. We have to select for each cluster representative boundary conditions that vary both randomly and spatially since each cluster includes different assemblies. This is performed in step 1.2. The selected boundary conditions are presented in Figure 8. We know that the REA is a local phenomenon located in the upper part of the core around the ejected control rod position as seen in the radial cross-section of the Figure. We thus expect large variations of H_{gap} on the upper part and low to negligible variations in the lower part. For the random aspects we use the results from Section 4. More specifically, we consider that P_{lin}^{max} gives a good indicator of H_{gap} variations in REA. Based on this we select samples corresponding to the mean, the upper 97.5% and lower 2.5% quantiles of P_{lin}^{max} . From these samples we extract the linear power and cladding wall temperature axial and temporal evolutions. We combine both random and spatial aspects by selecting representative assemblies in the upper part for the mean and upper quantiles while we select their mirror assemblies from the lower part. The selected assemblies are presented in Figure 8 where each assembly has the burn-up value of its cluster. The green circles correspond to the selection for the mean and upper quantile while the yellow circles for the lower quantile. For the 10 GWd/t and 52 GWd/t clusters there is only one possible assembly for each cluster. For the other clusters, from the many available options we prefer the assemblies close to the ejected control rod location. For 15 GWd/t and 30 GWd/t clusters we select two different assemblies while for the 45 GWd/t we select three, since we consider that this cluster will have the largest H_{gap} variations due to its high burn-up.

In step 2 the extracted boundary conditions are imposed in ALCYONE1 and the REA stand-alone calculations are performed for each cluster. A representative fuel pin for each selected assembly in each sampling is modeled with the same axial discretization as the BE

Table 4. Estimated calibration parameters of Hgap model.

Burn-up group:	15 GWd/t	30 GWd/t	45 GWd/t
θ_1	$1.7e^{-1}$	$-1.7e^{-2}$	$-7.3e^{-1}$
$\theta_2 [J^{-1}]$	$1.1e^{-5}$	$1.6e^{-5}$	$2.0e^{-5}$

REA) = 360. For 45 GWd/t cluster the size is: 30 (axial slices) \times 3 (quantiles and mean) \times 3 (assembly locations) \times 2 (H_{gap} values during REA) = 540. The calibration parameters of the H_{gap} models are estimated by minimizing the mean square error on these datasets. The resulting calibration errors for the three different models are presented in Figure 9 and the estimated values of the calibration parameters in Table 4. We observe that the calibration errors increase in general with burn-up. The maximum error is of the order of 8% for the 45 GWd/t cluster.

For the uncertainty quantification of the calibration parameters θ_1 , θ_2 we make the assumption that they are positively fully correlated, which makes it possible to simplify significantly their uncertainty quantification. Additionally, as for all the other inputs they are also fully correlated spatially. This means that the calibration parameters of each cluster vary homogeneously. We assign uniform distribution to each calibration parameter with ranges that cover the calibration errors (the uniform distribution maximizes the entropy amongst distributions with prescribed ranges). The results for the estimated ranges for each parameter are shown in Table 5.

The bounds of the uniform distributions are used for the prediction of the H_{gap} evolution during REA by the calibrated models. The results are compared to the ALCYONE1 calculations and are illustrated in Figures 10, 11 and 12. For the comparison the axial slice with the maximum H_{gap} value for the three main clusters is presented. The plotted H_{gap} predictions are also the ones with the largest errors and we can see that for all the predictions the ALCYONE1 calculation is within the uncertainty bounds created by the calibration parameters.

Finally, there are two different sources of uncertainties for the calibrated models. The first one is due to the calibration error and is quantified by the distributions of the calibration parameters. The parameters are assumed fully positively correlated. The second one as discussed previously is due to the initial conditions. At the end, two new uncertain parameters replace the constant H_{gap} of the BE modeling. The first one is related to the calibration error of the models $H_{g,m}$ and the other is related to the initial conditions $H_{g,i}$.

6 Improved best estimate uncertainty quantification

The calibrated H_{gap} models from Section 5 are introduced into the BE coupling to create an intermediate IBE multi-physics coupling. The complete UQ methodology

detailed in [17] is applied on this improved modeling. It is important to mention that the computational cost does not increase. As in the BE UQ, kriging models were trained on a LHS of size 250 and used in brute force Monte Carlo for uncertainty propagation with 10^5 samples for each output. The results are presented in Figure 13. The validation of the kriging model's training show a Q^2 close to 1 with the smallest being 0.987 for DNB^{min} and 0.945 for the second principal component of P_{lin}^{2D} . More detailed results are provided in Appendix B.

The obtained histogram for H_f^{max} is approximately normal as for the BE UQ. We observe small increase of 2% in the mean value and a reduced relative standard deviation from 20% to 16%. For P_{lin}^{max} the mean value significantly decreases by 10% with similar relative standard deviation. The relative standard deviation of P_{lin}^{2D} is not affected by the improved H_{gap} model. The output quantity that is the most impacted is the DNB^{min} with an increase of 14% of the mean value and a decrease of the relative standard deviation from 57% to 42%. This means that there is significantly smaller probability to reach boiling crisis. In Appendix B we present also the estimated relative standard deviations of the scalar quantities directly using the training LHS. Although there are some discrepancies due to the limited number of samples, the same trends are observed as well.

