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## Long-term Unit Commitment Problem with Optimal Zone Configuration: a Case Study in Martinique

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## Disclaimer

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### I. Introduction

Island regions are not interconnected with the mainland and the isolation of these regions has brought challenges to the electric power systems. For instance, the power grids in island regions are more fragile to the rapid variance of the electricity consumption or production than the continental grid. Meanwhile, more intermittent renewable energy, such as wind and solar, has been connected to the power grid. Some of the overseas territories of France are island territories in the Atlantic, Pacific and Indian Oceans.

In this work, we propose a long-term unit commitment (UC) model with simplified network (zone) constraints to apply in these areas.

One of the main purposes of this work is to examine whether a better zonal configuration could help to increase the performance of the long-term UC model. Also, by applying this long-term UC model, we can create a robust generation plan for these territories and would be able to test, for instance, whether a larger amount of renewable energy could be introduced in these areas and whether the performance of the system could be improving by constructing a new transmission line.

#### II. Method

The method is made of four steps (Fig. 1). The first step is to simulate short-term market outcomes by using an economic dispatch model with a detailed nodal network. We consider different levels of load and renewable generation. This nodal network model considers both the network and economic constraints, therefore, the solution provides price signals to optimally utilize the available resources. The second step is to find the optimal zonal configuration. The price signals given by the first step are used to decide the zonal configurations. The similarity of prices for interconnected nodes implies a lower degree of congestion. We cluster nodes with similar prices into one zone. The third step is to decide the simplified network constraints for the long-term unit commitment. There are two

different sets of simplified network constraints which could be applied in the longterm unit commitment problem, i.e., net transmission capacity (NTC) and flowbased market coupling (FBMC). In this study, we use the NTC network constraints for our study. The simplified network constraints are mainly to limit the power exchange between two zones and reduce the network congestion in real time. The fourth step is to apply the simplified network constraint in the long-term unit commitment problem.



Figure 1: Overview of the method

## 1. Step 1: Nodal economic dispatch model

The nodal economic dispatch model uses an optimal power flow approach, which takes into account the physical and technical constraints [23], to give the price of power for each node. Most power systems are alternating current (AC) and the problem that we ideally would like to solve is an alternating current optimal power flow (AC-OPF) problem. This is a difficult problem to solve, due to non-linearities and non-convexities. Thus, in practice, most of system operators us a lossless direct current (DC) approximation is used. The resulting problem is called direct current optimal power flow (DC-OPF). This approximation has been proved to efficiently approximate the real network [19]. The nodal economic dispatch model is an optimization problem given by,

$$\underset{G}{Min}\sum_{c}cg_{c}\times G_{c} \tag{1}$$

Subject to:

$$NI_n = \sum_{c \in C_n} G_{c,} + gwind_n + gsolar_n + gbio_n - Q_n, \forall n$$
<sup>(2)</sup>

$$G_c \le gmax_c, \forall c \in C \tag{3}$$

$$LF_{n,nn} = bvector_{n,nn} \left(\Delta_n - \Delta_{nn}\right), \forall n, nn$$
(4)

$$NI_n = \sum_{nn} LF_{n,nn} - \sum_{nn} LF_{nn,n}, \forall n$$
(5)

$$-pmax_{n,nn} \times St_{n,nn} \le LF_{n,nn} \le pmax_{n,nn} \times St_{n,nn}, \forall n, nn$$
(6)

$$\Delta_{n'} = 0, n' = slackbus \tag{7}$$

$$G_c \ge 0, Q_n \ge 0 \tag{8}$$

Where  $G_c$  is the generation of power plant c,  $NI_n$  is net injection of node n, and  $St_{n,nn}$  is the binary variable, 0 indicating the transmission line on an off statue and 1 indicating an on statue.

The objective of the nodal pricing model is to minimize the operation cost (Eq. (1)), considering the various constraints. The areas applying nodal pricing are constrained by the energy balance (Eq. (2)), the maximum generation capacity of thermal power plants (Eq. (3)), and the restrictions on power transmission (Eq. (4)-(6)). The energy balance (Eq. (2)) ensures that at node n, net input or withdrawal  $NI_n$  is equal to the difference between power generation (including all the conventional power generation  $G_c$  at node n, wind generation  $gwind_n$ , solar generation  $gsolar_n$  and biomass generation  $gbio_n$ ) and nodal demand  $Q_n$ . The generation of renewable is given exogenously. The dual variables of Eq. (2), which are the marginal costs/benefits of increasing injections in the nodes by one unit, are the nodal prices. Thermal power generation is restricted by the maximum generation requirement gmax<sub>c</sub> (Eq. (3)). The DC approximation (see [6] and [22]) is used to determine the load flows  $LF_{n,nn}$  (Eq. (4)) in each line and the resulting

injection or withdrawal  $NI_n$  (Eq. (5)). Eq. (6) is to ensure that the load flow over a line should not exceed its thermal capacity limit.  $St_{n,nn}$  describes the status of a line (on or off). It is used to enforce the N-1 security constraint. Under this constraint, the failure of a single power line should not cause power outages. Enforcing the N-1 constraint improves security, however, might at a cost. Eq. (7) is to specify the slack bus. Eq. (8) requires the generation and the demand to be positive.

### 2. Step 2: Zonal clustering

The zonal clustering algorithm groups nodes into a pre-defined number of zones. Generally, it is required that there is not much intra-zonal congestion and that nodes within a zone should have a similar impact on inter-zonal lines. Different clustering algorithms have been proposed in the literature. The two most used are the nodal pricing method [5] - [6] and nodal Power Transfer Distribution Factors (nodal PTDFs) method [16].

The capacity limitation of the transmission network prevents full uses the cheapest energy in the network, i.e., there is no enough capacity to transfer the power from the cheapest places to other places. The price at each node is also decided by the network topology and energy location. Nodal prices differences indicate the level of grid congestion. Less prices differences between nodes mean less congestion. Therefore, the clustering of nodes with similar nodal prices will result in a low intra-zonal congestion zone configuration.

The nodal PTDFs quantifies how the power injection at a given node impacts a given line. The nodal PTDF-values based method takes the congested lines as inter-zonal line, and clusters nodes with similar PTDF-values for the congested lines within the same zone. In this way, a zonal configuration is obtained with low intra-zonal congestion and nodes within the same zone have a similar impact on the interzonal links.

In this work, we apply the nodal pricing method to group the nodes into a zone. However, we also consider the bottlenecks (i.e., the most congested lines) in the systems. That is, we identify the bottlenecks and set them as the inter-zonal lines before we group the nodes with similar prices. The zonal clustering is an optimization problem given by,

Minimize:

$$Min\sum_{n}\sum_{z}(p_{n}m_{n,z}-c_{k}m_{n,z})^{2}$$
(9)

Subject to:

$$\sum_{z} m_{n,z} = 1 \forall n \tag{10}$$

$$\sum_{n} m_{n,z} \ge Z N_z \,\,\forall z \tag{11}$$

$$c_z \sum_n m_{n,z} = \sum_n (p_n m_{n,z}) \,\forall z \tag{12}$$

$$aa_{n,z}(\sum_{n} m_{n,z} - 1) \le 10000m_{n,z}(\sum_{n} m_{n,z} - 1) \,\forall n, z$$
(13)

$$aa_{n,z}(\sum_{n} m_{n,z} - 1) \ge [1 - 10000(1 - m_{n,z})](\sum_{n} m_{n,z} - 1) \,\forall n, z$$
(14)

$$aa_{n,z} = \sum_{nn} link_{n,nn} \times m_{nn,z} \times m_{n,z}, \ \forall n \neq nn$$
(15)

Where  $m_{n,z}$  is a binary variable.  $m_{n,z} = 1$  indicates that the node *n* is within zone *z* while  $m_{n,z} = 0$  indicates node *n* is not in zone *z*.  $aa_{n,z}$  is the total number of connections with the other nodes within the same zone *z* for node n.  $c_z$  is the average price for zone *z*.

