

Patient-Specific Computational Evaluation of Stiffness Distribution in Ascending Thoracic Aortic Aneurysm

Marzio Di Giuseppe, Solmaz Farzaneh, Massimiliano Zingales, Salvatore Pasta, Stéphane Avril

▶ To cite this version:

Marzio Di Giuseppe, Solmaz Farzaneh, Massimiliano Zingales, Salvatore Pasta, Stéphane Avril. Patient-Specific Computational Evaluation of Stiffness Distribution in Ascending Thoracic Aortic Aneurysm. Journal of Biomechanics, In press, pp.110321. 10.1016/j.jbiomech.2021.110321. hal-03139856

HAL Id: hal-03139856 https://hal.science/hal-03139856v1

Submitted on 12 Feb 2021

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

1	Patient-Specific Computational Evaluation of Stiffness Distribution in Ascending						
2	Thoracic Aortic Aneurysm						
3	Marzio Di Giuseppe ¹ , Solmaz Farzaneh ² , Massimiliano Zingales ³ ,						
4	Salvatore Pasta ³ , Stéphane Avril ²						
5							
6							
7	¹ Department of Health Promotion, Mother and Child Care, Internal Medicine and Medical						
8	Specialties, University of Palermo, 90128, Palermo, Italy						
9	² Mines Saint-Etienne, Univ Lyon, Univ Jean Monnet, INSERM, U1059 SAINBIOSE, Saint-						
10	Etienne, 42023, France						
11	³ Department of Engineering, Viale delle Scienze, Ed.8, University of Palermo, 90128,						
12	Palermo, italy						
14							
15							
16							
17							
18	Submitting for Original Article						
19							
20							
21							
22	Manuscript word count: 3360 words						
23							
24							
25	Corresponding outhor:						
20 27	Sténbane Avril						
28	Univ Lvon, INSERM U1059.						
29	Mines Saint-Etienne, SAINBIOSE, F-42023,						
30	158 cours Fauriel,						
31	42023 SAINT-ETIENNE cedex 2, France						
32	Phone: +33477420188						
33	Fax : +33477420000						
34	Email: avril@emse.fr						

36 Abstract

37	Quantifying local aortic stiffness properties in vivo is acknowledged as essential to assess
38	the severity of an ascending thoracic aortic aneurysm (ATAA). Recently, the LESI (local
39	extensional stiffness identification) methodology has been established to quantify non-
40	invasively local stiffness properties of ATAAs using electrocardiographic-gated computed
41	tomography (ECG-gated CT) scans. The aim of the current study was to determine the most
42	sensitive markers of local ATAA stiffness estimation with the hypothesis that direct measures
43	of local ATAA stiffness could better detect the high-risk patients.
44	A cohort of 30 patients (12 BAV and 18 TAV) referred for aortic size evaluation by ECG-
45	gated CT were recruited. For each patient, the extensional stiffness Q was evaluated by the
46	LESI methodology whilst computational flow analyses were also performed to derive
47	hemodynamics markers such as the wall shear stress (WSS).
48	A strong positive correlation was found between the extensional stiffness and the aortic pulse
49	pressure (R=0.644 and p<0.001). Interestingly, a significant positive correlation was also
50	found between the extensional stiffness and patients age for BAV ATAAs (R=0.619 and
51	p=0.032), but not for TAV ATAAs (R=-0.117 and p=0.645). No significant correlation was
52	found between the extensional stiffness and WSS evaluated locally. There was no significant
53	difference either in the extensional stiffness between BAV ATAAs and TAV ATAAs
54	(Q=3.6±2.5 MPa.mm for BAV ATAAs vs Q=5.3±3.1 MPa.mm for TAV ATAAs, p=0.094).
55	Future work will focus on relating the extensional stiffness to the patient-specific rupture risk
56	of ATAAs on larger cohorts to confirm the promising interest of the LESI methodology.
57	
58	Keywords: Ascending Thoracic Aortic Aneurysm, Bicuspid Aortic Valve, Extensional
59	Stiffness, Noninvasive Inverse Method, Shear Stress
60	
61	
62	

64 Introduction

Ascending thoracic aortic aneurysm (ATAA) is a life-threatening cardiovascular disease, 65 66 leading to weakening of the aortic wall and permanent dilation. ATAA affects approximately 10 out of 100,000 persons per year in the general population (Coady et al., 1999), and this 67 disease is associated with a high risk of mortality and morbidity (Elefteriades and Farkas, 68 2010). Bicuspid aortic valve (BAV) is a predisposing risk factor to ATAA formation and 69 70 development with patients having associated aortopathy on approximately 40% of whole bicuspid population (Verma and Siu, 2014) and higher rate of aortic dissection compared to 71 patients with the tricuspid aortic valve (TAV) (Januzzi et al., 2004). 72

73

74 To avoid aortic complications (i.e. rupture or dissection), the current clinical management of 75 ATAA is based on strict monitoring of the aneurysm size and elective repair is recommended 76 when aortic diameter reaches a critical size (Borger et al., 2018). However, aortic size is not 77 a sufficient predictor of the risk of ATAA failure (Pape et al., 2007). Aortic stiffness is 78 associated with progressive aortic dilatation and aneurysm formation as shown by imaging modalities (Longobardo et al., 2017; Teixeira et al., 2012), computational analyses (Farzaneh 79 et al., 2019a; Martin et al., 2013a; Pasta et al., 2017a) and biomechanical studies (Selvin et 80 al., 2010; Smoljkic et al., 2017). High aortic stiffness was associated with high rates of 81 82 surgical aortic replacement and aortic root dilation in children and adults with connective 83 tissue disorders (Prakash et al., 2015). In Marfan patients, aortic stiffness proved to be 84 important in predicting progressive aortic dilatation (Guala et al., 2019; Suleimani et al., 85 2017). A recent study of abdominal aortic aneurysms found that segmental stiffening of the 86 aorta preceded aneurysm growth and introduced the concept that stiffening may act as an 87 early mechanism triggering elastin breakdown and aneurysm growth (Raaz et al., 2015). 88 Imaging based on 4D Flow MRI (Mahadevia et al., 2014), in silico computational modeling 89 (Mendez et al., 2018; Pasta et al., 2017b) or combination of them (Youssefi et al., 2017) 90 have confirmed an altered hemodynamic environment in BAV ATAAs with well-functioning or

stenotic aortic valve leaflets (van Ooij et al., 2017). The underlying hypothesis is that flow
disturbances induce local wall shear stress (WSS) forces on the dilated aorta, portending to
adverse vascular remodeling by mechanotransduction. This can further lead to changes in
the biomechanical properties of ATAA wall as reflected by an increased stiffness for the
dilated aorta.

