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1	DART radiative transfer modelling for sloping landscapes
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10	Abstract
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12	Topography is one of the key factors that impact remotely sensed data and their interpretation.
13	Indeed, combined with the viewing geometry and neighbour effects, it strongly affects the direct,
14	diffuse and multi-scattered scene irradiance, which in turn impacts the radiative budget and
15	remote sensing signals of the landscapes. The increased availability of digital elevation models
16	(DEM) and the advancement of 3D radiative transfer (RT) models allow us to better address
17	these topographic effects. DART (Discrete Anisotropic Radiative Transfer) is one of the most
18	accurate and comprehensive 3D RT models that simulate remote sensing observations of
19	natural and urban landscapes with topography and atmosphere. It simulates environmental
20	effects (<i>i.e.</i> , impact of adjacent landscape on the observed landscape) using a so-called infinite
21	slope mode that infinitely duplicates the observed landscape while ensuring the continuity of
22	slope and altitude at the DEM edges. Up to DART version 5.7.4, this mode was slightly
23	inaccurate and computer intensive, depending on the topography. This paper presents an
24	innovative modelling strategy that greatly improves it in terms of accuracy, image quality and
	1

25 computer efficiency. For that, a fictive auxiliary oblique plane, adapted to the landscape 26 topography, is introduced for managing the scene illumination, the Earth-Atmosphere coupling 27 and the storage of the radiation that exits the scene before being projected onto the sensor plane. 28 Improvements and validations are illustrated both visually and quantitatively by DART images, 29 radiometric products and radiative budget. For example, the observed reflectance of a 30 Lambertian slope is equal to the expected analytical value. In addition, the solar plane 31 reflectance of a forest on a mountain slope (experimental scene) has an average error of about 32 0.01% relative to the reflectance of the same forest stand in the reference scene (*i.e.*, nine 33 duplications of the experimental scene). This new modelling is already integrated in the official 34 DART version (https://dart.omp.eu). 35 Key words 36 37 Topography, DART, Infinite slope, Radiative transfer, Environmental effects 38 39 40 Introduction 1 41 42 Mountain regions cover around a quarter of the Earth's land surface (Liang, 2005) and are home 43 to around one-tenth of the world's population (Denniston, 1996). They also provide vital economic and ecological resources to the world's population, thanks to their rich biodiversity, 44 45 water-storing capacity, mineral reserve, etc (Price, 1998). Therefore, mountain areas are more and more surveyed with remote sensing (RS) data (Boori et al., 2015; Barrachina et al. 2015; 46 47 Reinhold et al., 2016; Chimner et al., 2019). However, RS data are usually contaminated by

48 topographic effects, since slopes combined with the observation configuration (e.g., viewing

49 and sun geometry, atmosphere composition) impact the direct, diffuse and multi-scattered 50 irradiance, which in turn affects the RS signals and radiative budget (RB) of mountain regions 51 (Schaaf et al., 1994; Mousivand et al., 2015; Pellarin et al., 2016; Wen et al., 2018). In the last 52 four decades, a lot of work has been done to eliminate or to reduce these topographic effects 53 (Holben and Justice, 1980; Proy et al., 1989; Sandmeier et al., 1997; Richter and Schläpfer; 54 2011; Santini et al., 2019), notably through the development of numeric models (Table 1).

55

56 Table 1. Models that quantify topographic effects. Model category and references are indicated.

Model Category	Model Name	Model Reference
	Cosine Correction	Holben and Justice, 1980
Empirical	C correction	Teillet et al., 1982
	SCS	Gu and Gillespie, 1998
Geometric optical	GOMST	Schaaf et al., 1994
	GOST	Fan et al., 2013
	DART	Gastellu-Etchegorry et al., 1996; 2017
3D radiative transfer	LESS	Qi et al., 2018
	RAPID3	Huang, 2018
	Rayspread	Widlowski et al., 2007

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Empirical models (*e.g.*, Cosine Correction, C correction, SCS) are the simplest and most practical for topographic correction, but the lack of generality and physical considerations limits their accuracy. Geometric optical models (*e.g.*, GOMST, GOST) use a geometric approach to quantify how canopy directional reflectance depends on slopes, solar direct irradiance and 3D tree crowns. However, they usually neglect sky diffuse illumination and multiple scattering in 63 landscapes. Also, the solo slope is a theoretical assumption that rarely exists in the nature. Being 64 more sophisticated and comprehensive, 3D radiative transfer (RT) models (e.g., DART, LESS, RAPID, Rayspread) are assumed to be the most accurate. They can simulate complex 65 66 topography, realistic 3D landscape elements, multiple scattering in the landscape and possibly with diffused illumination from the atmosphere. Thanks to the development of computer 67 68 hardware and RT algorithms (e.g., PBRT, LuxCoreRender, Mitsuba) (Grimaldi and Vergauwen, 69 2008; Jakob, 2014; Pharr et al., 2016), 3D RT models become more and more efficient, which 70 opens new opportunity for removing or reducing topographic effects in RS observations. Most 71 3D RT models were developed for the Earth surface RT modelling with atmosphere being 72 treated as an interface that is usually computed by an atmospheric RT model such as 73 MODTRAN (Berk and Hawes, 2017). It is typically the case of the recently developed LESS 74 model that can simulate very large forest landscapes (Qi et al., 2018). Atmospheric RT 75 modelling in presence of complex mountainous topography is still a challenge due to the 76 complex Earth-Atmosphere radiative coupling. To our knowledge, DART is the only 3D RT 77 model that simulates the Earth-atmosphere radiative coupling and environmental effects in 78 mountain areas. The so-called environmental effects are the impact of the adjacent landscapes 79 on the observed landscape.

80

The accuracy of DART Earth surface RT modelling for vegetation canopy over flat terrain was already verified in the four phases of the RAMI project (RAdiative transfer Model Intercomparison) (Widlowski et al., 2007; Widlowski et al., 2013; Widlowski 2015) and experiments (Guillevic et al., 2003; Guillevic et al., 2013). DART atmospheric RT modelling was successfully tested with MODTRAN5 simulations (Grau and Gastellu-Etchegorry, 2013; Gastellu-Etchegorry et al, 2017; Wang and Gastellu-Etchegorry 2020), with reflectance accuracy better than 0.004 and TIR brightness temperature accuracy better than 1.0 K, at bottom 4 (BOA) and top (TOA) of atmosphere. DART is continuously improved in terms of accuracy,
efficiency and modelling. For example, sun induced fluorescence modelling was introduced in
2016 (Gastellu-Etchegorry et al., 2017), and the Embree ray tracing library was recently
introduced for reducing simulation time and memory demand (Wald et al., 2014; Qi et al., 2019).
The work presented here is an improvement concerning RT modelling over sloping landscapes.

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DART scene is a 3D array of cells that can contain turbid material, fluids and facets (i.e., 94 95 triangles). The scene is either spatially finite (*i.e.*, "isolated scene" mode) or infinite (*i.e.*, "repetitive scene" mode for simulating landscapes on flat terrain and "infinite slope" mode for 96 97 simulating landscapes on sloping terrain). A spatially infinite scene is an infinite repetition of 98 the actually simulated scene. Being designed for sloping landscapes, the infinite slope mode 99 ensures the altitude and slope continuity at the DEM edges of any duplicated scene. In DART, 100 RT is simulated by tracking rays along a finite number of discrete directions. The infinite slope 101 mode simulates the environmental effects by re-entering environmental rays into the observed 102 scene. These environmental rays are scattered from the neighbouring duplicated scenes. Rays 103 that exit the scene through its upper surface (*i.e.*, rays that constitute the observation) are spread 104 at their point of intersection with the horizontal plane at the scene bottom where they constitute 105 intermediate images, also called spread images (Yin et al., 2015). They are used to simulate the 106 Earth-atmosphere radiative coupling and RS images. The sloping topography explains that each 107 spread image has a specific polygon-shape and dimension per direction. Up to DART versions 108 5.7.4, scientists noted that the infinite slope mode could be inaccurate, as illustrated below in 109 this paper. An analysis of DART RT modelling allowed us to stress two major sources of 110 inaccuracy: (1) Scene illumination: depending on topography and illumination directions, it is 111 not uniform as expected. (2) Polygon-shape spread images: depending on topography and 112 viewing direction, these polygon-shapes can be very complex, which explains the presence of 5

border effects in simulated images and inaccurate Earth-Atmosphere radiative coupling. The initial infinite slope mode was also constrained by technical issues: the required random access memory (RAM) and simulation time could be unexpectedly large depending on the scene topography. For example, compared to the simulation of an urban or vegetation landscape on a horizontal surface, the simulation of this landscape on a 30° slope could increase the RAM demand by a factor of 8, and computation time by a factor of 1.5.

119

120 This paper presents a new modelling strategy of DART infinite slope mode designed to improve 121 the accuracy and efficiency of DART RT modelling for sloping landscapes. Section 2 presents 122 major DART characteristics related to the present work. Section 3 describes the initial DART 123 infinite slope modelling method and its issues. Section 4 details the new infinite slope modelling 124 strategy, with additional information in the appendix. Section 5 firstly illustrates DART 125 improvements with simulations of a solo slope and a tree on a solo slope, and secondly presents 126 the validation of the new strategy with two simulated scenes: 1) a rugged slope, 2) a realistic 127 forest on a rugged slope. Finally, section 6 presents concluding remarks and perspectives.

128

- 129 2 DART model and infinite slope mode
- 130 2.1 General description
- 131

DART (https://dart.omp.eu) has been developed at CESBIO since 1992 (Gastellu-Etchegorry
et al., 1996; Gastellu-Etchegorry et al., 2017). It is one the most accurate and comprehensive
3D RT model in the optical remote sensing community. It simulates the RB, bi-directional
reflectance factor (BRF) and directional brightness temperature (BTF), images of
spectroradiometers at any altitude of 3D natural and urban landscapes, with topography and

137 atmosphere (Figure 1), for any viewing direction, from visible to thermal infrared domain. It 138 simulates also the sun induced chlorophyll fluorescence of 3D vegetation canopies and the 139 terrestrial and aero-spatial LiDAR signal (point cloud, waveform, photon counting).

