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# A damage criterion based on energy balance for an isotropic cohesive zone model

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1 The objective of this paper is to present an energy damage criterion for cohesive zone models (CZM) within the  
2 framework of the non-linear thermodynamics of irreversible processes (TIP). An isotropic elastic damageable material  
3 is considered for isothermal transformations. Damage is then the only irreversible effect accompanying the deformation  
4 process and this mechanism is assumed to be fully dissipative. Once a separation law and a damage state variable  
5 have been chosen, it is demonstrated that the damage evolution law can be automatically derived from the energy  
6 balance. From this observation, a CZM is derived for a given choice of traction-separation law and damage state  
7 variable and the quality of its numerical predictions is analyzed using an experimental benchmark bending test.  
8 Damage, elastic and dissipated energy fields around the crack path are shown during this rupture test. Finally, a  
9 numerical simulation of a Brazilian test is proposed where no pre-crack is present in the specimen. Then, as before,  
10 the evolution of the dissipated energy fields are plotted during the loading until the total failure of the specimen.

11 Keywords cohesive zone, damage, fracture, thermodynamics of irreversible processes, energy balance, Finite element analy-  
12 sis, Brazilian test

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## 14 1 Introduction

15 In many industrial situations, the management of damage and failure of mechanical structures is crucial.  
16 This is the reason why many academic and industrial laboratories have intensively studied and still study  
17 this problem from an experimental, theoretical, and numerical point of view. Behavioral models taking  
18 into account the damage, cracking and failure of structures have followed roughly two distinct paths.  
19 Since the pioneering work of Dugdale [Dugdale 1960](#) and Barenblatt [Barrenblatt 1962](#), surface approaches  
20 were proposed. Their objective was to describe in a practical way the material behavior during its rupture,  
21 more precisely during the onset and the propagation of crack. The concept of traction-separation curve  
22 associated with the crack tip was introduced to depict the gradual separation of material elements. This  
23 type of approach has led to the so-called cohesive zone models. The other path can be characterized by  
24 continuum damage approaches that have gradually developed since the works of Kachanov [Kachanov 1986](#)  
25 and Rabotnov [Rabotnov et al. 1970](#). Volume descriptions have often used a scalar or tensorial damage  
26 variable to describe the progressive degradation of the material. These variables are still often linked to the  
27 loss of material elastic stiffness (e.g. [Lemaitre 1996](#)).

28 During these last thirty years, whether mechanical approaches are surface or volume, some have been  
29 progressively presented within a thermodynamics of irreversible processes (TIP) framework. (e.g., [Costanzo](#)

30 [et al. 1995](#); [Chandrakanth et al. 1995](#)). Thermodynamics provides indeed a consistent framework both for  
31 discussing the admissibility of the constitutive equations that account for the irreversibility of damage  
32 mechanisms, and for characterizing the energy properties of damage and crack growth phenomena.  
33 A significant number of works dealing with volume approaches used the TIP with internal variables  
34 including state variables related to the damage. The behavioral constitutive equations are then divided into  
35 two groups: the state equations derived from the thermodynamic potential, characterizing the properties  
36 of equilibrium states of the material, and the complementary (or evolution) equations derived either  
37 from threshold functions generally defined in the space of thermodynamic forces associated with the  
38 model, or from a dissipation potential in the framework of Generalized Standard Materials [Kondo et al.](#)  
39 [2007](#). Particular attention has been paid to the form of the evolution equations such that the model  
40 predictions conform to the 2nd principle of thermodynamics. For cohesive zone models, the introduction  
41 of thermodynamics has been much the same as for the bulk/continuum approaches. As [Costenzo et](#)  
42 [al. Costanzo et al. 1995](#) noted, [Gurtin Gurtin 1979](#) was probably the first to propose a thermodynamic  
43 framework for cohesive zones in fracture. He proposed to consider the crack surface as a two-dimensional  
44 thermodynamic system endowed with a potential, (e.g., free energy), dependent on the crack temperature  
45 and the crack tip opening displacement. Regarding the evolution laws, and particularly those related to  
46 the damage variables, some, like [Costenzo et al. Costanzo et al. 1995](#) advocate the use of a dissipation  
47 potential in the GSM framework. Others, probably more numerous, proposed forms of differential (kinetic)  
48 equations. Although it is impossible to mention all the works related to how damage kinetics were  
49 constructed, some references spanning the last 20 years include: [Ortiz and Pandolfi Ortiz et al. 1999](#), [Roe](#)  
50 [et al. 2003](#), [Evangelista et al. Evangelista et al. 2013](#), [Serpieri et al. Serpieri et al. 2015a](#), [Kuna and Roth](#)  
51 [Kuna et al. 2015](#), and more recently [Shu and Stanciulescu Shu et al. 2020](#). Here again, when the evolution  
52 law is not derived from a dissipation potential, it is necessary to check that the irreversible evolution  
53 of the system is in accordance with the second principle of thermodynamics, often formulated via the  
54 Clausius-Duhem inequality.

55 In this paper, we focus on the formulation of a CZ model for an isotropic elastic damageable material.  
56 Its main objective is to show that when the energy properties of the damage mechanisms are explicitly  
57 specified, it is no longer necessary to formulate any hypothesis concerning the damage evolution law, this  
58 one being entirely fixed by the energy balance. The potential interest of such an observation is that from  
59 now on, experimental techniques dealing with thermal and kinematic full-field measurements allow one to  
60 perform local energy balances whose results will help to identify the CZ model. [Richefeu et al. 2012](#).

61 The following sections are devoted to the construction of an energy damage criterion derived from the  
62 energy balance for an isotropic elastic damageable material within the TIP framework. Contrary to what is  
63 classically done, the damage kinetics is not derived, in this work, from an ad-hoc threshold criterion or  
64 a dissipation potential but is based on the premise that the damage progress is linked to a prescribed  
65 evolution in the maximum elastic energy that can be stored within the material for a given damage state.  
66 From an energy standpoint, it must be noted that the damage mechanisms are considered as the only

67 microstructural irreversible effects accompanying the deformation process and these mechanisms are  
68 fully dissipative (no energy storage induced by the material degradation). These restrictive hypotheses  
69 are however often implicitly present in the literature we have previously mentioned. To illustrate this  
70 statement, let us consider for example the paper proposed by Bouvard et al. [Bouvard et al. 2009](#). In  
71 this paper, the fact that the damage is the only dissipative mechanism is described by a traction force  
72 defined via a state law (i.e. no irreversibility is associated with the displacement jump). The fact that the  
73 damage mechanisms are considered as fully dissipative can be established once looking at the dissipation  
74 form: the dissipation is the product of the thermodynamic force associated with the damage multiplied  
75 by the damage rate. In such a case, no energy storage (or release) accompanying the damage progress  
76 should appear in the model simulations. Naturally, damage dissipation may induce self-heating leading to  
77 non-isothermal deformation processes that are consequently irreversible due to heat diffusion. However,  
78 for sake of simplicity, only isothermal transformations are considered in the following sections, and the  
79 chosen state variables are the displacement jump vector  $\mathbf{u}$  and a scalar damage variable, denoted by  $u_d$ .  
80 This damage variable  $u_d$  is the maximum of the equivalent opening displacement as used in many papers  
81 such as [Ortiz et al. 1999](#), [Bosch et al. 2006](#), [Park et al. 2009](#), [Daridon et al. 2011](#), [Blal et al. 2011](#) for example.

82 The layout of the paper is as follows. The energy criterion of the damageable elastic cohesive zone  
83 model is presented in Section 2 through a 1-D scenario within the TIP framework. In Section 3, a  
84 vectorial extension of the cohesive zone law is proposed for an isotropic damage evolution. In Section  
85 4, the capability of the model is investigated using an experimental benchmark test (i.e. a single-edge  
86 notch-bending specimen for fracture toughness testing) [Moës et al. 2011](#); [Wojtacki et al. 2015](#); [Galvez et al.](#)  
87 [1996](#). Mechanical and energy responses are shown and discussed. Several damage, elastic and dissipated  
88 energy fields around the fracture paths are plotted during the crack propagation. As already mentioned,  
89 the computation of the dissipated energy fields is of special interest since they can be compared with the  
90 ones derived from quantitative IR techniques. The reader interested in these techniques can refer to  
91 [Chrysochoos 2012](#); [Benaarbia et al. 2017](#). With this perspective, in the final section, a numerical simulation  
92 of a Brazilian disc test is proposed. This kind of test is well adapted to infrared imaging since the flat  
93 surface of the specimen remains perpendicular to the optical axis of the camera until the crack occurs.

## 94 **2 1D scenario**

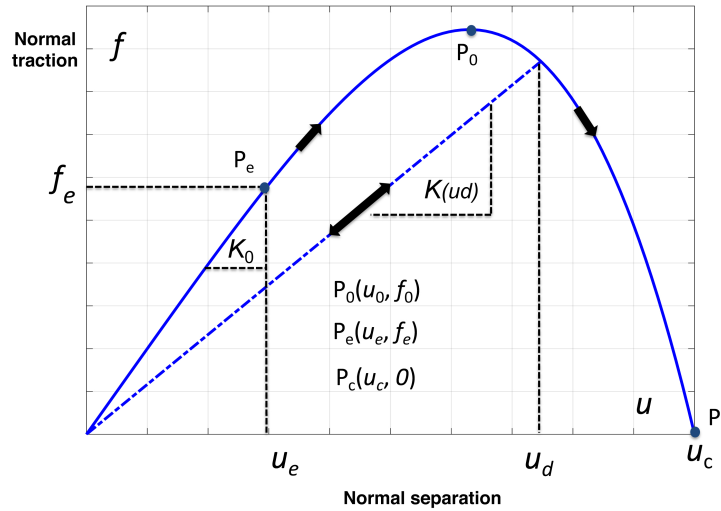
95 The objective of the following section is to briefly review the mechanical concepts classically introduced  
96 with CZM in the case of a 1D monotonic traction and to embed them into the TIP framework to derive,  
97 through an energy criterion, a damage evolution law.

