



HAL
open science

Simultaneous estimation of complementary moment independent and reliability-oriented sensitivity measures

Pierre Derennes, Jérôme Morio, Florian Simatos

► To cite this version:

Pierre Derennes, Jérôme Morio, Florian Simatos. Simultaneous estimation of complementary moment independent and reliability-oriented sensitivity measures. *Mathematics and Computers in Simulation*, 2021, 182, pp.721-737. 10.1016/j.matcom.2020.11.024 . hal-03102618v2

HAL Id: hal-03102618

<https://hal.science/hal-03102618v2>

Submitted on 15 Apr 2021

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Open Archive Toulouse Archive Ouverte (OATAO)

OATAO is an open access repository that collects the work of some Toulouse researchers and makes it freely available over the web where possible.

This is an author's version published in: <https://oatao.univ-toulouse.fr/27122>

Official URL : <https://doi.org/10.1016/j.matcom.2020.11.024>

To cite this version :

Derennes, Pierre and Morio, Jérôme and Simatos, Florian Simultaneous estimation of complementary moment independent and reliability-oriented sensitivity measures. (2021) Mathematics and Computers in Simulation. 721-737. ISSN 0378-4754

Any correspondence concerning this service should be sent to the repository administrator:

tech-oatao@listes-diff.inp-toulouse.fr

Simultaneous estimation of complementary moment independent and reliability-oriented sensitivity measures

Pierre Derennes^{a,b}, Jérôme Morio^{b,*}, Florian Simatos^c

^a *Université de Toulouse, UPS IMT, F-31062 Toulouse Cedex 9, France*

^b *ONERA/DTIS, Université de Toulouse, F-31055 Toulouse, France*

^c *ISAE-SUPAERO and Université de Toulouse, Toulouse, France*

Abstract

In rare event analysis, the estimation of the failure probability is a crucial objective. However, focusing only on the occurrence of the failure event may be insufficient to entirely characterize the reliability of the considered system. This paper provides a common estimation scheme of two complementary moment independent sensitivity measures, allowing to improve the understanding of the system's rare event. Numerical applications are performed in order to show the effectiveness of the proposed estimation procedure.

Keywords: Sensitivity analysis; Moment independent importance measure; Reliability; Reliability-oriented sensitivity measures; Risk analysis

1. Introduction

In diverse disciplines, systems modeling is often achieved by considering a black-box model for which the observation is expressed as a deterministic function of external parameters representing some physical variables. These basic variables are usually assumed random in order to take phenomenological uncertainties into account. Then, sensitivity analysis (SA) techniques play a crucial role in the handling of these uncertainties and in the comprehension of the system behavior. These techniques aim at identifying and ranking inputs with respect to their impact on the output. In addition, SA methods present two main objectives: decrease the output uncertainty by reducing uncertainty of the most influential inputs, and simplify the model by omitting contribution of least ones. The influence criterion depends on the considered SA approach. There are various SA techniques in literature and essentially two families stand out: local and global sensitivity analysis (GSA) methods, see [4,5,23,38] and associated references for a review. Local methods aim at studying the behavior of the output locally around a nominal value of inputs. In contrast, global methods consider the whole variation range of inputs.

Sensitivity analysis may also be performed with a rare event perspective. Reliability-oriented sensitivity analysis (ROSA) differs from the classical one in the nature of the output quantity of interest under study. Indeed, sensitivity analysis focuses on the model output whereas ROSA is broadly concerned with a reliability measure, typically the

* Corresponding author.

E-mail addresses: pierre.derennes@onera.fr (P. Derennes), Jerome.Morio@onera.fr (J. Morio), florian.simatos@isae.fr (F. Simatos).

failure probability associated to an unsafe and undesired state of the system. Various ROSA methods have been proposed. First, several global sensitivity methods have been developed: for instance, a failure probability-based method [14], variance decomposition-based methods [31,36,40,41], a method based on density perturbation [26] or, more recently, a quantile-oriented sensitivity approach [8]. Local sensitivity method (often based on partial derivatives of the failure probability with respect to distribution parameters) are also available, see for instance [12] for a comprehensive review of these methods.

Recently, this scope has been expanded by [29] which proposes to classify ROSA methods in two different families:

- First, target (or regional) sensitivity analysis, which aims at studying the impact of inputs over a function of the output, typically the indicator function of a critical domain.
- Second, conditional sensitivity analysis, which aims at studying the impact of inputs exclusively within the critical domain, namely, conditionally to the failure event.

These two points of view can lead to widely different answers. To illustrate this aspect, consider for instance the following simple toy model:

$$Y = X_1 + \mathbb{1}_{X_1 > 3} |X_2| \quad (1)$$

where X_1 and X_2 are independent centered Gaussian random variables with respective variance 1 and 5. The random variables X_1 and X_2 are viewed as the system input and Y as the system output. Let us consider that for this system, $\{Y > 3\}$ is the failure event, and try to answer the following question: which out of X_1 and X_2 is more important from a rare event perspective? Actually, the answer depends on the viewpoint considered:

- if one is interested in the **impact of the input on the failure occurring or not**, then of course X_1 is highly influential and X_2 , that only kicks in Y upon failure, plays no role;
- if one is now interested in the most influential input **upon failure** occurring, then X_2 should intuitively be more important than X_1 because of its higher variance.

In this paper we propose two new target and conditional ROSA moment-independent indices $\bar{\eta}_i$ and δ_i^f in order to alleviate some of the limitations of classical variance-based indices [31]. These proposed indices and variance-based indices require exactly the same simulation budget: for both methods, the entire simulation budget is devoted to sampling from the input distribution conditional on failure for which a variety of standard methods can be used, for instance adaptive importance sampling, subset simulations or, if the code is too expensive, surrogate models. Once this sampling is done, the estimation of $\bar{\eta}_i$ and δ_i^f is post-processing of the sample without new calls to the model.

The rest of this paper is organized as follows: Section 2 aims at introducing two different ROSA indices, $\bar{\eta}_i$ and δ_i^f , which are intrinsically linked to GSA method of Borgonovo [3]. In Section 3 we present our simultaneous estimation scheme for $\bar{\eta}_i$ and δ_i^f measures and numerical applications are performed in Section 4 to assess its efficiency. Section 5 discusses how this scheme can be extended to a more general context. Our estimation scheme relies on the maximum entropy method which is recalled in the [Appendix](#).

2. Two complementary moment independent sensitivity measures

In this paper we focus on Borgonovo's indices originally proposed in [3], although our method can be generalized to more general indices as discussed in Section 5. Let in the sequel $Z | Z'$ denote a random variable with random distribution the distribution of Z conditioned on Z' and a deterministic scalar function $\mathcal{M} : \mathbb{R}^d \rightarrow \mathbb{R}$. To measure the sensitivity of the output $Y = \mathcal{M}(\mathbf{X})$ with respect to one of its input X_i , where $\mathbf{X} = (X_1, \dots, X_d)$, Borgonovo [3] proposed in the case where (X_i, Y) is absolutely continuous with respect to Lebesgue measure the index

$$\delta_i = \frac{1}{2} \mathbb{E} \left[\|f_Y - f_{Y|X_i}\|_{L^1(\mathbb{R})} \right], \quad (2)$$

i.e., half the average of the L^1 distance between the density of Y and the random density of Y conditioned on X_i . If X_i has a high influence on Y , the conditional density should be different from the non-conditioned one and δ_i should thus take large values. For further references and more details on δ -sensitivity measures the reader can consult [5].

In this paper we will adopt a more general definition of Borgonovo's index, which will make it possible to consider cases where (X_i, Y) is not absolutely continuous with respect to Lebesgue measure. The motivation stems from considering the influence of X_i not only on Y but also on possibly discrete functions of Y such as $\mathbb{1}_{Y>s}$, where s is a fixed critical value and where $\mathbb{1}_{Y>s} = 1$ if $Y > s$ and 0 otherwise. It captures the influence of X_i on the failure occurring or not.

For this generalization, we see Borgonovo's index as a measure of dependency between X_i and Y . Namely, let $d_{\text{TV}}(Z_1, Z_2)$ denote the total variation distance between the distributions of the random variables Z_1 and Z_2 . When Z_1 and Z_2 are absolutely continuous with respect to Lebesgue measure, we have $d_{\text{TV}}(Z_1, Z_2) = \frac{1}{2} \|f_{Z_1} - f_{Z_2}\|_{L^1(\mathbb{R})}$ and so we adopt the following generalization of Borgonovo's index:

$$\delta_i = \mathbb{E}[d_{\text{TV}}(Y, Y | X_i)] = d_{\text{TV}}((X_i, Y), (X_i, Y')) \quad (3)$$

such that Y' and Y are independent and identically distributed random variables. The second equality holds when (X_i, Y) is absolutely continuous with respect to some product measure $\lambda(dx) \otimes \mu(dy)$ (typically, (X_i, Y) is absolutely continuous with respect to Lebesgue measure, or X_i is and Y is a discrete random variable).