96

Risk assessment based on the aortic stiffness of the ATAA wall are being developed (Duprey 97 98 et al., 2016; Farzaneh et al., 2019b; Martin et al., 2013a). In this way, the quantification of 99 local elastic properties of the ATAA wall from in vivo data is crucial to establish a reliable method for estimating the severity of an ATAA (Mousavi and Avril, 2017; Rooprai et al., 100 101 2019). Most importantly, new strategies of risk assessment should be accurate and 102 compatible with clinical time framework. For that purpose, the in vivo non-invasive 103 identification of aortic stiffness would be essential for clinicians to improve the clinical 104 decision making process. Recently, Farzaneh et al. (Farzaneh et al., 2019a) have presented a novel methodology, namely the LESI (local extensional stiffness identification) 105 106 methodology, to non-invasively quantify local stiffness properties on the basis of ECG-gated 107 CT scans and brachial arm pressure. The interrelationship between the obtained local stiffness with other established markers of aortic function remains unclear and this currently 108 limits the methodology's potential impact. The aim of the current study was to determine the 109 110 most sensitive markers of local ATAA stiffness estimation with the hypothesis that direct 111 measures of local ATAA stiffness could better detect the high-risk patients. First, the patterns of extensional stiffness obtained by the LESI methodology in a cohort of 30 patients with 112 ATAAs and different aortic valve phenotypes were analyzed. Then, the association of 113 114 stiffness with demographic data and computationally derived wall shear stress (WSS) was 115 investigated.

- 116
- 117
- 118

120 Methods

121 Study Population

122 After internal review board approval and informed consent, 30 patients (12 BAV and 18 TAV) referred for aortic size evaluation by electrocardiographic-gated computed tomography 123 (ECG-gated CT) were enrolled. Table 1 shows demographic data of the patient population as 124 well as aortic diameter. For all patients, ECG-gated CT scans were performed after 125 126 intravenous injection of contrast agent to improve image quality. Imaging was carried out on a GE VCT 64-channel scanner (GE Medical Systems, Milwaukee, Wisconsin), with gantry 127 rotation velocity of 0.5 m/s and spiral pitch of 0.984. Retrospective reconstruction of images 128 129 was performed to obtain images at cardiac phases corresponding to both end-diastole and 130 end-systole at the resolution of 512 x 512 and slice thickness of 0.625 mm. Prior to imaging, 131 diastolic and systolic blood pressures were measured by brachial sphygmomanometer for 132 each patient.

133

134 Images Analysis

For each patient, segmentation of ECG-gated CT images was performed at both diastolic 135 and systolic phases using Mimics v20 (Materialise, Leuven, BE). Specifically, semi-automatic 136 threshold-based segmentation of the aortic lumen was performed to obtain a point cloud of 137 138 ATAA geometries. The same smoothing factor was applied to all phases. The three-139 dimensional (3D) surface of the aorta was generated for each phase and exported as STL 140 file. Then, 3D aortic surfaces reconstructed at both cardiac phases were cut by identical cross-sectional planes in Rhinoceros (Robert McNeel & Associates, Seattle, USA) to define a 141 142 domain of the aorta larger than the final segment of interest. A set of nodes was defined 143 across each reconstructed aortic geometry, with the requirement that a node represented the 144 position of the same material point at each phase of the cardiac cycle. For this, it was 145 essential to reconstruct a structural mesh for all phases with an identical number of elements 146 and nodes. The Vascular Modeling Toolkit (VMTK, Orobix, Bergamo, Italy; www.vmtk.org)

(Antiga and Steinman, 2004) was employed to generate the structural mesh from STL files. The extracted data from VMTK were postprocessed in MATLAB to extract an accurate mesh using the longitudinal and circumferential metrics obtained from VMTK. A structural mesh composed of 3871 quadrilateral shell elements, 49 along the circumferential direction and 79 along the longitudinal direction, was defined on the template geometry. Each node of the structural mesh was related to assumedly the same material points for systole and diastole phases.

154 The LESI methodology for calculating the extensional stiffness was described by Farzaneh et al. (Farzaneh et al., 2019a). In brief, local principal strain components (ε_1 and ε_2) were 155 deduced by computing the spatial gradients of displacements between diastolic and systolic 156 configurations. Although the aortic tissue is globally anisotropic and nonlinear, its mechanical 157 158 behavior was linearized in the range of strains induced by pressure variations between diastole and systole, and anisotropic effects were neglected in this range. The local principal 159 stress components (τ_1^0 and τ_2^0) were derived by finite-element analysis (FEA) performed on 160 the ATAA diastolic geometry using average blood pressure evaluated over the cardiac cycle 161 (Joldes et al., 2016). To obtain radii of curvature (r_1^0 and r_2^0) and their variations (Δr_2 and Δr_1) 162 fast and efficiently, a method based on the principle of virtual work was developed, as 163 164 previously introduced in Bersi et al. (Bersi et al., 2016).