The objective of the clustering technique is to minimize the price differences within the same zone (Eq. (9)). Eq. (10) is to force each node to only belong to one zone. Eq. (11) is to enforce that each zone has at least  $ZN_z$  node (e.g., 1 or 2 nodes). Eq. (12) defines the average price  $c_k$  in zone z. Eq. (13) and (14) are to enforce that any node should have at least one connection with another node within the same zone if the number of nodes in a zone is greater than 1. Eq. (15) is to calculate the total number of connections with the other nodes within the

same zone, where  $link_{n,nn}$  is the connecting matrix, which tells if there is a direct connecting between two nodes *n* and *nn*.

### **Step 3: Optimal zonal parameters**

This section gives the procedure for implementing the NTC constraints. They are given by,

$$NEX_{z} = \sum_{zz} (BEX_{z,zz} - BEX_{zz,z}), \forall z \in [1, Z]$$
(16)

$$0 \le BEX_{z,zz} \le ntc_{z,zz}, \forall z, zz \tag{17}$$

Where NEX<sub>z</sub> is the net position of a zone and  $BEX_{z,zz}$  is total export from zone z to zone zz.

NEX<sub>z</sub> is defined as the difference of its total export  $BEX_{z,zz}$  and import  $BEX_{zz,z}$ (Eq. (20)). The NTC model does not have specific limitations on specified lines. However, it restricts the total transfer  $BEX_{z,zz}$  between two pricing areas to a predefined maximum trading volume  $ntc_{z,zz}$ , (Eq. (21)).

#### 3. Step 4: Long-term unit commitment (UC) model

For power system operation, one of the most important issue is to decide for each period which generating units should run to satisfy the demand. In a typical electrical system, there are a variety of resource and power plants available for generating electricity, and each of these units has its own characteristic. For instance, the start-up cost and the variable cost are different. Unit commitment problem is to help to make decisions in such a situation [21][24].

Unit commitment is one of the classic optimization problems in power systems. The goal is to decide the ON/OFF status of all the generating units, which meet the forecasted loads and reserve requirements and provide a least-cost power generation plan. There are two main ways of defining this least-cost objective function. The first one is used by TSO, which minimize the total cost (i.e., minimizing fuel costs and startup/shutdown cost) or maximize the social welfare while meeting a forecasted hourly load. The second way is used by the generation companies, which maximize the total profit based on their bidding strategy. In this study, we focus on the first type.

Different mathematical formulations of the UC problem exist. One of the most used formulations of UC problems is the mixed integer linear programming (MILP) methods. Due to fact that there could be thousands of generation units and transmission lines existing in a system, the unit commitment problem modeled by MILP could be a computationally challenging problem with many integer variables and constraints. Different optimization techniques including Lagrangian relaxation and branch-and-bound based MILP methods have been used to solve large-scale UC problems [1], [12].

The physical conditions of the operating generators are the main constraints for the UC model, including the generation capacity limits, minimum ON time, minimum OFF time, ramp up/down rate, reserve requirements. In the following, we will illustrate the typical constraints in a UC model used in this project. More UC constraints could be found on [14].

$$\min \sum_{c} \sum_{t} (st_{c} \times V_{ct} + sd_{c} \times W_{ct}) + \sum_{c} \sum_{t} (cg_{c} \times G_{c,t}) + VOLL \times \sum_{c} \sum_{t} LS_{c,t}$$
(18)

$$U_{c,t} - U_{c,t-1} \le U_{c,\tau} \forall c, t, \tau = t, ..., \min\{t + \min(r_c - 1, |T|)\}$$
(19)

$$U_{c,t-1} - U_{c,t} \le 1 - U_{c,\tau} \,\,\forall c, t, \tau = t, \dots, \min\{t + \min\{r_c - 1, |T|\}$$
(20)

$$V_{c,t} \ge U_{c,t} - U_{c,t-1} \,\forall c,t \tag{21}$$

$$W_{c,t} \ge -U_{c,t} + U_{c,t-1} \,\forall c,t$$
 (22)

$$gmax_c \times U_{c,t} \le G_{c,t} \le gmin_c \times U_{c,t}, \forall g, t$$
(23)

$$G_c \ge 0 \tag{24}$$

$$-rdown_c \le G_{c,t} - G_{c,t-1} \le rup_c \tag{25}$$

$$0 \le S_{c,t} \le s_c^{max} \tag{26}$$

$$\sum_{c} S_{c,t} \ge r s_{i,t} \tag{27}$$

Where  $U_{c,t}$ ,  $V_{c,t}$ ,  $W_{c,t}$  are binary value.  $U_{c,t}$  is the on/off status of the power plant c at time t,  $V_{c,t}$  is the startup action and  $W_{c,t}$  is the shutdown action.  $G_{c,t}$  is the generation of plant c at time t, and  $S_{c,t}$  represents the partial online generating capacity or off-line generation resources.

Eq. (22) is the UC objective function, which is composed of two component costs. The first component cost is determined by the startup  $V_{ct}$  decision and shutdown decision  $W_{ct}$  on each generator ( $st_c$  is the startup cost and  $sd_c$  is the shutdown cost). The second component cost comes is primarily made up of fuel cost  $cg_c$ and possible unserved energy penalty *VOLL* (i.e., load loss  $LS_{c,t}$ ). This penalty is usually used to avoid the load-shedding, where scheduled generators are not able to satisfy demands.

Based on two status of a generator  $U_c$ , we can know that when a generator is online and commits to supply capacity, i.e.,  $U_c = 1$  and when the generator commitment status is in an "off" state, i.e.,  $U_c = 0$ , the power dispatch level become zero and has no any operational cost.

Some specific operations are also enforce in the UC constraints, such as the minimum ON time, i.e., minion<sub>c</sub> and minimum OFF time, i.e., minioff<sub>c</sub>, and also specify startup action and shutdown action on each unit at a time period t, respectively. A generator can't be started up or shut down arbitrarily in consecutive hours, Eq (23) and (24) respectively indicate two generator's requirements: the shortest ON duration has to be met before a generator being shut

down and the shortest OFF duration is also required before a generator being restarted up.

The startup action  $V_{c,t}$  and the shutdown action  $W_{c,t}$  are determined by the generator commitment statuses in the previous time period t – 1 and the current time period t, as in Eq. (25) and (26). Any operational actions can incur start-up or shut-down costs, which are considered in the objective function.