In a rare event context, we are interested in the impact of X_i not only on Y but also on the occurrence of some rare event which we write $\{Y > s\}$. This means that we are interested in the influence of X_i on the random variable $\mathbb{1}_{Y>s}$: the corresponding generalized Borgonovo's index is therefore given by

$$\eta_i = \mathbb{E}[d_{\text{TV}}(\mathbb{1}_{Y>s}, \mathbb{1}_{Y>s} | X_i)] = \mathbb{E}[|\mathbb{P}(Y > s) - \mathbb{P}(Y > s | X_i)|] \quad (4)$$

which is actually twice the index proposed in Cui et al. [14]. One of the drawbacks of this index is that it is unnormalized as it is upper bounded by twice the rare event probability $2\mathbb{P}(Y > s)$. To obtain a $[0, 1]$ -valued index, we use the relation

$$\eta_i = 2\mathbb{P}(Y > s) \times d_{\text{TV}}(X_i, X_i | Y > s) \quad (5)$$

observed in [35] and that can be derived using Bayes' Theorem, to propose the $[0, 1]$ -valued index

$$\bar{\eta}_i = d_{\text{TV}}(X_i, X_i | Y > s) = \frac{1}{2} \|f_{X_i} - f_{X_i|Y>s}\|_{L^1(\mathbb{R})}. \quad (6)$$

Complementary to this approach, we may also be interested in the influence of X_i upon failure, which corresponds to considering δ_i but when all the random variables involved are conditioned upon the failure $Y > s$. Thus, this conditional index, denoted by δ_i^f , is given by

$$\delta_i^f = \mathbb{E}[d_{\text{TV}}(Y | Y > s, Y | \{Y > s, X_i\})]. \quad (7)$$

When (X_i, Y) is absolutely continuous, this is a particular case of (3) and so if we denote by (\tilde{X}_i, \tilde{Y}) a random variable distributed as (X_i, Y) conditioned on $Y > s$, then we have in this case

$$\delta_i^f = \frac{1}{2} \|f_{\tilde{X}_i, \tilde{Y}} - f_{\tilde{X}_i} f_{\tilde{Y}}\|_{L^1(\mathbb{R}^2)}. \quad (8)$$

Instead of focusing on Y , the indices η_i and $\bar{\eta}_i$ target a different output, namely $\mathbb{1}_{Y>s}$ and will thus be referred as target indices. Similarly, instead of working in the normal mode, the indices δ_i^f are concerned with the system conditioned upon failure and will thus be referred to as conditional indices. See Section 5 for more on this terminology.

For the toy model (1), we have $Y > s$ if and only if $X_1 > s$: this directly implies $\mathbb{P}(Y > s | X_1) = \mathbb{1}_{X_1>s}$ and $\mathbb{P}(Y > s | X_2) = \mathbb{P}(Y > s)$ and then

$$\bar{\eta}_1 = 1 - \mathbb{P}(X_1 > s) \approx 0.9987 \quad \text{and} \quad \bar{\eta}_2 = 0. \quad (9)$$

This confirms the intuition that, as far as we are concerned with the failure occurring or not, X_1 is highly influential and X_2 , not at all. However, in this simple Gaussian case we can directly compute the δ_i^f 's through numerical integration, which gives

$$\delta_1^f \approx 0.0781 \quad \text{and} \quad \delta_2^f \approx 0.7686. \quad (10)$$

Thus upon failure, X_2 has become much more influential than X_1 . This simple toy example illustrates the complementarity of the indices $\bar{\eta}_i$ and δ_i^f from a rare event perspective, and our goal in this paper is to show how

they can be simultaneously and accurately estimated with only one run of sequential Monte Carlo or importance sampling, regularly considered in the context of rare event probability estimation $\mathbb{P}(Y > s)$. In other words, we show that upon estimating this probability, one also gets “for free”, that is without additional calls to the function \mathcal{M} , an estimation of $\bar{\eta}_i$ and δ_i^f .

3. Simultaneous estimation of δ_i^f and $\bar{\eta}_i$

We consider throughout this article a general computer code $Y = \mathcal{M}(\mathbf{X})$ where the scalar output Y depends on a d -dimensional real valued random vector $\mathbf{X} = (X_1, \dots, X_d)$ of \mathbb{R}^d through a deterministic scalar function $\mathcal{M} : \mathbb{R}^d \rightarrow \mathbb{R}$ called “black box”. Without loss of generality, it is assumed that the failure event corresponds to the exceeding of a critical threshold s by the output Y , i.e., is of the form $\{Y > s\}$.

We further assume that for every i , (X_i, Y) is absolutely continuous with respect to Lebesgue measure with density $f_{X_i, Y}$ and marginals f_{X_i} and f_Y . As above, we denote by $\tilde{\mathbf{X}} = (\tilde{X}_1, \dots, \tilde{X}_d)$ a random variable distributed as \mathbf{X} conditioned on $Y > s$ and define $\tilde{Y} = \mathcal{M}(\tilde{\mathbf{X}})$. Thus, (\tilde{X}_i, \tilde{Y}) is also absolutely continuous with respect to Lebesgue measure with density $f_{\tilde{X}_i, \tilde{Y}}$ with marginals $f_{\tilde{X}_i}$ and $f_{\tilde{Y}}$. Our simultaneous estimation scheme is obtained by combining state-of-the-art estimation techniques which we recall next.

The approach proposed in this paper to provide an estimation of $\bar{\eta}_i$ and δ_i^f is based on three stages:

1. we apply a rare event simulation technique (Monte Carlo method, importance sampling, sequential Monte Carlo, etc.) to estimate the failure probability $\mathbb{P}(Y > s)$. It can be combined with the building of a surrogate model.
2. we get a failure conditioned sample $\tilde{\mathbf{X}}$ (see Section 3.2).
3. we estimate the two proposed ROSA indices δ_i^f and $\bar{\eta}_i$ from $\tilde{\mathbf{X}}$ (see Section 3.3).

The simulation budget required to perform these three steps is fully concentrated on the first and second stages.

3.1. Estimation of δ_i

We review in this section some general aspects of moment-independent sensitivity indices estimation. Initial estimations of δ -sensitivity measures relied on their original definition in terms of total variation distance between conditional and unconditional distributions. Involving L^1 norms of differences of conditional and unconditional output probability density functions, this approach typically necessitates expensive double-loop estimation procedures with a prohibitive cost [3,28,32]. Alternative approaches were proposed in [42,43], but these two methods rest on strong technical assumptions such as independence between input or approximation of the black box \mathcal{M} within the cut-HDMR (high-dimensional model representation) framework. An apparently efficient single-loop method was proposed in [39], but simulation results provided in [19] questioned its consistency. The interested reader is for instance referred to the introduction of [18] for a more detailed discussion on these estimation issues.

In the present paper, the estimation of δ_i is performed by using the method described in [18]: it does not rely on any assumption on the model and works in particular for dependent input. It rests on the copula-representation of δ_i noted in [37], namely

$$\delta_i = \frac{1}{2} \int_{0 \leq u, v \leq 1} |c_i(u, v) - 1| \, du \, dv, \quad (11)$$

where c_i is the density copula of (X_i, Y) , i.e., the density of $(F_{X_i}(X_i), F_Y(Y))$. Based on this representation, the approximation proposed in [18] uses a maximum entropy estimation \hat{c}_i of c_i imposing estimated fractional moments as constraints, and then a Monte Carlo estimation $\frac{1}{2N'} \sum_{k=1}^{N'} |\hat{c}_i(U_1^k, U_2^k) - 1|$ of the integral with the (U_1^k, U_2^k) being i.i.d. random variables uniformly distributed on $[0, 1]^2$.

At this point we stress an important point: all these estimation techniques assume that one can sample from the input distribution \mathbf{X} . As explained in the introduction however, estimating δ_i^f amounts to applying these techniques when the input distribution is that of \mathbf{X} conditioned on failure, which is in general unknown. Thus, before applying these methods one needs to be able to sample from $\tilde{\mathbf{X}}$.

3.2. Generating conditioned samples $\tilde{\mathbf{X}}$

3.2.1. General aspects

The most naive method for generating failure samples is the rejection method. For a given sample $(\mathbf{X}^1, \dots, \mathbf{X}^N)$ i.i.d. with common distribution $f_{\mathbf{X}}$, a subsample is obtained by recording samples which satisfy $\mathcal{M}(\mathbf{X}^k) > s$. However, this approach leads to a huge computational cost when the failure probability is low.

When some information is known on the failure event, this cost can be reduced by leveraging “good” auxiliary distributions in importance sampling techniques [10]. In reliability, a method widely used for designing auxiliary distributions is shifting the input distribution to a design point, which may be determined thanks to FORM/SORM methods [30]. Importance sampling is then combined with Monte Carlo Markov Chain to generate samples distributed as $\tilde{\mathbf{X}}$ [1].

Another efficient method to generate conditioned samples $\tilde{\mathbf{X}}$ is the adaptive Sequential Monte Carlo (SMC) procedure proposed and studied in [11] that we present in the next section. Several variants have been proposed in different scientific communities. It was adapted in [2] (called subset simulation) for rare event assessment purpose and studied theoretically from the Markov processes point of view in [11].

As a final remark, one can mention that importance sampling-based methods and subset simulation may be combined with a surrogate model such as Kriging as it is a powerful tool in the context of costly-to-evaluate computer models. For instance, we can mention the method AK-MCS (Active learning reliability method with Kriging and Monte Carlo Simulation) [20] which couples Kriging and Monte Carlo method, AK-IS (Active learning reliability method with Kriging and Importance Sampling) [21] which combines Kriging and importance sampling or AK-SS (Active learning reliability method with Kriging and Subset Simulation) [22] which associates Kriging and Subset Simulation. However, the counterpart (for the purpose of the present paper) remains the difficulty to catch and measure the impact of the modeling errors induced by the surrogate model itself.

We favor in this article the use of the SMC procedure. It is described in the next section and applied to all the numerical test-cases of this article. Nevertheless, any of the above mentioned techniques could be applied to generate samples with the same distribution as $\tilde{\mathbf{X}}$. For that purpose, we have also performed this generation with AK-IS [21] for one example of Section 4 to show that coupled with a surrogate model, it is possible to sample from $\tilde{\mathbf{X}}$ with a low simulation cost.

3.2.2. Sequential Monte Carlo

In what follows, by duplicating a finite set $\{x_k\}$ into N , we mean drawing N times independently and uniformly from $\{x_k\}$. The algorithm parameters are N_x , ρ , A_x and T , corresponding respectively to the number of particles, the threshold for the quantile, the number of steps of the Metropolis–Hastings sampler, and the exploration (or proposal) kernel in this sampler.