140

141 In DART, the atmosphere is a layered horizontally homogeneous volume (Figure 1). A SQL 142 database stores the spectral optical properties and vertical profiles of its constituents (*i.e.*, gases, aerosols, clouds). The Earth scene (*i.e.*, urban / vegetation landscape) is an array of cells (*i.e.*, 143 144 voxels) (Figure 1) where elements are made of facets, also called triangles, possibly combined 145 with cells filled with turbid vegetation medium or fluids (air, soot, water, etc). SQL databases 146 store optical properties that can be assigned to scene elements. The integrated PROSPECT / 147 FLUSPECT leaf model (Jacquemoud et al., 1990; Vilfan et al., 2016; Feret et al., 2017) 148 computes leaf optical properties and fluorescence using leaf biochemistry and structure. 149 Orthographic and perspective (pinhole, pushbroom, fisheye) cameras are also simulated in 150 order to generate satellite, airborne and in-situ RS images (Yin et al., 2015). Up to DART 5.7.4, 151 these images are generated by a bi-linear interpolation method.

152



Figure 1. DART 3D discrete mock-up. Landscape elements are made of triangles, and/or fluid and
 turbid vegetation cells. The landscape itself is a cell matrix in order to ease ray tracing. The
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atmosphere has three levels: upper level made of layers, middle level made of cells of any size,and lower level in the landscape.

158 DART simulates the RT in the Earth-atmosphere system with an iterative discrete ordinate 159 method (Gastellu-Etchegorry et al. 1996, 2004, 2008, 2017), *i.e.*, radiation intercepted at 160 iteration *n* is scattered at iteration n + 1, by tracking steady-state energy flux $W(r, \lambda, \Omega)$ (unit: 161 W/sr/µm) along a finite number of directions Ω at position r(x, y, z), at wavelength λ using the 162 RT equation for a monochromatic radiation

163

$$\left(\xi \frac{d}{dx} + \eta \frac{d}{dy} + \mu \frac{d}{dz} \right) W(r, \lambda, \Omega) = -\alpha_e(r, \lambda, \Omega) W(r, \lambda, \Omega) + \alpha_a(r, \lambda, \Omega) W_B(T, \lambda, \Omega)$$

$$+ \int_0^{4\pi} \alpha_s(r, \lambda, \Omega') \frac{P(r, \lambda, \Omega' \to \Omega)}{4\pi} W(r, \lambda, \Omega') d\Omega'$$

$$(1)$$

164

where the term on the left side of equation (1) is the divergence of spectral energy, with (ξ, η, μ) 165 166 being the unit vector of direction Ω . The three terms on the right side of equation (1) are the 167 extinction and thermal emission along direction Ω , and the integrated scattering radiant flux into direction Ω over 4π space (Subrahmanyan Chandrasekhar, 2013). The total extinction 168 coefficient α_e is the sum of absorption and scattering extinction coefficient ($\alpha_e = \alpha_a + \alpha_s$). 169 W_B is the thermal energy flux emitted by a black body. $\frac{P(r,\lambda,\Omega'\to\Omega)}{4\pi}$ is the scattering phase 170 function. It represents the proportion of incident flux along Ω' that is scattered per solid angle 171 along Ω . 172

Figure 2 illustrates the 5 major steps of DART RT modelling in the Earth-atmosphere system.
(1) Atmosphere thermal emission and sun illumination. (2) Earth surface RT. (3) Earth-

- 176 atmosphere radiative coupling. (4) Earth surface RT of atmosphere backscattered radiation. (5)
- 177 Transfer of BOA upward radiation to any altitude, including TOA.
- 178



Figure 2. Major steps for modelling RT in the Earth-atmosphere system. Thermal emission in mode (T) is shown by the red symbol (steps 1 and 2). Arrows indicate directly transmitted solar (orange) and thermal (red) radiation, and scattered radiation (yellow), either thermal or solar.

179

184 **2.2 Infinite slope mode**

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186 Earth surface RT is simulated with one of three modes. (1) Isolated scene mode (Figure 3.a). The Earth surface RT does not depend on neighbouring landscape: a ray that exits the scene 187 188 does not re-enter the scene. It corresponds to laboratory experiments where only the studied 189 scene is illuminated. (2) Repetitive scene mode (Figure 3.b). The landscape is an infinite 190 horizontal duplication of the actually simulated scene: a ray that exits the 3D scene through a 191 point M_{out} on a vertical face re-renters the scene along the same direction through a point M_{in} 192 symmetric to M_{out} , at the same altitude. (3) Infinite slope mode (Figure 3.c). The landscape is 193 an infinite duplication of the actually simulated scene with a continuity of slope and altitude at 194 the DEM edges: a ray that exits the scene at M_{out} on a scene vertical face re-enters the scene at M_{in} , with an altitude shift equal to the altitude difference of the actually simulated scene and 195 9

the duplicated scene at ray exit face. The infinite slope mode was designed for the simulation of sloping landscapes. Conversely to the repetitive scene mode that leads to unrealistic border effects in presence of slope. Only the repetitive scene mode and the infinite slope mode can simulate environmental effect. Both verify the energy conservation.

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Figure 3. The three DART modes for simulating RT in 3D scenes. a) Isolated scene mode. b) Repetitive
 scene mode. c) Infinite slope mode. The actually simulated scene is framed by a black box.
 The dotted box frames one of the fictive neighbourhoods of the actually simulated scene.

205

206 **2.3** Construction of infinite slope mock-up

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208 In the infinite slope mode, the mean altitude of each edge of the DEM is computed to get the 209 mean vertical shifts ΔZ_X and ΔZ_Y of the neighbour duplicated scenes, along the axes X and Y, 210 respectively (Figure 4). Figure 4 displays the infinite spatial repetition of this Earth scene. If 211 the altitudes of the opposite edges of a DEM are not parallel, the DEM edges and corners are 212 smoothly connected by Bezier triangles (Gerald, 2014) to ensure the continuity of slopes and 213 altitudes at the DEM edges of the actually simulated scene and its duplications. Whatever the 214 Earth scene topography, the atmosphere above the BOA interface is horizontal, since density, 215 pressure and temperature of DART atmosphere are assumed identical at the same altitude.





Figure 4. DART scene in infinite slope mode with its infinite duplications. Three duplications are shown here. The mean altitude differences between neighbour Earth scenes are indicated (ΔZ_X for axis X and ΔZ_Y for axis Y). DEM edges are smoothly connected with Bezier triangles.

221 **3** Initial results and problems

222 **3.1 Initial strategy**

223

224 In the initial infinite slope mode, illumination (Figure 5.a) ray sources depart from the top scene 225 and/or from a so-called "scene window". A scene window is the part of the scene vertical face 226 through which an exit-ray will not re-enter the scene. Its spatial extent depends on the slope and 227 ray direction. It is computed per illumination direction. Figure 5.a shows a simple 2D example 228 with rays parallel to the paper plane. In 3D, the scene window geometry can be very complex 229 to manage, which in turn can lead to serious illumination flaws. During the Earth surface RT 230 modelling, a ray that exits the scene top/scene window along direction Ω_n is projected to the spread image on the Horizontal Plane (HP) (Figure 5.b), whereas a ray that crosses a scene 231 232 vertical face outside the scene window re-enters the scene from the opposite face with an 233 altitude shift (*i.e.*, ΔZ_X along axis X and ΔZ_Y along axis Y as indicated in Figure 4). The shape 11

234 and dimension of spread images on HP depend on the slope and ray direction. For some 235 directions, the shape of spread images can be very complex polygons, possibly much larger 236 than the scene horizontal section. The impossibility to accurately define their shapes for any 237 configuration can introduce two other drawbacks. (1) Difficulty to connect the polygon-shape 238 spread images to generate parallelogram shape image products. (2) Impossibility to know if 239 pixels with zero value in the image plane corresponds to the spread image (i.e., the observed 240 scene), which can lead to images with overestimated mean radiance if totally shadowed zones 241 are observed (*i.e.*, apparent reflectance equal to zero).



Figure 5. 2D view of the infinite slope mode RT modelling of initial DART. a) Illumination stage. b) Spread image generation stage. The scene window for direction Ω_n is the dark blue region at the scene vertical face. Its shape depends on the DEM and the illumination direction. Red arrows are rays in the paper plane. Illumination ray sources start from the scene top and window. Rays that cross scene top/window never re-enter the scene, conversely to rays that cross other parts of the scene vertical face. HP is the horizontal plane that stores the spread images.

Atmosphere backscattered energy and RS images are derived from spread images on HP. In the
Earth-Atmosphere coupling stage, upward rays are assumed to come from the rectangular scene
top, since the shape of spread images is too complex to manage. In the RS image generation

stage, the centre of each sensor pixel (i, j) is projected onto HP along its viewing direction, Figure 6.a illustrates a pinhole camera image generation process. Then, a bi-linear interpolation method derives the pixel value $X_{\text{sensor}}(i, j)$ from the values of four pixels $(X_{\text{HP}}(i', j'),$ $X_{\text{HP}}(i' + 1, j'), X_{\text{HP}}(i', j' + 1), X_{\text{HP}}(i' + 1, j' + 1))$ on HP that surround the projected point (Eq. (2)).

$$X_{\text{sensor}}(i,j) = (X_{\text{HP}}(i',j') \cdot \Delta x_1 + X_{\text{HP}}(i'+1,j') \cdot \Delta x_2) \cdot \Delta y_1 + (X_{\text{HP}}(i',j'+1) \cdot \Delta x_1 + X_{\text{HP}}(i'+1,j'+1) \cdot \Delta x_2) \cdot \Delta y_2$$
(2)

259 where Δx and Δy are the scale coefficients between 0 and 1, they are shown in Figure 6.b.



Figure 6. Pinhole camera image generation using an interpolation method. a) Projection onto HP of the centre of a pixel in the sensor image. b) Nadir view of the projected point. Δx and Δy are the scale coefficients that vary from 0 to 1.