The impact on the different mean values is attributed to the more realistic modeling of the H_{gap} evolution during the REA. In the BE modeling the mean constant value of H_{gap} is $2.4e^4 \text{W/m}^{2K}$, much larger than the one predicted by the calibrated models, and it is applied during the whole duration of the transient. This leads to more heat transferred from the fuel to the coolant. The fuel temperatures are lower with a corresponding weaker Doppler feedback and thus a higher maximum linear power. The increased heat extracted from the coolant in the BE UQ explains also the smaller minimum distance to boiling crisis compared to the IBE UQ. The lower fuel temperatures induce also the observed lower stored enthalpy.

The global sensitivity analysis is performed by estimating Shapley indices for all the outputs. The results are presented in Figure 14. For P_{lin}^{max} , P_{lin}^{2D} and H_f^{max} as in the BE modeling the β_{eff} is responsible for around 50% of the outputs variances and the TD_1 and D_1 are responsible for the remaining 50%. A significant difference is observed for the DNB^{min} sensitivities. The gap heat transfer is not any more the dominant input, instead as for the other outputs the β_{eff} and the TD_1 and D_1 account for most of the DNB^{min} variations. This explains also the significant reduction of the DNB^{min} relative standard deviation.

Finally, we studied the 3D H_{gap} (H_{gap}^{3D}) as an output of interest and included it in the uncertainty quantification methodology. For H_{gap}^{3D} two principal components are needed to represent 95% of its variance. The estimated means and standard deviations for the radial and axial cross-sections at the location and instant of the local maximum are presented in Figures 15, 16. As expected by the calibrated H_{gap} models, the assemblies with higher

Table 5. Estimated distributions of Hgap model calibration parameters.

Burn-up group:	15 GWd/t	30 GWd/t	45 GWd/t
θ_1	$\mathcal{U}(1.4e^{-1}, 2.0e^{-1})$	$\mathcal{U}(-1.7e^{-1}, 1.3e^{-1})$	$\mathcal{U}(-1.3, -1.8e^{-1})$
$\theta_2 [J^{-1}]$	$\mathcal{U}(8e^{-6}, 1.4e^{-5})$	$\mathcal{U}(1.3e^{-5}, 1.8e^{-5})$	$\mathcal{U}(1.6e^{-5}, 2.4e^{-5})$

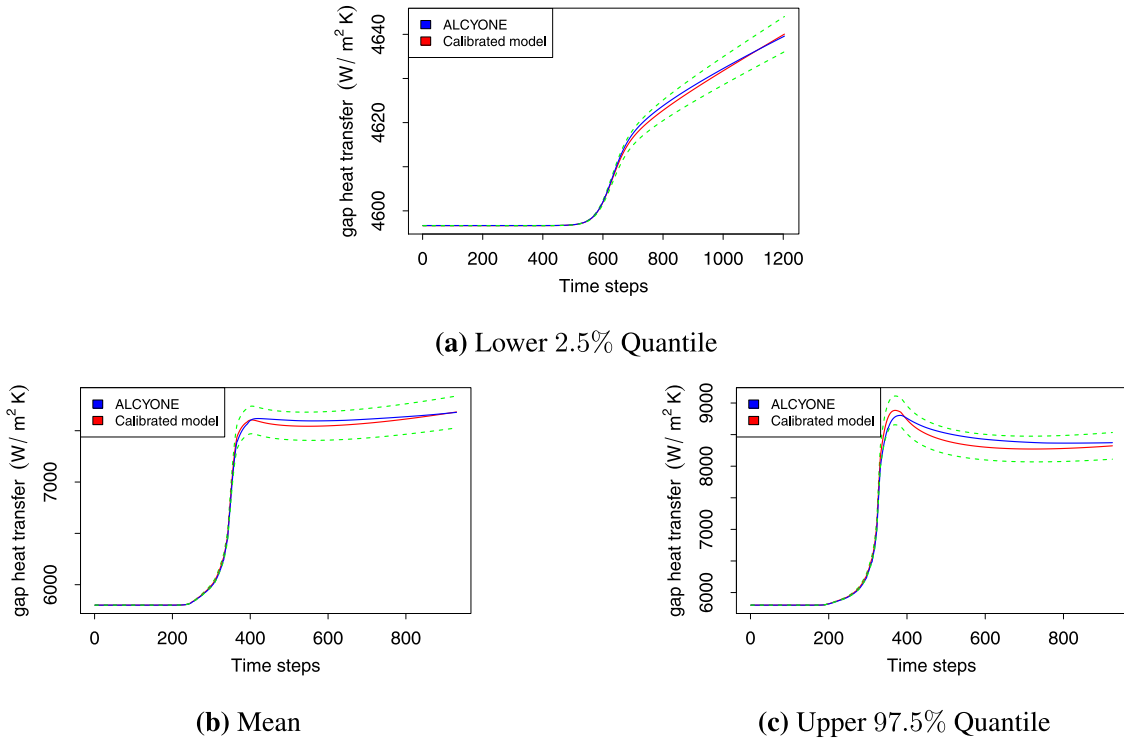


Fig. 10. 15 GWd/t H_{gap} model prediction with its uncertainty bounds in green.