### 98 **2.1 Mechanical aspects**

99 In the literature, the mechanical response of the cohesive zone is described by the correspondence between  
100 the “normal traction” force  $f$  supported by the interface and its normal opening displacement often called  
101 “separation” during a monotonic opening. Depending on the chosen form of the traction-separation

102 diagram, the relationships are called bilinear, polynomial or exponential cohesive laws. In Figure 1 a  
 103 polynomial form has been chosen to illustrate the most commonly characteristics of these curves. We find  
 104 the cohesive strength  $f_0$  corresponding to the maximum of the traction–separation curve or its associated  
 105 opening displacement  $u_0$ , the maximum value of separation  $u_c$  corresponding to the crack opening. An  
 106 energy parameter is also often mentioned [Ortiz et al. 1999](#): this is the fracture energy  $A_c = \int_0^{u_c} f(u)du$   
 107 (work of separation), which is the area below the traction-separation curve.

108 This traction-separation curve is considered as a threshold over which the damage develops irreversibly.  
 109 This threshold is an intrinsic characteristic of the cohesive zone behavior. When unloading is considered,  
 110 it is supposed to be purely elastic, assuming that the damage progress stops as soon as the loading point is  
 111 below the threshold curve. For convenience, the elastic unloading paths are often directed towards the  
 112 origin of the traction–separation diagram (see Figure 1). This implies that the elasticity remains linear and  
 113 that there is no residual opening at the end of the unloading.



**Figure 1:** Traction-separation diagram. Monotonic envelope (continuous line), elastic unload or reload (dashed line). An arbitrary polynomial cohesive law has been chosen.

114 The progress of the damage can be depicted by a continuous decrease of the secant stiffness  $K = \frac{f}{u}$   
 115 towards zero until rupture at  $u_c$ . A classical scalar definition of the damage variable can then be given by:

$$D_k = \frac{K_0 - K}{K_0}, \quad (1)$$

116 where  $K_0$  is the initial stiffness of the cohesive zone. The variable  $D_k$  progressively increases from 0 to  
 117 1 when the opening displacement increases from 0 to  $u_c$  (or from  $u_e$  to  $u_c$  when a pure elastic domain,  
 118  $[0, u_e]$ , is introduced in the traction-separation curve (see Figure 1)).

119 A second possibility is to consider a normalized deformation energy definition of the damage [Ortiz](#)

120 [et al. 1999](#) :

$$D_A = \frac{A}{A_c}, \text{ where } A = \int_0^u f(v)dv . \quad (2)$$

121 Here again, this last definition slightly changes when an elastic domain limited by the point  $(u_e, f_e)$  is  
122 introduced. In such a case, [Eq.\(2\)](#) requires a renormalization:

$$D_A^* = \frac{A^*}{A_c^*}, \text{ where } A^* = \int_{u_e}^u f(v)dv \text{ and } A_c^* = \int_{u_e}^{u_c} f(v)dv . \quad (3)$$

123 Then by construction  $D_A$  and  $D_A^*$  belong to  $[0, 1]$ . In fact, there are many ways to define damage. The  
124 damage process being assumed irreversible, the damage variable rate is often chosen to be non-negative  
125 whatever the loading history, to depict its monotonic evolution. Damage develops when the mechanical  
126 state  $(u, f)$  corresponds to a point of the cohesive threshold curve. In what follows we have chosen a  
127 kinematic definition of the damage variable. Like previously done by numerous authors (*e.g.* [Serpieri et al.](#)  
128 [2015b](#)), we have chosen the maximum value of the separation  $u_d$  ever reached by the cohesive zone until  
129 instant  $t$ . This damage variable is then defined at instant  $t$  by:

$$u_d = \max \{u(\tau), \forall \tau \leq t\} . \quad (4)$$

130 This variable monotonically increases during the damage progress from 0 to  $u_c$  whatever the loading  
131 path (see [Fig.1](#))).

## 132 **2.2 Energy aspects**

133 Usually during a load cycle, the deformation energy  $w_{def}$ , which corresponds to the area surrounded by  
134 the loading curve [Eq.\(7\)](#) is transformed into dissipated energy, denoted by  $w_d$ , and stored energy, denoted  
135 by  $w_s$ , due to the irreversible microstructural transformations accompanying the deformation process.  
136 Part of  $w_{def}$  can also involve strong thermomechanical coupling energy (heat)  $w_{thm}$  [Chrysochoos 2012](#).  
137 An illustrative example of the coupling effects on the mechanical response can be given by the famous  
138 thermoelastic damping presented by Zener in [Zener 1938](#). The general form of the energy balance over a  
139 loading cycle can then be written as:

$$w_{def} = w_d + w_s + w_{thm} . \quad (5)$$

140 For any other loading the elastic energy,  $w_e$ , has to be added so that :

$$w_{def} = w_e + w_d + w_s + w_{thm} , \quad (6)$$

141  $w_e$  vanishing, by construction, over a loading cycle. In the present situation, we only consider  
 142 isothermal transformations with no thermomechanical coupling. Moreover, we assume that damage is a  
 143 pure dissipative mechanism and that, consequently, no energy storage or release of stored energy, due to  
 144 microstructural changes, occurs during the loading. These assumptions imply  $w_s = 0$  and  $w_{thm} = 0$ . For  
 145 any kind of separation-controlled loading  $\{u(\tau), \forall \tau \leq t\}$ , the deformation energy at instant  $t$  is here  
 146 defined by:

$$w_{def}(t) = \int_0^t f(\tau) \dot{u}(\tau) d\tau . \quad (7)$$

147 For monotonic loadings, the mechanical state follows the traction-separation curve. The deformation  
 148 energy then represents the mechanical energy required to reach the damage state  $u_d = u(t)$ . This cost in  
 149 deformation energy can be defined by:

$$w_{def}^d(u_d) = \int_0^{u_d} f(v) dv . \quad (8)$$

150 Another important mechanical energy term is the elastic energy,  $w_e(u, u_d)$ , in the cohesive zone at a  
 151 given state of damage  $u_d$ . It is defined by:

$$w_e(u, u_d) = \frac{1}{2} K(u_d) u^2 . \quad (9)$$

152 Note that this energy is mechanically recoverable during the unloading. This is the reason why it did  
 153 not appear in the general form of the energy balance proposed in Eq.(5) for a complete loading cycle.

154 As previously done for the deformation energy during monotonic loading, we can define the elastic  
 155 energy  $w_e^d(u_d)$  by:

$$w_e^d(u_d) = \frac{1}{2} K(u_d) u_d^2 = w_e(u_d, u_d) , \quad (10)$$

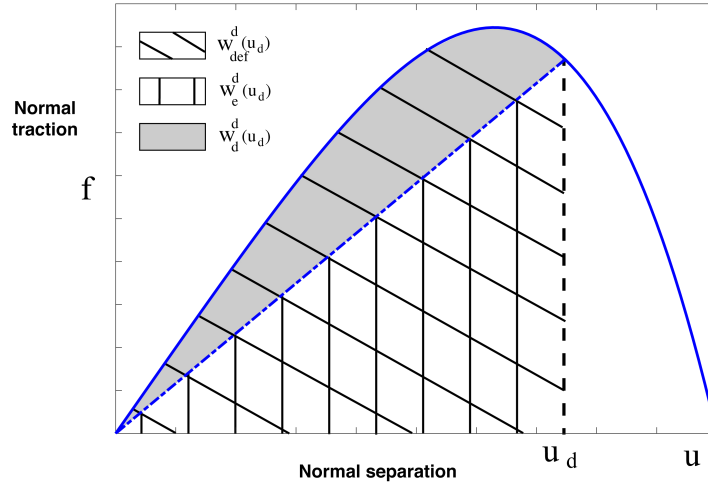
156 which represents the maximum elastic energy mechanically recoverable for a given damage state,  
 157 defined by  $u_d$ .

158 As previously supposed (no thermomechanical coupling energy, no energy storage) the difference

159 between  $w_{def}^d(u_d)$  and  $w_e^d(u_d)$  is attributed to the energy dissipation accompanying the irreversibility of  
 160 damage mechanisms. The dissipated energy,  $w_d^d(u_d)$ , is then defined by :

$$w_d^d(u_d) = w_{def}^d(u_d) - w_e^d(u_d), \quad (11)$$

161  $w_d^d(u_d)$ ,  $w_e^d(u_d)$  and  $w_{def}^d(u_d)$  are illustrated in Figure 2.

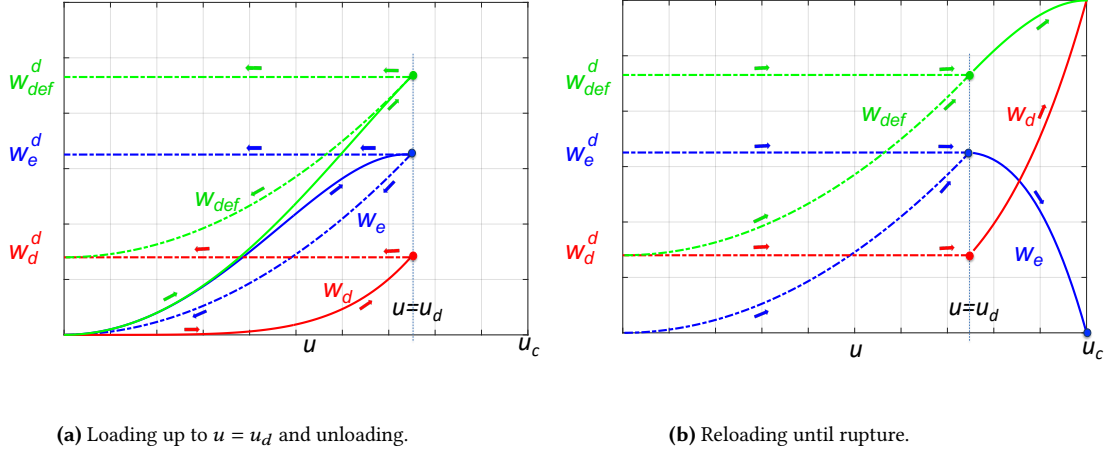


**Figure 2:** Energy illustration of the traction-separation diagram. Monotonic envelope (continuous blue line), elastic unload (dashed blue line).