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265 3.2 Results and problems

This section illustrates issues of the initial infinite slope mode through visual and statistical analysis of DART BRF profile, and RB and RS images (Figure 7 and Figure 8). To facilitate the analysis, two solo slope simulations are analysed, first a slope with a Lambertian bare ground (Figure 7.a), and then a slope with a tree (Figure 8.a). Table 2 lists DART input parameters. The solo slope is created by the DART DEM generator. Figure 7.b shows its energy 13

map (*i.e.*, intercepted flux $\sum_{z} W(i, j, z)$ (W/µm) per pixel (*i*, *j*)) with regular microgrooves and 272 polygon-shapes. The intercepted energy flux has a relative variability $(W_{max}-W_{min})/W_{mean}$ up 273 to 25% although it should be zero. It is due to a mismanagement of illumination and coupling 274 275 energy. Figure 7.c shows the scene reflectance in the solar plane, the BRF varies up to 11% 276 relative to nadir reflectance whereas it should be a constant. Its dependence on the viewing zenith angle θ_{ν} is due to the boarder effect when connecting polygon-shape spread images. It 277 is all the more serious if the viewing direction is close to the slope (viewing zenith angle $\theta_{\nu} < -$ 278 279 54° in Figure 7.c).

280

281 The simulation of a cherry tree on the solo slope illustrates other issues. Tree trunk, branches 282 and leaves are Lambertian surfaces. Figure 8.b-f shows DART RS images: satellite (orthographic) camera for viewing directions equal to ($\theta_{sensor}=41^\circ$, $\varphi_{sensor}=194^\circ$) (b) and 283 $(\theta_{sensor}=80^\circ, \varphi_{sensor}=355^\circ)$ (c), fisheye camera (d), pinhole camera (e) and pushbroom (f). 284 285 Several issues affect image quality: (1) microgrooves, (2) border effect, and (3) erroneous areas. 286 Microgrooves arise because the ray illumination mesh on the object surface is coarser than 287 DART cell dimensions, for some directions. As a result, triangles between two rays are less 288 illuminated. If the image resolution is high enough, these less illuminated triangles can lead to lines of darker pixels. Because of the microgrooves, the reflectance of ground (averagely 0.29) 289 290 in Figure 8.b has maximum difference 0.04 with standard deviation 0.004. The initial modelling 291 strategy did not manage the spatial variability of the density of illumination rays on local 292 topography. Hence, the density of illumination rays varies with the local slopes, although it is 293 spatially uniform on the BOA horizontal plane. The second and third issues arise with the 294 procedure that connects the spread images. In the initial strategy, the polygon-shape spread images are juxtaposed in order to obtain a parallelogram RS image. According to the definition 295 296 of the infinite slope, the opposite sides of any spread image should be continuous. However, 14

297 this is not always the case if the slope or the viewing direction is very oblique. Also, 298 discretization explains that pixel values on the borders of a spread image can be over or 299 underestimated. It results that the connected borders of the spread image appear with darkish 300 and whitish tones in the final image (Figure 8.b). The complex shape of the spread images also 301 gives rise to zones without signal (*i.e.*, yellow zones) or with overestimated neighbour zones (*i.e.*, whitish zones) (Figure 8.c). In addition, the yellow zone on the cherry tree in Figure 8.c 302 303 has zero reflectance. These zones are discarded since the initial algorithm cannot distinguish 304 zero radiance and no-signal pixel.

305

In short, Figure 7 and Figure 8 stress two major sources of inaccuracy of the initial infinite slope mode: scene illumination and polygon-shape spread image management. An important technical drawback must be noted as well: the required RAM to store images greatly increases with the obliquity of viewing directions. For example, in the above schematic example, the infinite slope mode requires more than 8 times RAM than the repetitive scene mode. The next section presents a new modelling strategy that was developed to improve this situation.

313	Table 2. DART input parameters. θ is a zenith angle, φ is an azimuth angle oriented anticlockwise
314	from South ($\varphi_{\text{South}} = 0^\circ$, $\varphi_{\text{East}} = 90^\circ$, $\varphi_{\text{North}} = 180^\circ$ and $\varphi_{\text{West}} = 270^\circ$). ρ is a reflectance.
315	Dash symbol stands for "no-value". USSTD76 atmospheric constituent profile and RURAL
316	aerosol model are defined in Anderson et al., 1986 and Shettle and Fenn, 1979, respectively.

Parameters	Solo slope	Solo slope + Cherry tree
Spectral band	0.56 μm	0.56 μm
Sun direction	$\theta_{\rm sun}$ =30°, $\varphi_{\rm sun}$ =225°	θ_{sun} =30°, φ_{sun} =225°
Atmosphere model	USSTD76	USSTD76

Aerosol model	RURAL_V23KM	RURAL_V23KM
Scene dimension	X = Y = 40 m	X = Y = 40 m
Spatial resolution	0.125 m	0.125 m
DEM	30° solo slope ($\varphi_{slope}=45^\circ$)	30° solo slope ($\varphi_{slope}=45^\circ$)
$ ho_{ m ground}$	0.5	0.5
Tree	-	Cherry tree
Tree position	-	x = y = 20 m
$ ho_{ ext{leaf}}$	-	0.11
$ au_{ ext{leaf}}$	-	0.1
$ ho_{ m trunk}$	-	0.075





Figure 7. Simulation of a solo slope, using the initial infinite slope mode. DEM mesh with indication of slope azimuth angle φ_{slope} , and zenith and azimuth angles ($\theta_{sun}, \varphi_{sun}$) of the direction in which the sun is seen from the Earth surface (a), φ is anticlockwise from South. Solo slope: spectral energy flux map (b) and angular reflectance in the solar plane (c).



Figure 8. Simulation of a cherry tree on a solo slope, using the initial infinite slope mode. Satellite (orthographic) camera images (b, c) with 2 viewing directions, fisheye camera image (d), pinhole camera image (e) and pushbroom image (f).

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328 4 The new infinite slope mode

329 4.1 Introduction of oblique planes OP

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The new modelling strategy of the infinite slope mode aims to get more accurate and more systematic modelling of the scene illumination, the Earth-atmosphere radiative coupling, and the image generation, for sloping landscapes. The innovation is to introduce an auxiliary oblique plane OP that depends only on topography to store spread images and to simulate scene illumination, instead of HP. OP ensures that the spread images have the same shape and size, and that the RAM demand is independent of topography. Geometrically, OP is a parallelogram, the four sides of which belong to the four vertical faces of the scene (Figure 9.b). The opposite sides of OP have altitude differences ΔZ_X along axis X and ΔZ_Y along axis Y equal to the altitude differences between the duplicated scenes (Figure 4, Figure 9.b). The vertical projection of any OP pixel on HP has the same size and shape as DART scene cells.

341

342 DART atmospheric RT and Earth surface RT modelling are sequential. In the scene 343 illumination and Earth-atmosphere radiative coupling stages, energy conservation is ensured. 344 To quantify downward radiation from the horizontal atmosphere to OP and upward radiation from OP to the horizontal atmosphere, the parallel projection of OP along Ω_n onto a horizontal 345 346 plane is computed per direction Ω_n . Its projected surface $\Sigma_p(\Omega_n)$ (Figure 9.c) is a parallelogram. The four corner coordinates (x_p, y_p, z_p) of $\Sigma_p(\Omega_n)$ depend on the direction vector Ω_n and the 347 348 coordinates (x_o, y_o, z_o) of the four corners of OP. Ω_n is characterized by its zenith angle θ and azimuth angle φ . We have $\theta = 0^\circ$ for nadir direction, ($\theta = 90^\circ, \varphi = 0^\circ$) for a direction parallel 349 350 to the x-axis, and ($\theta = 90^\circ, \varphi = 90^\circ$) for a direction parallel to the y-axis.

$$\begin{cases} z_p - z_o = d \cos \theta \\ x_p - x_o = d \sin \theta \cos \varphi \\ y_p - y_o = d \sin \theta \sin \varphi \end{cases}$$
(3)

where *d* is the distance between OP corner (x_o, y_o, z_o) and the projected point (x_p, y_p, z_p) . The norm of the cross product of any two adjacent sides of the projected parallelogram $\Sigma_p(\Omega_n)$ is its area $S_p(\Omega_n)$. Note that the parallel projection of OP on any horizontal plane, including the horizontal atmosphere, gives the same projected area $S_p(\Omega_n)$.

In presence of slope, if the viewing direction is more inclined than the slope (*i.e.*, $\Omega_n^{\dagger} \cdot \boldsymbol{n} < 0$, with \boldsymbol{n} the normal of OP), no signals can be observed along these upward directions Ω_n^{\dagger} . In addition, if the illumination direction is more inclined than the slope (*i.e.*, $\Omega_n^{\downarrow} \cdot \boldsymbol{n} > 0$), no light along these downward directions Ω_n^{\downarrow} can reach the scene. Therefore, these directions are set as inactive and called inactive directions $\Omega_{n,\text{inactive}}$. Inactive downward directions $\Omega_{n,\text{inactive}}^{\downarrow}$ are eliminated during the illumination stage, and inactive upward directions $\Omega_{n,\text{inactive}}^{\uparrow}$ are not considered to compute atmosphere backscattered energies.



Figure 9. DART infinite slope mode. a) Earth scene and its fictive oblique plane OP at the scene bottom. b) DEM altitude differences are ΔZ_X along axis X and ΔZ_Y along axis Y axis. c) Projected surface (blue parallelogram) $\Sigma_p(\Omega_n)$ of OP along direction Ω_n onto the horizontal plane that contains the highest point of OP, it has an area equal to $S_p(\Omega_n)$.