A generator output in an hour is subject to the maximum generation limit  $gmax_c$ , and the minimum generation limit  $gmin_c$ ,. When a generator is scheduled online ( $U_{c,t} = 1$ ), the generation capacity is active giving bounds on dispatch level, shown in Eq. (27); otherwise, a generator output is forced to zero. The generation must be positive Eq. (28).

In addition, a generator output can be adjusted, increasing  $rup_c$  or decreasing  $rdown_c$  between two successive time periods. The generation difference between two adjacent time periods is called ramping. A basic constraint to address generation ramping is presented in Eq (29).

Operating reserve is one type of ancillary operations to support the power balance on the demand sides. The current operating reserve services being offered in electric energy markets include synchronous or non-synchronous, regulation reserves, spinning reserves, and non-spinning reserves. Generally, the sources of energy provided from different reserve services are different: regulation service mainly supplied from online generators, partial spinning reserve provided from generators already connected to the grid or system resources, and non-spinning reserve provided from quick-start generators, system resources or interruptible loads. The response times of reserve services can vary greatly, depending on the control reserve deployment time. To achieve the optimization of energy and reserve in practice, one can obtain an efficient energy and reserve offering strategy by Heuristic method [18] or consider the reserve determination on precontingency and post-contingency conditions [4].

In our models, if we consider the spinning reserve problem, the spinning reserve  $S_{c,t}$  is generally accounted for partial online generating capacity or off-line generation resources. Their outputs are constrained by predetermined maximum spin reserve  $s_c^{max}$ , shown as Eq. (30).

Meanwhile, the generators that participate in biding spinning reserve must meet the spin reserve requirements given by TSOs. Eq (31) describes an operating condition that the total spinning reserve at bus i should not less than the fixed reserve requirement  $rs_{i,t}$ .

#### III. Case study

### 1. Presentation

We apply the method described in the section II to the power network of Martinique. Martinique is an island in the Caribbean Sea and is an overseas department of France. Martinique has a tropical and humid climate with an average temperature of 23 degrees to 29 degrees Celsius. The average monthly temperatures remain remarkably stable, varying by only a few degrees year-round. Therefore, the power demand is also very stable during the year.

In Martinique, the main renewable energy resource is solar energy (about 15 %). They also have little share of biomass and wind energy (less than 5 %) [31]. Currently, the system operator limits that the maximum share of intermittent renewable energies that can be injected into the network at a given time to 35% [31]. Beyond this threshold, disconnections are possible in order to preserve the stability of the electrical system. However, the system operator is considering relaxing this restriction. Figure 1 shows a typical generation curve in Martinique. In a normal day, there are two types of peak hours. The first peak hours are in the negative (10 h- 14 h) with solar power. The second peak hours are in the nighttime

18 h- 20 h) without solar power. As congestion happens mostly during the peak hours, we mostly focus in these periods in this work, especially in the first two-steps model.



Figure 2: Generation curve from Monday 22nd to Sunday28th, Oct. 2018. [source: opendata-martinique.edf.fr]

## 2. Results of step 1

We only consider the HTB grid (63 kV) in Martinique, as shown in Figure 3. In total, there are 14 hubs (nodes) and 25 HTB transmission lines. The thermal power plants are located at the nodes "Bellefontaine", "Hydrobase" and "Galion".

We choose four typical hours in the working days for our first two steps analysis as show in Table 1, which includes two peak hours and two off-peak hours with different solar generation.



Figure 3:HTB power network in Martinique [source: opendata-martinique.edf.fr]

	Peak hours		<b>Off-Peak hours</b>	
	With	Without	With	Without
	solar	solar	solar	solar
Reference load	210 MW		180 MW	
Wind generation	0.5 MW	0.5 MW	0.5 MW	0.5 MW
Solar generation	30 MW	0 MW	30 MW	0 MW
<b>Biomass generation</b>	0.4 MW	0.4 MW	0.4 MW	0.4 MW

Table 1: Reference load and generation for the case study

Note that the N-1 constraint might affect the optimal dispatch. For instance, different prices and quantities of power produced would be given even it is the same reference load and generation profiles. Even more, the bottleneck in the system might also be changed when different transmission lines are disable.

	Peak	hours	Off-Pea	lk hours
AC lines	With color	Without	With color	Without
AC IIIles	with solar	Solar	with solar	Solar
FL_LAMENTIN1	42 %	45 %	39 %	42 %
FL_LAMENTIN2	42 %	45 %	39 %	42 %
BF_SCHOELCHER1	49 %	60 %	47 %	54 %
BF_SCHOELCHER2	49 %	60 %	47 %	54 %
BF_ST_PIERRE	11 %	15 %	9 %	12 %
BF_FOND_LAILLET1	-28 %	-34 %	-26 %	-30 %
BF_FOND_LAILLET2	-28 %	-34 %	-26 %	-30 %
DESBROSSES_DILLON	61%	60%	64%	58%
DESBROSSES_SCHOELCHER	-85%	-84%	-84%	-78%
DILLON_HYDROBASE1	-22%	-23%	-10%	-21%
DILLON_HYDROBASE2	-22%	-23%	-10%	-21%
DILLON_HYDROBASE3	-25%	-27%	-12%	-24%
DILLON_LAMENTIN1	10%	11%	6%	10%
DILLON_LAMENTIN3	21%	23%	12%	22%
DILLON_LAMENTIN4	21%	23%	12%	22%
GALION_LAMENTIN	-47%	-45%	-29%	-53%
GALION_FRANCOIS	-9%	-7%	0%	-17%
GALION_TRINITE1	31%	43%	25%	37%
GALION_TRINITE2	32%	45%	26%	38%
LAMENTIN_FRANCOIS	39%	39%	30%	39%
LAMENTIN_PETIT_BOURG1	40%	40%	34%	35%
LAMENTIN_PETIT_BOURG2	40%	40%	34%	35%
FRANCOIS_MARIN	23%	24%	21%	19%
MARIGOT_TRINITE	-14%	-14%	-12%	-12%
MARIN_PETIT_BOURG	-25%	-26%	-21%	-23%

Table 2: Average utilization rate of the transmission lines

Data for the four study hours are used as input to run the first steps model. The utilization rate (i.e., the actual power flow divided by the line nominal capacity) of the AC transmission line is good indicator to check the bottlenecks in the system. Table 2 gives the average utilization rate under the N-1 constraints for the four different study hours. The transmission line between the "Desbrosses" and "Schoelcher" nodes has the highest utilization rate. The utilization rate for this transmission line is more that 80 % except for the off-peak hour without solar power (78 %). Therefore, we consider this transmission line to be the

bottleneck in the system. For the other transmission lines, the utilization rates generally are less than 60 %, therefore, they are not considered as the bottlenecks in the system for our analysis.

Finally, the average nodal prices given by the economic dispatch model are summarized in Table 3.