162 Based on the mechanical response chosen in Figure 1, the evolutions of the three different energies  
 163 associated with a loading-unloading tensile testing are shown in Figure 3. The deformation, elastic, and  
 164 dissipated energies are plotted in green, blue, and red respectively. The deformation energy  $w_{def}$  is  
 165 naturally the sum of the dissipated  $w_d$  and elastic  $w_e$  energies Eq.(6) since the damage is supposed to  
 166 be the only microstructural transformation which is fully dissipative during loading, see Eq.(11) (no  
 167 energy storage is induced by the microstructural transformations). Figure 3(a) illustrates that during the  
 168 elastic unloading  $w_e^d$  remains constant (no evolution of damage) while  $w_e$  returns to zero. In parallel,  
 169 the deformation energy  $w_{def}$  also decreases and tends towards the energy previously dissipated during  
 170 the first loading cycle,  $w_d^d$ . In Figure 3(b) the elastic reloading while  $u \leq u_d$  is shown (dashed lines) and  
 171 extended by a monotonic loading until rupture for  $u_d = u_c$  (full lines).

172 Under these restrictive assumptions, the area under the traction-separation curve, Figure 1 (equivalent  
 173 to a monotonic traction rupture) is completely dissipated when the cohesive zone vanishes. In the next  
 174 sub-section once the thermodynamic working framework has been specified, this important property is  
 175 discussed. Then, another point to underline is that if the traction-separation curve is classically considered  
 176 as the constituent element of the behavior of the cohesion zone, it is thus the same for the evolutions of  
 177  $w_{def}^d(u_d)$  and  $w_e^d(u_d)$ . Therefore, instead of using the tension-separation curve to describe the damage  
 178 progress, associated with the loss of stiffness, it is also possible to use the evolution of the allowable  
 179 maximum elastic energy  $w_e^d$  to define the threshold function associated with the damage rate.





**Figure 3:** Energy balance evolution during a load-unload-reload process - Continuous lines are associated with the monotonic envelope, dashed lines correspond to the elastic unload and reload.

### 180 2.3 Thermodynamics aspects

181 In this sub-section, the above results and comments are integrated into the TIP framework.

#### 182 2.3.1 Cohesive zone potential and state laws

In the case of isothermal transformations, the chosen state variables are  $(u, u_d)$ . A first gambling of the thermomechanical approach is to assume the existence of a potential  $\psi(u, u_d)$  capable of gathering all the state laws. Here we identify this potential to the elastic energy  $w_e$  defined in Eq.(10):

$$183 \quad \psi(u, u_d) = \frac{1}{2}K(u_d)u^2. \quad (12)$$

184 The state laws are by construction the partial derivatives of the potential with respect to the state  
185 variables. We then define the conjugate variable  $f^r$ , associated with  $u$  which represents the reversible part  
of the traction force, and  $A_d$  the conjugate variable associated with  $u_d$  respectively :

$$\left\{ \begin{array}{l} f^r = \frac{\partial \psi}{\partial u} = K(u_d)u \\ A_d = \frac{\partial \psi}{\partial u_d} = \frac{1}{2}K'(u_d)u^2 \end{array} \right., \quad (13)$$

186 where  $K'(u_d) = \frac{dK(u_d)}{du_d}$ .

#### 187 2.3.2 Clausius-Duhem inequality

The irreversibility of the mechanisms accompanying the opening of the cohesive zone is depicted by the Clausius-Duhem inequality which enables the definition of the intrinsic dissipation  $w_d^o$ . In the present framework, it can be written as :

$$188 \quad w_d^o = w_{def}^o - \dot{\psi} = f\dot{u} - \frac{\partial \psi}{\partial u}\dot{u} - \frac{\partial \psi}{\partial u_d}\dot{u}_d = f^{ir}\dot{u} + X_d\dot{u}_d \geq 0. \quad (14)$$

188 The terms  $w_d^o$  and  $w_{def}^o$  determine the dissipated and deformation energy rates, respectively. The symbol  
 189  $(-)^o$  is introduced to underline that  $w_d$  and  $w_{def}$  are not a priori state functions and are then path  
 190 dependent. Eq.(14) also introduce the irreversible part of the traction force,  $f^{ir} = f - f^r$ , and the  
 191 thermodynamic force  $X_d$  associated with  $\dot{u}_d$ . Note that during an irreversible transformation  $\dot{u}_d > 0$  we  
 192 get  $X_d = -A_d$ . If damage is the only irreversible process, no dissipation has to be associated with  $\dot{u}$ . In  
 193 such a case the irreversible traction force vanishes  $f^{ir} = 0$ . The traction force  $f$  can then be directly  
 194 defined via the state law:

$$f = f^r = K(u_d)u . \quad (15)$$

195 Moreover, the intrinsic dissipation becomes with Eq.(13) and Eq.(14) :

$$w_d^o = X_d \dot{u}_d = -\frac{1}{2} K'(u_d) u^2 \dot{u}_d \geq 0 . \quad (16)$$

196 The fact that  $\dot{u}_d \geq 0$  implies  $K'(u_d) \leq 0$  what is physically consistent. The irreversible nature of  
 197 damage leads to a degradation of the secant stiffness.

### 198 2.3.3 Threshold function and damage evolution law

199 In the TIP framework the thermodynamic forces are supposed to be function of the state variable rates. In  
 200 the case of the linear TIP proposed by Onsager [Onsager 1931](#), the correspondence between thermodynamic  
 201 forces and state variable fluxes is linear. The Onsager matrix is supposed to be symmetric positive definite  
 202 in order to verify the Clausius-Duhem inequality (positive dissipation) whatever the thermodynamic  
 203 process. Extension to non-linear theory exists as for example the formalism of Generalized Standard  
 204 Materials [Halphen et al. 1975](#). Based on the hypothesis of normal dissipation, the thermodynamic forces  
 205 derive from a convex dissipation potential or equivalently, state variables rates derived from a dual  
 206 dissipation potential, function of the thermodynamic forces. This dissipation potential can also involve the  
 207 state variables of the model as parameters [Lemaitre 1996](#). A common approach is then:

- 208 - to define a threshold function depending on the thermodynamic forces (and possibly state variables)
- 209 - to write that irreversibility occurs and develops if the thermodynamic state is on the threshold and  
 210 remains on it during a time increment.

211 Note that once the state laws (derived from the thermodynamic potential) and complementary laws  
 212 (derived from the dissipation potential) have been written, it is then possible to deduce the evolution of the  
 213 energy balance associated with the transformation.

In what follows in as much as our approach is directly based on the energy balance form imposing by  
 construction non-negative dissipation, the existence of the threshold function will not be associated with  
 the normal dissipation hypothesis. Indeed, the current elastic domain is characterized by  $w_e^d(u_d)$  the

maximum elastic energy available for a given damage state which also corresponds to the energy required to further damage the material. Then the damage energy criterion based on the energy balance is defined by :

$$w_e(u, u_d) \leq w_e^d(u_d) . \quad (17)$$

214 The evolution law for  $u_d$  is then derived from the fact that for the damage to occur the maximum  
215 elastic energy allowable in the material has to be and remain on the threshold during the loading step, i.e.

$$\begin{cases} w_e(u, u_d) = w_e^d(u_d) & \text{(a)} \\ \dot{w}_e(u, u_d) = \dot{w}_e^d(u_d) & \text{(b)} \end{cases} . \quad (18)$$

216 The first equality gives naturally  $u_d = u$ . The second equality leads to a proposal of evolution equation  
217 for the damage :

$$\dot{u}_d = \begin{cases} \dot{u} & \text{if } u = u_d \text{ and } \dot{u} \geq 0 \\ 0 & \text{if } u < u_d \text{ or } \dot{u} \leq 0 \end{cases} , \quad (19)$$

218 what is consistent if we remind the definition of the damage state variable *Eq.(4)* and the fact that the  
219 damage increases irreversibly,  $\dot{u}_d \geq 0$ .

220 To be fully compatible with non-linear TIP framework, the final step is to propose a threshold function  
221 that takes the thermodynamic force  $X_d$  into account. As previously stated, we consider a derivative form  
222 of the energy balance to get this threshold function *Eq.(18)b*. By using *Eq.(13)* and *Eq.(16)*, we get:

$$\frac{d w_e}{d t} = -X_d \dot{u}_d + K(u_d) u \dot{u} . \quad (20)$$

223 On the threshold, *Eq.(20)* becomes :

$$\frac{d w_e^d}{d u_d} \dot{u}_d = (-X_d + K(u_d) u_d) \dot{u}_d . \quad (21)$$

224 Then a threshold function  $F$  involving the thermodynamic force  $X_d$  and the state variables can be  
225 taken under the form :

$$F(X_d; u, u_d) = K(u_d) u - X_d - \frac{d w_e^d}{d u_d} \leq 0 . \quad (22)$$

226 To be consistent with the incremental form of the energy balance, the equality  $F(X_d; u, u_d) = 0$ , gives  
 227 once again  $u_d = u$  while the consistency condition  $dF = 0$  leads to  $du = du_d$ , or equivalently to Eq.(19).

228 To be precise, the full calculation of  $dF = 0$  at  $u = u_d$  leads to:

$$(K(u_d) + 2K'(u_d)u_d)(du - du_d) = 0, \quad (23)$$

229 then  $du = du_d$ , except possibly when  $u_d = -\frac{K(u_d)}{2K'(u_d)}$ .