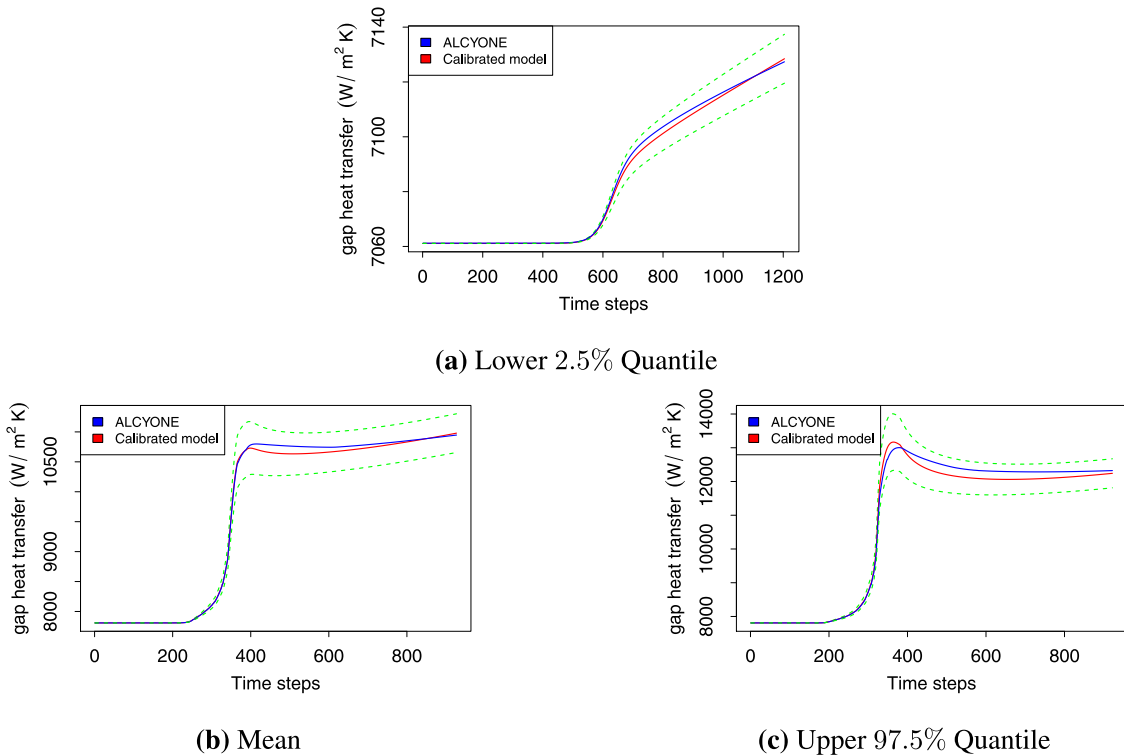


Fig. 11. 30 GWd/t H_{gap} model prediction with its uncertainty bounds in green.