	Peak hours		Off-Peak hours	
Node	With solar	Without Solar	With solar	Without Solar
Saint Pierre	148.02	148.01	146.10	154.33
FL	148.06	148.06	146.10	154.33
Bellefontaine	148.02	148.01	146.10	154.33
Schoelcher	146.79	148.21	145.89	155.93
Desbrosses	160.26	162.27	147.39	157.05
Dillon	157.54	159.10	147.22	156.56
Hydrobase	157.54	159.10	147.22	156.56
Lamentin	156.76	158.21	147.18	156.44
Petit Bourg	156.76	158.25	147.18	156.44
Marin	156.76	158.39	147.18	156.44
François	156.76	158.56	147.18	156.44
Galion	156.76	158.67	147.18	156.44
Trinité	156.76	158.67	147.18	156.44
Marigot	156.76	158.67	147.18	156.44

Table 3: Average nodal prices (EUR/MWh)<sup>1</sup>

# 3. Results of Step 2

Here, we cluster the nodes with similar nodal prices into zones, while excluding the bottleneck from them.

For nodes Lamentin, Petit Bourg, Marin, François, Galion, Trinité, Marigot, the nodal price differences for these nodes are less than 1% (Table 3). This means that there is no congestion between theses nodes. Therefore, it is reasonable that these nodes are grouped into a zone. The other nodes could be grouped into two

<sup>&</sup>lt;sup>1</sup> The average prices here exclude the case when load shedding is enforced in the model. The average prices here are lower than the price in realities. This is because that we don't consider the startup cost in the first step model and assume all the power in the network are available.

or three zones, depending on the clustering criteria, i.e., whether a zone can only include a single node. Figure 4 gives two proposed zonal configurations. The 3-zone configuration requires that there should be at least 2 nodes within the same zone (Eq. (11)), while the 4-zone configuration allows for zones with a single node. The objective value for the clustering model, as showed in *Table 4*, will be improved if we allow there is only one node in a zone, as show on the right hand side of Figure 4. Larger improvement could be found in the cases with high peak hours.



Figure 4: Proposed zonal configurations. The bottleneck is shown in blue.

	Pea	k hours	Off-P	eak hours
	With solar Without Solar		With solar	Without Solar
Case I:3-zone	106	114	13	1
Case II:4-zone	5	7	11	0

Table 4: Objective values for Step 2

### 4. Results of step 3

It is difficult to decide the NTC value accurately for the long-term UC problem. One possible way is to use the solution provided by the nodal pricing as a benchmark. The NTC constraints are used in the European day-head market, which sets a limitation on the commercial power exchanges among countries. An ideal NTC value in this case should allow the maximum utilization of the network. However, due to the loop flow effect, the real time dispatching given by the dayahead model might overload the lines and therefore, needs to be rescheduled. This rescheduling is also called re-dispatching or counter trading. One of the reasons for re-rescheduling is that the NTC model does not consider the limitation of the network constraints within a zone. It is important to point out that re-dispatching will lead to an extra cost.

However, the purpose of our cases study is not to increase the power exchange among zones, but to increase the efficiency of the whole system. Many studies show that nodal pricing model is consider to give a better result than NTC model. This has been proved by a large stream of literatures [13][15]. Therefore, we use the nodal economic dispatch model solution to calculate the NTC value.

Most congestion happens in the peak hours. NTC can limit the exchange in those hours and therefore could decrease the need for re-dispatching. In the off-peak hours, we could have less restriction because most of time, there is no or less congestion, and therefore the re-dispatching cost is not much.

Table 5 summarizes the power exchanges between zones for different configurations given by the second step model. The amount of power exchange for the hours without solar power is larger than that with solar power. In this case, if we use the result with the solar power, this might reduce the power exchange among zones and increase the total cost.

peak-hour with solar solution (Lower NTC)

peak-hour without solar solution (Higher NTC)

	zone1	zone2	zone3
zone1		67	61
zone2	67		63
zone3	61	63	

	zone1	zone2	zone3	zone4
zone1		56		55
zone2	56		49	
zone3		49		51
zone4	55		51	

	zone1	zone2	zone3	zone4
zone1		67		61
zone2	67		49	
zone3		49		63
zone4	61		63	

Table 5: Power exchanges based on nodal solution. Case I: 3-zonal configuration (Fig. 4a), Case II: 4-zonal configuration (Fig. 4b).

### **Results of step 4**

	3 Zone	4 Zone	Full network	
Lower NTC	197,300	237,600	108 000	
HIGHER NTC	201,600	252,900	198,000	

Table 6: Total dispatching cost (1000 EURO)

Table 6 summarizes the total dispatching cost given different zone configuration and 2 different set of NTC value. We compare the number to the model with full network details. We find that the total dispatching cost in the 3-zone case is the one mostly close to the one with the full network. Furthermore, the cases with a higher NTC value have a higher dispatching cost than the case with a lower NTC value. However, the results here cannot sufficiently conclude that one zone configuration is superior to the other one. To fully evaluate it, we much consider the re-dispatching cost given the generation plan.

Another possibility here to evaluate the performance of different zone configuration and NTC value is to check if the generators are on in the "correct" time. Table 7 summarize the total on hours for each generator in different cases. We compare these numbers to the cases with full network model, as show in Table

7. Generally, we could see the cases with a higher NTC model will perform better than the ones with lower NTC model. This is mainly because that the higher NTC value could cover more situation in the peak hours.

	3 zone		4 zone		EII
Generator	Lower	High	Lower	High	network
Generator	NTC	NTC	NTC	NTC	network
1	2903	3644	1981	3103	1745
2	8760	8760	8760	8760	8754
3	7061	273	5747	0	698
4	8544	5917	8760	8541	7227
5	8760	8434	8760	7232	4943
6	8760	8760	8760	8039	7782
7	6528	7303	8758	6934	6965
8	127	2334	0	5754	5373
9	0	4379	0	3972	3035
10	368	2569	0	1770	5897
11	0	1465	0	2262	7406
12	2197	6525	8719	4836	5050
13	8757	6480	8760	7769	7563
14	8721	6480	0	6029	7434
15	8760	8756	8723	5519	7991
16	28	261	87	89	732
17	0	5	0	0	77
18	1	0	0	205	62
19	0	21	0	0	46
20	4	14	13	6	53

Table 7: Total on hours for the generators

	3 zo	ne	4 zo	ne
Generator	Lower NTC	High NTC	Lower NTC	High NTC
1	166%	209%	114%	178%
2	100%	100%	100%	100%
3	1012%	39%	823%	0%
4	118%	82%	121%	118%
5	177%	171%	177%	146%
6	113%	113%	113%	103%
7	94%	105%	126%	100%
8	2%	43%	0%	107%
9	0%	144%	0%	131%
10	6%	44%	0%	30%
11	0%	20%	0%	31%
12	44%	129%	173%	96%
13	116%	86%	116%	103%
14	117%	87%	0%	81%
15	110%	110%	109%	69%
16	4%	36%	12%	12%
17	0%	6%	0%	0%
18	2%	0%	0%	331%
19	0%	46%	0%	0%
20	8%	26%	25%	11%

Table 8: On hours compared to the full network model

## **IV.** Future study

At this stage, we still could not conclude which zone configure would be a better choice for the long-term UC model with simplified network constraints. On of the main results is that we must consider the re-dispatching cost given by the generation plans. Another issue is about how to define the NTC values. as we can see from the preliminary results, the NTC values have a large impact on the results. In this study we use the same NTC value for all the hours. However, in the future study, we might need to designate different NTC values to different hours.