Finally it was possible, for each element, to relate the extensional stiffness to the pulsed pressure ΔP such as:

167
$$Q = \frac{\Delta P + \frac{\tau_1^0 \Delta r_1}{(r_1^0)^2} + \frac{\tau_2^0 \Delta r_2}{(r_2^0)^2}}{\frac{\varepsilon_1 + v\varepsilon_2}{r_1^0} + \frac{v\varepsilon_1 + \varepsilon_2}{r_2^0}}$$

In the current study we used the concept of "extensional stiffness" (intensive property) which
equals the material stiffness times the thickness and whose dimension is MPa.mm.
The aortic thickness could not be measured accurately due to the limited spatial resolution of
CT.

Once LESI results were obtained for each patient, the average extensional stiffness was evaluated in each of the four quadrants, including the major, minor, anterior and posterior regions (Fig.1).

175

176 Computational Flow Analysis

Computational flow modeling was applied to study ATAA hemodynamics at systolic peak 177 when the aortic valve is supposedly fully open (D'Ancona et al., 2013). For each patient, the 178 179 fluid domain of ATAA geometry at end-systole was meshed with unstructured tetrahedral 180 elements with size of 0.1 mm. The blood was assumed as a non-Newtonian incompressible 181 fluid (density of 1060 kg/m3 and viscosity of 0.00371 Pa*s) adopting the Carreau model 182 (Khanafer et al., 2006; Leuprecht and Perktold, 2001). The solution was obtained with 183 FLUENT v18 (ANSYS Inc., Canonsburg, PA) using the SIMPLE algorithm for the pressure-184 velocity coupling and second order accurate discretization scheme. To include patient-185 specific hemodynamics conditions, the transaortic jet velocity evaluated by Doppler echocardiography was set as the inflow velocity condition at the aortic valve plane. For each 186 187 outlet, we first computed the global vascular resistance and arterial compliance of each patient from echocardiographic measurements and clinical demographic data. Then, these 188 parameters were used to compute the outflow boundary conditions of a three-element 189 Windkessel model (comprising proximal resistance, compliance, and a distal resistance) 190 191 coupled to each outflow branch. Boundary conditions were adjusted to match brachial artery 192 pulse pressure.

After numerical solution, WSS values were obtained for the entire thoracic aorta, with further in-depth subanalysis in the ascending thoracic aorta by computing maxima at sinotubular junction (namely, analysis plane = AA1), proximal (AA2) and mid (AA3) ascending thoracic aorta for each quadrant (i.e., major, minor, anterior and posterior quadrants).

- 197
- 198
- 199

200 Statistical Analysis

201 The Rank Sum test was used to assess differences in the extensional stiffness between BAV 202 ATAAs and TAV ATAAs. One-way Anova, followed by Holm-Sidak post-hoc test for all pair-203 wise comparisons, was used to assess differences of extensional stiffness among aortic quadrants. The association of the extensional stiffness with patient age, aortic pulse 204 205 pressure, aortic diameter, WSS, aortic strain and stress was explored by Pearson's correlation. Statistical analyses were performed using SigmaPlot (Systat Software Inc., San 206 207 Jose, California), with statistical significance set at p=0.05 in all cases. Data are shown as Mean ± SEM. 208

209

210

of all data computed for each patient. First two principal components were analyzed to
assess separation of BAV ATAA versus TAV ATAA. The tolerance ellipse based on

In addition, Principal Component Analysis (PCA) was performed for dimensionality reduction

Hotelling's T2 at a significance level of 0.05 was calculated and shown in the score plots.

214 Principal Component Analysis was performed using SPSS software (IBM SPSS Statistics

215 v.17, New York, NY).

216

217 Results

Table 1 summarizes patient demographic data, systolic and diastolic pressures and aortic diameter. The distribution of age in BAV ATAAs differs significantly from that of TAV ATAAs patients (50.2 ± 7.5 years for BAV ATAAs vs 64.7 ± 7.8 years for TAV ATAAs, p<0.01), and this difference was confirmed by the analysis of the age on a different cohort of 159 patients (Agnese et al., 2019).

223

Fig. 2 and Fig. 3 show representative extensional stiffness and WSS maps obtained by the LESI methodology and CFD analyses for BAV ATAAs and TAV ATAAs, respectively. There was no significant difference in the extensional stiffness (Q) between BAV ATAAs and TAV ATAAs (Q=3.6±2.5 MPa.mm for BAV ATAAs vs Q=5.3±3.1 MPa.mm for TAV ATAAs,

p=0.094). Similarly, the mean values of the extensional stiffness did not significantly change
 among aortic quadrants (see Fig.4), although many patients had high values of the
 extensional stiffness in the minor and anterior quadrants of the ascending aorta.

231

The relationship of extensional stiffness as averaged among quadrants with the ascending 232 aortic diameter and the aortic pulse pressure are shown in Fig.5A and Fig.5B. A strong 233 positive correlation was found between the extensional stiffness and the aortic pulse 234 235 pressure (R=0.644 and p<0.001), but was not significant between the extensional stiffness and the aortic diameter (R=0.341 and p=0.065). Interestingly, a significant positive 236 correlation was found between extensional stiffness and patients age for BAV ATAAs 237 (R=0.619 and p=0.032), but not for TAV ATAAs (R=-0.117 and p=0.645) as shown by 238 Fig. 5C and Fig. 5D. Fig. 5E and Fig. 5F show the relationship of both strain and stress 239 240 obtained in the circumferential direction with the average extensional stiffness. The 241 extensional stiffness was inversely correlated with the circumferential strain (R=-0.522 and p=0.00324) and positively with the circumferential stress (R=0.474 and p=0.008). Correlation 242 243 analysis of extensional stiffness with age (Fig.5C) also revealed that BAV ATAAs can be divided into two subgroups: 1) patients younger than 50 years old who had a relatively low 244 extensional stiffness, 2) patients older than 55 years old who had a relatively high 245 extensional stiffness. All analysis in Fig.5 were also broken down by aneurysm type, results 246 247 are reported in Fig.A1.