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369 4.2 Illumination of the Earth scene

371 Atmospheric RT modelling, including sun radiation and atmosphere thermal emission and 372 scattering, gives a spectral energy flux $W_h(\Omega_n)$ [W/µm] per direction $(\Omega_n, \Delta\Omega_n)$ per spectral 373 band in three fictive layers (Gastellu-Etchegorry et al., 1996). (1) BOA: $W_{BOA}(\Omega_n^{\downarrow})$ [W/µm]

374 per downward direction Ω_n^{\downarrow} including solar direction Ω_s . (2) TOA: $W_{\text{TOA}}(\Omega_n^{\uparrow})$ [W/µm] per 375 upward direction Ω_n^{\uparrow} . (3) Sensor layer at any altitude *h*: $W_{\text{sensor}}(\Omega_n)$ [W/µm] per upward and 376 downward direction Ω_n . Equation (4) gives the irradiance of each fictive layer.

$$E_{\text{BOA}}^{\text{dir}} = \frac{W_{\text{BOA}}(\Omega_s)}{S_{\text{scene}}}, \qquad E_{\text{BOA}}^{\text{diff}} = \frac{\sum_{\Omega_n^{\downarrow}} W_{\text{BOA}}(\Omega_n^{\downarrow})}{S_{\text{scene}}}$$

$$E_{\text{sensor}}^{\text{dir}} = \frac{W_{\text{sensor}}(\Omega_s)}{S_{\text{scene}}}, \qquad E_{\text{sensor}}^{\text{diff}} = \frac{\sum_{\Omega_n^{\downarrow}} W_{\text{sensor}}(\Omega_n^{\downarrow})}{S_{\text{scene}}}$$
(4)

377 with S_{scene} the area of scene horizontal section, E^{dir} the direct irradiance and E^{diff} the diffused 378 irradiance.

379

380 The downward flux incident along direction Ω_n^{\downarrow} on a pixel (i, j) at BOA level, knowing that the 381 BOA interface has $I_{BOA} \cdot J_{BOA}$ pixels, is

$$W_{\rm BOA}(i,j,\Omega_n^{\downarrow}) = \frac{W_{\rm BOA}(\Omega_n^{\downarrow})}{I_{\rm BOA} \cdot J_{\rm BOA}}$$
(5)

Using the law of conservation of energy, the incident energy flux per direction Ω_n^{\downarrow} on pixel (*i*, *j*) of OP (*i.e.*, I_{BOA} lines and J_{BOA} columns) is

$$W_{\rm OP}(i,j,\Omega_n^{\downarrow}) = W_{\rm BOA}(i,j,\Omega_n^{\downarrow}) \cdot \frac{S_p(\Omega_n^{\downarrow})}{S_{\rm scene}}$$
(6)

with $S_p(\Omega_n^{\downarrow})$ the projected surface of OP onto the horizontal atmosphere along direction Ω_n^{\downarrow} .

In the illumination stage, *M* equal energy rays are sent per OP pixel per downward direction to illuminate the Earth scene. To uniformly illuminate sloping terrains (*i.e.*, same user-defined ray density *M* per direction), the illumination position $P_{OP}(x, y, z)$ on OP is first sampled using a semi-random method per pixel (*i*, *j*). Note a larger *M* improves the accuracy of results but increases computation time. Default M = 100 is a compromise between accuracy and time cost. 391 Then, $P_{OP}(x, y, z)$ is projected to the scene top and scene window per downward direction Ω_n^{\downarrow} 392 with a backward ray tracing method to set the ray source position $P_{ray}(x, y, z)$ (Figure 10) at 393 scene top or scene window. Ray energy flux $W_{ray}(i, j, \Omega_n^{\downarrow}, P_{ray})$ is computed only for active 394 directions.

$$W_{\rm ray}(i,j,\Omega_n^{\downarrow},P_{\rm ray}) = \frac{W_{\rm OP}(i,j,\Omega_n^{\downarrow})}{M}$$
(7)

395



Figure 10. 2D (a) and 3D (b) views of the scene illumination stage. $\Sigma_{BOA}(\Omega_n)$ is the projected surface of OP onto the horizontal BOA plane with backward ray tracing method; its area is $S_p(\Omega_n)$. After atmospheric RT modelling, rays through $\Sigma_{BOA}(\Omega_n)$ along direction Ω_n illuminates the scene. $P_{ray}(x, y, z)$ (**x**) is the source point of an incident ray, on the scene top or scene window. $P_{OP}(x, y, z)$ (**x**) is the projection on OP of $P_{ray}(x, y, z)$ along incident direction Ω_n .

402

396

403 4.3 Spread of ray energy on OP during Earth surface RT modelling

405 After the illumination and landscape thermal emission stages, the scene surface and volume 406 elements iteratively scatter all or part of the intercepted radiation, *i.e.*, radiation intercepted at 407 iteration *n* is scattered at iteration n + 1 (*i.e.*, step 2 in Figure 2). The number of iterations must

408 be large enough in order to get accurate results. It depends on the spectral domain and on 409 landscape characteristics. Generally, the energy flux cumulated on the spread images follows 410 an exponential relation with iteration number n (Kallel Abdelaziz, 2018). Hence, at the end of the Earth surface RT process, the energy fluxes per pixel per direction $W^{\text{iter }n}(i, j, \Omega_n^{\uparrow})$ at 411 different iteration orders *n* are extrapolated to get $W^{\text{iter } X}(i, j, \Omega_n^{\uparrow})$ at an infinite iteration order. 412 Upward radiation that exits the scene top/window is projected onto OP (Figure 11.a) at the 413 414 scene bottom along its propagation direction instead of HP at scene bottom (Figure 5.b) as in the original DART RT modelling in Gastellu-Etchegorry et al., 1996. Storing ray energy in a 415 416 plane at the bottom of the scene minimizes the shift of Earth objects in directional images and 417 simplifies the generation of RS images (Yin et al., 2015).



419

Figure 11. Ray projection on OP. a) The red triangle gives rise to a ray along direction r (red arrow) that reaches the scene top. The green triangle is its projection onto OP. P is the projection on OP of a corner l_0 of the red triangle. d is the distance $||P - l_0||$. P_0 is the highest point of OP. b) Parallel projection for the orthographic camera and perspective projection for the perspective camera. c) Nadir view of the projected triangle on OP and its break-down into four polygons.

The projection process is presented here. Let a facet Σ in the 3D scene gives rise to an emitted and/or scattered energy flux along direction r that exits the scene top or scene window. In that case, Σ is projected along r onto OP where the energy flux is stored per pixel in a spread image. Its projected surface is Σ_{OP} (Figure 11.a). Let a corner P of Σ_{OP} be the projection of a corner l_0 of Σ along direction r onto OP (normal n) (Figure 11.a), P_0 the highest point of OP, and d the distance $||P - l_0||$. The coordinate of P is computed with

$$\begin{cases} (P_0 - P) \cdot \boldsymbol{n} = 0\\ P = l_0 + d \cdot \boldsymbol{r} \end{cases} \Rightarrow \begin{cases} d = \frac{(P_0 - l_0) \cdot \boldsymbol{n}}{\boldsymbol{r} \cdot \boldsymbol{n}}\\ P = l_0 + d \cdot \boldsymbol{r} \end{cases}$$
(8)

In Figure 11.c, the projected surface Σ_{OP} is at the intersection of four pixels. Hence, it is partitioned into four polygons with one polygon Σ_{OP}^{k} per pixel k. The energy flux distributed per pixel k is proportional to the surface ratio $\Sigma_{OP}^{k}/\Sigma_{OP}$.

435

436 After the Earth surface RT stage, DART products (reflectance $\rho^{\text{iterX}}(i, j, \Omega_n^{\uparrow})$, radiance 437 $L^{\text{iterX}}(i, j, \Omega_n^{\uparrow})$, brightness temperature $T_B^{\text{iterX}}(i, j, \Omega_n^{\uparrow})$, etc.) and their mean values are derived 438 (Eq. (9)) from the energy fluxes $W_{\text{OP}}^{\text{iterX}}(i, j, \Omega_n^{\uparrow})$ per pixel per direction on the spread images. 439

$$L^{\text{iterX}}(i,j,\Omega_{n}^{\uparrow}) = \frac{W_{\text{OP}}^{\text{iter X}}(i,j,\Omega_{n}^{\uparrow})}{S_{p}(i,j,\Omega_{n}^{\uparrow})\cdot\cos\theta_{n}\cdot\Delta\Omega_{n}^{\uparrow}}, \rho^{\text{iterX}}(i,j,\Omega_{n}^{\uparrow}) = \frac{\pi \cdot L^{\text{iter X}}(i,j,\Omega_{n}^{\uparrow})}{E_{\text{BOA}}^{\text{dir}} + E_{\text{BOA}}^{\text{diff}}},$$

$$\overline{L}^{\text{iter X}}(\Omega_{n}^{\uparrow}) = \frac{\sum_{i} \sum_{j} L^{\text{iter X}}(i,j,\Omega_{n}^{\uparrow})}{I_{\text{BOA}} \cdot J_{\text{BOA}}}, \omega_{\text{scene}}^{\text{iter X}} = \frac{\sum_{\Omega_{n}^{\uparrow}} \overline{L}^{\text{iter X}}(\Omega_{n}^{\uparrow})\cos\theta_{n}\Delta\Omega_{n}^{\uparrow}}{E_{\text{BOA}}^{\text{dir}} + E_{\text{BOA}}^{\text{diff}}}$$
(9)

440

441 with $S_p(i, j, \Omega_n^{\dagger})$ the projected surface of OP pixel (i, j) onto HP along direction Ω_n^{\dagger} , $\Delta \Omega_n^{\dagger}$ the 442 solid angle of direction Ω_n^{\dagger} , and θ_n the zenith angle of direction Ω_n^{\dagger} . $\overline{L}(\Omega_n^{\dagger})$ is the average 443 exitant radiance along direction Ω_n^{\dagger} and ω_{scene} is the scene albedo.