# V. Appendix I: nomenclature

Sets

c∈C	Set of conventional power plants
C <sub>n</sub>	Set of conventional power plants located in node n
Cz	Set of conventional power plants located in zone z
l	Set of cluster
n, nn ∈ N	Set of all nodes
$l \in L$	Set of all transmission lines
z, zz ∈ Z	Set of all zones
Parameters	
bvector <sub>n,nn</sub>	Series susceptance of line n, nn $[1/\Omega]$
cg <sub>c</sub>	The electricity generation cost for power plant c [EUR/MWh]
gmax <sub>c</sub>	Maximum generation of plant c [MW]
gsolar <sub>n</sub>	Solar generation at node n [MW]
gwind <sub>n</sub>	Wind generation at node n [MW]
gbio <sub>n</sub>	Biomass generation at node n [MW]
ntc <sub>z,zz</sub>	Net transfer capacity between zone z and zz [MW]
pmax <sub>n,nn</sub>	Thermal transmission limit of transmission line l, n, nn [MW]
St <sub>n,nn</sub>	On or off status of transmission line l, n, nn
qda <sub>n</sub>	Contracted demand at node n in the day-ahead market [MW]
p <sub>n</sub>	Price at node n
link <sub>n,nn</sub>	Connecting matrix
nptdf <sub>l,i</sub>	Nodal ptdf matrix
gsk <sub>i,z</sub>	GSK matrix
zptdf <sub>l,z</sub>	Zonal ptdf matrix
st <sub>c</sub>	Startup cost for generator c
sd <sub>c</sub>	Shutdown cost for generator c
minion <sub>c</sub>	Minimum ON time of generator c
minioff <sub>c</sub>	Minimum Off time of generator c
rdown <sub>c</sub>	Ramp down rate of generator c
rup <sub>c</sub>	Ramp up rate of generator c
s <sub>c</sub> <sup>max</sup>	Maximum spin reserve of generator c
rs <sub>i,t</sub>	Fixed reserve requirement
VOLL	Unserved energy penalty

## Variables

$\Delta_{n}$	Voltage angle at node n [rad]
G <sub>c</sub>	Generation of plant c [MW]
LOADSHED <sub>n</sub>	Load curtailment at node n [MW]
LF <sub>n,nn</sub>	Power flow between nodes n and nn [MW]
NIn	Net input at node n [MW]
p <sub>n</sub>	Price at node n
Q <sub>n</sub>	Demand at node n [MW]
SOLSHED <sub>n</sub>	Solar power curtailment at node n [MW]
WINDSHED <sub>n</sub>	Wind power curtailment at node n [MW]
aa <sub>n,k</sub>	Number of connections with the other nodes within the same zone
C <sub>k</sub>	Average price for cluster k
NEX <sub>z</sub>	Net position of a zone
BEX <sub>z,zz</sub>	Power transfer from zone z to zone zz
LS <sub>c,t</sub>	Load loss of generator c at time t
S <sub>c,t</sub>	spinning reserve

# **Binary variable**

m <sub>n,k</sub>	Node n belong to cluster k
V <sub>ct</sub>	Startup decision of generator c at time t
W <sub>ct</sub>	Shutdown decision of generator c at time t
U <sub>c,t</sub>	On/off statue of generator c at time t

# VI. Appendix II: GAMS Code for step 1 and 3

\$ontext
Author: Hong Cai
\$offtext
option solprint = on;

#### set

```
n

p

map_pn(p,n)

c(p)

l

i

map_pi(p,i)

map_pn(p,n)

map_ln(l,n,n)
```

;

alias (n,nn), (c,cc), (l,ll), (i,ii)

;

parameter lineup

nodeup

genup

techup

fuelup

nodeup

genup

g\_max(p)

g\_min(p)

Q(n)

```
g_wind
g_solar
g_bio
p_maxN(n,nn)
react(l)
resis(l)
Voltage(l)
p_max(l)
circuits(l)
incidence(l,n)
b(n,n)
h(l,n)
bvector(l)
gvector(l)
slack(n)
g_max(p)
g_min(p)
circuits(l)
cg(p)
Bin(n,nn)
ptdf(l,n)
```

```
;
```

## \$onecho >temp.tmp

set=l	rng=AClines!A2:A836	rdim=1 cdim=0
set=n	rng=nodes!A2:A540	rdim=1 cdim=0
set=p	rng=plants!A2:A412	rdim=1 cdim=0
set=f	rng=fuels!A2:A12	rdim=1 cdim=0
set=i	rng=technologies!A2:A23	rdim=1 cdim=0
set=map_	pn rng=plants!D2:E412	rdim=2 cdim=0
set=map_	pi rng=plants!A2:B412	rdim=2 cdim=0
set=map_	ln rng=AClines!A2:C836	rdim=3 cdim=0
par=lineu	p rng=AClines!A1:H836	rdim=1 cdim=1

par=nodeup	rng=nodes!A1:L540	rdim=1 cdim=1	
par=genup	rng=plants!A1:L412	rdim=1 cdim=1	
\$offecho			

```
$onUNDF
```

\$call "gdxxrw %datadir%%data%.xls MaxDupeErrors=9999999999 cmerge=1
squeeze=N @temp.tmp"
\$gdxin %data%

\$load l n p map\_pn map\_ln z zonemember \$load lineup nodeup genup

```
$offmulti
```

```
circuits(l) = lineup(l,"Circuits");
p_max(l) = lineup(l,"ThermalLimit")*circuits(l);
voltage(l) = lineup(l,"Voltage");
slack(n) = 1$nodeup(n,'Slack bus');
react(l) = lineup(l,"Reactance")/circuits(l);
resis(l) = lineup(l,"Resistance")/circuits(l);
```

```
incidence(l,n) = 0;
incidence(l,n)$(lineup(l,"From") eq n.val) = 1;
incidence(l,n)$(lineup(l,"To") eq n.val) = -1;
```

```
bvector(l) = (react(l) / (react(l)^{**2} + resis(l)^{**2})) (react(l) \text{ or } resis(l));
gvector(l) = (resis(l) / (react(l)^{**2} + resis(l)^{**2})) (react(l) \text{ or } resis(l));
```

```
h(l,n) = bvector(l) * incidence(l,n);
b(n,nn) = sum(l$incidence(l,n), incidence(l,n) * h(l,nn));
```

```
b(n,nn)$slack(n)=0;
b(n,nn)$slack(nn)=0;
```

```
g_max(p) = genup(p,'Generation capacity');
```

```
g_min(p) = genup(p,'Min Generation');
cg(p) = genup(p,'Cost');
Q(n) = nodeup(n,'Demand share')*210;
g_wind(n) = nodeup(n,'Wind share')*0;
g_solar(n) = nodeup(n,'Solar share')*0;
g_bio(n)= nodeup(n,'Biomass share')*0.4;
```

Variable

WELFARE COST\_GEN LINEFLOW NETINPUT DELTA

;

Positive Variable

G

;

binary variable STATUS

;