### 230 2.3.4 Some comments about the damage evolution equations

231 To depict the evolution of damage, in addition to the traction-separation curve data, the literature often  
 232 proposes a specific evolution equation in the form of  $\dot{D} = \dot{D}(f, D, \dot{u})$  whatever the definition of the damage  
 233 variable  $D$  [Roe et al. 2003](#); [Bouvard et al. 2009](#); [Kuna et al. 2015](#).

234 In the foregoing, because of the hypotheses explicitly made on the energy balance (i.e. damage is  
 235 the only dissipative mechanism and it is totally dissipative), the damage evolution law is fixed by the  
 236 definition of the damage variable itself and by the explicit form of the energy balance. Note that the  
 237 damage evolution law Eq.(19) deduced from the energy criterion Eq.(18) is perfectly compatible with the  
 238 definition of the damage variable itself given in Eq.(4). We can also note that this evolution law is an  
 239 extremely simple form of the general equation proposed by [Roe et al. 2003](#), but here this law is totally  
 240 imposed by the shape of the traction-separation curve or equivalently by the threshold  $w_e^d(u_d)$  of Eq.(10)

To set ideas, let's consider the following simple case: let  $f(u)$  be a 1D traction-separation law. We suppose that the elastic energy is, as often, written as:  $\psi(u, D) = (1 - D)K_0 \frac{u^2}{2}$ , where  $D$  is the isotropic damage variable,  $u$  the displacement jump, and  $K_0$  the elastic stiffness of the virgin cohesive zone. We consider a monotonic loading. The deformation energy rate is given by definition:

$$(w_{def})^0 = f(u) \frac{du}{dt}$$

where  $f(u)$  follows the traction-separation curve. The elastic energy rate can be split in two parts:

$$(w_e)^0 = (1 - D)K_0 u \frac{du}{dt} - K_0 \frac{u^2}{2} \frac{dD}{dt}$$

If we assume now that the damage is the only irreversible mechanism, then the traction force is the conjugate variable of the displacement jump, where  $f(u) = \frac{\partial \psi(u, D)}{\partial u} = (1 - D)K_0 u$  and  $(w_e)^0 = (w_{def})^0 - K_0 \frac{u^2}{2} \frac{dD}{dt}$

If now the damage is supposed to be exclusively dissipative (no internal stored energy), then the dissipation is given by:

$$(w_d)^0 = K_0 \frac{u^2}{2} \frac{dD}{dt} = (w_{def})^0 - (w_e)^0$$

Following the traction-separation curve, the damage evolution has to verify:

$$\frac{dD}{dt} = 2 \frac{[(w_{def})^0 - (w_e)^0]}{K_0 \frac{u^2}{2}}$$

Noting that for each current point  $(u, f(u))$  of the traction separation curve, we have  $w_e = \frac{1}{2}f(u)u$ , the time derivation, following the curve, reads :

$$(w_e)^0 = \frac{1}{2}f(u) \frac{du}{dt} + \frac{1}{2} \frac{df(u)}{dt} u$$

Then,

$$\frac{dD}{dt} = \frac{f(u) \frac{du}{dt} - \frac{df(u)}{dt} u}{K_0 \frac{u^2}{2}}$$

241 The right-hand member of this equation is fully determined by the traction-separation curve. Any form of  
 242 damage evolution law, incompatible with this previous equation, would lead to an energy balance form  
 243 incompatible with the initial energy assumptions (i.e. form of the free energy, damage unique and exclusive  
 244 dissipative mechanism). The consequences could be the appearance of energy storage mechanisms, i.e.  
 245  $\dot{w}_d^d < \dot{w}_{def}^d - \dot{w}_e^d$ , or internal energy transformation into dissipated energy (release of stored energy), i.e.  
 246  $\dot{w}_d^d > \dot{w}_{def}^d - \dot{w}_e^d$ . Taking into account this stored energy variations should lead to the introduction of new  
 247 internal state variables and/or to a change of the deformation energy rate definition [Fremond 2002](#).

## 248 3 3D cohesive zone model

249 In this paragraph, we propose an extension to a 3D vectorial version of the CZM where the isotropic  
 250 damage is controlled by the evolution of the maximum recoverable elastic energy,  $w_d^e(u_d)$ . Isotropic  
 251 damage means here that a scalar state variable is solely used to describe the damage evolution. This  
 252 generalization has been made by following the same approach as the one previously proposed, namely  
 253 define a damage variable and a energy balance where the damage is the only dissipative phenomenon.

### 254 3.1 Mechanical variables

255 Regarding the mechanical description of the cohesive zone, the traction force and the separation become  
 256 now vectors. Let us introduce a frame of reference where directions 1 and 2 correspond to the tangent  
 257 plane of the cohesive zone while direction 3, is the normal direction. The traction vector,  $\mathbf{f}$ , whose  
 258 components are  $(f_{t_1}, f_{t_2}, f_n)$  and the separation vector,  $\mathbf{u}$ , which has 3 components denoted by  $(u_{t_1}, u_{t_2}, u_n)$   
 259 are introduced. As is conventionally admitted in CZM, the normal move jump denoted by  $u_n$  is positive  
 260 or null. This unilateral condition is taken into account by a Signori type relationship in the numerical  
 261 simulations, using the open source software [LMGc90 Dubois et al. 2006](#), performed at the end of this article.

### 262 3.2 Cohesive zone potential and state equations

A set of state variables has first to be chosen. Here we selected the components  $(u_{t_1}, u_{t_2}, u_n)$  of the separation vector and a scalar damage variable denoted by  $u_d$ . Then, to generalize the form of the cohesive zone potential proposed in Eq.(12), the following form, inspired by Bouvard et al. 2009, is adopted :

$$\begin{aligned}
 \psi(\mathbf{u}, u_d) &= w_e(\mathbf{u}, u_d) \\
 &= \frac{1}{2} \left( K_n(u_d)u_n^2 + K_t(u_d)u_{t_1}^2 + K_t(u_d)u_{t_2}^2 \right) , \\
 &= \frac{1}{2} K_n(u_d)(u_n^2 + \alpha u_{t_1}^2 + \alpha u_{t_2}^2) \\
 &= \frac{1}{2} K_n(u_d)u_{eq}^2
 \end{aligned} \tag{24}$$

where:

$$u_{eq} = (u_n^2 + \alpha u_{t_1}^2 + \alpha u_{t_2}^2)^{\frac{1}{2}} . \tag{25}$$

263 The parameter  $\alpha$  is the ratio between  $K_t(u_d)$ , the tangential and  $K_n(u_d)$ , the normal secant stiffnesses  
 264 at a given  $u_d$ . In the case of isotropic damage  $\alpha$  is a constant.

265 In Eq.(26), a 3D formulation of the scalar depicting the isotropic damage is given. By construction,  $u_d$   
 266 takes the 3D aspect of the separation vector  $\mathbf{u}$  into account and then  $\dot{u}_d$  is non-negative and de facto  
 267 respects the irreversibility of the damage progress.

$$u_d = \max \{ u_{eq}(\tau), \forall \tau \leq t \} . \tag{26}$$

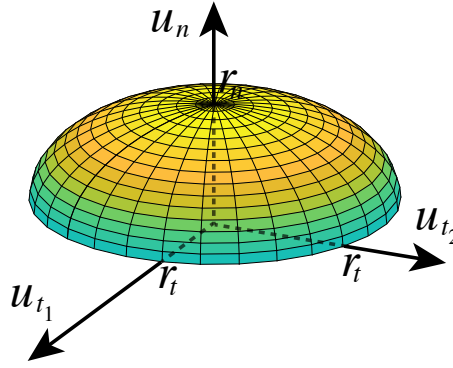
268 By definition, the state laws are the partial derivatives of the cohesive zone potential Eq.(24). They  
 269 introduce the components of the reversible traction vector  $\mathbf{f}^r$  and the conjugate variable  $A_d$  associated  
 270 with  $(u_{t_1}, u_{t_2}, u_n)$  and  $u_d$  respectively :

$$\left\{ \begin{array}{l}
 f_n^r = \frac{\partial \psi}{\partial u_n} = K_n(u_d)u_n \\
 f_{t_1}^r = \frac{\partial \psi}{\partial u_{t_1}} = \alpha K_n(u_d)u_{t_1} = K_t(u_d)u_{t_1} \\
 f_{t_2}^r = \frac{\partial \psi}{\partial u_{t_2}} = \alpha K_n(u_d)u_{t_2} = K_t(u_d)u_{t_2} \\
 A_d = \frac{\partial \psi}{\partial u_d} = \frac{1}{2} K'(u_d)u_{eq}^2
 \end{array} \right. . \tag{27}$$

271 Because only damage induces irreversibility, no dissipation has to be associated with the component of  
 272 the separation vector. The reversible part  $\mathbf{f}^r$  of the separation can therefore be identified with  $\mathbf{f}$ , then  
 273  $\mathbf{f} = \mathbf{f}^r$  .

### 274 3.2.1 Energy definition of the damage threshold

275 To extend the damage energy criterion to a 3D isotropic damageable CZM, it is possible to choose the  
 276 damage variable,  $u_d$ , whose evolution is directly related to that of the elastic energy  $w_e^d$ . In the 3D case, this  
 277 maximum elastic energy, for a given damage state  $u_d$ , describes in the displacement space a half spheroid of  
 278 radii  $r_n(u_d) = \left(\frac{2w_e^d(u_d)}{k_n(u_d)}\right)^{\frac{1}{2}}$  and  $r_t(u_d) = \left(\frac{2w_e^d(u_d)}{\alpha k_n(u_d)}\right)^{\frac{1}{2}} = \frac{r_n(u_d)}{\sqrt{\alpha}}$  as shown in Figure 4. As the normal jump  
 279 denoted  $u_n$  is by definition positive or null only half of the spheroid is reachable for any separation states.