- 444
- 23

445 4.4 Earth surface RT of the atmosphere backscattered radiation

446

447 After the Earth surface RT stage (*i.e.*, step 2 in Figure 2), part of the upward flux 448 $W_{OP}^{\text{iter X}}(i, j, \Omega_n^{\uparrow})$ that exits the scene is backscattered by the atmosphere to the Earth surface (*i.e.*, 449 step 3 in Figure 2). The backscattered flux is computed by convolving upward radiation from 450 the Earth scene with transfer function TF_{BA-BA}($\Omega_n^{\uparrow}, \Omega_n^{\downarrow}$) (Grau and Gatellu-Etchegorry, 2013)

$$W_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow}) = \frac{1}{1 - \omega_{\text{scene}} \cdot \bar{S}} \sum_{\Omega_n^{\uparrow}} W_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow}) \cdot \text{TF}_{\text{BA-BA}}(\Omega_n^{\uparrow}, \Omega_n^{\downarrow})$$
(10)

451 with \bar{S} the average atmosphere albedo and $W_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow}) = \sum_i \sum_j W_{\text{OP}}^{\text{iter X}}(i, j, \Omega_n^{\uparrow}) \cdot \frac{S_{\text{scene}}}{S_p(\Omega_n^{\uparrow})}$ the 452 upward energy flux at BOA along direction Ω_n^{\uparrow} . $W_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow})$ is used to get backscattered 453 energy flux per pixel per direction at BOA $W_{\text{BOA}}^{\text{backscat}}(i, j, \Omega_n^{\downarrow}) = \frac{W_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow})}{I_{\text{BOA}}I_{\text{BOA}}}$ and the 454 atmosphere backscattered irradiance $E_{\text{BOA}}^{\text{backscat}} = \frac{\sum_{\Omega_n^{\downarrow}} W_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow})}{S_{\text{scene}}}$. More Details are given in 455 appendix A.

456

457 Atmosphere backscattering gives a new Earth scene illumination (*i.e.*, step 4 in Figure 2). The
458 resulting backscattered flux per OP pixel (Eq. (11)) ensures the conservation of energy (Eq. (6))

$$W_{\rm OP}^{\rm backscat}(i,j,\Omega_n^{\downarrow}) = W_{\rm BOA}^{\rm backscat}(i,j,\Omega_n^{\downarrow}) \cdot \frac{S_p(\Omega_n^{\downarrow})}{S_{\rm scene}}$$
(11)

459 Then, the Earth surface RT is simulated again, and upward energy $W_{OP}(i, j, \Omega_n^{\uparrow})$ per direction 460 is cumulated per OP pixel per direction. The resulting upward flux $W_{OP}^{coupl}(i, j, \Omega_n^{\uparrow})$ is used to 461 compute pixel and scene radiance and reflectance products (marked as coupl in equation (12)).

$$L^{\text{coupl}}(i,j,\Omega_n^{\uparrow}) = \frac{W_{\text{OP}}^{\text{coupl}}(i,j,\Omega_n^{\uparrow})}{S_p(i,j,\Omega_n^{\uparrow}) \cdot \cos \theta_n \cdot \Delta \Omega_n^{\uparrow}}, \rho^{\text{coupl}}(i,j,\Omega_n^{\uparrow}) = \frac{\pi \cdot L^{\text{coupl}}(i,j,\Omega_n^{\uparrow})}{E_{\text{BOA}}^{\text{dir}} + E_{\text{BOA}}^{\text{dirf}} + E_{\text{BOA}}^{\text{backscat}}}$$
(12)

$$\overline{L}^{\text{coupl}}(\Omega_n^{\uparrow}) = \frac{\sum_i \sum_j L^{\text{coupl}}(i,j,\Omega_n^{\uparrow})}{I_{\text{BOA}} J_{\text{BOA}}}, \ \omega_{\text{scene}}^{\text{coupl}} = \frac{\sum_{\alpha_n^{\uparrow}} \overline{L}^{\text{coupl}}(\Omega_n^{\uparrow}) \cos \theta_n \Delta \Omega_n^{\uparrow}}{E_{\text{BOA}}^{\text{dir}} + E_{\text{BOA}}^{\text{dir}} + E_{\text{BOA}}^{\text{backscat}}}$$

Fluxes $W_{OP}^{coupl}(i, j, \Omega_n^{\uparrow})$ are tracked in the atmosphere and then cumulated at TOA and sensor levels (*i.e.*, step 5 in Figure 2) (Grau and Gatellu-Etchegorry, 2013). More details are given in appendix B.

465

466 4.5 Image generation

467

468 Once the radiometric products are computed as spread images, they are projected to the sensor 469 plane. Here, the initial algorithm (Gastellu-Etchegorry et al., 2008; Yin et al., 2015) is improved 470 to get more accurate sensor images: sensor image pixel value is computed with a precise 471 projection method instead of the bi-linear interpolation method. In addition, the lambert 472 azimuthal equal-area projection is introduced to generate fisheye images.

473

474 Although the interpolation method is simple to implement and computer efficient, it degrades 475 images, and the associated error increases for sloping landscapes and oblique viewing directions. 476 Hence, we implemented a precise projection method that costs reasonable calculation time. For 477 satellite (orthographic) camera, spread image pixels are parallelly projected to sensor plane 478 along the viewing direction Ω_n (Figure 12.a). For pinhole and pushbroom camera, spread image 479 pixels are perspectively projected to sensor plane along the local viewing direction Ω_n to camera focus (Figure 12.b, c). For fisheye camera, pixels are projected to a unit sphere along 480 481 its local viewing direction to the camera focus and then this pixel on the unit sphere is spread 482 on the image plane at the bottom of the unit sphere using the Lambert azimuthal equal-area 483 projection equation (Eq. (13)) that projects any point (x, y, z) on the unit sphere onto its bottom plane at (X, Y, -1) (Figure 13). 484

$$(X, Y, Z) = \left(\sqrt{\frac{2}{1-z}}x, \sqrt{\frac{2}{1-z}}y, -1\right)$$
(13)

486



488 Figure 12. Projection processes for simulating images. Parallel projection along direction Ω_n for 489 satellite (orthographic) camera (a), and perspective projection along local viewing direction 490 for pinhole camera (b) and pushbroom camera (c).



491

Figure 13. Projection processes for simulating fisheye images. First, pixel on OP is projected onto a unit sphere. Then, it is spread on the sensor plane with Lambert azimuthal equal-area projection method that projects a point (x, y, z) of the unit sphere onto the sensor plane at point (X, Y, Z). θ_{max} is the maximum viewing zenith angle.

497 Image dimensions, resolutions and field of view (FOV) are user-defined for perspective and 498 fisheve cameras whereas image resolution is that of DART cell dimensions for satellite 499 (orthographic) cameras. Projected images are further rasterized by the pixel grid in the sensor 500 plane. For that, the four corners of each pixel (i', j') on OP are projected to the sensor plane along the viewing direction Ω_n^{\uparrow} , where they make up a new quadrilateral $\Sigma_{i',j'}^{\text{sensor}}$. As in section 501 4.3, $\Sigma_{i',j'}^{\text{sensor}}$ is spread over sensor pixels, and $f(i, j, i', j', \Omega_n^{\uparrow})$ stores the part of $\Sigma_{i',j'}^{\text{sensor}}$ in a 502 sensor pixel (i, j). For example, $f(i, j, i', j', \Omega_n^{\uparrow}) = 0.5$ if $\Sigma_{i', j'}^{\text{sensor}}$ occupies 50% surface of a 503 sensor pixel (i, j). For any radiometric product, sensor pixel values $X_{\text{sensor}}(i, j, \Omega_n^{\uparrow})$ are 504 resampled (Eq. (14)) using the values $X_{OP}(i', j', \Omega_n^{\uparrow})$ of the projected OP pixels. 505

$$X_{\text{sensor}}(i,j,\Omega_n^{\uparrow}) = \sum_{i'} \sum_{j'} X_{\text{OP}}(i',j',\Omega_n^{\uparrow}) \cdot f(i,j,i',j',\Omega_n^{\uparrow})$$
(14)

506 Coordinates $(x_{\text{DART}}, y_{\text{DART}}, z_{\text{DART}})$ in the scene reference are transformed into coordinates 507 $(x_{\text{sensor}}, y_{\text{sensor}}, z_{\text{sensor}})$ in the sensor reference with a transfer matrix A (Eq. (15)), where 508 $(\theta, \varphi) = \text{sensor}(\text{zenith}, \text{azimuth})$ angles in the DART scene coordinate reference.

$$\begin{bmatrix} x_{\text{sensor}} \\ y_{\text{sensor}} \\ z_{\text{sensor}} \end{bmatrix} = A \begin{bmatrix} x_{\text{DART}} \\ y_{\text{DART}} \\ z_{\text{DART}} \end{bmatrix} \quad \text{with } A = \begin{bmatrix} \cos\theta\cos\varphi & \cos\theta\sin\varphi & -\sin\theta \\ -\sin\varphi & \cos\varphi & 0 \\ \sin\theta\cos\varphi & \sin\theta\sin\varphi & \cos\theta \end{bmatrix}$$
(15)

509 Due to the discretization, some pixels on the boarders of the sensor image cannot be entirely 510 covered by the projected pixels of the spread image. Therefore, this leads to underestimated 511 pixel values. To manage this problem, we eliminate the pixels in the sides of the sensor image 512 that are not entirely filled by the projected pixels of the spread image.