Initialization: set $p = 0$, generate $(\mathbf{X}_p^1, \dots, \mathbf{X}_p^{N_x})$ i.i.d. according to $f_{\mathbf{X}}$ and compute $Y_p^k = \mathcal{M}(\mathbf{X}_p^k)$ for $k = 1, \dots, N_x$;

Selection: let γ_p be the ρ -quantile of the Y_p^k : if $\gamma_p > s$, then stop, otherwise duplicate the ρN_x particles with $Y^k > \gamma_p$ into N_x particles.

Mutation: apply A_x times the Metropolis–Hastings algorithm with exploration kernel T and target distribution $\mathbf{X} \mid \mathcal{M}(\mathbf{X}) > \gamma_p$ to each of the N_x particles, denote by $(\mathbf{X}_{p+1}^1, \dots, \mathbf{X}_{p+1}^{N_x})$ the newly obtained particles with corresponding $Y_{p+1}^k = \mathcal{M}(\mathbf{X}_{p+1}^k)$, increment p and go back to the selection step.

The black box is called for every particle at every step of the Metropolis–Hastings sampler in order to compute the acceptance probability, so that if m denotes the (random) number of steps of this algorithm, then the number of calls to the black box \mathcal{M} is equal to $N_x(1 + mA_x)$.

As noted in [11], at the end of this algorithm the $(\mathbf{X}_m^1, \dots, \mathbf{X}_m^{N_x})$ are approximately distributed according to $\mathbf{X} \mid Y > \gamma_m$ but are not independent. To improve independence and tune the final size of the sample, an additional step is considered. There are thus two additional parameters, the size N of the sample and the number of steps A of the Metropolis–Hastings sampler in this additional step.

Sampling: duplicate the N_x particles $(\mathbf{X}_m^1, \dots, \mathbf{X}_m^{N_x})$ into N particles, and apply A times to each particle the Metropolis–Hastings algorithm with exploration kernel T and target distribution $\mathbf{X} \mid \mathcal{M}(\mathbf{X}) > s$.

This adds $N \times A$ calls to the black box, and the output of this algorithm is a sample $(\tilde{\mathbf{X}}^1, \dots, \tilde{\mathbf{X}}^N)$ which is approximately i.i.d. according to $\tilde{\mathbf{X}} = \mathbf{X} \mid \mathcal{M}(\mathbf{X}) > s$ together with the corresponding values $\tilde{Y}^k = \mathcal{M}(\tilde{\mathbf{X}}^k)$.

3.3. Simultaneous estimation of δ_i^f and $\bar{\eta}_i$

We now explain how to combine the method for estimating δ_i with the adaptive SMC sampler described above to have a simultaneous estimation of δ_i^f and $\bar{\eta}_i$.

Step 1 — Input realizations generation. Using the adaptive SMC procedure of Section 3.2, obtain $(\tilde{\mathbf{X}}^1, \dots, \tilde{\mathbf{X}}^N)$ approximately i.i.d. from $f_{\tilde{\mathbf{X}}}$ and their corresponding value $\tilde{Y}^k = \mathcal{M}(\tilde{\mathbf{X}}^k)$ by \mathcal{M} .

Step 2 — Density estimation. Use the sample $((\tilde{X}_i^k, \tilde{Y}^k), k = 1, \dots, N)$ to obtain estimates $\hat{f}_{\tilde{X}_i}$ and \hat{c}_i of the density $f_{\tilde{X}_i}$ of \tilde{X}_i and of the copula c_i of (\tilde{X}_i, \tilde{Y}) , respectively. In this article, they are both estimated with the maximum entropy method with estimated fractional moments (see Appendix) but any other efficient density and copula estimation technique can be chosen.

Step 3 — Indices estimation. Use the estimates $\hat{f}_{\tilde{X}_i}$ and \hat{c}_i to obtain estimates of $\bar{\eta}_i$ and δ_i^f as follows:

- for $\bar{\eta}_i$, estimate the one-dimensional integral $\|f_{X_i} - \hat{f}_{\tilde{X}_i}\|_{L^1(\mathbb{R})}$ either by direct numerical approximation, or if f_{X_i} can be sampled from, by Monte Carlo method via

$$\hat{\bar{\eta}}_i = \frac{1}{N'} \sum_{k=1}^{N'} \left| \frac{\hat{f}_{\tilde{X}_i}(X_i^k)}{f_{X_i}(X_i^k)} - 1 \right| \quad (12)$$

where the X_i^k are i.i.d. with common distribution X_i ;

- for δ_i^f , generate $((U_1^k, U_2^k), k = 1, \dots, N')$ i.i.d. uniformly distributed on $[0, 1]^2$ and estimate δ_i^f by

$$\hat{\delta}_i^f = \frac{1}{2N'} \sum_{k=1}^{N'} |\hat{c}_i(U_1^k, U_2^k) - 1|. \quad (13)$$

It has to be pointed out that the proposed procedure can be applied to output models with correlated inputs even if the interpretation of the results could remain difficult. A potential perspective is to combine this proposed work with Shapley effect estimation of Borgonovo's indices [33] as Shapley effects are easier to interpret.

As promised, the proposed algorithm also provides simultaneous estimation of both δ_i^f and $\bar{\eta}_i$ from one common SMC procedure: indeed, after the first step no more call to the black box \mathcal{M} is needed. In particular, the (random) number of calls to the black box is $N_x + mA_x N_x + AN$ as explained in Section 3.2 ($N_x + mA_x N_x$ calls for the failure probability estimation and AN calls for sensitivity analysis). If this number of calls is too expensive for a given application, all these procedures can be combined with active learning of a surrogate model for probability estimation such as in [21,22]. In that case, the AN calls to the black box for sensitivity analysis become AN calls to the surrogate model.

4. Numerical applications

In this section, the proposed estimation scheme is applied to four output models. Firstly, we consider two analytical cases for which the unconditional and conditional output distributions are known so that theoretical values of the importance measures δ_i^f and $\bar{\eta}_i$ are available by using numerical integration. We then consider a single degree of freedom oscillator with $d = 6$ independent and lognormally distributed inputs. Finally, as a last test case, we study a launcher stage fallout model which takes $d = 6$ input parameters into account.

For each example, computation time and number of model calls are given to assess the efficiency of the proposed method. Results are obtained with a computer equipped with a 3.5 GHz Intel Xeon 4 CPU. The number of samples N' for the Monte Carlo integration (13) can be taken as large as possible as this stage does not require any calls to \mathcal{M} . In the following simulations, we set $N' = 10^7$. This number may be tuned more adaptively by computing the variance of the Monte Carlo estimates.

When the input $\mathbf{X} \sim N(\mathbf{v}, \Sigma)$ is normally distributed, mutation steps in the adaptive SMC algorithm are performed by using the natural exploration kernel so-called Crank–Nicholson shaker and defined by

$$T(\mathbf{x}, \cdot) \sim \mathbf{L} \left(\sqrt{1-a} \times \mathbf{L}^{-1}(\mathbf{x} - \mathbf{v}) + \sqrt{a}Z \right) + \mathbf{v}, \quad (14)$$

where $a \in (0, 1)$ is a parameter of the kernel, $Z \sim N(0, I_d)$ and \mathbf{L} is the lower triangular matrix in the Cholesky decomposition of Σ , i.e., $\Sigma = \mathbf{L}\mathbf{L}^T$.

Standard deviations (Sd) of estimators are computed by performing 100 runs of the proposed scheme in order to study its variability. When a theoretical value θ is available, the accuracy of an estimator $\hat{\theta}$ is measured by the mean of the relative difference (RD) $\frac{\theta - \hat{\theta}}{\theta}$.

4.1. Comparison with ROSA Sobol indices

It consists in analyzing the influence of the inputs X_i on the variance of $\mathbb{1}_{Y>s}$ [27]. First-order Sobol indices on this indicator function can thus be defined in the following way:

$$S_i^{\mathbb{1}_{Y>s}} = \frac{\mathbb{V}[\mathbb{E}[\mathbb{1}_{Y>s}(\mathbf{X})|X_i]]}{\mathbb{V}[\mathbb{1}_{Y>s}(\mathbf{X})]}, \quad (15)$$

where \mathbb{V} is the variance and $S_i^{\mathbb{1}_{Y>s}}$ is the first-order Sobol index associated to the variable X_i . Advanced sampling-based estimation schemes for these first-order Sobol indices have been investigated in [36] but still require a lot of simulations to achieve convergence. Another efficient estimation procedure using SMC has been proposed recently by [31] as the first-order $S_i^{\mathbb{1}_{Y>s}}$ can be rewritten as follows:

$$S_i^{\mathbb{1}_{Y>s}} = \frac{\mathbb{P}(Y > s)}{1 - \mathbb{P}(Y > s)} \mathbb{V} \left[\frac{f_{\tilde{X}_i}(X_i)}{f_{X_i}(X_i)} \right]. \quad (16)$$

SMC enables to generate a set of samples $(\tilde{\mathbf{X}}^1, \dots, \tilde{\mathbf{X}}^N)$ approximately i.i.d. from $f_{\tilde{\mathbf{X}}}$ from which it is possible to estimate a density $\hat{f}_{\tilde{X}_i}$ and finally, the Sobol indices are computed with the empirical variance. The following steps describe the complete procedure.

Step 1 — Input realizations generation. Using the adaptive SMC procedure of Section 3.2, obtain $(\tilde{\mathbf{X}}^1, \dots, \tilde{\mathbf{X}}^N)$ approximately i.i.d. from $f_{\tilde{\mathbf{X}}}$ and estimate $\mathbb{P}(Y > s)$ with \hat{P}_f .