**Figure 4:** 3D representation of the reachable separation states for a given damage state  $u_d$ . The color variation represents the value of  $u_n$ .

280 As long as the further separation states,  $\mathbf{u}$ , respect the damage energy criterion (i.e.  $w_e(\mathbf{u}, u_d) <$   
 281  $w_e^d(u_d)$ ), the behavior remains elastic. Then for a given opening such that  $u_{eq} = u_d$ , the elastic energy  
 282 reaches the maximal value associated with this damage state (i.e.  $w_e(\mathbf{u}, u_d) = w_e^d(u_d)$ ). Once the surface  
 283 of the spheroid is reached:

- 284 • either the separation increment  $\delta\mathbf{u}$  is directed towards the inside of the spheroid, and an elastic  
 285 unloading at constant damage can be observed,
- 286 • or  $\delta\mathbf{u}$  is directed towards the outside of the spheroid, and then the damage develops defining a new  
 287 elastic limit surface.

288 For isotropic damage, a single evolution equation for  $u_d$  is required. We have already underlined that for  
 289 threshold behavior law, the yield function depends on the thermodynamic forces and possibly on the states  
 290 variables themselves, acting as parameters. In the present case, the thermodynamic force of the model,  
 291 associated with the damage variable rate, is  $X_d$ . A generalized form of the yield criterion proposed in  
 292 Eq.(22) is chosen where the role of  $u$  used in the 1D scenario is played by  $u_{eq}$ . So, the proposed yield  
 293 energy criterion Eq.(17), may be rewritten using the thermodynamic force,  $X_d$  as:

$$F(X_d; u_{eq}, u_d) = K_n(u_d) u_{eq} - X_d - \frac{d w_e^d}{d u_d} \leq 0. \quad (28)$$

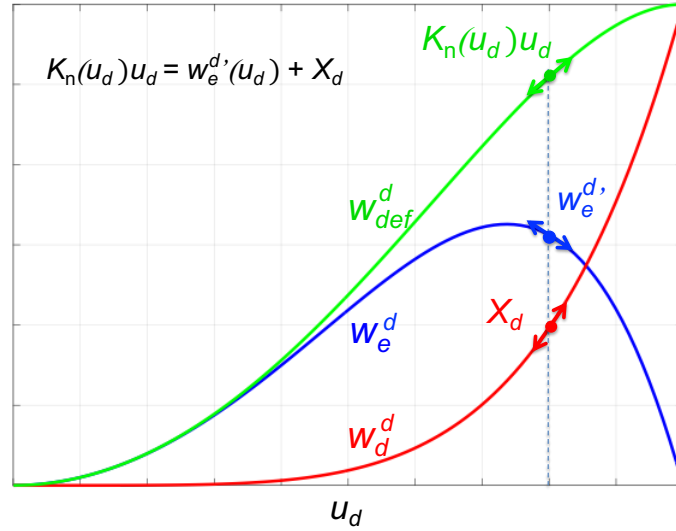
294 Damage develops if the threshold is reached,  $F(X_d; u_{eq}, u_d) = 0$  and if the consistency condition is  
 295 verified,  $\dot{F}(X_d; u_{eq}, u_d) = 0$ . For the same reasons as the ones shown for the 1D model, the evolution law of

296 the parameter  $u_d$  is written as:

$$\dot{u}_d = \dot{u}_{eq} \text{ if } u_d = u_{eq} \text{ and } \dot{u}_{eq} \geq 0, \quad (29)$$

297 results which, as already underlined, are imposed by the very definition of the damage variable.

298 An illustration of the energy criteria is given in Figure 5. Following a monotonic loading (i.e. remaining  
299 on the  $w_e^d(u_d)$  curve),  $K_n(u_d)u_d$  is the slope of the deformation energy  $w_{def}^d$ ,  $X_d$  is the slope of the  
300 dissipated energy  $w_d^d$  and  $(w_e^d)'$  is naturally the slope of the maximal allowable elastic energy  $w_e^d$ .



**Figure 5:** Illustration of the damage energy criterion -  $u_{eq} = u_d$

301 To conclude section 3, we would like to stress once more the fact that the damage evolution law is not  
302 here a matter of choice. It is imposed by the chosen form of the energy balance and by the definition of the  
303 damage state variable.

304 The state equations Eqs(27) and the evolution equation Eq.(29) will be, in what follows, implemented  
305 in a home-made finite element code. The different material parameter of the constitutive equations will be  
306 specified. In order to show the capabilities of such a CZM, two types of simulations are made here after.  
307 The first one is a bending test whose numerical results are compared with experimental one's. The second  
308 one is a Brazilian disc test whose the material is made of heterogeneous elastic grains.

## 309 4 Numerical Implementation

310 To illustrate the potentiality of the proposed model, simulations reproducing a common benchmark  
311 extracted from the literature Galvez et al. 1996 were carried out. It is important to notice that the objective  
312 of this practical comparison is simply to show the operability of the model and not to optimize its  
313 parameters in order to fit the benchmark. The numerical implementation of the previous model is then  
314 done in the code L'Gc90 based on Non-Smooth Contact Dynamics (NSCD) Moreau 1988; Jean 1999; Jean



315 et al. 2001. The NSCD method is dedicated to solving problems related to dynamic systems with unilateral  
 316 constraints. It is therefore particularly suitable for contact friction problems. It proposes a non-smooth  
 317 treatment (no compliance, no penalty) of the conditions of contact Jean 1999, which is explicit in the  
 318 definition of  $u_n$ . The way which adhesion is taken into account in this method makes it possible to  
 319 consider each point of contact as a cohesive zone. Then the mechanical behavior of the cohesive zones  
 320 may vary at any point of the spatial discretization of the problem. This relevant modeling framework was  
 321 then adopted to numerically simulate crack propagation with cohesive zone Champagne et al. 2014 .  
 322

### 323 4.1 Bending test

324 To compare the proposed model with a benchmark found in literature Galvez et al. 1996, the form of the  
 325 maximum storable elastic energy, which we remember is  $w_e^d(u_d)$ , must be specified in order to be able to  
 326 implement it in LMGC90, the open source platform <sup>1</sup> used to carry out the simulations Dubois et al. 2011.  
 327 This benchmark, illustrated Figure 6, traces the evolution of a crack in mixed mode to be followed. In the  
 328 context of this feasibility study, a simple quadratic form of  $w_e^d(u_d)$  is proposed. In what follows, we also  
 329 assumed the existence of a pure elastic domain and thus the existence of a threshold equivalent elastic  
 330 displacement  $u_{eq}^e$ , simply denoted by  $u_e$ . The maximum storable elastic energy as a function of the damage  
 331 parameter  $u_d$  simply reads:

$$w_e^d(u_d) = A(u_d - u_c)^2 + B(u_d - u_c), \text{ if } u_e \leq u_d \leq u_c \quad (30)$$

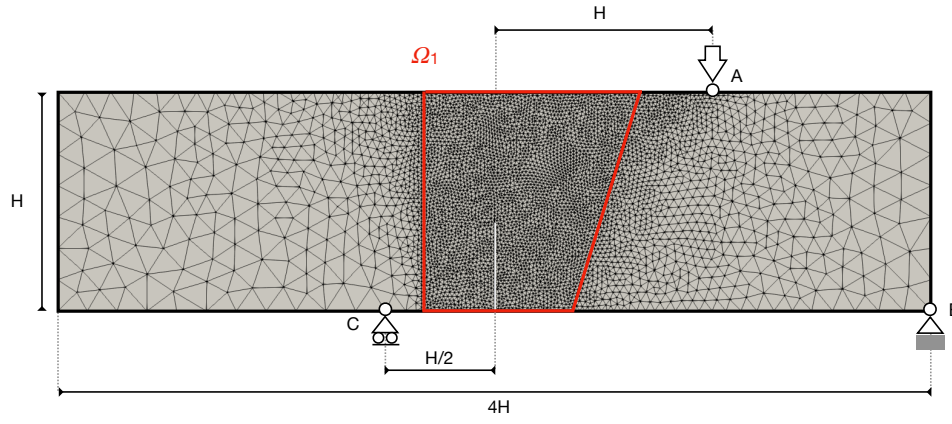
where  $u_c$  is the critical equivalent displacement corresponding to the crack onset. Parameters  $A$  and  $B$   
 are two constants chosen to ensure the  $C_1$  continuity of the maximum storable elastic energy,  $w_e^d(u_d)$ , at  
 the threshold equivalent elastic displacement,  $w_e^d(u_e) = \frac{1}{2} K_n^0 u_e^2$ . They are defined by:

$$\begin{cases} A = -\frac{1}{2} K_n^0 u_e \frac{(2u_c - u_e)}{(u_c - u_e)^2} \\ B = -K_n^0 \frac{u_c u_e}{u_c - u_e} \end{cases}, \quad (31)$$

332 where  $K_n^0$  is the initial normal stiffness of the CZM.