513

514 **5** Results and validation

518 With the new modelling strategy, conversely to the initial infinite slope mode, scene irradiance 519 is spatially uniform, spread images have the same shape and dimension for any viewing direction, and energy conservation is ensured during the Earth-Atmosphere radiative coupling. 520 521 These improvements allow DART to simulate accurate RS signals of sloping landscapes. In 522 addition, image accuracy is further improved thanks to the new projection method instead of 523 the previous bi-linear interpolation method. Here, these results are illustrated with DART 524 simulations of the same scenes as in section 3.2 (Figure 7, Figure 8). As expected, the issues 525 previously noted are corrected. For the solo slope scene, the intercepted energy flux is spatially 526 constant (Figure 14.b) and reflectance in the solar plane is constant (Figure 14.c). Also, all 527 sensor images have a correct visual aspect (Figure 15.b-f): no more microgrooves, border effect, 528 and over or underestimated radiance values in parts of the images. Improvements on the 529 intercepted energy flux $\sum_{z} W(i, j, z)$ (W/µm) per pixel (*i*, *j*) and the scene average reflectance $\rho(\theta_v)$ in the solar plane $\varphi_v = 225^\circ$ per zenith angle, with a step $\Delta \theta_v = 1^\circ$, are quantified using 530 two quantities (*i.e.*, absolute relative error $\varepsilon_X(q)$ and mean absolute relative error $\overline{\varepsilon}_X$) defined 531 in equation (16). 532

$$\varepsilon_X(q) = \frac{|X_{\text{ref}}(q) - X(q)|}{X_{\text{ref}}(q)} \times 100\% \qquad \bar{\varepsilon}_X = \frac{1}{N} \sum_{q=1}^N \varepsilon_X(q) \tag{16}$$

where X indicates a type of DART product $(X = \rho \text{ for reflectance}; X = w \text{ for intercepted}$ energy flux), X(q) is an element q in X product. Subscript ref is the reference value under the same simulation condition. $\bar{\varepsilon}_{\rho}$ is the average value of $\varepsilon_{\rho}(\theta_{v})$ for each zenith angle θ_{v} in the solar plane, and $\bar{\varepsilon}_{w}$ is the average value of $\varepsilon_{w}(i, j)$ per pixel (i, j).

538 The new infinite slope mode is assumed to be the reference. This is fully justified for the solo slope for which results have been computed analytically. For example, the directional 539 reflectance factor of {solo slope with slope normal n and Lambertian reflectance ρ_{ground} } for 540 the sun direction Ω_{sun} (zenith angle θ_{sun}) is $\rho_{ground} \cdot \frac{|\Omega_{sun} \cdot n|}{\cos \theta_{sun}}$ for any viewing direction. Figure 541 542 14.c, Figure 16 and Table 3 show the errors in the initial infinite slope mode. For the solo slope scene, $\bar{\epsilon_{\rho}} \approx 4.6\%$ and $\bar{\epsilon_{w}} \approx 2.8\%$. For the scene of solo slope with a cherry tree, $\bar{\epsilon_{\rho}} \approx 4.0\%$ and 543 $\bar{\varepsilon}_w \approx 3.1\%$. Two technical improvements must be noted. (1) The new Lambert azimuthal equal-544 area projection improves the realism of fisheye image (see Figure 15.d and Figure 8.d). (2) 545 546 RAM demand and computer time are greatly decreased for oblique slopes. For example, for the "Solo slope + Tree" simulation, RAM demand is reduced by 90% and simulation time is 547 548 reduced by 10%.



550 Figure 14. DART simulations with the new infinite slope mode. Solo slope. Same legend as Figure 7.



551

Figure 15. DART simulations with the new infinite slope mode. Solo slope plus a cherry tree. Same
legend as Figure 8.



Figure 16. Absolute relative error of DART energy flux images (*i.e.*, $\sum_{z} W(i, j, z)$ (W) per pixel (*i*, *j*)) simulated with the initial infinite slope mode. a) Solo slope. b) Solo slope with a cherry tree.

Table 3. Summary of the relative error of the initial infinite slope mode for a solo slope and a soloslope with a cherry tree, the results simulated with the new infinite slope are used as reference.

Error	Solo slope	Solo slope + Cherry tree
$ar{arepsilon_ ho}$	4.6%	4.0%
$\max(\varepsilon_{ ho})$	14.2%	7.0%
$ar{arepsilon_w}$	2.8%	3.1%
$\max(\varepsilon_w)$	14.5%	29.9%

558

559 5.2 Validation

560

Ideally, the validation of a modelling approach should be performed with actual measurements. As a first step, here we validate the new modelling strategy of the infinite slope mode using a purely modelling approach. The new DART infinite slope mode is tested with a rugged slope and a rugged slope with realistic forest. For that, two scenes are simulated:

565 1) Experimental scene: it was simulated with the initial (index init) and new (index new)566 infinite slope modes.

2) Reference scene: nine duplications of the experimental scene are juxtaposed with respect to the continuity of slopes and altitudes. Its central sub-zone corresponds to the experimental scene, which is called "reference experimental scene" (index ref). Although simulated with the new infinite slope mode, there is no fictive ray tracing (*i.e.*, application of the infinite slope mode) at the borders of the "reference experimental scene". Therefore, the "reference experimental scene" is used as the reference.

573

576 The rugged slope (Figure 17.a) in the experimental scene $(34 \text{ m} \times 34 \text{ m})$ is created by Blender software (<u>www.blender.org</u>). It has relatively large mean altitude shifts: $\Delta Z_X = 15$ m and 577 578 $\Delta Z_{Y} = 15$ m along the axes X and Y, respectively. Figure 17.b shows its slope map. The rugged 579 slope has an average slope 38° and a maximum slope 70°. By repeating 9 times the experimental 580 scene with respect to the continuity of slope and altitude, the reference scene (102 m \times 102 m) 581 (Figure 17.c) is created, it has mean altitude shifts $\Delta Z_X = 45$ m and $\Delta Z_Y = 45$ m along the 582 axes X and Y, respectively. DART simulations are for a direct sun illumination ($\theta_{sun} =$ 40°, $\varphi_{sun} = 300^\circ$), a 0.125 m spatial resolution and a NIR (near infrared: 0.87 µm) spectral 583 584 band. Ground optical properties are derived from the DART optical properties database. In addition, the roughness of the slope is adjusted by a z-scale factor F_z . For example, $F_z = 2$ 585 586 means all altitude values in the 3D slope are multiplied by 2. In this study, we investigated 3 rugged slopes with different roughness ($F_z = 0.8$, 1.0 and 1.2) to assess the robustness of the 587 588 new method.



589

Figure 17. The rugged slope. a) 3D view. b) slope map (unit °). c) 9 duplications of the rugged slope
(a) with respect to the continuity of slopes and altitudes.

592 Figure 18.a, b shows two satellite images simulated with initial infinite slope mode ($F_z = 1.0$),

593 the boarder effect and erroneous areas are obvious. These defects do not appear in the images 32 594 simulated by the new infinite slope mode. The microgrooves do not appear in Figure 18.a, b 595 because the variation of pixel reflectance masks the minor reflectance change due to the non-596 uniform illumination. Figure 18.c, f show the BRFs (*i.e.*, $\rho_{ref}(\theta_v)$, $\rho_{init}(\theta_v)$ and $\rho_{new}(\theta_v)$) in the solar plane (*i.e.* $\varphi_{\nu} = 300^{\circ}$) with zenith angle step $\Delta \theta_{\nu} = 2^{\circ}$ for 3 different z-scale factors 597 $(F_z = 0.8, 1.0 \text{ and } 1.2)$. They illustrate that the roughness can greatly impact the results of the 598 initial infinite slope mode ($\bar{\epsilon}_{\rho_{\text{init}}} \approx 33.3\%$, 69.0% and 174.8% for $F_z = 0.8$, 1.0 and 1.2) whereas 599 it has no impact on the new infinite slope mode ($\bar{\epsilon}_{\rho_{\text{new}}} < 10^{-4}$ for $F_z = 0.8$, 1.0 and 1.2). As 600 explained in section 3.1, the BRF in $[-90^\circ, \sim 50^\circ]$ region is overestimated because the initial 601 602 method discards total shadow (i.e., apparent reflectance equal to zero) when computing the 603 scene average reflectance (yellow zone in Figure 18.a). For images in the $[\sim 50^\circ, 90^\circ]$ region, 604 nearly no shadows are observed. Then, the underestimated BRF is due to the presence of black 605 borders (black lines in Figure 18.b), and mismanagement of image connections (yellow zone in 606 Figure 18.b).



Figure 18. DART simulated satellite images of the rugged slope (experimental scene) with the initial (a, b) and new (d, e) infinite slope modes. The reflectance profile of near infrared band (0.87 (a, b) and new (d, e) infinite slope modes. The reflectance profile of near infrared band (0.87 (a, b) and new (d, e) infinite slope modes. The reflectance profile of near infrared band (0.87 (b) μ m) in the solar plane are computed for 3 different z-scale factors ($F_z = 0.8$, 1.0 and 1.2).

607

612 **5.2.2** Rugged slope with a realistic forest

613

The scene is a 3D forest over a rugged slope (Figure 17.a). The forest stand is the central part of the Järvselja Birch stand (HET09_JBS_SUM) in RAMI experiment (<u>https://rami-</u> <u>benchmark.jrc.ec.europa.eu</u>). It contains 143 trees with 67 birch trees, 48 linden trees, 13 aspen trees, 5 common alder trees, 5 spruce trees, and 5 ash and maple trees (Figure 19.a). After the duplication of the experimental scene, the reference scene has 1287 trees in total. Figure 19.b shows the tree spatial distribution in the reference scene. The repetitive pattern of trees can benoted. DEM in the reference scene is the same as Figure 17.c.

621

DART simulations are conducted with direct sun illumination ($\theta_{sun} = 40^\circ, \varphi_{sun} = 300^\circ$), a 622 0.25 m spatial resolution and 4 spectral bands at NIR (near infrared: 0.87 µm), R (red: 0.66 µm), 623 G (green: 0.57 µm), B (blue: 0.44 µm). Specific optical properties were assigned per tree 624 625 species. They were simulated by the PROSPECT model using leaf biochemistry parameters obtained by inversion of the optical properties provided by the RAMI experiment (https://rami-626 627 benchmark.jrc.ec.europa.eu) (Jacquemoud et al., 1990, Feret et al., 2017). Figure 19.c shows the nadir colour satellite image of the reference scene. A red square outlines the reference 628 629 experimental scene in the centre.