Step 2 — Density estimation. Use the sample $(\tilde{X}_i^k, k = 1, \dots, N)$ to obtain an estimate $\hat{f}_{\tilde{X}_i}$ of the density $f_{\tilde{X}_i}$ of \tilde{X}_i ; In this article, this density is estimated with the maximum entropy method with estimated fractional moments (see Appendix) but any other efficient density estimation technique can be chosen;

Step 3 — Indice estimation. Estimate the first-order Sobol indices $S_i^{\mathbb{1}_{Y>s}}$ from $\hat{f}_{\tilde{X}_i}$ and \hat{P}_f as follows:

$$\hat{S}_i^{\mathbb{1}_{Y>s}} = \left(\frac{\hat{P}_f}{1 - \hat{P}_f} \right) \left(\frac{1}{N'} \sum_{k=1}^{N'} \left(\frac{\hat{f}_{\tilde{X}_i}(X_i^k)}{f_{X_i}(X_i^k)} \right)^2 - \left(\frac{1}{N'} \sum_{k=1}^{N'} \frac{\hat{f}_{\tilde{X}_i}(X_i^k)}{f_{X_i}(X_i^k)} \right)^2 \right) \quad (17)$$

where the X_i^k are i.i.d. with common distribution X_i .

Sobol indices take values between 0 and 1. Higher order Sobol indices can also be defined but are more complicated to estimate as they require the estimation of multivariate densities. For the same reason, total Sobol indices are also difficult to estimate as they imply the estimation of $(d - 1)$ -dimensional densities. The sum of all Sobol indices at all order is equal to 1.

There are mainly three limits to this approach: the inputs have to be independent for a correct interpretation of the results and the variance should be a valuable indicator of the output variability which is not always the case in practice [3,6,15]. Moreover, there is good chance for all individual Sobol indices $S_i^{\mathbb{1}_{Y>s}}$ to tend to zero when the failure probability is too low. Perrin and Defaux [31] underlined this limit for the use of Sobol indices in a sensitivity analysis context. The proposed indices δ_i^f and $\tilde{\eta}_i$ do not suffer from ROSA Sobol limitations as the input random variables could be dependent even if the interpretation of the indices may remain complicated. The

Table 1

Estimates of δ_i^f , $\bar{\eta}_i$ and $S_i^{\mathbb{1}_{Y>s}}$ of example 1. 34,640 calls to the function \mathcal{M} . Failure probability estimated to 1.35×10^{-3} with 17% coefficient of variation. Set of parameters for the adaptive SMC algorithm: $N_x = 500$, $A_x = 3$, $\rho = 0.3935$, $a = 0.5$, $A = 5$ and $N = 3000$.

Input	Theoretical value δ_i^f (rank)	Estimation $\hat{\delta}_i^f$		
		Mean (rank)	Sd	RD
X_1	0.0781 (2)	0.0930 (2)	0.0101	-0.1908
X_2	0.7686 (1)	0.7200 (1)	0.0077	0.0632
Input	Theoretical value $\bar{\eta}_i$ (rank)	Estimation $\hat{\bar{\eta}}_i$		
		Mean (rank)	Sd	RD
X_1	0.9987 (1)	0.9997 (1)	0.0095	-0.001
X_2	0 (2)	0.0315 (2)	0.0103	-
Input	Theoretical value $S_i^{\mathbb{1}_{Y>s}}$ (rank)	Estimation $\hat{S}_i^{\mathbb{1}_{Y>s}}$		
		Mean (rank)	Sd	RD
X_1	1 (1)	1.0225 (1)	0.0672	-0.0225
X_2	0 (2)	1.26×10^{-5} (2) (2)	5.53×10^{-6} (2)	-

indices δ_i^f and $\bar{\eta}_i$ are also moment independent indices and thus do not rely on output variance. Furthermore, the proposed indices are not impacted by a too significant rarity of the failure event.

The estimation of $S_i^{\mathbb{1}_{Y>s}}$, δ_i^f and $\bar{\eta}_i$ is based on the same sample $(\tilde{\mathbf{X}}^1, \dots, \tilde{\mathbf{X}}^N)$ and thus the computational cost for the estimation of these ROSA indices is similar.

4.2. Example 1: back to the toy model of the introduction

We go back to the toy model (1) of the introduction, i.e., $Y = X_1 + \mathbb{1}_{X_1>s}|X_2|$ where $s = 3$, X_1 and X_2 are independent, $X_1 \sim N(0, 1)$ and $X_2 \sim N(0, 5)$. We compare in Table 1 theoretical values with estimates obtained with the proposed method. The failure probability can also be evaluated with SMC to 1.35×10^{-3} with 17% coefficient of variation. In average, runs last 317 s and make 34,640 calls to the black box (19,460 calls for the failure probability estimation, 15,000 calls for sampling with $\tilde{\mathbf{X}}$ and 0 call for the ROSA index estimation). From the different relative differences, one can see that δ_i^f and $\bar{\eta}_i$ estimates are close to their respective reference values and present reasonable variability with regard to the budget allocated to the estimation. Sobol indices $S_i^{\mathbb{1}_{Y>s}}$ and target sensitivity index $\bar{\eta}_i$ gives very similar results and share thus the same ROSA interpretation.

4.3. Example 2: an analytical test case

Let us consider the following output model:

$$Y = X_1 + X_2^2 \quad (18)$$

where X_1 and X_2 are i.i.d. standard Gaussian random variables and the failure event is $\{Y > 15\}$. This model is in the same vein as the previous toy model but slightly more realistic. Unconditional and conditional output distributions are known: $Y | X_1$ follows a χ^2 -distribution shifted by X_1 and $Y | X_2$ is normally distributed with unit variance and mean X_2 . We thus have the following expressions for the densities:

$$f_Y(y) = \int_0^\infty \frac{e^{-\frac{(y-t)^2}{2}} - \frac{t}{2}}{2\pi\sqrt{t}} dt \quad (19)$$

and

$$f_{Y|X_1}(y) = \frac{e^{-\frac{(y-X_1)}{2}}}{\sqrt{2\pi(y-X_1)}} \mathbb{1}_{y \geq X_1} \quad \text{and} \quad f_{Y|X_2}(y) = \frac{e^{-\frac{(y-X_2)^2}{2}}}{\sqrt{2\pi}} \quad (20)$$

Table 2

Estimates of δ_i^f , $\bar{\eta}_i$ and $S_i^{\mathbb{1}_{Y>s}}$ of example 2. 25,200 calls to the function \mathcal{M} . Failure probability estimated to 1.24×10^{-4} with 18% coefficient of variation. Set of parameters for the adaptive SMC algorithm: $N_x = 300$, $A_x = 3$, $\rho = 0.5507$, $a = 0.5$, $A = 3$ and $N = 5000$.

Input	Theoretical value δ_i (rank)	Theoretical value δ_i^f (rank)	Estimation $\hat{\delta}_i^f$		
			Mean (rank)	Sd	RD
X_1	0.4930 (1)	0.001 (2)	0.0721 (2)	0.0266	-71.1
X_2	0.3049 (2)	0.4136 (1)	0.3998 (1)	0.0343	0.0334
Input	\	Theoretical value $\bar{\eta}_i$ (rank)	Estimation $\hat{\bar{\eta}}_i$		
			Mean (rank)	Sd	RD
X_1	\	0.2093 (2)	0.2066 (1)	0.0605	0.0129
X_2	\	0.9969 (1)	0.9723 (2)	0.0567	0.0247
Input	\	Theoretical value $S_i^{\mathbb{1}_{Y>s}}$ (rank)	Estimation $\hat{S}_i^{\mathbb{1}_{Y>s}}$		
			Mean (rank)	Sd	RD
X_1	\	4.05×10^{-5} (2)	5.50×10^{-5} (2)	3.35×10^{-5}	-0.3481
X_2	\	0.7074 (1)	0.7814 (2)	0.1012	-0.1046

for the conditional densities. Thus, theoretical values of sensitivity measures (δ_1, δ_2) , (δ_1^f, δ_2^f) , $(\bar{\eta}_1, \bar{\eta}_2)$ and $(S_1^{\mathbb{1}_{Y>s}}, S_2^{\mathbb{1}_{Y>s}})$ are available via numerical integration. We gathered in [Table 2](#) the estimates of δ_i^f and $\bar{\eta}_i$ obtained from SMC. The failure probability can also be evaluated with SMC to 1.24×10^{-4} with 18% coefficient of variation. In average, runs need 350 s to compute all the δ and η -indices and make 25,200 calls to the black box (10,200 calls for the failure probability estimation, 15,000 calls for sampling with $\tilde{\mathbf{X}}$ and 0 call for the ROSA index estimation).

One can see that estimates $\{\hat{\delta}_i^f\}$ respect the good importance ranking, namely $X_2 > X_1$. However, the estimation of δ_1^f exhibits an important difference between average values and reference ones. This difference is due to the fact that the samples $\{\mathbf{X}^k\}$ obtained with the SMC procedure are not completely independent and distributed from $f_{\tilde{\mathbf{X}}}$ since only $A = 3$ steps of the Metropolis–Hastings sampler are performed in the final sampling step. Indeed, increasing A from 3 to 30 leads to average values of $\hat{\delta}_1^f$ of 0.0206 with a standard deviation of 0.0091.

In this example, the indices $\{\delta_i^f\}$ enable to detect a drastic change in the importance ranking. Indeed, the contribution of the first input X_1 becomes negligible at the failure of the system whereas it is the most influential under nominal operation. The indices $\{\bar{\eta}_i\}$ and Sobol indices $\hat{S}_i^{\mathbb{1}_{Y>s}}$ lead to the same conclusion, namely that the influence of the input X_2 at the failure predominates with $\bar{\eta}_2$ close to 1.