333 The thickness of the sample, denoted by  $H$ , is equal to 0.3 m while its length is equal to 1.2 m. A 0.15 m  
 334 pre-crack is located in the middle on the lower edge. The point B is fixed in both x and y directions  
 335 whereas the point A is only fixed in the y direction. A displacement is imposed on the point A to load  
 336 the structure. The mesh is composed of 3 parts: Two coarse meshes, the left and the right parts of the  
 337 structure composed respectively of 958 and 2 063 T3 elements, where no interface elements have been  
 338 introduced between the different meshes and a finer mesh, assuring the continuity of the structure (domain  
 339  $\Omega_1$  in Figure 6), composed of 6 723 T3 elements where the crack path is supposed to appear and where

<sup>1</sup> <https://git-xen.lmgc.univ-montp2.fr/lmgc90/>



**Figure 6:** Characteristics of the benchmark issued from Galvez et al. 1996 used for simulation

$K_n^0$ (N m <sup>-1</sup> )	$\alpha$	$u_e$ (m)	$u_c$ (m)
$2.48 \cdot 10^9$	0.5	$0.5 \cdot 10^{-6}$	$1.5 \cdot 10^{-6}$

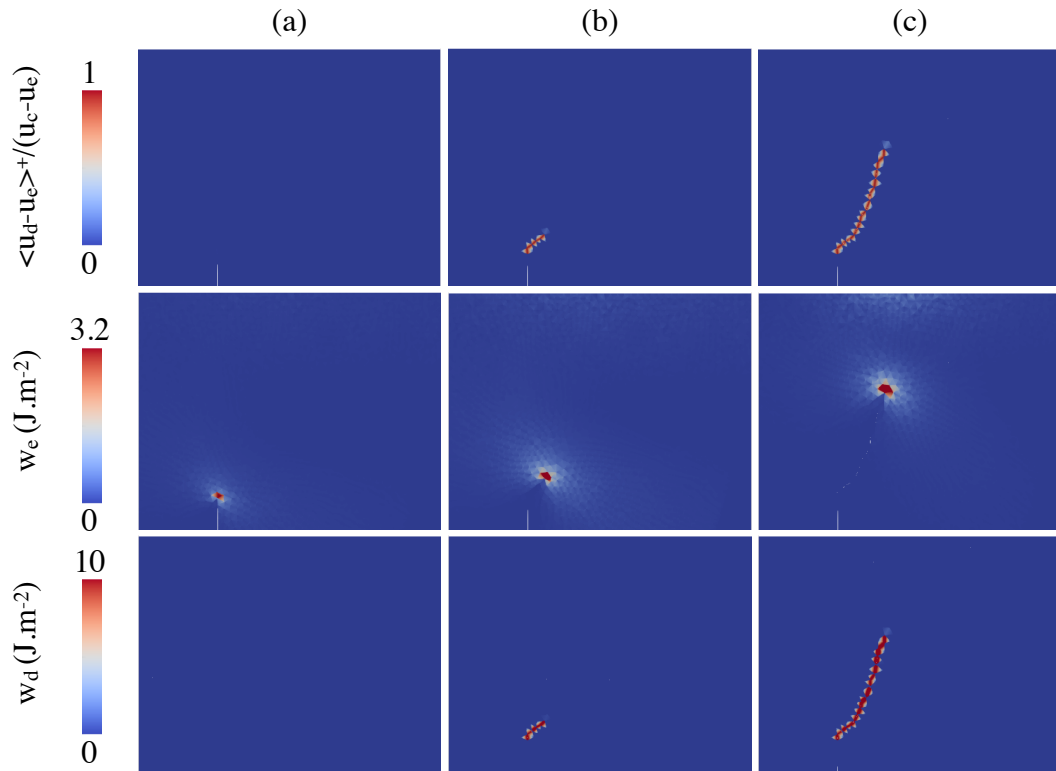
**Table 1:** Parameter values of the CZM

340 interface elements are therefore introduced between each element. The interactions between elements of  
 341  $\Omega_1$  are governed by the proposed cohesive zone model where the initial secant elastic stiffness,  $K_n^0$  and  $K_t^0$ ,  
 342 are chosen to satisfy the criterion proposed in Blal et al. 2011 to limit the reduction of stiffness due to the  
 343 presence of CZM. It is important to underline that the objective of this practical comparison is simply to  
 344 show the operability of the model and not to optimize its parameters in order to fit the benchmark. The  
 345 values of the CZM parameters are summarized in Table 1.

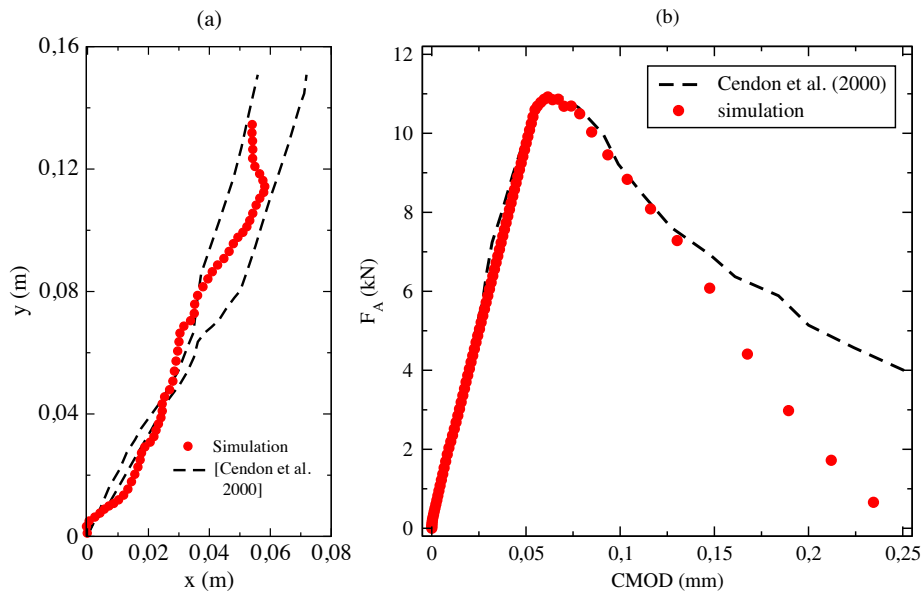
346 Figure 7 shows the evolution, for different simulation times, of different characteristic quantities  
 347 associated with the model : the damage variable, the elastic energy  $w_e$  and the dissipated energy  $w_d$ . In  
 348 order to present a quantity varying from 0 to 1 the damage ratio, as a function the damage variable, is  
 349 introduced and defined by  $\frac{\langle u_d - u_e \rangle^+}{u_c - u_e}$ . To improve the visibility of these different quantities supported by  
 350 the interfaces, they are projected on adjacent elements.

351 Figure 7(a), corresponding to a pre-cracking state, shows a concentration of the elastic energy at the  
 352 outset of the crack tip. However, the damage criterion has not been reached within the cohesive zone so  
 353 that no damage or dissipation has yet occurred (see Eq.(17)). The corresponding map to  $\frac{\langle u_d - u_e \rangle^+}{u_c - u_e}$  and  $w_d$   
 354 are then uniformly equal to 0. As expected, Figure 7 (b) and (c), corresponding to two post-cracking steps,  
 355 highlight the correlation between the evolution of the dissipated energy and the damage ratio. The elastic  
 356 energy is still concentrated ahead of the crack tip, then returns to zero along the crack lips. In contrast, the  
 357 dissipated energy related to the damage evolution can be exhibited all along the crack path. Similarly, the  
 358 damage field allows the cracking path to be tracked.

359 To exhibit the capability of our CZM where only the shape of the cohesive energy associated with a  
 360 simple energy balance is needed (cf. Eq.(30)), different quantities, numerically obtained, are compared with  
 361 experimental measurements present in the literature Cendón et al. 2000. For such comparisons, Figure 8  
 362 presents both the classical crack path monitoring and the load vs. CMOD curve (Crack Mouth Opening  
 363 Displacement).



**Figure 7:** Visualization of the damage ratio (top row), the elastic energy (center) and the dissipated energy (bottom row) during the crack propagation



**Figure 8:** Comparison of numerical macroscopic measurements associated to the crack evolution with experimental results [Cendón et al. 2000](#): a) The crack path and b) the load vs. CMOD curve.

364 In Figure 8(a) and Figure 8(b), the red dot line corresponds to the simulation result while the black  
 365 dashed lines represent the crack envelop obtained experimentally Cendón et al. 2000. In Figure 8a, the  
 366 crack obtained numerically corresponds closely to the experimental envelope. The starting angle is  
 367 strongly related to the discretization around the initiation point, explaining the slight difference at the  
 368 beginning of the initiation. Then, the path is corrected and repositioned in the experimental envelope until  
 369 the end of the simulation.

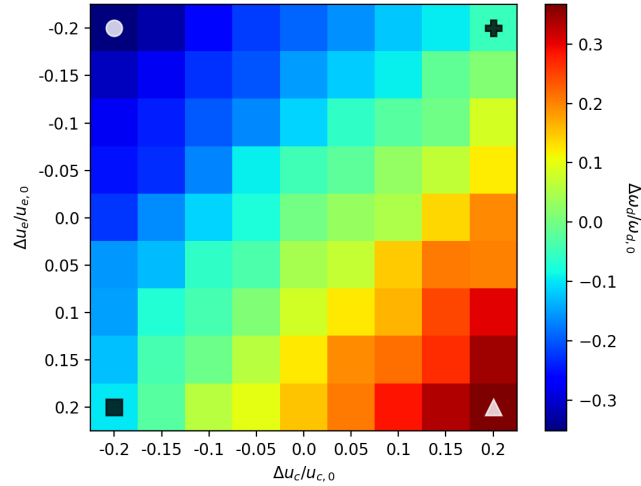
370 Concerning the force vs. CMOD curves, they fit perfectly in the section corresponding to the linear  
 371 increase. This highlight that the introduction of a 2D interface element, where the values of  $K_n^0$  and  $K_t^0$   
 372 satisfy the criterion proposed in Blal et al. 2011 between each elements of  $\Omega_1$  do not affect the global  
 373 stiffness of the sample. The maximum force obtained is also in good agreement with that obtained in the  
 374 experiment, as well as the beginning of the non-linear decreasing part of the CMOD curve occurring at the  
 375 initiation of cracking. In the last part, the curves diverge. This difference is partly explained by the fact that  
 376 the numerical simulation is two-dimensional while the experiments are three-dimensional. Indeed, not all  
 377 deformation modes are taken into account (especially out-of-plane modes), which explains this different  
 378 behavior at the end of the simulation. Moreover, we have arbitrarily chosen a 2nd degree polynomial to  
 379 characterize the damage of the cohesive zone model, Eq.(30). This choice could be fine-tuned in order to  
 380 better account for experiences by taking a Needleman-type damage, Bosch et al. 2006; Needleman 1990.

