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Influence of Mn and Fe addition on the NOx storage-reduction properties and SO₂ poisoning of a Pt/Ba/Al₂O₃ model catalyst.

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Abstract

This work deals with the effect of Mn or Fe addition on the NOx storage-reduction properties of a Pt/Ba/Al₂O₃ model catalyst. NOx storage capacity, SO₂ poisoning and regeneration and NOx removal efficiency under rich/lean cycling conditions are studied.

Fe addition to Pt/Ba/Al₂O₃ leads only to a small increase of NOx storage capacity, and more interestingly, to a better sulfur removal due to the inhibition of bulk barium sulfate formation. Unfortunately, the NOx storage property cannot be fully recovered. Moreover, Fe addition results in a decrease in the NOx removal efficiency. Mn addition also improves the NOx storage capacity, but no significant influence on the sulfur elimination is observed. Mn-doped catalyst does not improve the NOx removal efficiency, but NH₃ selectivity is found to drastically decrease at 400°C, from 20% to 3%. In addition, the NOx conversion can be improved at higher H₂ concentration in the rich pulse, always keeping NH₃ selectivity at low level.

Keywords: NOx, storage, reduction, SO₂ poisoning, Pt, Ba, Fe, Mn.

Introduction

The NOx storage reduction (NSR) process is presented as a possible solution to reduce NOx emissions from lean burn engine. A drawback to this system is the catalyst deactivation, mainly due to (i) sulfur poisoning [1,2] even if the sulfur content in fuels is lowered and (ii) thermal aging [3]. Another problem arises from ammonia emissions. Indeed, NH₃ can be formed during short excursions under rich conditions which are necessary to reduce trapped NOx species [4,5].

The impact of the support oxide on the NOx storage properties of Pt–Ba catalysts, especially toward sulfur resistance and sulfur regeneration, was studied in previous works [6,7]. The aim of this work is to determine the effect of Mn and Fe addition on the properties of a Pt/Ba/Al₂O₃ model catalyst. Mn is known to be active in NO oxidation, a crucial step for the storage process [8,9]. Moreover, Mn can also participate to the NOx storage [10,11] and presents an activity in the NOx reduction by NH₃ reaction [12,13]. Fe is generally added in NSR formulations to improve the catalyst sulfur resistance. Iron oxide is reported to inhibit the bulk barium sulfates formation [14,15].

In addition to the NOx storage capacity measurements and the sulfur impact evaluation, the NOx removal efficiency of the studied catalysts was measured under cycling conditions. Activity and selectivity, especially toward NH₃ emission, are considered.

Experimental

The reference catalyst contains 1wt% Pt and 10wt% BaO on alumina. In addition, the modified samples contain 3.8wt% Mn or 3.9wt% Fe, corresponding to a Ba/additive molar ratio of 1. Ba and additives were deposited by co-precipitation. Alumina powder (230 m².g⁻¹) was suspended in a solution at 60°C and pH 10, in order to ensure complete precipitation of the barium and transition metal. The nitrate salts of the desired compounds (Ba^{II}, Mn^{IV}, Fe^{III}) were then added under vigorous stirring, and the pH was maintained constant by ammonia addition. After 30 min, the solution was evaporated at 80°C under air and the resulting powder was dried at 120°C. After calcination at 700°C, platinum (1wt%) was impregnated using a Pt(NH₃)₂(NO₂)₂ aqueous solution. After drying, the catalyst was pretreated at 700°C for 4h under N₂, and finally stabilized at 700°C for 4h under a mixture containing 10% O₂, 5% H₂O in N₂. As previously reported [16], the intermediate nitrogen treatment allows a higher platinum-barium dispersion. The obtained catalysts, named stabilized, are noted Pt/10Ba/AI, Pt/10BaMn/AI and Pt/10BaFe/AI. They exhibit BET specific surface areas of 172 m².g⁻¹, 150 m².g⁻¹ and 151 m²g⁻¹, respectively.

X-ray powder diffraction was performed at room temperature using a Bruker D5005 diffractometer equipped with a K α Cu radiation (λ =1.54056 Å).

NOx storage capacities were measured at 300°C under dynamic conditions with a mixture containing 350ppm NO, 10% O₂, 10% CO₂ and 10% H₂O in N₂ (GHSV=100000 h⁻¹). The NOx storage capacity was estimated by the integration of the recorded profile after subtraction of the contribution of the apparatus (dead volume) deduced from a test without catalyst. The reported data correspond to 100s of storage. In this case, 67 µmol NOx per gram of catalyst passed through the catalyst. The sulfating treatment was performed at 300°C with SO₂ and corresponds to a 2.0 wt% S theoretical content if all the sulfur is stored on the catalyst. The regeneration of sulfated catalysts was carried out at 550°C for 30 min under rich conditions with a mixture containing 2.5% H₂, 10% CO₂, and 10% H₂O in N₂.