4.4. Example 3: a single degree of freedom (SDOF) oscillator

In this subsection, a non linear SDOF oscillator [9] made of a mass m and two springs with free length r and respective stiffness c_1 and c_2 is considered. It is subjected to a rectangular load pulse with random duration t and amplitude F . The model output is defined as

$$Y = -3r + \left| \frac{2F}{c_1 + c_2} \sin \left(\sqrt{\frac{c_1 + c_2}{m}} \frac{t}{2} \right) \right|, \quad (21)$$

i.e., the difference between the maximum displacement response of the system and $3r$. The six input variables c_1 , c_2 , r , m , t and F are assumed to be independent and lognormally distributed with respective parameters given in [Table 3](#). The failure of the system is achieved when the output Y exceeds the threshold 0.

We gathered in [Table 4](#) the estimates of δ_i^f and $\bar{\eta}_i$ obtained from SMC. The associated failure probability is estimated to 8.54×10^{-5} with 91% coefficient of variation. The δ_i 's are obtained with the method described in [18]. In average, runs last 960 s and make 51,725 calls to the black box (21,725 calls for the failure probability estimation, 30,000 calls for sampling with $\tilde{\mathbf{X}}$ and 0 call for the ROSA index estimation). It appears that the global importance ranking $X_4 < X_2 < X_5 < X_1 < X_6 < X_3$ drastically differs from the importance ranking provided by the conditional sensitivity indices δ_i^f . Especially, the most influential input $X_3 = r$ becomes negligible conditionally on the failure event. Changes are more nuanced as far as target indices are concerned. Indeed, target sensitivity indices $\bar{\eta}_i$ give approximately the same ranking, except that X_1 and X_2 predominate. The Sobol indices $\hat{S}_i^{\mathbb{1}_{Y>s}}$ are very low

Table 3

Distribution parameters (the mean and the standard deviation of the associated normal distribution) of input variables of the SDOF oscillator.

Input	Mean	Sd
c_1	2	0.2
c_2	0.2	0.02
r	0.6	0.05
m	1	0.05
t	1	0.2
F	1	0.2

Table 4

Estimates of δ_i^f , $\bar{\eta}_i$ and $S_i^{\mathbb{1}_{Y>S}}$ for the SDOF oscillator. 51,725 calls to the function \mathcal{M} . Failure probability estimated to 8.54×10^{-5} with 91% coefficient of variation. Set of parameters for the adaptive SMC algorithm: $N_x = 500$, $A_x = 3$, $\rho = 0.4866$, $A = 10$ and $N = 3000$.

Input	Estimation $\hat{\delta}_i$		Estimation $\hat{\delta}_i^f$		Estimation $\hat{\bar{\eta}}_i$		Estimation $\hat{S}_i^{\mathbb{1}_{Y>S}}$	
	Mean (rank)	Sd	Mean (rank)	Sd	Mean (rank)	Sd	Mean (rank)	Sd
$X_1 = c_1$	0.0769 (3)	0.0066	0.0995 (1)	0.0210	0.8332 (2)	0.0653	0.0062 (2)	0.0062
$X_2 = c_2$	0.0231 (5)	0.0050	0.0322 (6)	0.0090	0.1352 (5)	0.0340	0 (5)	0
$X_3 = r$	0.4441 (1)	0.0063	0.0329 (5)	0.0117	0.6494 (3)	0.0690	0.0017 (3)	0.0014
$X_4 = m$	0.0219 (6)	0.0051	0.0343 (4)	0.0101	0.1306 (6)	0.0874	0 (6)	0
$X_5 = t$	0.0751 (4)	0.0075	0.0474 (3)	0.0150	0.3312 (4)	0.0710	0.0001 (4)	0
$X_6 = F$	0.1554 (2)	0.0074	0.0871 (2)	0.0191	0.9078 (1)	0.0317	0.0142 (1)	0.0431

Table 5

Estimates of δ_i^f , $\bar{\eta}_i$ and $S_i^{\mathbb{1}_{Y>S}}$ for the SDOF oscillator with a higher budget allocated to the adaptive SMC algorithm. 262,500 calls to the function \mathcal{M} . Failure probability estimated to 9.11×10^{-5} with 27% coefficient of variation. Set of parameters for the adaptive SMC algorithm: $N_x = 500$, $A_x = 10$ (instead of 3), $\rho = 0.1813$, $A = 10$ and $N = 3000$.

Input	Estimation $\hat{\delta}_i^f$		Estimation $\hat{\bar{\eta}}_i$		Estimation $\hat{S}_i^{\mathbb{1}_{Y>S}}$	
	Mean (rank)	Sd	Mean (rank)	Sd	Mean (rank)	Sd
c_1	0.0674 (2)	0.0150	0.7949 (2)	0.0325	0.0037 (2)	0.0017
c_2	0.0275 (5)	0.0064	0.1131 (5)	0.0173	0 (5)	0
r	0.0346 (4)	0.0089	0.5651 (3)	0.0375	0.0008 (3)	0.007
m	0.0267 (6)	0.0056	0.0459 (6)	0.0196	0 (6)	0
t	0.0366 (3)	0.0074	0.2812 (4)	0.0200	0.0001 (4)	0.0001
F	0.1147 (1)	0.0164	0.9205 (1)	0.0149	0.0315 (1)	0.0270

for all the inputs even if they give the same ranking as $\bar{\eta}_i$. It is due to the fact that the failure probability is too low as underlined in [31] and thus limits the use of ROSA Sobol indices in a sensitivity analysis context.

As in the previous example, variability of obtained estimates is non negligible. Here, inputs are lognormally distributed and there is no natural exploration kernel like in the Gaussian case. We can find in [13] a discussion about implementation issues for the choice of the exploration kernel. In the current example, a candidate is drawn by adding a Gaussian noise with the same standard deviation as inputs. With this choice, it appears that we respect standard practice which is to tune the proposal distribution to get around 20%–25% acceptance rate [34]. Then, the only way to improve previous results is to increase the budget allocated to Metropolis–Hastings steps by increasing parameter A and decreasing the parameter ρ which regulates values of thresholds involved in the SMC procedure. From Table 5 which displays associated results, one can see that previous observed variability has been reduced. The associated failure probability is now estimated to 9.11×10^{-5} with 27% coefficient of variation. The new computation budget is about 262,500 calls to the model (232,500 calls for the failure probability estimation, 30,000 calls for sampling with $\tilde{\mathbf{X}}$ and 0 call for the ROSA index estimation), which is quite substantial. Nevertheless, it remains substantially less expensive than the budget required by a classical Monte Carlo procedure. Furthermore, associated computational cost may be reduced by using a surrogate model. For that purpose, we have performed the same reliability analysis with AK-IS algorithm [21]. The sample size of importance sampling population evaluated on

Table 6

Estimates of δ_i^f , $\hat{\eta}_i$ and $S_i^{\mathbb{1}_{Y>s}}$ for the SDOF oscillator with AK-IS algorithm. 72 calls to the function \mathcal{M} . Failure probability estimated to 9.12×10^{-5} with 32% coefficient of variation. IS sample size: 10,000.

Input	Estimation $\hat{\delta}_i^f$		Estimation $\hat{\eta}_i$		Estimation $\hat{S}_i^{\mathbb{1}_{Y>s}}$	
	Mean (rank)	Sd	Mean (rank)	Sd	Mean (rank)	Sd
c_1	0.0517 (2)	0.0192	0.7932 (2)	0.0322	0.0022 (2)	0.0023
c_2	0.0220 (6)	0.0110	0.1342 (5)	0.0220	0 (5)	0
r	0.0342 (4)	0.0099	0.5412 (3)	0.0210	0.0018 (3)	0.0012
m	0.0290 (5)	0.089	0.0620 (6)	0.0123	0 (6)	0
t	0.0456 (3)	0.084	0.2504 (4)	0.0185	0.0002 (4)	0.0001
F	0.1356 (1)	0.0183	0.9101 (1)	0.0178	0.0255 (1)	0.0231

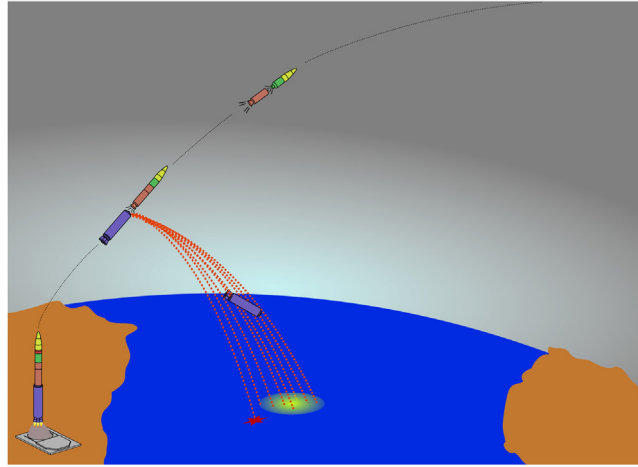


Fig. 1. Illustration scheme of a launch vehicle first stage fallout phase into the Atlantic Ocean. Multiple fallout trajectories are drawn (red dotted lines), leading to the safe zone (yellow circular surface). Due to uncertainties, one fallout trajectory may lead to a failure impact point (red star) [cf. [17]].

the surrogate model is 10,000. The failure probability is estimated by AK-IS to 9.12×10^{-5} with 32% coefficient of variation for a reduced simulation budget of 72 calls to the function (72 calls for the failure probability estimation, 0 call for sampling with $\tilde{\mathbf{X}}$ and 0 call for the ROSA index estimation). The estimated ROSA indices are displayed in Table 6 and are of course very similar to those obtained with SMC. The use of a surrogate model does not increase here the variability of the ROSA index estimation as the failure probability is estimated accurately with AK-IS.