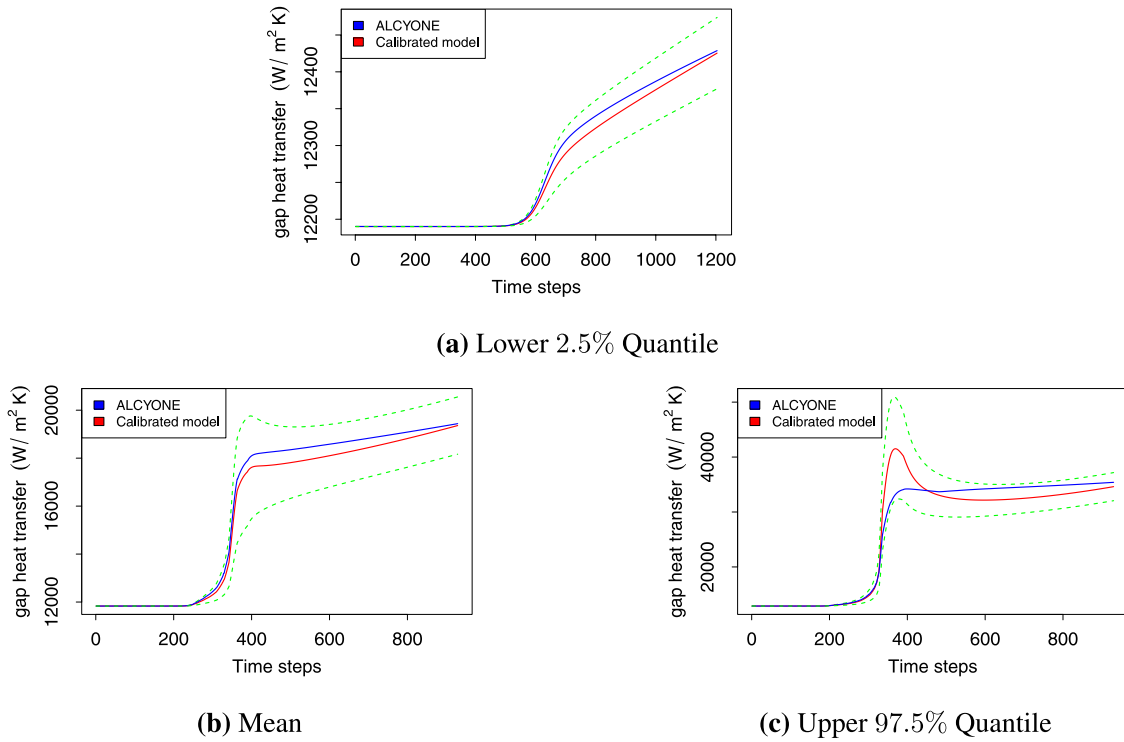


Fig. 12. 45 GWd/t H_{gap} model prediction with its uncertainty bounds in green.

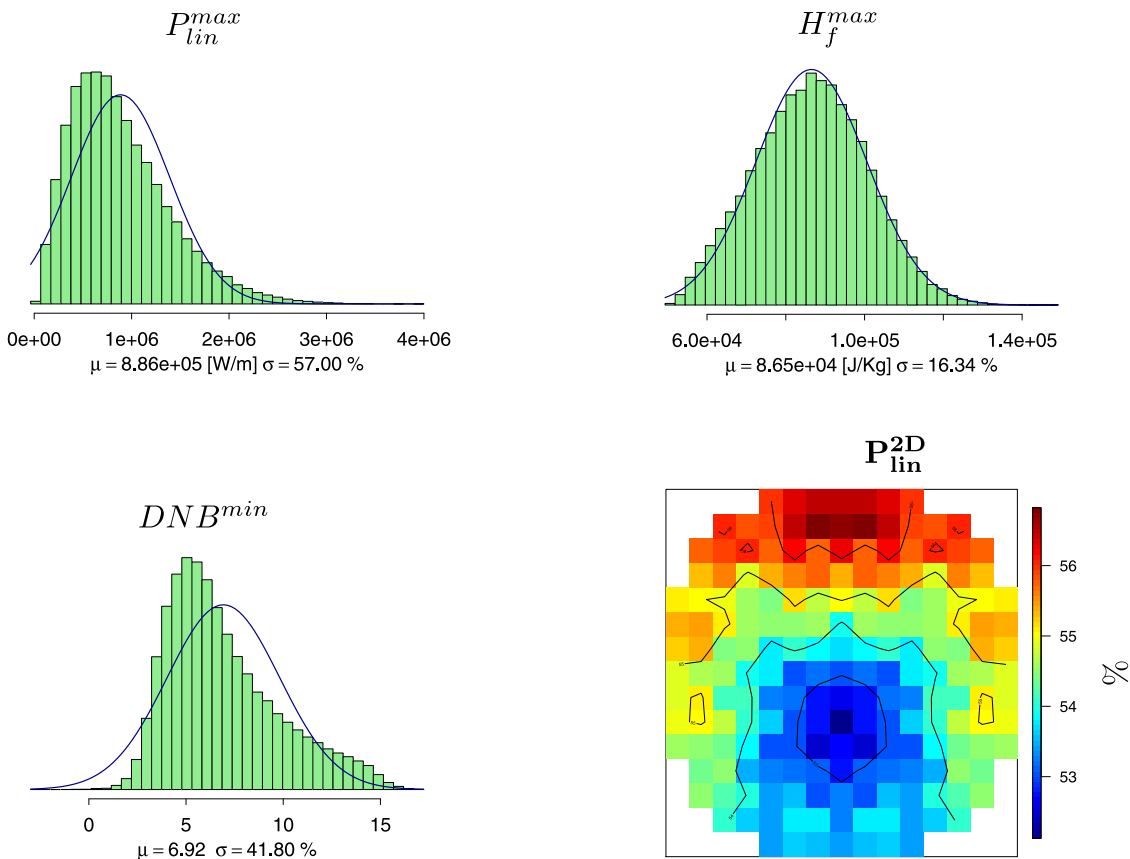


Fig. 13. P_{lin}^{max} , H_f^{max} and DNB^{min} histograms and P_{lin}^{2D} relative standard deviation distribution for IBE UQ analysis.