248

Peak systolic WSSs were correlated to the average extensional stiffness for each ascending aortic level and aortic quadrant. The correlation analysis between extensional stiffness and WSS values evaluated at proximal ascending thoracic aorta (AA2) appears promising (R=0.343 and p=0.080 for AA2), but no significant correlation was found between stiffness and WSS evaluated locally for Major, Minor and Anterior quadrants. For the Posterior quadrant a correlation was identified although the obtained p-value was very close to the threshold

(p=0.05) and a low coefficient was obtained. Results are presented in Fig.6. All analysis werealso broken down by aneurysm type, results are reported in Fig.A2.

257

A PCA based on patient's age, aortic diameter, aortic pulse pressure, extensional stiffness and WSS showed no separation of BAV ATAAs from TAV ATAAs (see Fig. 7). However, the loading plot revealed that the most important variables responsible for differences between BAV ATAAs and TAV ATAAs are the pulsed pressure and the patient's age.

262

263 Discussion

This study aimed to investigate the patterns of extensional stiffness from in vivo dynamic 264 265 imaging of ATAAs and to evaluate potential correlations with clinical data and blood shear 266 forces. The extensional stiffness did not show any significant difference between BAV ATAAs 267 and TAV ATAAs. This supports recent evidence and observations for which there should be 268 no distinction in the surgical management of BAV patients versus TAV patients (Agnese et al., 2019). Recently, we performed equibiaxial mechanical testing on ascending aortic tissues 269 270 with either BAV or TAV (Di Giuseppe et al., 2019) and found no difference in the mean values of the aortic tissue stiffness between BAV ATAAs and TAV ATAAs as reported here. 271 However, other groups who performed mechanical testing on ascending aortic tissues found 272 differences in the mean values of the aortic tissue stiffness between BAV patients and TAV 273 274 patients (Choudhury et al., 2009; Duprey et al., 2010; Okamoto et al., 2002; Pham et al., 275 2013; Pichamuthu et al., 2013). We did not measure the extensional stiffness in non 276 aneurysmatic subjects as healthy subjects cannot undergo CT scans. However the stiffness 277 of healthy aortas was measured by a variety of other techniques in the literature and values 278 in a range between 150 kPa and 1000 kPa were reported, with ATAA exhibiting generally a 279 higher stiffness than healthy aortas (Azadani et al., 2013; Walraevens et al., 2008). 280

The correlation of patients' age with the extensional stiffness obtained by the LESI methodology was strongly affected by the valve phenotype. For TAV patients, the

283 extensional stiffness did not vary with the patient age but increased with the age of BAV 284 patients. This is likely a consequence of the significant difference in the age of BAV versus TAV patients. Indeed, TAV ATAAs were older than 50 years while most of patients with BAV 285 286 were <50 years. We also found that BAV ATAAs can be divided into two subgroups: 1) patients younger than 50 years old who had a relatively low extensional stiffness, 2) patients 287 older than 55 years old who had a relatively high extensional stiffness. Martin et al. (Martin et 288 289 al., 2013b) showed that the biomechanical properties of dilated ascending aorta change 290 between 50 and 60 years, and this could explain either the difference in the extensional stiffness of two subgroups of BAV ATAAs or the lack of correlation between the extensional 291 292 stiffness and patient age for TAV ATAAs.

293

As expected, no significant correlation was found between extensional stiffness and shear stress for Major, Minor and Anterior quadrant, thereby suggesting there is no direct link between hemodynamics and biomechanical properties of ATAA wall. For the posterior quadrant, instead, a significant correlation was observed.

298

The extensional stiffness was significantly correlated with both the pulsed pressure and the circumferential strain and stress. Although these variables are directly involved in the derivation of the aortic stiffness in the LESI methodology, these significant correlations can also be interpreted with physiological principles.

303 Relations between the aortic stiffness and the pulsed pressure have been known for 304 decades. Indeed, as the aorta becomes stiffer, the central pulsed pressure is higher due to 305 the increase in the pulse wave velocity and the early return of reflected waves to the heart 306 from following junctions (Fung, 1998). In a young and healthy aorta, the reflected wave tends 307 to hit the aortic root during diastole, serving to increase diastolic pressure and hence 308 improving perfusion of coronary arteries. In aged and stiffened aortas, the reflected hits the 309 aortic root earlier, increasing the systolic pressure and decreasing the diastolic one. The 310 amplitude of reflected waves increases as the arterial stiffness increases, further augmenting

central systolic pressure (Chirinos and Segers, 2010a, b; Fung, 1998; Laurent et al., 2005;
Mackenzie et al., 2002; O'Rourke and Nichols, 2005). The effects of this supplemental load
onto the aorta, which are direct expressions of the stiffness increase, should be reckoned for
estimating the risk of rupture or dissection of ATAAs.

As expected, the extensional stiffness was also significantly correlated to the circumferential 315 strain since circumferential strains are a direct expression of the aortic stiffness. Stiffening 316 often triggers degradation and/or loss of a fraction of elastin fibers, leading to a reduction of 317 318 the wall extensibility (Sokolis et al., 2012). Another consequence is also a decrease of the 319 axial stretch of the aorta, producing an increase of the aortic arch curvature named unfolding 320 (Redheuil et al., 2011). The degradation of protein networks in the extracellular matrix of 321 ATAAs can be explained by the unbalance between protein synthesis by vascular cells and 322 protein destruction by matrix metalloproteases (MMPs) (LeMaire et al., 2005). In the cohort 323 from which this study group was extracted, we found that the expression level of MMP-9 is altered in BAV ATAAs vs TAV ATAAs (Gallo et al., 2018). The significant correlation between 324 extensional stiffness and stress is very common for fibrous soft tissues, owing to their 325 326 exponential stress-strain curve (García-Herrera et al., 2012). This reflects reorientation and straightening of collagen bundles upon loading (Sokolis et al., 2006). 327

328 When analyzing BAV and TAV ATAAs together, the PCA analysis suggested that BAV

329 ATAAs are likely forming a cluster in the lower quadrants of the multivariate score plot in the

direction of the loading associated to patient age. This is not surprising because BAV

patients are known to commonly develop ATAA at younger age than TAV (Agnese et al.,

332 2019; LeMaire et al., 2005).