4.5. Example 4: a launcher stage fallout model

Space launcher complexity arises from the coupling between several subsystems, such as stages or boosters and other embedded systems. Optimal trajectory assessment is a key discipline since it is one of the cornerstones of the mission success. However, during the real flight, aleatory uncertainties can affect the different flight phases at different levels (due to weather perturbations, stage combustion etc.) and be combined to lead to a failure state of the space vehicle trajectory. After their propelled phase, the different stages reach successively their separation altitudes and may fall back into the ocean (see Fig. 1). Such a dynamic phase is of utmost importance in terms of launcher safety since the consequence of a mistake in the prediction of the fallout zone can be dramatic in terms of human security and environmental impact. That is the reason why it is of prime importance to take it into account during the rare event analysis.

We consider in this section a simplified trajectory simulation code of the dynamic fallout phase of a generic launcher first stage [17] which takes six input parameters into account. The input vector \mathbf{X} contains the following

Table 7

Input probabilistic model of the launcher phase fallout model.

Input	Distribution	Mean	Sd
$X_1 = \Delta a$ (m)	Normal	0	165
$X_2 = \Delta v$ (m s ⁻¹)	Normal	0	3.7
$X_3 = \Delta \gamma$ (rad)	Normal	0	0.001
$X_4 = \Delta \psi$ (rad)	Normal	0	0.0018
$X_5 = \Delta m$ (kg)	Normal	0	70
$X_6 = \Delta C_d$ (1)	Normal	0	0.1

Table 8

Estimates of δ_i^f and $\tilde{\eta}_i$ for the launcher phase fallout model. 193,520 calls to the function \mathcal{M} . Failure probability estimated to 1.36×10^{-4} with 35% coefficient of variation. Set of parameters for the adaptive SMC algorithm: $N_x = 800$, $A_x = 10$, $\rho = 0.4$, $A = 10$ and $N = 5000$.

Input	Estimation $\hat{\delta}_i$		Estimation $\hat{\delta}_i^f$		Estimation $\hat{\tilde{\eta}}_i$	
	Mean (rank)	Sd	Mean (rank)	Sd	Mean (rank)	Sd
X_1	0.0156 (5)	0.0046	0.0149 (5)	0.0060	0.1235 (4)	0.0367
X_2	0.1535 (2)	0.0056	0.0848 (1)	0.0095	0.8218 (1)	0.0518
X_3	0.0683 (3)	0.0058	0.0406 (2)	0.0084	0.5768 (2)	0.0514
X_4	0.1832 (1)	0.0050	0.0143 (6)	0.0052	0.0722 (6)	0.0478
X_5	0.0153 (6)	0.0046	0.0160 (4)	0.0059	0.1230 (5)	0.0330
X_6	0.0399 (4)	0.0058	0.0284 (3)	0.0083	0.3809 (3)	0.0660

basic variables (i.e., physical variables) representing some initial conditions, environmental variables and launch vehicle characteristics:

- X_1 : stage altitude perturbation at separation (Δa (m));
- X_2 : velocity perturbation at separation (Δv (m s⁻¹));
- X_3 : flight path angle perturbation at separation ($\Delta \gamma$ (rad));
- X_4 : azimuth angle perturbation at separation ($\Delta \psi$ (rad));
- X_5 : propellant mass residual perturbation at separation (Δm (kg));
- X_6 : drag force error perturbation (ΔC_d dimensionless).

These variables are assumed to be independent and normally distributed with parameters gathered in [Table 7](#). As an output, the code will give back the scalar distance $Y = \mathcal{M}(\mathbf{X})$ which represents the distance between the theoretical fallout position into the ocean and the estimated one due to the uncertainty propagation. The failure event is $\{Y > 15\}$ and the associated failure probability is estimated by SMC to 1.36×10^{-4} with 35% coefficient of variation.

Estimates of both target and conditional indices are available in [Table 8](#). The δ_i 's are obtained with the method described in [18]. In average, runs need 750 s to compute all the δ and η -indices and make 193,520 model calls (143,520 calls for the failure probability estimation and 50,000 calls for sampling with $\tilde{\mathbf{X}}$ and 0 call for the ROSA index estimation).

On the one hand, the global ranking provided by δ_i shows that X_4 is the most influential input, followed by X_2 and X_3 . On the other hand, both target and conditional indices underline that the impact of X_4 becomes negligible from a rare event perspective. The rest of the ranking remains relatively unchanged and seems to indicate that X_2 and X_3 are the most influential input upon the launcher's failure regime. Like the example 2, this test case highlights the importance to perform reliability-oriented sensitivity analysis since the impact of an input parameter (here X_2) may depend heavily on the support of the output distribution on which the study is focused.

5. Generalization: target and conditional sensitivity analysis

Following the approach of [29], we explain here how to generalize our estimation scheme in two directions: (1) considering a more general notion of distance between distributions; (2) assessing the impact of X_i on functions of Y .

5.1. More general distance

As explained in the introduction, Borgonovo's index is the total variation distance between (X_i, Y) and (X_i, Y') with Y' independent from X_i . In the absolutely continuous case, this corresponds to the L_1 distance between the joint density $f_{X_i, Y}$ and the product $f_{X_i} f_Y$ of its marginals, which reflects that this index is a measure of dependency between X_i and Y . Of course, many other dependency measures exist, for instance the Csiszár dependency measure.

Let $\phi : \mathbb{R}_+ \rightarrow \mathbb{R} \cup \{+\infty\}$ be a convex function with $\phi(1) = 0$: then the Csiszár divergence between two probability measures P and Q is given by

$$\text{div}_\phi(P, Q) = \int \phi\left(\frac{dP}{dQ}\right) dQ \quad (22)$$

where P is assumed to be absolutely continuous with Radon–Nikodym derivative $\frac{dP}{dQ}$ with respect to Q . For instance, for $\phi(x) = \frac{1}{2}|1 - x|$ this is the total variation distance, and for $\phi(x) = -\log(x)$ this is the Kullback–Leibler divergence. From this divergence, we can then define the Csiszár dependency measure (CDM_ϕ) between two random variables Z_1 and Z_2 as

$$\text{CDM}_\phi(Z_1, Z_2) = \text{div}_\phi((Z_1, Z_2), (Z_1, Z'_2)) \quad (23)$$

with Z'_2 equal in distribution to Z_2 and independent from Z_1 (identifying in the above a random variable and its distribution). Because the total variation distance corresponds to the case $\phi(\cdot) = \frac{1}{2}|1 - \cdot|$, we recover Borgonovo's index with this choice, i.e., we have $\text{CDM}_{\frac{1}{2}|\cdot-1|}(X_i, Y) = \delta_i$. Moreover, we note that this dependency measure can still be expressed in a straightforward manner from the copula c of (Z_1, Z_2) provided it exists, namely

$$\text{CDM}_\phi(Z_1, Z_2) = \int \phi(c(u, v)) du dv, \quad (24)$$

thereby generalizing the relation (11) at the heart of our estimation scheme for δ_i^f .

5.2. Impact on a function of Y

Consider any function $w : \mathcal{M}(\mathbb{R}^d) \rightarrow \mathbb{R}_+$ such that $w(Y)$ is integrable and let $\tilde{\mathbb{P}}^w$ be the probability measure which is absolutely continuous with respect to \mathbb{P} with Radon–Nikodym derivative $w(Y)$. Thus, $\tilde{\mathbb{P}}^w$ is the unique probability measure defined on (Ω, \mathcal{F}) such that

$$\tilde{\mathbb{P}}^w(A) = \frac{\mathbb{E}(w(Y)\mathbb{1}_A)}{\mathbb{E}(w(Y))} \quad (25)$$

for any measurable set $A \in \mathcal{F}$. Adopting the terminology of [29], we can generalize the two problems laid out in the introduction as follows:

Target sensitivity analysis: what is the influence of X_i on $w(Y)$ (rather than on Y)?

Conditional sensitivity analysis: what is the influence of X_i on Y under $\tilde{\mathbb{P}}^w$ (rather than under \mathbb{P})?

What we have done before corresponds to the case $w(y) = \mathbb{1}_{y>s}$. Indeed, for this choice of w the measure $\tilde{\mathbb{P}}^w \circ \mathbf{X}^{-1}$ is the law of $\tilde{\mathbf{X}}$ as defined earlier:

$$\tilde{\mathbb{P}}^w(\mathbf{X} \in A) = \mathbb{P}(\mathbf{X} \in A \mid Y > s) = \mathbb{P}(\tilde{\mathbf{X}} \in A). \quad (26)$$

Thus, we generalize $\tilde{\mathbf{X}}$ to $\tilde{\mathbf{X}}^w = (X_1^w, \dots, X_d^w)$ by defining it as a random variable with law $\tilde{\mathbb{P}}^w \circ \mathbf{X}^{-1}$, and we define $\tilde{Y}^w = \mathcal{M}(\tilde{\mathbf{X}}^w)$.

5.3. Generalization

In view of Eqs. (4), (6) and (7) defining η_i , $\bar{\eta}_i$ and δ_i^f , respectively, the above extensions suggest the following more general version of these indices:

$$\eta_i^{\phi, w} = \text{CDM}_\phi(X_i, w(Y)), \quad \bar{\eta}_i^{\phi, w} = \text{div}_\phi(\tilde{X}_i^w, X_i) \quad \text{and} \quad \delta_i^{\phi, w} = \text{CDM}_\phi(\tilde{X}_i^w, \tilde{Y}^w). \quad (27)$$

We will assume that (X_i, Y) is absolutely continuous with respect to Lebesgue measure with density $f_{X_i, Y}$, and that $(X_i, w(Y))$ is absolutely continuous with respect to the product measure $dx\mu(da)$ with μ a measure on $\mathcal{M}(\mathbb{R}^d)$ with density $f_{X_i, w(Y)}$. If $w(Y)$ takes values in \mathbb{R} , one should typically think of μ as Lebesgue measure, but this more general formalism also makes it possible to encompass the important case where $w(Y)$ follows a discrete distribution: in this case, μ should simply be the counting measure and $(X_i, w(Y))$ is automatically absolutely continuous (with respect to $dx\mu(da)$).