Equations

OBJ\_generation\_cost MKT\_lp\_1 RES\_gmax\_1 RES\_gmin\_1 DEF\_lineflow\_1 DEF\_netinput\_1 RES\_pmax\_1 RES\_pmin\_1 RES\_slack\_1

;

```
OBJ_generation_cost..
    COST_GEN
                =E= SUM(p$g_max(p),
              cg(p) * G(p)
;
MKT_lp_1(n)..
    NETINPUT(n) =E SUM(p(map_pn(p,n) and g_max(p)), G(p))
              +g_wind(n) + g_solar(n) + g_bio(n)
              -Q(n)
;
RES_gmax_1(p)$g_max(p)..
            =L= g_max(p)*STATUS(p)
    G(p)
;
RES_gmin_1(p)$g_max(p)..
    G(p) = G = g_{min}(p) * STATUS(p)
;
DEF_netinput_1(n)..
    NETINPUT(n) =E= sum(nnb(n,nn), b(n,nn)*DELTA(nn))
;
RES_pmax_1(l)..
    LINEFLOW(l) =L= 0.95 * p_max(l)
;
RES_pmin_1(l)..
    - LINEFLOW(l) =L= 0.95 * p_max(l)
;
DEF_lineflow_1(l)..
    LINEFLOW(l) =E= sum(n$h(l,n), h(l,n)*DELTA(n))
;
RES_slack_1(n)..
    DELTA(n)*slack(n) =E= 0
;
```

```
MODEL FIRST_STEP the hybrid model
```

/ OBJ\_generation\_cost MKT\_lp\_1 RES\_gmax\_1 RES\_gmin\_1 DEF\_lineflow\_1 DEF\_netinput\_1 RES\_pmax\_1 RES\_pmin\_1 RES\_slack\_1

/;

\$onecho >cplex.opt
lpmethod 4
threads -1
numericalemphasis 1
scaind 1
EpMrk 0.99999
\$offecho

\$onecho >conopt.opt rtnwma 1.e-6 rtnwmi 1.e-7 \$offecho

SOLVE FIRST\_STEP min COST\_GEN using minlp;

# VII. Appendix II: GAMS Code for step 2

\$ontext
Author: Hong Cai
\$offtext

option solprint = on;

set k/k1\*k5/

```
n/p1*p14/
ll
```

Alias (n,nn); Parameter p(n,ll);

\$call "gdxxrw %datadir%%data%.xls MaxDupeErrors=9999999999 cmerge=1
squeeze=N@temp.tmp"
\$gdxin %data%
\$load ll
\$LOADDC p

### table link(n,nn) conection matrix

ŗ	<b>b</b> 1	p2	р3	p4	p5	5	p6	p7	p8	р9	p1	0	p11	p12	p13	p14
p1	0	0	1	0	0	0	0	0	0	0	0	0	0	0		
p2	0	0	1	0	0	0	0	1	0	0	0	0	0	0		
р3	1	1	0	0	1	0	0	0	0	0	0	0	0	0		
p4	0	0	1	0	1	0	0	0	0	0	0	0	0	0		
p5	0	0	0	1	0	1	0	0	0	0	0	0	0	0		
р6	0	0	0	0	1	0	1	1	0	0	0	0	0	0		
p7	0	0	0	0	0	1	0	0	0	0	0	0	0	0		
p8	0	1	0	0	0	1	0	0	1	0	1	1	0	0		
p9	0	0	0	0	0	0	0	1	0	1	0	0	0	0		
p10	0	0	0	0	0	0	0	0	1	0	1	0	0	0		
p11	0	0	0	0	0	0	0	1	0	1	0	1	0	0		
p12	0	0	0	0	0	0	0	1	0	0	1	0	1	0		
p13	0	0	0	0	0	0	0	0	0	0	0	1	0	1		
p14	0	0	0	0	0	0	0	0	0	0	0	0	1	0		

```
Variable pri_dif
    price(n,k)
    mean
    sum_price(k)
    sum_node(k)
    c(k)
    num(k)
    bb
    aa
```

binary variable m(n,k)

;

;

Equations

Obj\_cluster objective for clustering assign\_limit1 assign\_limit2 assign\_limit3 assign\_limit4 assign\_limit5 assign\_limit6 assign\_limit7 kluster\_mean

```
;
```

```
Obj_cluster..
```

```
pri_dif =E = sum((n,k),mean(n,k)*mean(n,k))
```

```
;
```

```
assign_limit1(n)..
    sum(k,m(n,k)) = e = 1
```

```
assign_limit2(k)..
    sum(n,m(n,k)) = g = 1
;
kluster_mean(n,k)..
    mean(n,k) = e = p(n)*m(n,k)-c(k)*m(n,k)
;
assign_limit3(k)..
    c(k)^* sum(n,m(n,k)) = e = sum(n,p(n)^*m(n,k))
;
assign_limit4(k)..
    sum(n,m(n,k)) = g = 2
;
assign_limit5(n,k)..
    aa(n,k)=e= sum(nn,link(n,nn)*m(nn,k)*m(n,k));
;
assign_limit6(n,k)..
    aa(n,k) = l = 10000*m(n,k)
;
assign_limit7(n,k)..
    aa(n,k) =g= 1-10000*(1-m(n,k))
;
model kmeans /all/;
```

```
option miqcp = COUENNE;
option optcr=0;
solve kmeans minimizing pri_dif using miqcp;
```

```
parameter cc;
cc(n,k)= sum(nn,link(n,nn)*m.l(nn,k)*m.l(n,k));
```

display m.l,cc;

# VIII. Appendix II: GAMS Code for step 4

\$ontext Author: Hong Cai \$offtext

```
set
```

```
n

p

map_pn(p,n)

c(p)

l

i

map_pi(p,i)

map_pn(p,n)

map_ln(l,n,n)

z

zonemember(n,z)

t

char / ch1*ch2 /
```

```
alias (n,nn), (c,cc), (l,ll), (i,ii), (z,zz),(t,tt);
```

parameter lineup nodeup genup

;

techup

infup

nodeup

ntcup

genup

g\_max(p)

g\_min(p)

Q g\_wind g\_solar g\_bio p\_maxN(n,nn) react(l) resis(l) Voltage(l) p\_max(l) circuits(l) incidence(l,n) b(n,n) h(l,n)bvector(l) gvector(l) slack(n) g\_max(p) g\_min(p) circuits(l)

cstart(p) cdown(p) cg(p) zonecap\_fwd(z,zz)

;

\$onecho >temp.tmp

set=l	rng=AClines!A2:A836	rdim=1 cdim=0
set=n	rng=nodes!A2:A540	rdim=1 cdim=0
set=p	rng=plants!A2:A412	rdim=1 cdim=0

set=f ri	ng=fuels!A2:A12	rdim=1 cdim=0
set=i rı	ng=technologies!A2:A23	rdim=1 cdim=0
set=t ri	ng=Inf!A2:A10000	rdim=1 cdim=0
set=map_pn	rng=plants!D2:E412	rdim=2 cdim=0
set=map_pi	rng=plants!A2:B412	rdim=2 cdim=0
set=map_ln	rng=AClines!A2:C836	rdim=3 cdim=0
set=z r	ng=zone!D2:D100	rdim=1 cdim=0
set=zonemei	nber rng=zone!C2:D100	rdim=2 cdim=0
par=lineup	rng=AClines!A1:H836	rdim=1 cdim=1
par=nodeup	rng=nodes!A1:L540	rdim=1 cdim=1
par=genup	rng=plants!A1:T412	rdim=1 cdim=1
par=infup	rng=Inf!A1:E10000	rdim=1 cdim=1
par=ntcup	rng=NTC!A1:D10	rdim=2 cdim=1
\$offecho		