## 381 4.2 Sensitivity study

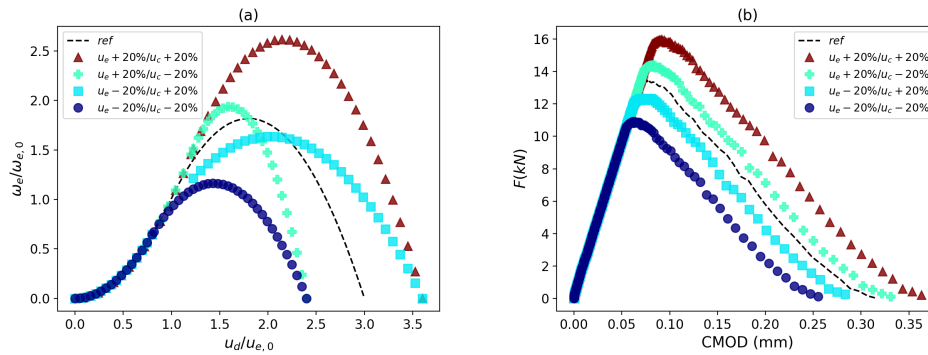
382 Finally, in order to see the impact of a variation in the parameters  $u_e$  and  $u_c$  on the overall behavior of  
 383 the system and more particularly on the evolution of the force vs. CMOD curves, a sensitivity study is  
 384 proposed. The influence of these parameters on the crack path is not presented because it is not very  
 385 significant. The influence of these parameters on the energy available to be dissipated in the model  
 386 is pointed out in Figure 9. The parametric study is carried out relative to the reference point (0, 0)  
 387 corresponding to the results presented in Figure 8(b) with the parameters define in table 1. With the chosen  
 388 law, a variation of  $u_c$  has almost the same consequence as a variation of  $u_e$  in terms of the energy available  
 389 to be dissipated. Then the map presented in Figure 9 is symmetric in the regard of the circle-triangle  
 390 diagonal. During the different parametric studies, the color code used for the curves will refer to the one  
 391 defined in Figure 9.

392 Figure 10 presents the normalized plots of  $w_e^d(u_d)$  for different values of  $u_e$  and  $u_c$  (Figure 10(a)) and the  
 393 corresponding force vs. CMOD curves (Figure 10(b)). The normalization parameters are  $u_{e,0} = 0.5 \cdot 10^{-2}$  and  
 394  $w_{e,0} = w_{e,0}^d(u_{e,0})$  using the values of parameters in Tab. 1. Even if the shape of the curves is significantly  
 395 different in Figure 10 (a), the energies available to be dissipated for the case represented by a cross and the  
 396 one represented by a square are of same order of magnitude. The maxima order observed at the scale of  
 397 the CZM models (Figure 10(a)) is conserved at the scale of the structure (Figure 10(b)).

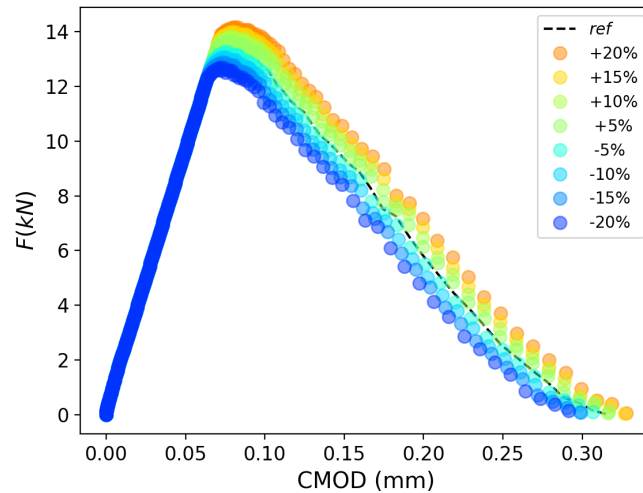
398 In Figures 11 to 13, we observe respectively the influence of  $u_c$  and  $u_e$  on the force vs. CMOD curves.  
 399 These figures show that the influence of the variation of  $u_c$  is less than that of  $u_e$ . Indeed, where we



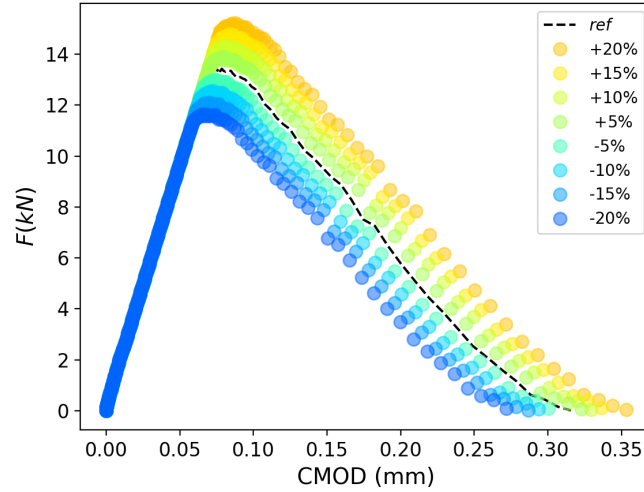
**Figure 9:** Map of the normalized dissipated energy variations as a function of the variations of  $u_e$  and  $u_c$ . The symbols used at the four corners of the map identify the curves shown in Figure 10.



**Figure 10:** (a) Normalized plots of  $w_e^d(u_d)$  for different values of  $u_e$  and  $u_c$ . The normalization parameters are  $u_{e,0} = 0.5 \cdot 10^{-2}$  and  $w_{e,0} = w_{e,0}^d(u_{e,0})$  using the values of parameters in Tab.1. (b) Corresponding force vs. CMOD curves.

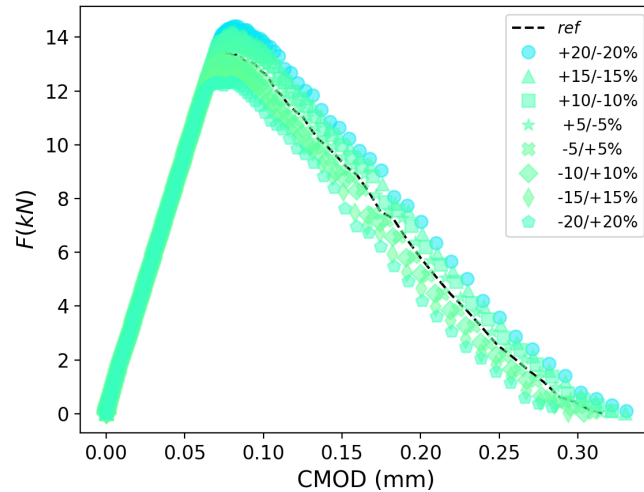


**Figure 11:** Comparison between the reference Load vs. CMOD curve (dash line) and the ones related to the variation of  $u_c$  of  $\pm 20\%$  while  $u_e$  constant.



**Figure 12:** Comparison between the reference Load vs. CMOD curve (dash line) and the ones related to the variation of  $u_e$  of  $\pm 20\%$  while  $u_c$  constant.

400 observe for a variation of  $u_c$  a variation of less than 10% on the critical values of the curve ( $F_{max}$  and  
 401  $CMOD_{max}$ ), while a variation of more than 20% for an equivalent variation of  $u_e$  is observed. Nevertheless,  
 402 in both cases, an increase of the damage energy  $w_d$  induces an increase of the CMOD and loading maxima  
 403 in the Load vs. CMOD curve. In this model where an elastic domain is assumed,  $u_e$  is the threshold where  
 404 the damage begins to occur. This value determines the outset of the non-linear response of the structure.  
 405 This is exhibited in Figure 12 where an increase of  $u_e$  at the local scale induces an increase of the maximal  
 406 force at the macroscopic scale and a delay of the occurrence of the nonlinear response of the curves.



**Figure 13:** Comparison between the reference Load vs. CMOD curve (dash line) and the ones related to the variation of  $u_c$  and  $u_e$  of  $\pm 20\%$  while  $w_d^0$  is constant.

407 Figure 13 demonstrates that the non-linear region of the curve is also governed by the shape of the  
 408 energy curve (cf. Figure 10). Although the dissipative energy in this parametric study is almost constant,  
 409 we observe a variation of about 10% on the characteristic values of the response curve. So by combining  
 410 the effects of  $u_e$ ,  $u_c$  and the shape of the local curve (cf. Figure 10) it is possible to obtain a better optimal

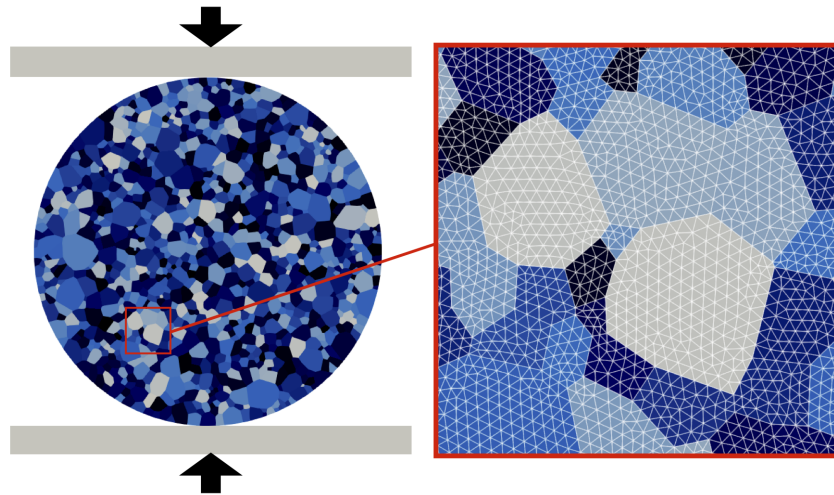
$K_n^0$ (N m <sup>-1</sup> )	$\alpha$	$u_e$ (m)	$u_c$ (m)
$2.48 \cdot 10^{15}$	0.4	$0.8 \cdot 10^{-6}$	$1.0 \cdot 10^{-6}$

**Table 2:** Parameter values of the CZM

411 result to fit experiments. Thus the experimental characterization of this type of local curve depicting the  
 412 micro-structural phenomenon linked to fracture is relevant and is still an ongoing problem.