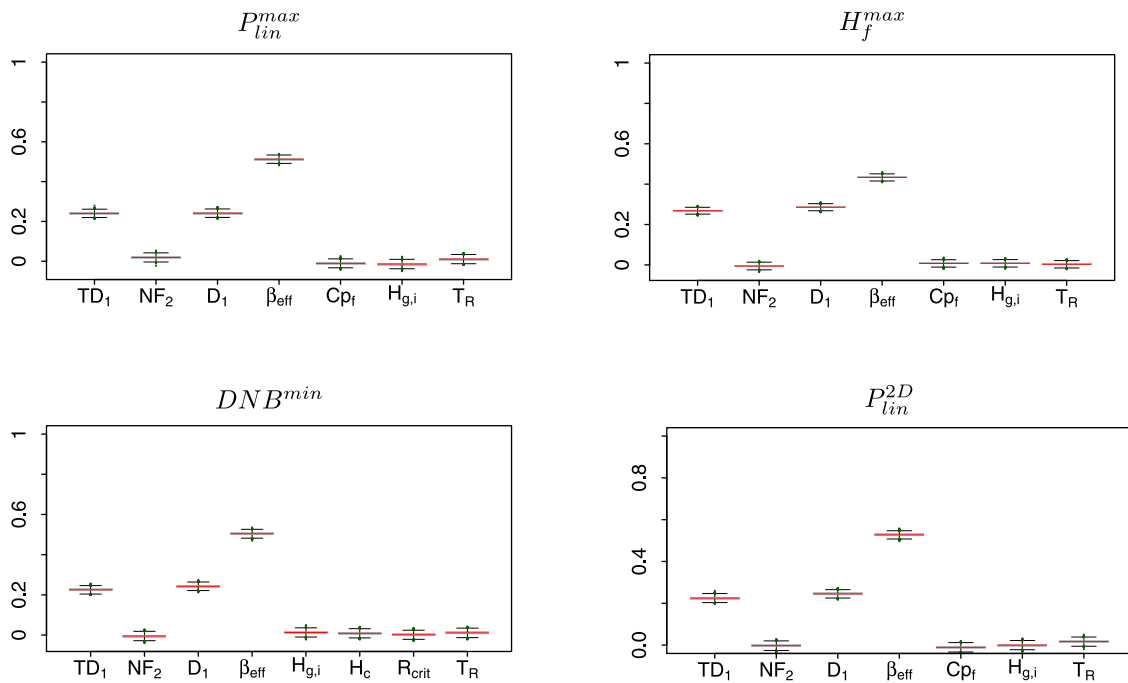


Fig. 14. P_{lin}^{max} , H_f^{max} and DNB^{min} Shapley indices and P_{lin}^{2D} aggregate Shapley indices for IBE UQ analysis.

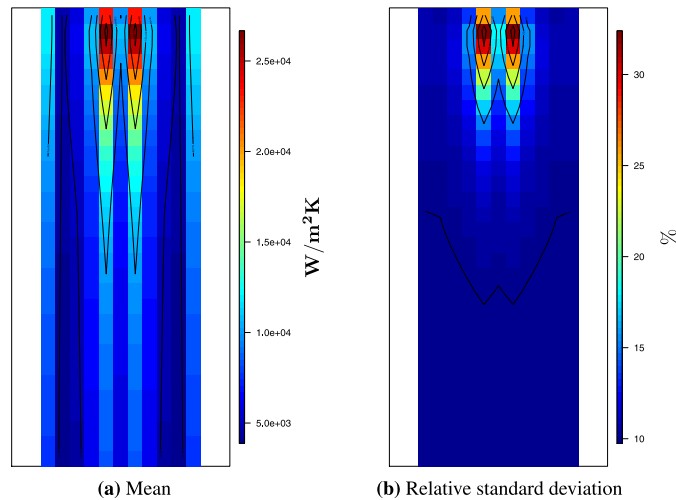


Fig. 15. H_{gap}^{3D} estimated mean and relative standard deviation in the axial cross-section for IBE UQ analysis.

burn-up have also higher H_{gap} . The maximum value is obtained at the assemblies on the right and left of the assembly with the ejected control rod. This is due to the important power seen by these assemblies in combination with their high burn-up. The relative standard deviation distribution exhibits strong variations from 10% up to 32%. The 10% lower bound on the H_{gap} is related to the initial conditions uncertainties.

The aggregate Shapley indices for H_{gap}^{3D} are estimated and presented in Figure 17. In this case the $H_{g,i}$ is the dominant input responsible for 80% of the outputs variances. The remaining 20% is mainly explained by β_{eff} . This result is not surprising since the initial conditions determine the H_{gap} evolution.

7 Conclusion and perspectives

In this work we have presented a High to Low H_{gap} model methodology for REA uncertainty quantification in a PWR core. A simplified H_{gap} model based on fuel thermal expansion has been considered. The CORPUS multi-physics coupling framework is used for the transient modeling. The fuel-thermomechanics code ALCYONE1 is used as the high fidelity code. The available Best Estimate (BE) coupling scheme involves a coupling between core neutronics code APOLLO3[®] and core thermal-hydraulics code FLICA4. For APOLLO3[®] a two-group diffusion modeling is used while for FLICA4 an axial multi-channel 1D modeling. The internal fuel thermal modeling of