333

334 Limitations

The LESI approach relies on local equilibrium equations as it is based on the principle of virtual work (Bersi et al., 2016). As for the generalized Laplace's law, the LESI approach considers the local equilibrium between pressures and tensions in a membrane, indicating that the aortic wall experience no shear through the thickness. This may not be a realistic

assumption in regions near the aortic branches but these were excluded from the analysis. 339 340 The peripheral pulsed pressure rather than central aortic pressure was used. However, the mismatch of aortic compliance between the brachial artery and the aorta should be likely 341 342 reduced or even reversed with the advanced age of our patients. The effect of brachial blood pressure on the extensional stiffness evaluations will be likely minimal in this study. 343 Validation of in silico modeling has to be established. A large sample size including BAV 344 ATAAs matched with the age of TAV ATAAs would be ideal to confirm observations. 345 346 Unfortunately, we could not compare results with those relative of non aneurysmatic subjects because healthy control volunteers are not allowed to undertake multiphase gated CT scans 347 348 due to x-ray radiations risks. We are trying to extend our methodology to other imaging 349 modalities (ultrasounds, MRI).

350

351 **Conclusions**

We evaluated the patterns of extensional stiffness from the in vivo imaging of ATAAs on a cohort of 30 patients using the LESI methodology. We found no appreciable differences between BAV and TAV patients. Regional differences appeared marginal due to interindividual variability. The correlation of patients' age with the extensional stiffness strongly depended on the valve phenotype. Strong relationship of the extensional stiffness with the pulsed pressure was found, supported by biomechanical explanations.

358

359 Acknowledgments

Stéphane Avril is grateful to the European Research Council (ERC grant Biolochanics, grant
 number 647067) for financial support. This work was supported by a "Ricerca Finalizzata" grant
 from the Italian Ministry of Health (GR-2011-02348129) to Salvatore Pasta, and by grant from
 PON FSE-FESR Ricerca Innovazione 2014–2020 to Marzio Di Giuseppe.

364

365 Conflict of interest statement

366 The authors confirm there are not conflict of interest associated with this publication.

368

370

371

369 Reference

372 predictors of surgical replacement of the aorta: A comparison of bicuspid and tricuspid aortic valve 373 patients over eight years of follow-up. Journal of Molecular and Cellular Cardiology 135, 31-39. 374 375 Antiga, L., Steinman, D.A., 2004. Robust and objective decomposition and mapping of bifurcating 376 vessels. IEEE Transactions on Medical Imaging 23, 704-713. 377 378 Azadani, A.N., Chitsaz, S., Mannion, A., Mookhoek, A., Wisneski, A., Guccione, J.M., Hope, M.D., Ge, L., 379 Tseng, E.E., 2013. Biomechanical properties of human ascending thoracic aortic aneurysms. The Annals 380 of Thoracic Surgery 96, 50-58. 381 382 Bersi, M.R., Bellini, C., Di Achille, P., Humphrey, J.D., Genovese, K., Avril, S., 2016. Novel methodology 383 for characterizing regional variations in the material properties of murine aortas. Journal of 384 Biomechanical Engineering 138, 071005. 385 386 Borger, M.A., Fedak, P.W.M., Stephens, E.H., Gleason, T.G., Girdauskas, E., Ikonomidis, J.S., 387 Khoynezhad, A., Siu, S.C., Verma, S., Hope, M.D., Cameron, D.E., Hammer, D.F., Coselli, J.S., Moon, 388 M.R., Sundt, T.M., Barker, A.J., Markl, M., Della Corte, A., Michelena, H.I., Elefteriades, J.A., 2018. The 389 american association for thoracic surgery consensus guidelines on bicuspid aortic valve-related 390 aortopathy: full online-only version. The Journal of Thoracic and Cardiovascular Surgery 156, e41-e74. 391 392 Chirinos, J.A., Segers, P., 2010a. Noninvasive evaluation of left ventricular afterload: part 1: pressure 393 and flow measurements and basic principles of wave conduction and reflection. Hypertension 56, 555-394 562. 395 396 Chirinos, J.A., Segers, P., 2010b. Noninvasive evaluation of left ventricular afterload: part 2: arterial 397 pressure-flow and pressure-volume relations in humans. Hypertension 56, 563-570. 398 399 Choudhury, N., Bouchot, O., Rouleau, L., Tremblay, D., Cartier, R., Butany, J., Mongrain, R., Leask, R.L., 400 2009. Local mechanical and structural properties of healthy and diseased human ascending aorta 401 tissue. Cardiovascular Pathology 18, 83-91. 402 403 Coady, M.A., Rizzo, J.A., Goldstein, L.J., Elefteriades, J.A., 1999. Natural history, pathogenesis and 404 etiology of thoracic aortic aneurysms and dissections. Cardiology Clinics 17, 615-635.

Agnese, V., Pasta, S., Michelena, H.I., Minà, C., Romano, G.M., Carerj, S., Zito, C., Maalouf, J.F., Foley,

T.A., Raffa, G., Clemenza, F., Pilato, M., Bellavia, D., 2019. Patterns of ascending aortic dilatation and

405

D'Ancona, G., Amaducci, A., Rinaudo, A., Pasta, S., Follis, F., Pilato, M., Baglini, R., 2013. Haemodynamic
predictors of a penetrating atherosclerotic ulcer rupture using fluid–structure interaction analysis.
Interactive Cardiovascular and Thoracic Surgery 17, 576-578.

409

Di Giuseppe, M., Alotta, G., Agnese, V., Bellavia, D., Raffa, G.M., Vetri, V., Zingales, M., Pasta, S., Pilato,
M., 2019. Identification of circumferential regional heterogeneity of ascending thoracic aneurysmal
aorta by biaxial mechanical testing. Journal of Molecular and Cellular Cardiology 130, 205-215.