#### \$onUNDF

\$call "gdxxrw %datadir%%data%.xls MaxDupeErrors=9999999999 cmerge=1
squeeze=N @temp.tmp"
\$gdxin %data%

\$load l n p t map\_pn map\_ln z zonemember \$load lineup nodeup genup infup ntcup

\$offmulti

circuits(l) = lineup(l,"Circuits");

p\_max(l) = lineup(l,"ThermalLimit")\*circuits(l);

voltage(l) = lineup(l,"Voltage");

zonecap\_fwd(z,zz)=ntcup(z,zz,"cap\_fwd");

slack(n) = 1\$nodeup(n,'Slack bus');

react(l) = lineup(l,"Reactance")/circuits(l);

resis(l) = lineup(l,"Resistance")/circuits(l);

incidence(l,n) = 0; incidence(l,n)\$(lineup(l,"From") eq n.val) = 1;

```
incidence(l,n)$(lineup(l,"To") eq n.val) = -1;
```

```
bvector(l) = (react(l) / (react(l)**2 + resis(l)**2)) (react(l) \text{ or } resis(l));
gvector(l) = (resis(l) / (react(l)**2 + resis(l)**2)) (react(l) \text{ or } resis(l));
h(l,n) = bvector(l) * incidence(l,n);
b(n,nn) = sum(l (l,n), incidence(l,n) * h(l,nn));
```

```
g_max(p) = genup(p,'Pmax');
g_min(p) = genup(p,'Pmin');
cg(p) = genup(p,'Cost');
```

```
Parameter unit(p,char);
unit(p,'ch1') = 8760;
unit(p,'ch2') =(genup(p,'UT') - genup(p,'U0'))*genup(p,'Uini');
```

```
Parameter unit2(p,char),check1;
unit2(p,'ch1') = 8760;
unit2(p,'ch2') =(genup(p,'DT') - genup(p,'S0'))*(1 - genup(p,'Uini'));
genup(p,'Lj') = smin(char,unit(p,char));
genup(p,'Fj') = smin(char,unit2(p,char));
```

```
Q(n,t) = nodeup(n,'Demand share')*infup(t,'supply');
g_wind(n,t) = nodeup(n,'Wind share')*infup(t,'wind');
g_solar(n,t) = nodeup(n,'Solar share')*infup(t,'solar');
g_bio(n,t) = nodeup(n,'Biomass share')*infup(t,'bio');
```

Variable

COST\_GEN LINEFLOW NETINPUT DELTA StC

```
SDC
G
NEX(z,t)
;
```

Positive Variable G

StC SDC BEX(z,zz,t)

;

;

binary variable

u(p,t) y(p,t) sz(p,t)

# Equations

OBJ_generation_cost generation cost definition (for the first step model)
MKT_lp_1 market clearing equation (for the first step model
RES_gmax_1 maximum generation restriction (for the first step model)
RES_gmin_1 minimum generation restriction (for the first step model)
DEF_lineflow_1 lineflow definition (for the first step model)
DEF_netinput_1 netinput definition (for the first step model)
RES_pmax_1 maximum transmission restriction (for the first step model)
RES_pmin_1 minimum transmission restriction (for the first step model)
RES_slack_1 slack bus restriction (for the first step model)
Uptime1
Uptime2
Uptime3
Dntime1
Dntime2
Dntime3

```
startc
shtdnc
Genconst2
export
sdbl
capforward_aggr(z,zz,t)
intertrading(z,t)
```

```
MKT_lp_1(n,t)..
    NETINPUT(n,t) =E SUM(p(map_pn(p,n) and g_max(p)), G(p,t))
               + g_wind(n,t) + g_solar(n,t) + g_bio(n,t)
               -Q(n,t)
;
RES_gmax_1(p,t)$g_max(p)..
    G(p,t)
              =L= g_max(p)^*u(p,t)
;
RES_gmin_1(p,t)$g_max(p)..
    G(p,t)
             =G= g_{min}(p)^*u(p,t)
;
DEF_netinput_1(n,t)..
    NETINPUT(n,t) =E= sum(nnb(n,nn), b(n,nn)*DELTA(nn,t))
;
RES_pmax_1(l,t)..
    LINEFLOW(l,t) = L = 10000000
*
    LINEFLOW(l,t) = L = p_max(l)
;
RES_pmin_1(l,t)..
```

```
- LINEFLOW(l,t) =L= 1000000
*
    - LINEFLOW(l,t) =L= p_max(l)
;
DEF_lineflow_1(l,t)..
    LINEFLOW(l,t) = E = sum(n$h(l,n), h(l,n)*DELTA(n,t))
;
RES_slack_1(n,t)..
    DELTA(n,t)*slack(n) = E = 0
;
Genconst2(p,tt)$(ord(tt)>0)..
 U(p,tt) = e = U(p,tt-1)(ord(tt)>1) + genup(p,"Uini")(ord(tt)=1) + y(p,tt) - sz(p,tt);
Uptime1(p)$(genup(p,"Lj")>0)..
 sum(t$(ord(t)<(genup(p,"Lj")+1)), 1 - u(p,t)) = e = 0;
Uptime2(p)$(genup(p,"UT")>1)..
 sum(t(ord(t)>24-genup(p,"UT")+1), u(p,t) - y(p,t)) = g = 0;
Uptime3(p,t)$(ord(t)>genup(p,"Lj")
                                                ord(t)<24-genup(p,"UT")+2
                                       and
                                                                               and
not(genup(p,"Lj")>24-genup(p,"UT"))).
 sum(tt$((ord(tt)>ord(t)-1) and (ord(tt)<ord(t)+genup(p,"UT"))), u(p,tt)) =g=
genup(p,"UT")*y(p,t);
Dntime1(p)$(genup(p,"Fj")>0)..
 sum(t$(ord(t)<(genup(p,"Fj")+1)), u(p,t)) = e = 0;
Dntime2(p)$(genup(p,"DT")>1)..
 sum(t$(ord(t)>24-genup(p,"DT")+1), 1 - u(p,t) - sz(p,t)) =g= 0;
Dntime3(p,t)$(ord(t)>genup(p,"Fj")
                                       and
                                                ord(t) < 24-genup(p,"DT")+2
                                                                               and
not(genup(p,"Fj")>24-genup(p,"DT"))).
 sum(tt$((ord(tt)>ord(t)-1) and (ord(tt)<ord(t)+genup(p,"DT"))), 1-u(p,tt)) =g=
genup(p,"DT")*sz(p,t);
startc(p,t).. StC(p,t) =g= genup(p,"costst")*y(p,t);
```

```
shtdnc(p,t).. SDC(p,t) =g= genup(p,"CostsD")*sz(p,t);
```

```
export(z,t)..
```

```
NEX(z,t) =e= sum(n$zonemember(n,z),NETINPUT(n,t));
```

```
sdbl(t)..
sum(z,NEX(z,t))=e=0;
```

```
capforward_aggr(z,zz,t)..
BEX(z,zz,t) =l= zonecap_fwd(z,zz);
```

intertrading(z,t)..