Under these assumptions, we have that:

- $\eta_i^{\phi, w} = \mathbb{E}[\text{div}_\phi(w(Y), w(Y) | X_i)]$;
- $(\tilde{X}^w, \tilde{Y}^w)$ is absolutely continuous with respect to Lebesgue measure with density

$$f_{\tilde{X}_i^w, \tilde{Y}^w}(x, y) = \frac{w(y)f_{X_i, Y}(x, y)}{\mathbb{E}(w(Y))}. \quad (28)$$

For $w(y) = \mathbb{1}_{y>s}$ and $\phi(x) = |1 - x|$, we have the relation (5) between $\eta_i^{\phi, w}$ and $\bar{\eta}_i^{\phi, w}$ which reads

$$\eta_i^{\phi, w} = \mathbb{E}(w(Y)) \times \bar{\eta}_i^{\phi, w}. \quad (29)$$

However, this relation does not seem to hold outside this case, and so in general it is not clear whether $\eta_i^{\phi, w}$ and $\bar{\eta}_i^{\phi, w}$ can be easily related. Guided by the choice made in the case $w(y) = \mathbb{1}_{y>s}$, we consider in the sequel the index $\bar{\eta}_i^{\phi, w}$ even though it may seem at first glance less natural than $\eta_i^{\phi, w}$.

In order to generalize our estimation scheme, we first need a generalization of the adaptive SMC algorithm of Section 3.2. To sample from the tilted distribution $\tilde{\mathbb{P}}^w$, usual particle algorithms can be used such as the Metropolis–Hastings sampler with input target density $w(\mathcal{M}(\cdot))f_{\tilde{\mathbf{X}}}(\cdot)/\mathbb{E}(w(Y))$. In the case $w(y) = \mathbb{1}_{y>s}$ it is hard to sample directly from $\tilde{\mathbb{P}}^w$ and intermediate distributions, say $\tilde{\mathbb{P}}^{w_p}$ with $w_p = \mathbb{1}_{y>\gamma_p}$, are needed. In this case and with a general w , one can for instance use the sequential Monte Carlo samplers proposed in [16].

Assume now that one is given a sample $(\tilde{\mathbf{X}}^{w,1}, \dots, \tilde{\mathbf{X}}^{w,N})$ approximately i.i.d. with common distribution $\tilde{\mathbf{X}}^w$ and their values $\tilde{Y}^{w,k} = \mathcal{M}(\tilde{\mathbf{X}}^{w,k})$ by \mathcal{M} . As discussed above, in the case $w(y) = \mathbb{1}_{y>s}$ this is precisely the purpose of the adaptive SMC algorithm of Section 3.2. Then Step 2 of our estimation scheme remains unchanged and leads to:

- an estimate $\hat{f}_{\tilde{X}_i^w}$ of the density $f_{\tilde{X}_i^w}$ of \tilde{X}_i^w ;
- an estimate \hat{c}^w of the copula c^w of $(\tilde{X}_i^w, \tilde{Y}^w)$.

Using (24) we then have the following two estimations of $\bar{\eta}_i^{\phi, w}$ and $\delta_i^{\phi, w}$: for $\bar{\eta}_i^{\phi, w}$, an estimation $\hat{\bar{\eta}}_i^{\phi, w}$ can be obtained by numerically integrating the one-dimensional integral

$$\text{div}_\phi(\tilde{X}_i^w, X_i) = \int \phi \left(\frac{f_{\tilde{X}_i^w}(x)}{f_{X_i}(x)} \right) f_{X_i}(x) dx \quad (30)$$

or by a Monte Carlo approximation:

$$\hat{\bar{\eta}}_i^{\phi, w} = \frac{1}{N'} \sum_{k=1}^{N'} \phi \left(\frac{f_{\tilde{X}_i^w}(X_i^k)}{f_{X_i}(X_i^k)} \right) \quad (31)$$

with the X_i^k i.i.d. with common distribution f_{X_i} . For $\delta_i^{\phi, w}$, draw i.i.d. random variables (U_1^k, U_2^k) uniformly distributed on $[0, 1]^2$ and consider

$$\hat{\delta}_i^{\phi, w} = \frac{1}{N'} \sum_{k=1}^{N'} \phi(\hat{c}^w(U_1^k, U_2^k)). \quad (32)$$

6. Conclusion

The aim of this paper is twofold:

- first, it expands the GSA method of Borgonovo in a reliability context. Two different ROSA indices, δ_i^f and $\bar{\eta}_i$, have been introduced and a generalization in the more general framework of Csiszár dependency measure

has been formalized. The complementarity of δ_i^f and $\bar{\eta}_i$ has been illustrated through several test cases of increasing complexity. Indeed, on the one hand, the target ROSA measure $\bar{\eta}_i$ aims at studying the impact of an input over the failure probability $\mathbb{P}(Y > s)$ or, more precisely, over the indicator function $\mathbb{1}_{Y>s}$. On the other hand, the conditional ROSA measure δ_i^f aims at quantifying the influence of an input upon the failure, namely, conditionally on the failure event.

- second, it shows that both indices δ_i^f and $\bar{\eta}_i$ can be simultaneously estimated from one common sample $\{\tilde{\mathbf{X}}^k, \tilde{Y}^k\}$ verifying $\mathcal{M}(\tilde{\mathbf{X}}^k) = \tilde{Y}^k > s$ which can be obtained for the most common rare event probability estimation techniques. The estimation of $\bar{\eta}_i$ and δ_i^f is thus a post-processing of the sample without new calls to the model. When the latter is costly-to-evaluate, the rare event probability estimation can lead to a simulation cost which is not reasonable in practice. Nevertheless, this constraint may be overcome by considering a surrogate model. We show that the indices δ_i^f and $\bar{\eta}_i$ can then be estimated with a surrogate model at low computational cost and are of interest in an industrial context.

Appendix. Maximum entropy principle

A.1. General principle

The maximum entropy principle was introduced by Jaynes [24], and the reader is for instance referred to [25] for more details. Let $\mathcal{P}_d(S)$ be the set of probability density functions on $S \subset \mathbb{R}^d$, and for $f \in \mathcal{P}_d(S)$ let $H(f)$ be its differential entropy, defined as

$$H(f) = - \int_S \log f(x) f(x) dx \in [-\infty, +\infty]. \quad (\text{A.1})$$

In order to choose a density satisfying some constraints $\mathcal{C} \subset \mathcal{P}_d(S)$ (for instance, prescribed first and second moments), the maximum entropy principle asserts to choose among these densities the one with highest entropy, i.e.,

$$\begin{aligned} \arg \min_{f \in \mathcal{P}_d(S)} \quad & H(f) \\ \text{subject to} \quad & f \in \mathcal{C} \end{aligned} \quad (\text{A.2})$$

When the constraints are linear equality constraints, i.e., are of the form $\mathcal{C} = \{f \in \mathcal{P}_d(S) : \int \varphi(x) f(x) dx = \mu\}$ for some $\varphi : \mathbb{R}^d \rightarrow \mathbb{R}^d$ and $\mu \in \mathbb{R}^d$, then the above optimization problem is convex and a solution is of the form $f(x) = c e^{-\langle \Lambda^*, \varphi(x) \rangle} \mathbb{1}_S(x)$ where $\langle \cdot, \cdot \rangle$ denotes the inner product in \mathbb{R}^d , c is the normalization constant and Λ^* is a feasible solution of the dual optimization problem

$$\Lambda^* = \arg \min_{\Lambda \in \mathbb{R}^n} \left\{ \langle \Lambda, \mu \rangle + \log \left(\int_S e^{-\langle \Lambda, \varphi(x) \rangle} dx \right) \right\}, \quad (\text{A.3})$$

see for instance [7] for more details. The above objective function is strictly convex on the set of feasible points and so admits respectively a unique minimum which can be found using standard convex optimization techniques, for instance interior-point algorithms.

The above method can be used to estimate a given density f_0 : if one knows some moments of the sought density f_0 , then the idea is simply to put this information as constraints in (A.2).

A.2. Application to Step 2 of our estimation scheme

In our case, we want to apply the above maximum entropy principle in Step 2 of our estimation scheme (see Section 3.3) to estimate the density $f_{\tilde{X}_i}$ of \tilde{X}_i , and the density c_i of $(F_{\tilde{X}_i}(\tilde{X}_i), F_{\tilde{Y}}(\tilde{Y}))$. Ideally, we would like to consider solutions to (A.2) with linear equality constraints but the problem is that moments of the sought distributions are unknown. To circumvent this difficulty, we use the sample $((\tilde{X}_i^k, \tilde{Y}^k), k = 1, \dots, N)$ provided by the first step to estimate these moments. Also, for reasons discussed in [18] we consider fractional moments for the constraints.