Sulfates stability was evaluated by H_2 -TPR. The sample was first in-situ pretreated at 300°C under pure oxygen. The reduction was carried out with 1% H_2 from room temperature up to 800°C.

NOx removal efficiency was measured over stabilized catalysts under cycling conditions (60s lean / 3s rich) at 200, 300 and 400°C. The lean and reach reaction mixtures are described in Table 1. NO and NOx concentrations (NO+NO₂) were followed by chemiluminescence, N₂O by FT-IR and H₂ using a mass spectrometer. For each tested temperature, water was condensed at 0°C at the reactor outlet and before the analyzers, during 30 min for each temperature after signals stabilization. The ammonia and the nitrate/nitrite amounts trapped in the condensed water were analyzed using two HPLC. Some tests were also performed using a multigas FT-IR detector (MKS 2030).

Table1: Rich and lean gas compositions used for the NOx conversion test (60s lean / 3s rich). GHSV=100000 h^{-1}

Gas	NO	H ₂	O ₂	CO ₂	H ₂ O	N ₂
Rich	-	3, 6 or 9%	0.02%	10%	10%	Balance
Lean	500ppm	-	10%	10%	10%	Balance

Results and discussion

Characterization of the stabilized catalysts.

The three samples were characterized by X-ray diffraction before and after platinum impregnation (diffractogramms not shown). The BaAl₂O₄ structure is detected in all samples but at higher intensity before platinum impregnation and consecutive calcination. Indeed, BaAl₂O₄ is partially soluble in the platinum impregnation solution and it was not fully reformed, even after the two final thermal treatments at 700°C. In opposition, BaCO₃ is clearly identified after stabilization of the catalysts whereas this structure was not evidenced before the platinum impregnation. In addition to BaCO₃ and BaAl₂O₄, weak reflections attributed to Fe₂O₃ are observed in Pt/10BaFe/AI. For Pt/10BaMn/AI, the BaMnO₃ phase was detected before the platinum impregnation, but the diffraction peaks nearly disappeared in the stabilized catalyst. No other manganese oxide phase have been detected whatever the preparation step.

H₂-TPR profiles of the stabilized catalysts are reported in Figure 1. No significant H₂ consumption is observed in the 100-800°C temperature range for the Pt/10Ba/Al catalyst. Addition of Mn induces a main reduction peak around 300°C. This peak is assigned to the reduction of manganese oxides into MnO. According to Laberty et al. [17], the reduction of MnO₂ into MnO occurs between 250 and 450°C, with intermediate formation of the Mn₂O₃ and Mn₃O₄ phases. Taking into account the H₂ consumption in the 100-800°C temperature range, a mean oxidation state of 3.22 is calculated for Mn, indicating mainly the presence of Mn^{III} (for instance Mn₂O₃) and Mn^{IV} (*i.e.* BaMnO₃ as detected by XRD, and/or MnO₂) before reduction.

The iron oxide reduction occurs at high temperature, with a broad reduction peak between 450 and 800°C. Tang et al. [18] have established that Fe_2O_3 is firstly reduced into Fe_3O_4 between 300 and 470°C and formation of Fe^{II}/Fe^{III} -based aluminates are observed. Reduction of the aluminates occurs from 500 to 1000°C. Then, iron in Pt/10Fe/AI should mainly exist as aluminates, even if no corresponding XRD peaks were observed. Assuming

a Fe^{III} into Fe^{\circ} reduction, the H₂ consumption in the 100-800^{\circ}C temperature range would correspond to a reduction rate in metallic iron of 57%. It means that iron is not fully reduced, and should partially remains as hardly reducible aluminate species.

NOx storage capacity, SO2 poisoning and regeneration.

The storage capacities of the stabilized catalysts, measured at 300°C, are reported in Table 2. Mn and Fe addition is found to slightly improve the NOx storage capacity. Pt/10BaMn/Al exhibits the higher value, with 39.5 μ mol.g⁻¹, versus 35.8 μ mol.g⁻¹ and 31.2 μ mol.g⁻¹ for Pt/10BaFe/Al and Pt/Ba/Al, respectively. In order to clarify the role of Fe and Mn, additional tests were performed at 300°C without H₂O and CO₂ in the reaction mixture. Compared to Pt/Ba/Al, the storage capacity at saturation (after 900 s) was 15% higher after Mn addition, indicating an increase in the storage sites number, but no improvement of the NO oxidation rate was observed (NO₂/NOx molar ratio after saturation close to 25%). However, a 10BaMn/Al sample without platinum is able to store NOx (75% of the capacity obtained at 100s with Pt/10BaMn/Al), with a NO₂/NOx ratio at saturation of 20%. Then, Mn may participate to the NO oxidation and to the NOx storage as mentioned by Bentrup et al. [10] and Xiao et al. [11].