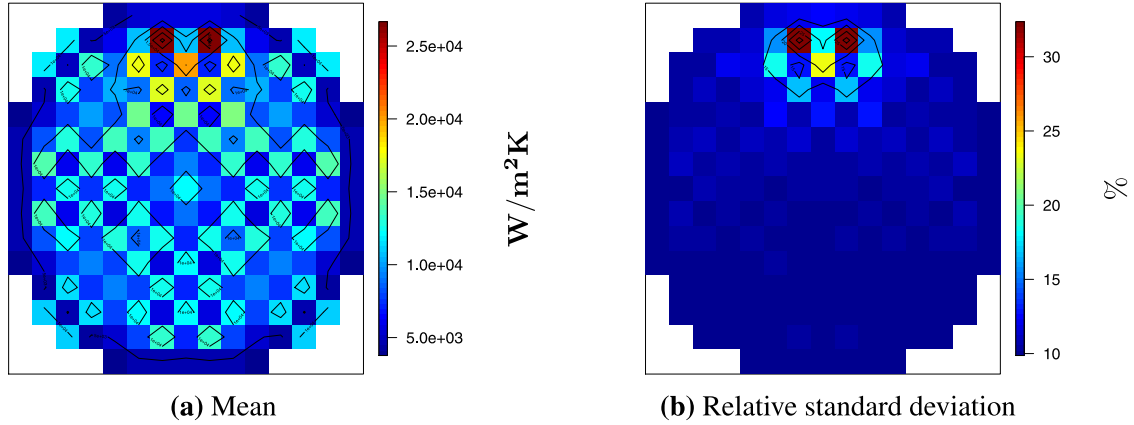


Fig. 16. H_{gap}^{3D} estimated mean and relative standard deviation in the radial cross-section for IBE UQ analysis.

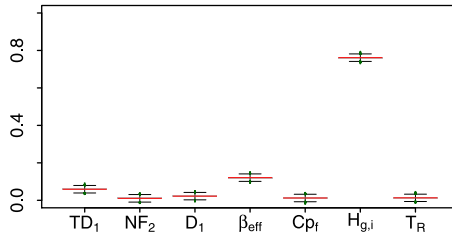


Fig. 17. H_{gap}^{3D} Shapley indices for IBE UQ analysis.

FLICA4 is updated to include the H_{gap} predicted by the calibrated model. This creates an Improved Best Estimate (IBE) coupling scheme.

The calibration methodology involves different steps. The starting point is a previous BE REA uncertainty propagation that creates the set of available results from which representative ones will be selected for the calibration. Then the first step is to cluster the assemblies and use one H_{gap} model for each cluster. The assemblies are clustered based on their burn-up, which creates 3 main clusters: 15, 30 and 45 GWd/t. The next step is to select the fuel-thermomechanics boundary conditions on which ALCYONE1 is run for each cluster. REA power pulses are selected from the available BE results in such a way to cover the extreme cases and in locations where the higher and lower power variations are observed. The ALCYONE1 calculations are performed for each cluster power pulses and the H_{gap} and temperatures evolutions are extracted. The H_{gap} model calibration is performed for all the axial slices at two time instances: the instance of the maximum H_{gap} during the REA and the last value of H_{gap} . The calibration parameters are estimated for these datasets and the calibration error for all the time steps is computed. The assumption has been made that the calibration parameters are fully positively correlated. Their uncertainty bounds are selected in order to create H_{gap} intervals that cover the ALCYONE1 results. The results indicate that the uncertainty of the parameters increases with burn-up, which shows the limitation of such a simplified model for high burn-up fuel rods. Additionally, an

uncertainty of 10% on the initial rod conditions is considered as a result of ALCYONE1 evolution calculations. Finally, the last step is to include the calibrated H_{gap} model into the BE coupling and to create the IBE.

An uncertainty quantification study is performed using the IBE and compared to the BE results. The most significant impact is on the distance to boiling crisis with an increase of 14% in its mean value reducing the probability of boiling crisis. The relative standard deviation of DNB^{min} is reduced from 57% to 42%. The reason is the decreased sensitivity on the H_{gap} due to its better uncertainty quantification and modeling. This is observed in the estimated Shapley indices, where the H_{gap} sensitivity reduces from 50% to almost 0. These results, although in an academic proof of concept study, show the potential gain of High to Low approaches for H_{gap} modeling in REA uncertainty quantification.

Many future prospects open following this work. On the one hand a more elaborated H_{gap} model could be sought with incorporation of the burn-up parameter to avoid creating one model for each burn-up. Besides that, a more direct High to Low modeling could be investigated in order to inform specific low level code models, such as simplified dynamical H_{gap} models, from the high level code. On the other hand, different transient scenarios and different reactor types could be studied in order to cover a larger spectrum of applications since they all share the common need for High to Low H_{gap} modeling.