630

Figure 19.d shows the BRFs (*i.e.*, $\rho_{ref}(\theta_v)$, $\rho_{init}(\theta_v)$ and $\rho_{new}(\theta_v)$) of the three simulations in 631 the solar plane (*i.e.* $\varphi_v = 300^\circ$) with zenith angle step $\Delta \theta_v = 2^\circ$. Compared to the reference 632 $\rho_{\rm ref}$, the average absolute relative error of the initial infinite slope mode $\rho_{\rm init}$ is $\bar{\epsilon}_{\rho_{\rm init}} \approx 35.4\%$, 633 with maximum absolute relative error max($\varepsilon_{\rho_{init}}$) up to 65.6%. These large error values are 634 635 mostly due to inaccurate illumination with the strong topography, the mismanagement of image 636 connection and also the fact that pixels in total shadow are discarded when computing the scene 637 average radiance (cf. section 3.1). As expected, the new infinite slope mode greatly improves the situation: $\rho_{\text{new}}(\theta_v) \approx \rho_{\text{ref}}(\theta_v)$ with $\bar{\varepsilon}_{\rho_{\text{new}}} \approx 0.01\%$. Pixel-wise comparison of the nadir 638 639 radiance images L(i, j) at NIR band between the experimental scene and the reference 640 experimental scene is shown in Figure 19.e and Figure 19.f, respectively for scatter plot " $L_{ref}(i,j)$, $L_{init}(i,j)$ " and scatter plot " $L_{ref}(i,j)$, $L_{new}(i,j)$ ". Radiance values " $L_{ref}(i,j)$, 641 642 $L_{init}(i, j)$ " are very scattered in Figure 19.e. It is consistent with the relatively low coefficient

of determination $R^2 \approx 0.935$. The radiance intercept 0.13 and slope 0.97 indicates the tendency 643 644 to overestimate radiance in shadow area and to underestimate radiance in brilliant area due to 645 non-uniform scene illumination in presence of strong and asymmetric topography. Figure 19.f shows $R^2 > 0.999$, a slope 1.0001 and an intercept as low as 0.0015. The slim difference 646 647 between the new infinite slope mode and the reference is probably due to DART discretisation (*i.e.* illumination mesh) combined with the limit of double precision (*i.e.* 16 decimal digits). 648 649 For example, altitude shift ΔZ of 15 m or 45 m can have a double coding inaccuracy of magnitude 10⁻¹⁴ in both the experimental scene and the reference scene, which implies slightly 650 651 different starting points for the illumination rays. As a result, in the mountain forest scene that 652 is simulated with tens of millions of facets, a ray intercepted by a facet edge in the experimental 653 scene could pass through in the reference scene, which leads to very minor difference between 654 few pixels of the experimental and reference scene.

655



Figure 19. Tree spatial distribution in the experimental (a) and reference (b) scene. c) Nadir colour
composite satellite image of the reference scene simulated with the new infinite slope mode.
Its central red square outlines the "reference experimental scene". d) NIR BRF in the solar
plane for "experimental scene + initial infinite slope mode" (-), "experimental scene + new
infinite slope mode" (-) and "reference experimental scene + new infinite slope mode" (-).
Scatter plots of pixel NIR nadir radiance for "Initial - Reference" (e) and "New - Reference"
(f).

664

665 6 Concluding remarks

666

667 This paper presents a new modelling strategy for DART infinite slope mode. This strategy leads to accurate and efficient simulations of RS signals and radiative budget for sloping landscapes. 668 669 Five key points must be noted: (1) The horizontal atmosphere surface crossed by the upward 670 flux from the landscape or the downward flux from atmosphere is computed per direction in 671 order to ensure energy conservation during the Earth-Atmosphere coupling. (2) The illumination ray-mesh is computed per direction in order to ensure uniform scene illumination 672 673 for any sloping landscape. (3) The spread images are stored on an oblique plane OP that is topography-adapted instead of the previous horizontal plane HP. It allows DART to generate 674 675 accurate and high-quality RS images with less RAM demand. (4) Pixels on the spread image 676 are projected on the sensor plane with a precise projection method instead of the bi-linear interpolation method, which further improves the accuracy of the simulated RS image. (5) The 677 678 Lambert azimuthal equal-area projection is applied to fisheye cameras, which increases the 679 realism of the simulated fisheye images. We simulated four scenarios to assess this 680 improvement:

....

682-Solo slope: the initial infinite slope mode gives the intercepted energy flux map that has683a spatial relative variability $(W_{max}-W_{min})/W_{mean}$ up to 25% and a reflectance relative684difference up to 11%. In addition, it underestimates the reflectance in the solar plane by6854.6%. The new infinite slope mode simulates uniform and accurate intercepted energy686flux map and BRF.

687

Solo slope with a cherry tree: the initial infinite slope mode leads to images with
 microgrooves, border effects, and erroneous zones. The BRF in the solar plane has an
 average relative error 4.0% as well. The new infinite slope mode simulates accurate and
 high-quality RS images without the defects of the initial method.

692

693- Rugged slope: the initial infinite slope mode gives reflectance in the solar plane that has694an average relative error up to 69.0%. Indeed, border effects and erroneous zones appear695in the simulated images. These errors and defects increase with the slope roughness and696obliquity. The new infinite slope improves the accuracy of results with relative error697less than 10^{-4} whatever the slope roughness and obliquity. It also simulates accurate698and high-quality RS images without defects.

699

700- Rugged slope with a realistic forest: the initial infinite slope mode gives reflectance in701the solar plane that has an average relative error up to 35.4%. In addition, the pixel-wise702comparison between the reference experimental scene and the experimental scene gives703a coefficient of determination R^2 as low as 0.935. Conversely, the new infinite slope704mode gives accurate BRF profiles in the solar plane, and a coefficient of determination705 R^2 larger than 0.999 in the pixel-wise comparison.

707	In short, these results stress the great improvements of DART infinite slope mode. One should
708	note that the four considered scenarios are a bit extreme because the slopes are relatively large.
709	With less oblique slope, the initial infinite slope mode is less inaccurate.
710	
711	Current DART infinite slope mode is only available for stratified homogeneous atmosphere. In
712	order to simulate adjacent effect risen by the heterogeneous backscattering, multi-cell in each
713	atmosphere layer should be considered in the future work. Also, the accuracy of this modelling
714	strategy should be assessed through the comparison of DART and satellite images, using field
715	measurements in order to ensure an accurate modelling of the scene.
716	
717	Acknowledgements
718	
719	This research is supported by the Occitanie region and by the CNES TOSCA program. We are
720	very thankful to computer scientists Jordan Guilleux and Eric Chavanon in DART team.
721	
722	Appendix A. Atmosphere backscattering
723	
724	The backscattered flux is computed by convolving upward radiation from the Earth scene with
725	transfer function TF_{BA-BA} , at interface BOA (Grau and Gatellu-Etchegorry, 2013).
726	$\text{TF}_{\text{BA-BA}}(\Delta i, \Delta j, \Omega^{\uparrow}, \Omega'^{\downarrow})$, with $\Delta i = i - i'$ and $\Delta j = j - j'$, gives the flux $W_{\text{BOA}}(i', j', \Omega'^{\downarrow})$ that the
727	atmosphere backscatters to pixel (i', j') onto BOA interface for any downward direction Ω'^{\downarrow} ,

direction Ω^{\uparrow} . With an atmosphere spherical albedo \bar{S} and scene albedo ω_{scene} , backscattered energy of infinite coupling order is assumed to be

$$W_{\text{BOA}}^{\text{backscat}}(i',j',\Omega'^{\downarrow}) = \frac{1}{1-\omega_{\text{scene}}\cdot\bar{S}}\sum_{i}\sum_{j}\sum_{\Omega^{\uparrow}}W_{\text{BOA}}^{\text{iterX}}(i,j,\Omega^{\uparrow}).\text{TF}_{\text{BA-BA}}(\Delta i,\Delta j,\Omega^{\uparrow},\Omega'^{\downarrow})$$

Transfer functions $\text{TF}_{\text{BA-BA}}$, $\text{TF}_{\text{BA-sensor}}$ and $\text{TF}_{\text{BA-TA}}$ are computed in the atmospheric RT stage. Their use greatly decreases computer time since it avoids repeated RT calculation per pixel. The new infinite slope mode is adapted to the case where each atmosphere MA layer consists of a single cell. Then, pixels (i, j) cannot be distinguished in the backscattering process, and $\text{TF}_{\text{BA-BA}}(\Delta i, \Delta j, \Omega^{\uparrow}, \Omega'^{\downarrow})$ is simplified as $\text{TF}_{\text{BA-BA}}(\Omega^{\uparrow}, \Omega'^{\downarrow})$. The flux $W_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow})$ at BOA level is calculated by subsampling the flux $W_{\text{OP}}^{\text{iter X}}(i, j, \Omega_n^{\uparrow})$ per pixel at OP

level is calculated by subsampling the flux
$$W_{OP}^{\text{opt}}(l, j, \Omega_n)$$
 per pixel at O

$$W_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow}) = \sum_i \sum_j W_{\text{OP}}^{\text{iter X}}(i, j, \Omega_n^{\uparrow}) \cdot \frac{S_{\text{scene}}}{S_p(\Omega_n^{\uparrow})}$$

737 with S_{scene} the area of scene horizontal section, $S_p(\Omega_n^{\uparrow})$ the projected surface of OP onto the 738 horizontal atmosphere along direction Ω_n^{\uparrow} .