Iron addition does not modify the total number of available sites for the NOx storage, estimated at saturation without H_2O and CO_2 in the feed stream, in accordance with the results of Yamakasi et al. [12]. The improvement of the NOx storage capacity at 100s with H_2O and CO_2 in the feed stream could be attributed to a decrease of the catalyst basicity. Indeed, Pt/10BaFe/Al is less sensitive to H_2O and CO_2 than Pt/10Ba/Al, the loss of storage capacity being 16% and 27%, respectively. This suggests a lower adsorption competition between NOx and CO_2 (mainly) when Fe is added to the Pt/10Ba/Al catalyst, which is typical of a basicity decrease [19].



Figure 1: TPR profile of a) Pt/10Ba/Al, b) Pt/10BaFe/Al and c) Pt/10BaMn/A). (++) stabilized catalysts, (-) sulfated catalysts; (-) regenerated catalysts.

Catalyst	Pt/10Ba/Al	Pt/10BaFe/Al	Pt/10BaMn/Al	
Stabilized	31.2	35.8	39.5	
Sulfated	13.2	20.3	24.6	
(Deposited sulfur wt%)	(1.7%S)	(1.8%S)	(1.7%S)	
Regenerated at 550°C	29.7	28.0	33.8	
(S elimination rate)	(58%)	(80%)	(50%)	
NSC recovery (%)	95%	78%	86%	

Table 2: NOx storage capacity (NSC) measured at 100s at 300°C (μ mol.g⁻¹); impact of the sulfur poisoning

After the sulfating treatment, the NOx storage capacities strongly decrease (Table 2). For Pt/10Ba/AI, a loss of 48% is observed. Fe and Mn doped samples are more resistant toward the poisoning treatment, with a loss of only 30%. Thus, the obtained NOx storage capacities are significantly higher, between 20.3 and 24.6 μ mol.g⁻¹ versus 13.2 μ mol.g⁻¹ for Pt/10Ba/AI. The sulfated catalysts were characterized by H₂-TPR (Figure 1). As previously described [7], the TPR profile of the sulfated Pt/10Ba/AI catalyst exhibits two main peaks around 500 and 600°C. The first one is attributed to the simultaneous reduction of aluminum sulfates and some well dispersed barium sulfates located in platinum proximity. The second peak, around 600°C, is ascribed to the reduction of surface barium sulfates, and the observed shoulder near 750°C corresponds to bulk barium sulfate reduction.

Addition of Mn or Fe does not strongly modify the sulfates stabilities. The more interesting point is that Pt/10BaFe/AI exhibits a reduction ending below 700°C while 750°C is needed for the two other samples. This is attributed to a limitation of bulk barium sulfate formation in the Fe-doped catalyst, as previously mentioned [12-13]. Then, even if X-ray diffraction does not evidence the presence of Ba-Fe mixed-oxide species, interactions between these two compounds cannot be excluded. Assuming a H_2/SO_4^{2-} ratio of 4 for the sulfate reduction (X-SO₄ + 4H₂ \rightarrow X-S + 4H₂O and/or X-SO₄ + 4H₂ \rightarrow X-O + H₂S + 3H₂O), a total sulfur content of about 1.7 wt% was deduced from hydrogen consumption whatever the catalyst, after subtraction of the contribution of the Mn and Fe oxides reduction (Table 2).

The catalysts were also characterized by H₂-TPR after the sulfur regeneration treatment (Figure 1). For Pt/10Ba/AI, the H₂ consumption indicates that 58% of the deposited sulfur is removed, but a stabilization of the remaining sulfates is observed. Similar result is observed with Pt/10BaMn/AI, with 50% sulfur elimination and stabilization of the remaining sulfates. As expected, the sulfur removal is improved over Pt/10BaFe/AI since 80% of the initially deposited sulfur is eliminated after the regeneration procedure. This is in accordance with a weaker sulfate stability, with nearly no bulk sulfate formation.

Concerning the NOx storage capacities, 95% of the initial value is recovered over Pt/10Ba/AI (Table 2), indicating an efficient regeneration of the NOx storage sites. This rate decreases to 86% and to only 78% for Pt/10Ba/Mn/AI and Pt/10Fe/AI, respectively. Then, the Fe-doped catalyst exhibits the lower NOx storage capacity after regeneration (28.0 μ mol.g⁻¹, Table 2). In addition to a possible incomplete surface cleaning, the reducing treatment can induce some structural changes in the doped catalysts. Indeed, a slight deactivation of the Pt/10Ba/Mn/AI catalyst was also observed after the sulfur regeneration treatment without previous sulfating procedure. The H₂-TPR experiment (not shown) indicates a lower mean oxidation degree for Mn, even after re-oxidation at 550°C.