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Author contribution statement

G. Delipei has performed the calculations and written the manuscript. J. Garnier, J.-C. Le Pallec, and B. Normand

Fuel-thermal	
λ_f	N(1,0.05)
λ_c	N(1,0.05)
C_{pf}	N(1,0.05)
C_{pc}	N(1,0.05)
H_{gap}	U(2000,50000)
P_r	U(0,0.04) + N(0,0.0175)
T_R	U(0,1)
Thermal-hydraulics	
H_c	N(1,0.15)
R_{crit}	N(1,0.15)
R_{v0}	N(1,0.125)
H_{dmb}	U(0.8,1.2)

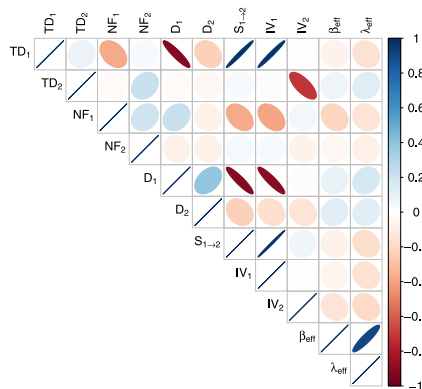


Fig. A.1. Input uncertainty quantification, where $U(a,b)$ is a uniform distribution over (a,b) and $N(a,b)$ is a normal distribution with mean a and standard deviation b . P_r is the sum of two independent random variables.

have performed scientific advisory roles and provided support through expert judgement, critical verification, and proofreading of the manuscript.

Appendix A: Input uncertainty quantification

The input uncertainty quantification is performed by using the UAM recommendations when they are available and by using expert opinions for the rest. The resulting pdf for the inputs are presented in Figure A.1.

A multivariate normal distribution is used for the neutronic inputs. The mean vector of the pdf is the reference cross-sections produced at CEA Σ_{CEA} and the covariance matrix \mathbf{C}_{UAM} is empirically estimated by the results of UAM. The UAM provides a dataset of two-group macroscopic cross-sections obtained by neutronic lattice uncertainty propagation simulations. This dataset of 100 realizations was adapted to the cross-sections used by APOLLO3[®] by assuming:

1. Negligible uncertainties on the up-scattering cross-section $S_{2 \rightarrow 1}$.
2. Negligible $n - 2n, n - 3n \dots$ cross-sections uncertainties.

The adapted macroscopic cross-sections dataset is used to estimate the correlation matrix and the relative standard deviations of the cross-sections. Finally, \mathbf{C}_{UAM} is calculated using the correlation matrix, the relative standard deviations and the reference CEA cross-sections. The UAM correlation matrix is illustrated in Figure A.1, where we can observe large positive and negative correlations. The TD_1 is strongly positively correlated with $S_{1 \rightarrow 2}$ and IV_1 and negatively correlated with D_1 . The β_{eff} is also strongly positively correlated with λ_{eff} .

The rest of the inputs are considered independent of the neutronic inputs and between them. The thermal-hydraulic inputs are mainly based on CEA experts

opinions and are applied as multiplicative coefficients on the different parameters. The R_{crit} usually is penalized to 1.3 and in this work we consider this value as the 95% upper quantile of a normal distribution with mean value 1 and standard deviation 0.15. For H_{DNB} a uniform distribution is used reflecting the limited current knowledge about this phenomenon. In fuel-thermomechanics inputs and more specifically for the thermal conductivities and specific heat capacities the UAM recommendations are used. For the Rowlands temperature a uniform distribution is considered on the weight fraction of the fuel centerline temperature. In the reference situation the Rowlands temperature has a 4/9 weight on the fuel centerline temperature and 5/9 on the fuel external surface temperature. By using an uncertain multiplicative factor with $U(0,1)$ distribution on the centerline temperature weight we consider that it can only decrease uniformly between 4/9 and zero with a corresponding increase in the external surface temperature weight. The H_{gap} is a particular input quantity since in the BE coupling it is an uncertain constant in FLICA4 with uniform pdf bounded from below by its value for a complete open gap ($2000 \text{ Wm}^{-2}\text{K}^{-1}$) and from above by its value for a pellet-cladding contact ($50000 \text{ Wm}^{-2}\text{K}^{-1}$). In the IBE coupling H_{gap} is a result and thus is not considered, instead the calibration parameter's uncertainty and the initial conditions of the model are used. Finally, the power radial profile uncertainty is modeled by a multiplicative factor on the fuel external surface power with a pdf resulting from the convolution of a normal and a uniform distribution. The power radial profile is peaked towards the periphery for the high burn-up fuel pins. The deformation is increasing with burn-up and to model it an explicit function of burn-up is used. The uncertainty is a convolution of two effects: the uncertainty of the function used $\mathcal{N}(0,0.0175)$ and the uncertainty due to the presence or not of a guide tube near the fuel pin $U(0,0.04)$. The latter effect is a result of a previous CEA study.

Appendix B: Uncertainty quantification methodology additional results

In Section 4 we apply the UQ methodology developed in a previous work [17] on the BE coupling. The methodology consists of an initial screening of the inputs based on HSIC statistical significance tests, a training of a surrogate kriging model between each output and the reduced inputs and the use of the kriging models to perform uncertainty propagation and global sensitivity analysis. The computational cost of this modeling is 3h in average. In this Appendix we provide additional results regarding the identified reduced input space and the validation of the kriging models. Concerning the screening process, a random sampling of size 125 is used as a Design of Experiments (DOE). The result for the identified important input parameters for each output of interest are gathered in Table B.1. They can be grouped into two subspaces: $I_1 = (TD_1, NF_2, D_1, S_{1 \rightarrow 2}, IV_1, IV_2, \beta_{eff}, Cp_f, H_{gap}, T_R)$ and $I_2 = (TD_1, NF_2, D_1, S_{1 \rightarrow 2}, IV_1, \beta_{eff}, H_{gap}, H_c)$.