- 414 Duprey, A., Khanafer, K., Schlicht, M., Avril, S., Williams, D., Berguer, R., 2010. In vitro characterisation 415 of physiological and maximum elastic modulus of ascending thoracic aortic aneurysms using uniaxial
- 416 tensile testing. European Journal of Vascular and Endovascular Surgery 39, 700-707.
- 417
- 418 Duprey, A., Trabelsi, O., Vola, M., Favre, J.-P., Avril, S., 2016. Biaxial rupture properties of ascending 419 thoracic aortic aneurysms. Acta Biomaterialia 42, 273-285.
- 420
- 421 Elefteriades, J.A., Farkas, E.A., 2010. Thoracic aortic aneurysm: clinically pertinent controversies and 422 uncertainties. Journal of the American College of Cardiology 55, 841-857.
- 423 Farzaneh, S., Trabelsi, O., Avril, S., 2019a. Inverse identification of local stiffness across ascending 424 thoracic aortic aneurysms. Biomechanics and Modeling in Mechanobiology 18, 137-153.
- 425
- Farzaneh, S., Trabelsi, O., Chavent, B., Avril, S., 2019b. Identifying local arterial stiffness to assess the
 risk of rupture of ascending thoracic aortic aneurysms. Annals of Biomedical Engineering 47, 10381050.
- 429
- 430 Fung, Y.-C., 1998. Biomechanics: circulation. Springer 9, 155.
- 431
 432 Gallo, A., Agnese, V., Coronnello, C., Raffa, G.M., Bellavia, D., Conaldi, P.G., Pilato, M., Pasta, S., 2018.
 433 On the prospect of serum exosomal miRNA profiling and protein biomarkers for the diagnosis of
 434 ascending aortic dilatation in patients with bicuspid and tricuspid aortic valve. International journal of
 435 Cardiology 273, 230-236.
- 436

- García-Herrera, C.M., Atienza, J., Rojo, F., Claes, E., Guinea, G., Celentano, D.J., García-Montero, C.,
 Burgos, R., 2012. Mechanical behaviour and rupture of normal and pathological human ascending
 aortic wall. Medical & Biological Engineering & Computing 50, 559-566.
- Guala, A., Rodriguez-Palomares, J., Dux-Santoy, L., Teixido-Tura, G., Maldonado, G., Galian, L., Huguet,
 M., Valente, F., Gutiérrez, L., González-Alujas, T., 2019. Influence of aortic dilation on the regional
 aortic stiffness of bicuspid aortic valve assessed by 4-dimensional flow cardiac magnetic resonance:
 comparison with Marfan syndrome and degenerative aortic aneurysm. JACC: Cardiovascular Imaging
 12, 1020-1029.
- 446
- Januzzi, J.L., Isselbacher, E.M., Fattori, R., Cooper, J.V., Smith, D.E., Fang, J., Eagle, K.A., Mehta, R.H.,
 Nienaber, C.A., Pape, L.A., 2004. Characterizing the young patient with aortic dissection: results from
 the international registry of aortic dissection (IRAD). Journal of the American College of Cardiology 43,
 665-669.
- Joldes, G.R., Miller, K., Wittek, A., Doyle, B., 2016. A simple, effective and clinically applicable method
 to compute abdominal aortic aneurysm wall stress. Journal of the Mechanical Behavior of Biomedical
 Materials 58, 139-148.
- 455
- Khanafer, K.M., Gadhoke, P., Berguer, R., Bull, J.L., 2006. Modeling pulsatile flow in aortic aneurysms:
 effect of non-Newtonian properties of blood. Biorheology 43, 661-679.
- 458
- Laurent, S., Boutouyrie, P., Lacolley, P., 2005. Structural and genetic bases of arterial stiffness.
 Hypertension 45, 1050-1055.
- 461
- LeMaire, S.A., Wang, X., Wilks, J.A., Carter, S.A., Wen, S., Won, T., Leonardelli, D., Anand, G., Conklin,
 L.D., Wang, X.L., 2005. Matrix metalloproteinases in ascending aortic aneurysms: Bicuspid versus
 trileaflet aortic valves. Journal of Surgical Research 123, 40-48.
- 465

466 Leuprecht, A., Perktold, K., 2001. Computer simulation of non-Newtonian effects on blood flow in large 467 arteries. Computer Methods in Biomechanics and Biomedical Engineering 4, 149-163. 468 469 Longobardo, L., Carerj, M.L., Pizzino, G., Bitto, A., Piccione, M.C., Zucco, M., Oreto, L., Todaro, M.C., 470 Calabrò, M.P., Squadrito, F., Di Bella, G., Oreto, G., Khandheria, B.K., Carerj, S., Zito, C., 2017. 471 Impairment of elastic properties of the aorta in bicuspid aortic valve: relationship between 472 biomolecular and aortic strain patterns. European Heart Journal - Cardiovascular Imaging 19, 879-887. 473 Mackenzie, I., Wilkinson, I., Cockcroft, J., 2002. Assessment of arterial stiffness in clinical practice. Qjm 474 95, 67-74. 475 476 Mahadevia, R., Barker, A.J., Schnell, S., Entezari, P., Kansal, P., Fedak, P.W., Malaisrie, S.C., McCarthy, 477 P., Collins, J., Carr, J., 2014. Bicuspid aortic cusp fusion morphology alters aortic three-dimensional 478 outflow patterns, wall shear stress, and expression of aortopathy. Circulation 129, 673-682. 479 480 Martin, C., Sun, W., Pham, T., Elefteriades, J., 2013a. Predictive biomechanical analysis of ascending 481 aortic aneurysm rupture potential. Acta Biomaterialia 9, 9392-9400. 482