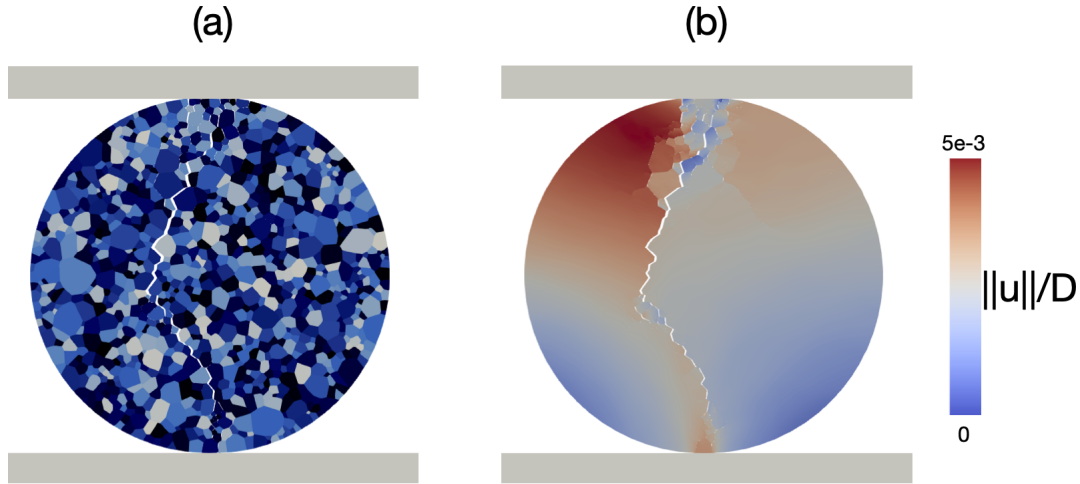
### 413 4.3 Brazilian test

414 As a complement to the previous numerical simulation and as an opening to the continuation of the  
 415 present work, the developed CZM law is used in the simulation of a Brazilian test. This test consists  
 416 of compressing a circular sample located between two rigid plates. Contrary to the previous case, no  
 417 pre-crack is introduced in the numerical model. The microstructure of the sample used is presented on the  
 418 left side of Figure 14. This microstructure has been generated using the open-source Software Neper  
 419 [Quey et al. 2011](#). It is composed of 1 000 elastic grains following a normal size distribution to make the  
 420 microstructure heterogeneous [Ma et al. 2018](#). In these case, the cohesive zones are only introduced at the  
 421 grain boundaries. The mesh size used for meshing is identical for all grains and calibrated so that the  
 422 smallest grains have at least two elements on their smallest side. The total number of elements is 98 378. A  
 423 zoom of the mesh is shown on the right hand side of Figure 14. For the sake of simplicity the diameter of  
 424 the sample is unitary. A vertical velocity is imposed on both walls to compress the sample. The simulation  
 425 is carried out in large deformations in order to manage possible strain localisation and grain rotations. The  
 426 elastic constitutive equations are those of the linear elasticity where stresses and strains are respectively  
 427 represented by the 2<sup>nd</sup>e Piola-Kirchoff stress tensor and the Green-Lagrange strain tensor.

**Figure 14:** Visulation of the meshed microstructure used in the simulation of the Brazilaian disc test

428 For homogeneous material during Brazilian test a tensile state is induced in the center of the disc  
 429 perpendicular to the load direction. Increasing the load leads to an increase in tensile stress until a crack  
 430 appears in the center of the disc. Under the effect of the load, the crack develops until the disc eventually  
 431 separates into at least two parts. For a heterogeneous material the damage occurs near the rigid plates and

432 then develops along the loading axis until the disk breaks [Na et al. 2017](#). Figure 15 shows a visual of the  
 433 sample at the end of the simulation.



**Figure 15:** Final state of the simulation: Visualization of a) the crack through the microstructure and b) the norm of displacement field normalized by the value,  $D$ , of the diameter within the sample.

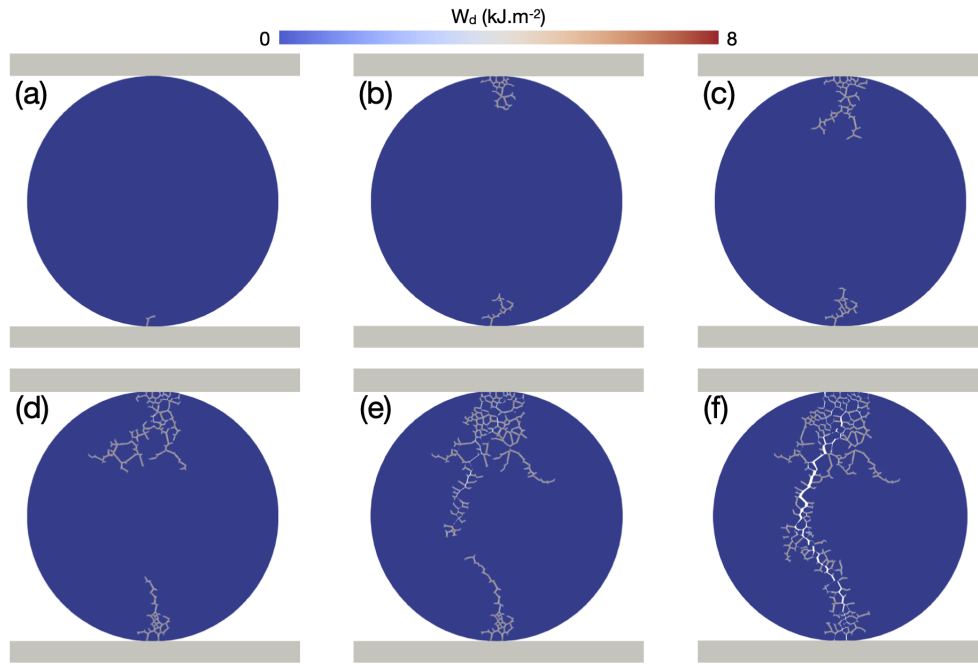
434 Figure 15(a) shows the macro crack zigzagging through the microstructure. This extends from the  
 435 contact between the sample and the rigid plates away from the centre of the sample. Figure 15(b) shows  
 436 the norm of the adimensionalized displacement field within the sample. The discontinuities within this  
 437 field allow the observation of multiple cracking paths generated during compression. Numerous disjointed  
 438 fragments can be particularly seen in the volume near the top wall.

439 To complete these observations, the evolution of the dissipated energy fields is presented in Figure 16.  
 440 The image (a) corresponds to the initiation of the crack while the image (f) corresponds to the end of the  
 441 simulation. The other images are captured at intermediate times. Through the figures 16 (a) to (f) the  
 442 damage evolution is exhibited where branching is observed until the coalescence of the macro crack.  
 443 The next step is to experimentally perform the same type of test using an experimental setup coupling  
 444 kinematic and thermal full-field measurements. The kinematic measurements will allow us to locate zones  
 445 of strain localization and even discontinuities of the displacement fields while the thermal measurements  
 446 will be used to determine the zones where the dissipation is localized. The confrontation of this two  
 447 informations should help us to check the relevance of this energy approach of cohesive zones.

## 448 5 Conclusion

449 In this paper we present an energy criterion for cohesive zone models where the damage progress is  
 450 assessed together with the ability of the material to store energy elastically. The damage parameter used  
 451 is  $u_d(t) = \text{Sup} \{u_{eq}(\tau), \tau \leq t\}$  where  $u_{eq}$  is an equivalent displacement compatible with the isotropic  
 452 evolution of the damage progress. The paper shows that if damage is the unique and exclusive dissipative  
 453 mechanisms, the damage evolution law is automatically fixed by the evolution of the maximum storable  
 454 elastic energy  $w_e^d(u_d)$ . We have also underlined that the data of this energy is equivalent in a 1D formalism





**Figure 16:** Evolution of the dissipated energy field from the crack initiation (a) to the end of simulation (f).

455 to the one of a traction-separation law. The interest of this energy approach is its immediate generalization  
 456 to 3D cohesive zone models. In order to check the operational character of this type of approach, the  
 457 isotropic damage model has been implemented in the open source software L<sup>3</sup>Gc90 based on Non-Smooth  
 458 Contact Dynamics (NSCD) and used to perform numerical simulations in the case of bending and Brazilian  
 459 tests. The results obtained for this plain stress modeling are encouraging. Using a simple quadratic function  
 460  $w_e^d(u_d)$  for the interface, we obtained a close correlation between the simulations and the experimental  
 461 observations of the crack path for the bending test, and realistic multicrack propagations in the case of the  
 462 Brazilian test. A parametric study of the macroscopic response of the structure naturally demonstrates the  
 463 importance of the shape of the function  $w_e^d(u_d)$  which characterize the interface behavior between two  
 464 elements. It is indeed this quantity that we will have to identify experimentally. In subsequent theoretical  
 465 developments, first we will consider an extension to a non isotropic degradation of the material elastic  
 466 properties. From an experimental stand point Brazilain test will be performed by using full field techniques  
 467 during monotonic loadings, the goal being to extract from the experimental data valuable information on  
 468 the form of the energy balance and particularly on  $w_e^d(u_d)$ .

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