More precisely, consider $\tilde{n}, n \in \mathbb{N}$ and real numbers $\alpha_1 < \dots < \alpha_{\tilde{n}}$ and $\beta_1 < \dots < \beta_n$, and let

$$\hat{M}_{r,s} := \frac{1}{N} \sum_{k=1}^N \left(\hat{F}_{\tilde{X}_i}(\tilde{X}_i^k) \right)^{\alpha_r} \left(\hat{F}_{\tilde{Y}}(\tilde{Y}^k) \right)^{\alpha_s}, \quad r, s = 1, \dots, \tilde{n}, \quad (\text{A.4})$$

where $\tilde{F}_{\tilde{X}_i}$ and $\tilde{F}_{\tilde{Y}}$ are the empirical cumulative distribution functions of \tilde{X}_i and \tilde{Y} , respectively, obtained from the sample $((\tilde{X}_i^k, \tilde{Y}^k), k = 1, \dots, N)$, and

$$\hat{M}_t^i := \frac{1}{N} \sum_{k=1}^N (\tilde{X}_i^k)^{\beta_t}, \quad t = 1, \dots, n. \quad (\text{A.5})$$

Then the estimates $\hat{f}_{\tilde{X}_i}$ and \hat{c}_i of $f_{\tilde{X}_i}$ and c_i , respectively, are given by

$$\begin{aligned} \hat{f}_{\tilde{X}_i} &= \arg \min_{f \in \mathcal{P}_1(\text{Supp}(\tilde{X}_i))} H(f) \\ \text{subject to} \quad & \int_{\text{Supp}(\tilde{X}_i)} x^{\beta_t} f(x) dx = \hat{M}_t^i, \quad t = 1, \dots, n, \end{aligned} \quad (\text{A.6})$$

and

$$\begin{aligned} \hat{c}_i &= \arg \min_{f \in \mathcal{P}_2([0,1]^2)} H(f) \\ \text{subject to} \quad & \int_{[0,1]^2} x^{\alpha_r} y^{\alpha_s} f(x, y) dx dy = \hat{M}_{r,s}, \quad r, s = 1, \dots, \tilde{n}. \end{aligned} \quad (\text{A.7})$$

These solutions are obtained by the method described above. Note that the number of constraints is then n for estimating $f_{\tilde{X}_i}$ and \tilde{n}^2 for estimating c_i . In this article, n and \tilde{n} are set to 3.

References

- [1] S. Au, Probabilistic failure analysis by importance sampling Markov chain simulation, *J. Eng. Mech.* 130 (2004) 303–311.
- [2] S.-K. Au, J.L. Beck, Estimation of small failure probabilities in high dimensions by subset simulation, *Probab. Eng. Mech.* 16 (2001) 263–277.
- [3] E. Borgonovo, A new uncertainty importance measure, *Reliab. Eng. Syst. Saf.* 92 (2007) 771–784.
- [4] E. Borgonovo, G.B. Hazen, E. Plischke, A common rationale for global sensitivity measures and their estimation, *Risk Anal.* 36 (2016) 1871–1895.
- [5] E. Borgonovo, E. Plischke, Sensitivity analysis: a review of recent advances, *European J. Oper. Res.* 248 (2016) 869–887.
- [6] E. Borgonovo, S. Tarantola, Moment independent and variance-based sensitivity analysis with correlations: An application to the stability of a chemical reactor, *Int. J. Chem. Kinet.* 40 (2008) 687–698.
- [7] S. Boyd, L. Vandenberghe, *Convex Optimization*, Cambridge university press, 2004.
- [8] T. Browne, J.-C. Fort, B. Iooss, L. Le Gratiet, Estimate of quantile-oriented sensitivity indices, 2017, <https://hal.archives-ouvertes.fr/hal-01450891>.
- [9] C. Bucher, Y. Chen, G. Schuëller, Time variant reliability analysis utilizing response surface approach, in: *Reliability and Optimization of Structural Systems*, Vol. 88, Springer, 1989, pp. 1–14.
- [10] J. Bucklew, *Introduction to Rare Event Simulation*, Springer Science & Business Media, 2013.
- [11] F. Cérou, P. Del Moral, T. Furon, A. Guyader, Sequential Monte Carlo for rare event estimation, *Statist. Comput.* 22 (2012) 795–808.
- [12] V. Chabridon, *Analyse de Sensibilité Fiabiliste Avec Prise en Compte D'incertitudes sur le Modèle Probabiliste—Application aux Systèmes Aérospatiaux* (Ph.D. thesis), Université Clermont Auvergne, 2018.
- [13] S. Chib, E. Greenberg, Understanding the Metropolis-Hastings algorithm, *Amer. Statist.* 49 (1995) 327–335.
- [14] L. Cui, Z. Lü, X. Zhao, Moment-independent importance measure of basic random variable and its probability density evolution solution, *Sci. China Technol. Sci.* 53 (2010) 1138–1145.
- [15] S. Da Veiga, Global sensitivity analysis with dependence measures, *J. Stat. Comput. Simul.* 85 (2015) 1283–1305.
- [16] P. Del Moral, A. Doucet, A. Jasra, Sequential Monte Carlo samplers, *J. R. Stat. Soc. Ser. B Stat. Methodol.* 68 (2006) 411–436.
- [17] P. Derennes, V. Chabridon, J. Morio, M. Balesdent, F. Simatos, J.-M. Bourinet, M. Gayton, Nonparametric importance sampling techniques for sensitivity analysis and reliability assessment of a launcher stage fallout, in: G. Fasano, J. Pinte (Eds.), *Optimization in Space Engineering*, Springer, 2019.
- [18] P. Derennes, J. Morio, F. Simatos, Estimation of moment independent importance measures using a copula and maximum entropy framework, in: *2018 Winter Simulation Conference (WSC)*, IEEE, 2018, pp. 1623–1634.
- [19] P. Derennes, J. Morio, F. Simatos, A nonparametric importance sampling estimator for moment independent importance measures, *Reliab. Eng. Syst. Saf.* 187 (2019) 3–16.

- [20] B. Echard, N. Gayton, M. Lemaire, Ak-mcs: an active learning reliability method combining Kriging and Monte Carlo simulation, *Struct. Saf.* 33 (2011) 145–154.
- [21] B. Echard, N. Gayton, M. Lemaire, N. Relun, A combined importance sampling and Kriging reliability method for small failure probabilities with time-demanding numerical models, *Reliab. Eng. Syst. Saf.* 111 (2013) 232–240.
- [22] X. Huang, J. Chen, H. Zhu, Assessing small failure probabilities by AK–SS: an active learning method combining Kriging and subset simulation, *Struct. Saf.* 59 (2016) 86–95.
- [23] B. Iooss, P. Lemaître, A review on global sensitivity analysis methods, in: *Uncertainty Management in Simulation–Optimization of Complex Systems*, Springer, 2015, pp. 101–122.
- [24] E.T. Jaynes, Information theory and statistical mechanics, *Phys. Rev.* 106 (1957) 620.
- [25] J. Kapur, H. Kesavan, *Entropy optimization principles with applications*, 1992.
- [26] P. Lemaître, E. Sergienko, A. Arnaud, N. Bousquet, F. Gamboa, B. Iooss, Density modification-based reliability sensitivity analysis, *J. Stat. Comput. Simul.* 85 (2015) 1200–1223.
- [27] L. Li, Z. Lu, B. Feng, Jun and Wang, Moment-independent importance measure of basic variable and its state dependent parameter solution, *Struct. Saf.* 38 (2012) 40–47.
- [28] Q. Liu, T. Homma, A new computational method of a moment-independent uncertainty importance measure, *Reliab. Eng. Syst. Saf.* 94 (2009) 1205–1211.
- [29] A. Marrel, V. Chabridon, *Statistical developments for target and conditional sensitivity analysis: application on safety studies for nuclear reactor*, 2020, <https://hal.archives-ouvertes.fr/hal-02541142/document>.
- [30] R. Melchers, Radial importance sampling for structural reliability, *J. Eng. Mech.* 116 (1990) 189–203.
- [31] G. Perrin, G. Defaux, Efficient evaluation of reliability-oriented sensitivity indices, *J. Sci. Comput.* 79 (2019) 1433–1455.
- [32] E. Plischke, E. Borgonovo, C.L. Smith, Global sensitivity measures from given data, *European J. Oper. Res.* 226 (2013) 536–550.
- [33] G. Sarazin, P. Derennes, J. Morio, Estimation of high-order moment-independent importance measures for Shapley value analysis, *Appl. Math. Model.* 88 (2020) 396–417.
- [34] C. Sherlock, G. Roberts, Optimal scaling of the random walk metropolis on elliptically symmetric unimodal targets, *Bernoulli* (2009) 774–798.
- [35] Y. Wang, S. Xiao, Z. Lu, A new efficient simulation method based on Bayes’ theorem and importance sampling Markov chain simulation to estimate the failure-probability-based global sensitivity measure, *Aerosp. Sci. Technol.* 79 (2018) 364–372.
- [36] P. Wei, Z. Lu, W. Hao, J. Feng, B. Wang, Efficient sampling methods for global reliability sensitivity analysis, *Comput. Phys. Comm.* 183 (2012) 1728–1743.
- [37] P. Wei, Z. Lu, J. Song, Moment-independent sensitivity analysis using copula, *Risk Anal.* 34 (2014) 210–222.
- [38] P. Wei, Z. Lu, J. Song, Variable importance analysis: a comprehensive review, *Reliab. Eng. Syst. Saf.* 142 (2015) 399–432.
- [39] P. Wei, Z. Lu, X. Yuan, Monte Carlo simulation for moment-independent sensitivity analysis, *Reliab. Eng. Syst. Saf.* 110 (2013) 60–67.
- [40] W. Yun, Z. Lu, X. Jiang, An efficient method for moment-independent global sensitivity analysis by dimensional reduction technique and principle of maximum entropy, *Reliab. Eng. Syst. Saf.* (2018).
- [41] W. Yun, Z. Lu, X. Jiang, S. Liu, An efficient method for estimating global sensitivity indices, *Internat. J. Numer. Methods Engrg.* 108 (2016) 1275–1289.
- [42] L. Zhang, Z. Lu, L. Cheng, C. Fan, A new method for evaluating Borgonovo moment-independent importance measure with its application in an aircraft structure, *Reliab. Eng. Syst. Saf.* 132 (2014) 163–175.
- [43] X. Zhang, M.D. Pandey, Structural reliability analysis based on the concepts of entropy, fractional moment and dimensional reduction method, *Struct. Saf.* 43 (2013) 28–40.