- Martin, C., Sun, W., Primiano, C., McKay, R., Elefteriades, J., 2013b. Age-dependent ascending aorta
 mechanics assessed through multiphase CT. Annals of Biomedical Engineering 41, 2565-2574.
- 486 Mendez, V., Di Giuseppe, M., Pasta, S., 2018. Comparison of hemodynamic and structural indices of
 487 ascending thoracic aortic aneurysm as predicted by 2-way FSI, CFD rigid wall simulation and patient488 specific displacement-based FEA. Computers in Biology and Medicine 100, 221-229.
- Mousavi, S.J., Avril, S., 2017. Patient-specific stress analyses in the ascending thoracic aorta using a
 finite-element implementation of the constrained mixture theory. Biomechanics and Modeling in
 Mechanobiology 16, 1765-1777.
- 493

- 494 O'Rourke, M.F., Nichols, W.W., 2005. Aortic diameter, aortic stiffness, and wave reflection increase
 495 with age and isolated systolic hypertension. Hypertension 45, 652-658.
- 496
 497 Okamoto, R.J., Wagenseil, J.E., DeLong, W.R., Peterson, S.J., Kouchoukos, N.T., Sundt, T.M., 3rd, 2002.
 498 Mechanical properties of dilated human ascending aorta. Annal of Biomedical Engineering 30, 624499 635.
- 500
- Pape, L.A., Tsai, T.T., Isselbacher, E.M., Oh, J.K., O'Gara P, T., Evangelista, A., Fattori, R., Meinhardt, G.,
 Trimarchi, S., Bossone, E., Suzuki, T., Cooper, J.V., Froehlich, J.B., Nienaber, C.A., Eagle, K.A., 2007.
 Aortic diameter >or = 5.5 cm is not a good predictor of type A aortic dissection: observations from the
 International Registry of Acute Aortic Dissection (IRAD). Circulation 116, 1120-1127.
- 505
- Pasta, S., Agnese, V., Di Giuseppe, M., Gentile, G., Raffa, G.M., Bellavia, D., Pilato, M., 2017a. In vivo
 strain analysis of dilated ascending thoracic aorta by ECG-gated CT angiographic imaging. Annals of
 Biomedical Engineering 45, 2911-2920.
- Pasta, S., Gentile, G., Raffa, G., Bellavia, D., Chiarello, G., Liotta, R., Luca, A., Scardulla, C., Pilato, M.,
 2017b. In silico shear and intramural stresses are linked to aortic valve morphology in dilated ascending
 aorta. European Journal of Vascular and Endovascular Surgery 54, 254-263.
- 513
 514 Pham, T., Martin, C., Elefteriades, J., Sun, W., 2013. Biomechanical characterization of ascending aortic
 515 aneurysm with concomitant bicuspid aortic valve and bovine aortic arch. Acta Biomaterialia 9, 7927516 7936.
- 517

- Pichamuthu, J.E., Phillippi, J.A., Cleary, D.A., Chew, D.W., Hempel, J., Vorp, D.A., Gleason, T.G., 2013.
 Differential tensile strength and collagen composition in ascending aortic aneurysms by aortic valve
 phenotype. Annals of Thoracic Surgery 96, 2147-2154.
- Prakash, A., Adlakha, H., Rabideau, N., Hass, C.J., Morris, S.A., Geva, T., Gauvreau, K., Singh, M.N., Lacro,
 R.V., 2015. Segmental aortic stiffness in children and young adults with connective tissue disorders:
 relationships with age, aortic size, rate of dilation, and surgical root replacement. Circulation 132, 595602.
- Raaz, U., Zöllner, A.M., Schellinger, I.N., Toh, R., Nakagami, F., Brandt, M., Emrich, F.C., Kayama, Y.,
 Eken, S., Adam, M., 2015. Segmental aortic stiffening contributes to experimental abdominal aortic
 aneurysm development. Circulation 131, 1783-1795.
- Redheuil, A., Yu, W.-C., Mousseaux, E., Harouni, A.A., Kachenoura, N., Wu, C.O., Bluemke, D., Lima,
 J.A.C., 2011. Age-related changes in aortic arch geometry: relationship with proximal aortic function
 and left ventricular mass and remodeling. Journal of the American College of Cardiology 58, 1262-1270.
- Rooprai, J., Boodhwani, M., Beauchesne, L., Chan, K.L., Dennie, C., Nagpal, S., Messika-Zeitoun, D.,
 Coutinho, T., 2019. Thoracic aortic aneurysm growth in bicuspid aortic valve patients: role of aortic
 stiffness and pulsatile hemodynamics. Journal of the American Heart Association 8, e010885.
- Selvin, E., Najjar, S.S., Cornish, T.C., Halushka, M.K., 2010. A comprehensive histopathological
 evaluation of vascular medial fibrosis: Insights into the pathophysiology of arterial stiffening.
 Atherosclerosis 208, 69-74.
- 543 Smoljkic, M., Fehervary, H., Van den Bergh, P., Jorge-Penas, A., Kluyskens, L., Dymarkowski, S., 544 Verbrugghe, P., Meuris, B., Vander Sloten, J., Famaey, N., 2017. Biomechanical characterization of 545 ascending aortic aneurysms. Biomechanics and Modeling in Mechanobiology 16, 705-720.
- 546
 547 Sokolis, D.P., Kefaloyannis, E.M., Kouloukoussa, M., Marinos, E., Boudoulas, H., Karayannacos, P.E.,
 548 2006. A structural basis for the aortic stress–strain relation in uniaxial tension. Journal of Biomechanics
 549 39, 1651-1662.
- 550

521

526

530

- Sokolis, D.P., Kritharis, E.P., Giagini, A.T., Lampropoulos, K.M., Papadodima, S.A., Iliopoulos, D.C., 2012.
 Biomechanical response of ascending thoracic aortic aneurysms: association with structural
 remodelling. Computer Methods in Biomechanics and Biomedical Engineering 15, 231-248.
- Sulejmani, F., Pokutta-Paskaleva, A., Ziganshin, B., Leshnower, B., Iannucci, G., Elefteriades, J., Sun, W.,
 2017. Biomechanical properties of the thoracic aorta in Marfan patients. Annals of Cardiothoracic
 Surgery 6, 610.
- 558
- Teixeira, R., Moreira, N., Baptista, R., Barbosa, A., Martins, R., Castro, G., Providência, L., 2012.
 Circumferential ascending aortic strain and aortic stenosis. European Heart Journal Cardiovascular
 Imaging 14, 631-641.
- 562