Consequently, high Mn oxidation state is needed to improve the NOx storage properties. For the iron modified catalyst, some Pt-Fe interaction can occur [20], and decrease the platinum activity.

NOx removal efficiency.

The NOx removal efficiencies measured under lean/rich cycling conditions are reported in Table 3. Typical recorded curves, obtained with Pt/10Ba/Al at 400°C, are presented in Figure 2. Whatever the catalyst and the test temperature, no significant amount of N₂O was measured. For all the catalysts, the NOx conversion as well as the H₂ consumption rate increase with temperature. With 3% H₂ in the rich mixture, the H₂ conversion is found to increase from 84-88% at 200°C to 98-100% at 400°C.

For Pt/10Ba/Al, the NOx conversion varies from 20% at 200°C to 46% at 400°C. The NH₃ selectivity remains around 20%, whatever the reaction temperature. Pt/10FeBa/Al exhibits a lower NOx removal efficiency, especially at 300 and 400°C with only 21% and 33%, respectively. Compared to Pt/10Ba/Al, the NOx conversion is not strongly affected by the Mn addition, even if slightly lower conversions are obtained at 300 and 400°C. The most interesting point is that the Mn adding results in a dramatically decrease in the NH₃ selectivity to only 3% at 400°C, while H₂ conversion is complete. In order to verify if the NOx removal efficiency can be improved with this catalyst, always keeping the ammonia selectivity a low value, additional tests were performed at 400°C by increasing the H₂ concentration in the rich pulse. Increasing the H₂ concentration up to 6% leads to an almost total NOx conversion, and N₂ selectivity still reaches 99% (Table 3). Note that the H₂ consumption is still 100%. Increasing the H₂ concentration up to 9% leads only to a slightly higher NH₃ selectivity (7%), and H₂ is no more totally converted.

These results clearly indicate that the NOx reduction to N₂ is strongly promoted at 400°C by Mn addition. A significant improvement of the NOx reduction by NH₃, produced in-situ in the course of the rich pulse, is suggested to be responsible of the high N₂ selectivity observed over the Mn-doped catalyst. Finally, 6% H₂ is the optimal concentration with our test conditions between the ammonia formation rate and the quantity of stored NOx. Indeed, a higher H₂ concentration induces a too high ammonia formation rate toward the stored NOx, a NH₃/NOx=1 ratio being optimal assuming $2NH_3+NO+NO_2 \rightarrow 2N_2+3H_2O$.



Figure 2: Typical storage-reduction experimental curves. Results obtained on Pt/10Ba/Al at 400°C with 3%H₂ in the rich pulse. a) NOx, NO₂ (chemiluminescence) and NH₃ concentrations (FTIR multigas analyzer), b) H₂ signal (mass spectrometer).

catalyst	Pt/10Ba/Al		Pt/10BaFe/Al			Pt/10BaMn/Al					
temperature test (°C)	200	300	400	200	300	400	200	300	400	400	400
H ₂ in the rich pulse (%)	3	3	3	3	3	3	3	3	3	6	9
NOx conversion (%)	20	39	46	17	21	33	20	34	41	97	97
N ₂ selectivity (%)	80	78	81	79	76	80	83	77	97	99	93
NH ₃ selectivity (%)	20	22	19	21	24	20	17	23	3	1	7
H ₂ consumption (%)	88	95	98	86	92	99	84	97	100	100	87

Table 3: NOx removal efficiency tests: NOx conversion, selectivity in N-compound and H_2 consumption.

Conclusion

Compared to Pt/10Ba/AI, Fe addition leads to a small increase in NOx storage capacity, and more interestingly to a better sulfur regeneration due to bulk barium sulfate formation inhibition. Unfortunately, the NOx storage property is not fully recovered after the sulfur regeneration. Moreover, Fe addition induces rather a degradation of the NOx removal efficiency under rich/lean cycling conditions, especially at high temperature. Mn addition also improves the NOx storage capacity, but no significant influence on the sulfur elimination

is observed. With $3\%H_2$ in the rich pulse, slightly lower NOx conversion is obtained at $400^{\circ}C$ with the Mn-doped catalyst, but, compared to Pt/10Ba/AI, the NH₃ selectivity is drastically decreased from 20% to 3%. The NOx conversion can be improved over the Mn-based catalyst, always keeping a low NH₃ selectivity, by increasing H₂ concentration in the rich pulse. 6% H₂ is determined as the optimal concentration under our test conditions between the ammonia formation rate and the amount of stored NOx.

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