Concerning the training of the kriging models a LHS of size 250 optimized in both the complete input space and the two important subspaces is used as DOE. The kriging models are trained on the identified input subspaces. The resulting Q^2 includes thus the dimension reduction error. The R^2 , the leave-one-out cross validation R_{loo}^2 and the Q^2 are presented in Table B.2. The Q^2 is estimated on an independent LHS of size 125. For all the outputs the Q^2 is close to 1 with smallest values for DNB^{min} (0.98%) and the second principal component of P_{lin}^{2D} (0.945%).

The same methodology is applied afterwards in the IBE coupling, where the calibrated H_{gap} models are introduced into the BE coupling. It is important to mention that the computational cost does not increase. The uncertain inputs and outputs of the previous study are used with the replacement of the constant H_{gap} uncertain input by the H_{gap} model uncertain parameters. The two new uncertain inputs are $H_{g,m}$ and $H_{g,i}$ related to the H_{gap} model calibration error and initial conditions. For the screening, as before, a random sampling of size 125 is used as DOE. The result for the identified important input parameters are gathered in Table B.3. They can be grouped into two subspaces: $I_1 = (TD_1, NF_2, D_1, \beta_{eff}, Cp_f, H_{g,i}, T_R)$ and $I_2 = (TD_1, NF_2, D_1, \beta_{eff}, H_{g,i}, H_c, R_{crit}, T_R)$.

Compared to the BE study we observe the inclusion of the parameter $H_{g,i}$ in both subspaces while the parameter $H_{g,m}$ is rejected. This means that for the outputs of interest the initial conditions are more important than the calibration parameters uncertainties. For the kriging models a training LHS of size 250 with optimized subspaces I_1 and I_2 is constructed. The result for the R^2 , R_{loo}^2 and Q^2 are presented in Table B.4. The Q^2 is estimated on an independent LHS of size 125. For all the outputs the Q^2 is close to 1 with smallest values for DNB^{min} (0.987) and the second principal component of P_{lin}^{2D} (0.945).

Finally, we present in Table B.5 the estimated relative standard deviations using directly the training LHS code evaluations. We observe some differences compared to the kriging model's brute force Monte Carlo due to the limited number of samples. However, similar trends are observed

Table B.1. Screening results for BE coupling.

Selected inputs	
P_{lin}^{max}	$TD_1, NF_2, D_1, S_{1 \rightarrow 2}, \beta_{eff}, H_{gap}$
$P_{lin,pc1}^{2D}$	$TD_1, NF_2, D_1, S_{1 \rightarrow 2}, \beta_{eff}, H_{gap}$
$P_{lin,pc2}^{2D}$	$TD_1, NF_2, D_1, S_{1 \rightarrow 2}, \beta_{eff}, H_{gap}$
H_f^{max}	$TD_1, NF_2, D_1, \beta_{eff}, Cp_f, H_{gap}, T_R$
DNB^{min}	$TD_1, NF_2, D_1, S_{1 \rightarrow 2}, IV_1, \beta_{eff}, H_{gap}, H_c$

Table B.2. Kriging models validation for BE coupling.

	R^2	R_{loo}^2	Q^2
P_{lin}^{max}	1.00	0.999	0.999
$P_{lin,pc1}^{2D}$	1.00	0.998	0.999
$P_{lin,pc2}^{2D}$	1.00	0.994	0.945
H_f^{max}	1.00	0.999	0.995
DNB^{min}	1.00	0.979	0.981

Table B.3. Screening results for IBE coupling.

Selected inputs	
P_{lin}^{max}	$TD_1, NF_2, D_1, \beta_{eff}, T_R$
$P_{lin,pc1}^{2D}$	$TD_1, NF_2, D_1, \beta_{eff}, T_R$
$P_{lin,pc2}^{2D}$	TD_1, D_1, β_{eff}
H_f^{max}	$TD_1, NF_2, D_1, \beta_{eff}, Cp_f, H_{g,i}, T_R$
DNB^{min}	$TD_1, NF_2, D_1, \beta_{eff}, H_{g,i}, H_c, R_{crit}, T_R$

Table B.4. Kriging models validation for IBE coupling.

	R^2	R_{loo}^2	Q^2
P_{lin}^{max}	1.00	0.995	0.995
$P_{lin,pc1}^{2D}$	1.00	0.998	0.999
$P_{lin,pc2}^{2D}$	1.00	0.994	0.945
H_f^{max}	1.00	0.992	0.992
DNB^{min}	1.00	0.986	0.987

Table B.5. Relative standard deviations estimated by the training LHS of size 250 for BE and IBE.

	BE	IBE
P_{lin}^{max}	61.00%	56.63%
H_f^{max}	20.37%	16.25%
DNB^{min}	50.32%	36.63%

between the BE and IBE study. The most noticeable is the decrease of the DNB^{min} relative standard deviation from 50.32% to 36.63%.

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