NEX(z,t) =e= sum(zz,(BEX(z,zz,t)-BEX(zz,z,t)));

```
MODEL FIRST_STEP uc
```

/ OBJ\_generation\_cost MKT\_lp\_1

RES\_gmax\_1 RES\_gmin\_1

```
DEF_lineflow_1
DEF_netinput_1
RES_pmax_1
RES_pmin_1
RES_slack_1
Uptime1
Uptime2
Uptime3
Dntime1
Dntime2
Dntime2
Dntime3
```

startc shtdnc Genconst2 export sdbl capforward\_aggr intertrading

/;

\$onecho >cplex.opt
lpmethod 4
threads -1
numericalemphasis 1
scaind 1
EpMrk 0.99999
\$offecho

\$onecho >conopt.opt rtnwma 1.e-6 rtnwmi 1.e-7 \$offecho

SOLVE FIRST\_STEP min COST\_GEN using mip;

## IX. References

- [1] Barth R, Brand H, Meibom P, Weber C (2006) A stochastic unit commitment model for the evaluation of the impacts of integration of large amounts of intermittent wind power. In: International conference on probabilistic methods applied to power systems, pp 1–8, June 2006
- [2] BJØRNDAL, Endre, BJØRNDAL, Mette, et CAI, Hong. Nodal pricing in a coupled electricity market. In : 11th International Conference on the European Energy Market (EEM14). IEEE, 2014. p. 1-6.
- [3] BJORNDAL, Endre, BJORNDAL, Mette Helene, et CAI, Hong. The flowbased market coupling model and the bidding zone configuration. NHH Dept. of Business and Management Science Discussion Paper, 2018, no 2018/15
- [4] Bouffard F, Galiana FD, Conejo AJ (2005) Market-clearing with stochastic securitypart I: formulation. IEEE Trans Power Syst 20(4):1818–1826
- [5] B. Burstedde, "From nodal to zonal pricing: a bottom-up approach to the second-best," in Proc. 9th International Conference on the European Energy Market (EEM), 2012.
- [6] C. Breuer, N. Seeger, and A. Moser, "Determination of alternative bidding areas based on a full nodal pricing approach," in Proc. IEEE Power and Energy Society General Meeting (PES), 2013.
- [7] Chao, H. P., Peck, S., Oren, S., & Wilson, R. (2000). "Flow-based transmission rights and congestion management." The Electricity Journal, 13(8), 38-58.
- [8] Christie, Richard D., Bruce F. Wollenberg, and Ivar Wangensteen. "Transmission management in the deregulated environment." Proceedings of the IEEE 88.2 (2000): 170-195.
- [9] de Maere d'Aertrycke G., Smeers Y. (2013) Transmission Rights in the European Market Coupling System: An Analysis of Current Proposals. In: Rosellón J., Kristiansen T. (eds) Financial Transmission Rights. Lecture Notes in Energy, vol 7. Springer, London.
- [10] Epexspot (2011), "CWE\_Flow\_Based\_Questions\_and\_Answers". https://www.epexspot.com/document/14065/CWE\_Flow\_Based\_Question s\_and\_Answers.pdf
- [11] JAO.EU (2014) "Documentation of the CWE FB MC solution As basis for the formal approval-request." JAO.EU, 2014

- [12] Hobbs BF, Rothkopf MH, O'Neil RP, Chao H (2001) The next generation of electric power unit commitment models. Kluwer Academic Publishers, Norwell
- [13] Hogan, William W. "Transmission congestion: the nodal-zonal debate revisited." Harvard University, John F. Kennedy School of Government, Center for Business and Government. Retrieved August 29, no. 4 (1999).
- [14] Huang, Yuping, Panos M. Pardalos, and Qipeng P. Zheng. Electrical power unit commitment: deterministic and two-stage stochastic programming models and algorithms. Springer, 2017.
- [15] Leuthold, Florian, Hannes Weigt, and Christian Von Hirschhausen. "Efficient pricing for European electricity networks-The theory of nodal pricing applied to feeding-in wind in Germany." Utilities Policy 16, no. 4 (2008): 284-291.
- [16] M. Klos, K. Wawrzyniak, M. Jakubek, and G. Orynczak, "The scheme of a novel methodology for zonal division based on power transfer distribution factors," in Proc. 40th Annual Conference of the Industrial Electronics Society, 2014.
- [17] J. A. Muckstadt and S. A. Koenig, "An application of Lagrangian relaxation to scheduling in power generation systems", Operations Research, 25(3):387-403, May-June 1977.
- [18] Ni E, Luh PB, Rourke S (2004) Optimal integrated generation bidding and scheduling with risk management under a deregulated power market. IEEE Trans Power Syst19(1):600–609
- [19] Overbye, Thomas J., Xu Cheng, and Yan Sun. "A comparison of the AC and DC power flow models for LMP calculations." In System Sciences, 2004. Proceedings of the 37th Annual Hawaii International Conference on, pp. 9-pp. IEEE, 2004.
- [20] Ruiz P, Philbrick C, Zak E, Cheung K, Sauer P (2009) Uncertainty management in the unit commitment problem. IEEE Trans Power Syst 24(2):642–651 May
- [21] Samer Takriti, John R. Birge, Erik Long, "A Stochastic Model for the Unit Commitment Problem", The University of Michigan; 1995.
- [22] Sauma, E. E., & Oren, S. S. (2006). "Proactive planning and valuation of transmission investments in restructured electricity markets." Journal of Regulatory Economics, 30(3), 261-290.

- [23] Schweppe, Fred C., Richard D. Tabors, M. C. Caraminis, and Roger E. Bohn. "Spot pricing of electricity." (1988).
- [24] Shahidehpour M, Yamin H, Li Z (2002) Market operations in electric power systems. Wiley, New York
- [25] Soroudi, Alireza. Power system optimization modeling in GAMS. Vol. 78. Switzerland: Springer, 2017.
- [26] Tuohy A, Meibom P, Denny E, O'Malley M (2009) Unit commitment for systems with significant wind penetration. IEEE Trans Power Syst 24(2):592–601
- [27] Wang J, BotterudA, ConzelmannG,MirandaV,Monteiro C, Sheble,G
   (2009) Impact of wind power forecasting on unit commitment and dispatch.
   In: 8th International wind integration workshop, Bremen, Germany,
   October 2009
- [28] Zheng QP, Wang J, Liu AL (2015) Stochastic optimization for unit commitment-a review. IEEE Trans Power Syst 30:1913–1924
- [29] Yang Y, Wang J, Guan X, Zhai Q (2012) Subhourly unit commitment with feasible energy delivery constraints. Appl Energy 96:245–252
- [30] https://weather-and-climate.com/average-monthly-Rainfall-Temperature-Sunshine-in-Martinique
- [31] https://opendata-martinique.edf.fr/