- van Ooij, P., Markl, M., Collins, J.D., Carr, J.C., Rigsby, C., Bonow, R.O., Malaisrie, S.C., McCarthy, P.M.,
 Fedak, P.W., Barker, A.J., 2017. Aortic valve stenosis alters expression of regional aortic wall shear
 stress: New insights from a 4-dimensional flow magnetic resonance imaging study of 571 subjects.
 Journal of the American Heart Association 6, e005959.
- Verma, S., Siu, S.C., 2014. Aortic dilatation in patients with bicuspid aortic valve. New England Journalof Medicine 370, 1920-1929.

- Walraevens, J., Willaert, B., De Win, G., Ranftl, A., De Schutter, J., Vander Sloten, J., 2008. Correlation
 between compression, tensile and tearing tests on healthy and calcified aortic tissues. Medical
 Engineering & Physics 30, 1098-1104.
- 574 Youssefi, P., Gomez, A., He, T., Anderson, L., Bunce, N., Sharma, R., Figueroa, C.A., Jahangiri, M., 2017.
- 575 Patient-specific computational fluid dynamics—assessment of aortic hemodynamics in a spectrum of
- aortic valve pathologies. The Journal of Thoracic and Cardiovascular Surgery 153, 8-20. e23.

-

- ----

599 Figure Legends

626

and TAV (H) patients.

Figure 1: Representation of ATAA: anterior, posterior, major and minor regions are shown inboxes.

Figure 2: Representative extensional stiffness maps of 6 patients reconstructed using LESI

603 methodology for TAV ATAA and BAV ATAA patients.

604 **Figure 3**: Representative wall shear stress maps of 2 patients obtained by CFD analysis for

605 TAV ATAA and BAV ATAA patients.

Figure 4: Comparisons of average extensional stiffness of BAV ATAAs and TAV ATAAs
evaluated at different quadrants.

Figure 5: (A) Correlation between average extensional stiffness and ascending aortic

diameter; (B) correlation between average extensional stiffness and aortic pulse pressure;

610 (C) correlation between average extensional stiffness and patients' age of BAV ATAAs; (D)

611 correlation between average extensional stiffness patients' age of TAV ATAAs; (E) average

612 extensional stiffness vs circumferential strain data with regression curve; (F) correlation

613 between average extensional stiffness and circumferential stress.

Figure 6: Correlation between extensional stiffness and peak systolic WSSs evaluated at
proximal ascending aorta from (A) major, (B) minor, (C) anterior and (D) posterior regions.
Figure 7: Two-dimensional score plots of PC1 versus PC2 with loading showing the main
variables responsible for clustering BAV ATAAs (black dots) from TAV ATAAs (red dots); the
plot shows patient's age, aortic diameter, aortic pulse pressure, extensional stiffness and wall
shear stress. Solid lines represent 95% tolerance ellipse of TAV ATAAs (red color) and BAV
ATAAs (black color).

Figure A1: Correlation between average extensional stiffness vs circumferential strain data
with regression curve for BAV (A) and TAV (B) patients; correlation between average
extensional stiffness vs circumferential stress for BAV (C) and TAV (D) patients; correlation
between average extensional stiffness vs aortic pulse pressure for BAV (E) and TAV (F)
patients; correlation between average extensional stiffness vs aortic diameter for BAV (G)

627	Figure A2: Correlation between extensional stiffness and peak systolic WSSs evaluated at						
628	proximal ascending aorta from major, minor, anterior and posterior regions for BAV						
629	(A,C,E,G) and TAV patients (B,D,F,H).						
630							
631							
632							
633							
634							
635							
636							
637							
638							
639							
640							
641							
642							
643							
644							
645							
646							
647							
648							
649							
650							
651							
652							

654 Figure 1



- 0, 1













749 Figure 7







			Age	Systolic Pressure	Diastolic Pressure	Aortic Diameter
ID	Sex	Valve	[years]	[mmHg]	[mmHg]	[mm]
1	М	TAV	56	140	74	45.9
2	Μ	TAV	55	136	76	41.7
3	Μ	BAV	62	135	77	40.13
4	Μ	BAV	43	125	88	36.32
5	Μ	BAV	48	135	85	42.15
6	Μ	TAV	71	145	70	50.5
7	Μ	BAV	58	150	70	48.04
8	Μ	TAV	73	100	77	47.3
9	Μ	TAV	61	180	86	43.5
10	Μ	TAV	67	136	75	49.05
11	Μ	TAV	67	140	80	45.01
12	Μ	TAV	68	122	70	46.27
13	F	TAV	83	150	75	42.23
14	Μ	TAV	65	116	73	46.1
15	Μ	TAV	61	136	70	44.8
16	Μ	BAV	48	130	80	37.2
17	Μ	BAV	49	136	75	28.56
18	Μ	TAV	68	129	77	40.27
19	Μ	TAV	53	126	72	46.7
20	F	TAV	64	144	68	44.67
21	Μ	TAV	73	144	84	48.47
22	Μ	BAV	41	136	75	30.13
23	Μ	BAV	42	131	68	46.59
24	Μ	TAV	64	120	80	37.43
25	Μ	BAV	48	148	90	47.05
26	Μ	TAV	64	130	80	37.71
27	Μ	BAV	45	124	78	49.21
28	F	BAV	61	144	77	48.36
29	F	TAV	52	125	70	42.1
30	Μ	BAV	58	136	76	40.86
			58.9±10.4	135.0±13.8	76.5±5.8	43.1±5.4