739

740 It leads to backscattered flux $W_{BOA}^{backscat}(\Omega_n^{\downarrow})$ and backscattered flux per pixel $(I_{BOA} \cdot J_{BOA}$ 741 pixels) at BOA

$$W_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow}) = \frac{1}{1 - \omega_{\text{scene}} \cdot \bar{S}} \sum_{\Omega_n^{\uparrow}} W_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow}) \cdot \text{TF}_{\text{BA}-\text{BA}}(\Omega_n^{\uparrow}, \Omega_n^{\downarrow})$$
$$W_{\text{BOA}}^{\text{backscat}}(i, j, \Omega_n^{\downarrow}) = \frac{W_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow})}{I_{\text{BOA}} \cdot J_{\text{BOA}}}$$

The atmosphere albedo \bar{S} and backscattered irradiance $E_{BOA}^{backscat}$ are calculated as

$$\bar{S} = \frac{\sum_{\Omega_n^{\uparrow}} \sum_{\Omega_n^{\uparrow}} w_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow}) \cdot \text{TF}_{\text{BA}-\text{BA}}(\Omega_n^{\uparrow}, \Omega_n^{\downarrow})}{\sum_{\Omega_n^{\uparrow}} w_{\text{BOA}}^{\text{iter X}}(\Omega_n^{\uparrow})}, E_{\text{BOA}}^{\text{backscat}} = \frac{\sum_{\Omega_n^{\downarrow}} w_{\text{BOA}}^{\text{backscat}}(\Omega_n^{\downarrow})}{S_{\text{scene}}}$$

744 Appendix B. Simulation of DART products at sensor level and TOA

745

746 The Earth surface RT of atmosphere backscattered radiance (step 4 in Figure 2) gives $W_{\rm OP}^{\rm coupl}(i, j, \Omega_n^{\uparrow})$. Then (step 5 in Figure 2), energies at BOA are transferred to TOA and sensor 747 levels. Fluxes at these levels are calculated using $W_{OP}^{coupl}(i, j, \Omega_n^{\uparrow})$, direct transmittances 748 {T_{BA-TOA}, T_{BA-sensor}} and transfer functions {TF_{BA-TOA}($\Omega_n^{\uparrow}, \Omega_{n'}^{\uparrow}$), TF_{BA-sensor}($\Omega_n^{\uparrow}, \Omega_{n'}^{\uparrow}$)} 749 (Grau and Gatellu-Etchegorry, 2013) (*i.e.*, step 5 in Figure 2). $TF_{BA-TOA (sensor)}(\Omega_n^{\uparrow}, \Omega_{n'}^{\uparrow})$ gives 750 the upward flux $W_{\text{TOA(sensor)}}(\Omega_{n'}^{\uparrow})$ per upward direction $\Omega_{n'}^{\uparrow}$ at TOA (sensor) level, due to a 751 unit flux $W_{\text{BOA}}(\Omega_n^{\uparrow}) = 1$ from BOA level along the upward direction Ω_n^{\uparrow} . The energy flux 752 $W_{\text{TOA}}(i, j, \Omega_n^{\uparrow})$ per pixel (i, j), in the images $(I_{\text{BOA}} \cdot J_{\text{BOA}} \text{ pixels})$ per viewing direction Ω_n^{\uparrow} at 753 754 TOA and sensor levels is computed as:

755

$$\begin{split} & W_{\text{TOA}}(i,j,\Omega_n^{\dagger}) \\ &= W_{\text{OP}}^{\text{coupl}}(i,j,\Omega_n^{\dagger}) \cdot \text{T}_{\text{BA-TOA}} \\ &+ \frac{W_{\text{TOA}}(\Omega_n^{\dagger}) \cdot \frac{S_p(\Omega_n^{\dagger})}{S_{\text{scene}}} + \sum_{\Omega_{n'}^{\dagger}} \sum_i \sum_j W_{\text{OP}}^{\text{coupl}}(i,j,\Omega_n^{\dagger}) \cdot \text{TF}_{\text{BA-TOA}}(\Omega_n^{\dagger},\Omega_{n'}^{\dagger})}{I_{\text{BOA}} \cdot J_{\text{BOA}}} \\ & W_{\text{sensor}}(i,j,\Omega_n^{\dagger}) \\ &= W_{\text{OP}}^{\text{coupl}}(i,j,\Omega_n^{\dagger}) \cdot \text{T}_{\text{BA-sensor}} \\ &+ \frac{W_{\text{sensor}}(\Omega_n^{\dagger}) \cdot \frac{S_p(\Omega_n^{\dagger})}{S_{\text{scene}}} + \sum_{\Omega_{n''}^{\dagger}} \sum_i \sum_j W_{\text{OP}}^{\text{coupl}}(i,j,\Omega_n^{\dagger}) \cdot \text{TF}_{\text{BA-sensor}}(\Omega_n^{\dagger},\Omega_{n''}^{\dagger})}{I_{\text{BOA}} \cdot J_{\text{BOA}}} \end{split}$$

with S_{scene} the area of scene horizontal section, $S_p(\Omega_n^{\uparrow})$ the projected surface of OP onto the horizontal atmosphere along direction Ω_n^{\uparrow} . 41 The backscattered irradiance $E_{sens}^{backscat}$ at sensor level is calculated as

$$E_{\text{sensor}}^{\text{backscat}} = \sum_{\Omega_n^{\downarrow}} \sum_{\Omega_n^{\uparrow}} \frac{\sum_i \sum_j W_{\text{OP}}^{\text{coupl}}(i, j, \Omega_n^{\uparrow})}{S_p(\Omega_n^{\uparrow})} \cdot \text{TF}_{\text{BA-sensor}}(\Omega_n^{\uparrow}, \Omega_n^{\downarrow})$$

760 Associated radiometric products are also computed

$$L_{\text{sensor}}^{\text{coupl}}(i,j,\Omega_{n}^{\uparrow}) = \frac{W_{\text{sensor}}(i,j,\Omega_{n}^{\uparrow})}{S_{p}(i,j,\Omega_{n}^{\uparrow}) \cdot \cos \theta_{n} \cdot \Delta \Omega_{n}^{\uparrow}}, \rho_{\text{sensor}}^{\text{coupl}}(i,j,\Omega_{n}^{\uparrow}) = \frac{\pi \cdot L_{\text{sensor}}^{\text{coupl}}(i,j,\Omega_{n}^{\uparrow})}{E_{\text{sensor}}^{\text{dir}} + E_{\text{sensor}}^{\text{dir}} + E_{\text{sensor}}^{\text{backscat}}}$$
$$L_{\text{TOA}}^{\text{coupl}}(i,j,\Omega_{n}^{\uparrow}) = \frac{W_{\text{TOA}}(i,j,\Omega_{n}^{\uparrow})}{S_{p}(i,j,\Omega_{n}^{\uparrow}) \cdot \cos \theta_{n} \cdot \Delta \Omega_{n}^{\uparrow}}, \rho_{\text{TOA}}^{\text{coupl}}(i,j,\Omega_{n}^{\uparrow}) = \frac{\pi \cdot L_{\text{sensor}}^{\text{coupl}}(i,j,\Omega_{n}^{\uparrow})}{E_{\text{TOA}}^{\text{dir}}}$$

with $L_{\text{sensor}}^{\text{coupl}}$ and $\rho_{\text{sensor}}^{\text{coupl}}$ the radiance and reflectance at sensor level, $L_{\text{TOA}}^{\text{coupl}}$ and $\rho_{\text{TOA}}^{\text{coupl}}$ the radiance and reflectance at TOA. $E_{\text{TOA}}^{\text{dir}}$ is the direct irradiance at TOA. $\Delta\Omega_n^{\uparrow}$ is the solid angle of direction Ω_n^{\uparrow} and θ_n is the zenith angle of direction Ω_n^{\uparrow} . Superscript "coupl" refers to DART products after the radiative coupling with the atmosphere.

765

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3-D plant canopies." *Computational methods in transport*. Springer, Berlin, Heidelberg, 2006.
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912

913 List of Figure Captions

914

915 Figure 1. DART 3D discrete mock-up. Landscape elements are made of triangles, and/or fluid 916 and turbid vegetation cells. The landscape itself is a cell matrix in order to ease ray tracing. The 917 atmosphere has three levels: upper level made of layers, middle level made of cells of any size, 918 and lower level in the landscape.

Figure 2. Major steps for modelling RT in the Earth-Atmosphere system. Thermal emission in
mode (T) is shown by the red symbol (steps 1 and 2). Arrows indicate directly transmitted solar
(orange) and thermal (red) radiation, and scattered radiation (yellow), either thermal or solar.

Figure 3. The three DART modes for simulating RT in 3D scenes. a) Isolated scene mode. b)
Repetitive scene mode. c) Infinite slope mode. The actually simulated scene is framed by a
black box. The dotted box frames one of the fictive neighbourhoods of the actually simulated
scene.

928

929 Figure 4. DART scene in infinite slope mode with its infinite duplications. Three duplications 930 are shown here. The mean altitude differences between neighbour Earth scenes are indicated 931 (ΔZ_X for axis X and ΔZ_Y for axis Y). DEM Edges are smoothly connected with Bezier triangles. 932

Figure 5. 2D view of the infinite slope mode RT modelling of initial DART. a) Illumination stage. b) Spread image generation. The scene window for direction Ω_n is the dark blue region at the scene vertical face. Its shape depends on the DEM and the illumination direction. Red arrows are rays in the paper plane. Illumination ray sources start from the scene top and window. Rays that cross scene top / window never re-enter the scene, conversely to rays that cross other parts of the scene vertical face. HP is the horizontal plane that stores the spread images.

939

Figure 6. Pinhole camera image generation using an interpolation method. a) Projection onto HP of the centre of a pixel in the sensor image. b) Nadir view of the projected point. Δx and Δy are the scale coefficients that vary from 0 to 1.

Figure 7. Simulation of a solo slope, using the initial infinite slope mode. DEM mesh with indication of slope azimuth angle φ_{slope} , and zenith and azimuth angles ($\theta_{sun}, \varphi_{sun}$) of the direction in which the sun is seen from the Earth surface (a), φ is anticlockwise from South. Solo slope: spectral energy flux map (b) and angular reflectance in the solar plane (c).

948

Figure 8. Simulation of a cherry tree on a solo slope, using the initial infinite slope mode.
Satellite (orthographic) camera images (b, c) with 2 viewing directions, fisheye camera image
(d), pinhole camera image (e) and pushbroom image (f).

952

Figure 9. DART infinite slope mode. a) Earth scene and its fictive oblique plane OP at the scene bottom. b) DEM altitude differences are ΔZ_X along axis X and ΔZ_Y along axis Y axis. c) Projected surface (blue parallelogram) $\Sigma_p(\Omega_n)$ of OP along direction Ω_n onto the horizontal plane that contains the highest point of OP, it has an area equal to $S_p(\Omega_n)$.

957

Figure 10. 2D (a) and 3D (b) views of the scene illumination stage. $\Sigma_{BOA}(\Omega_n)$ is the projected surface of OP onto the horizontal BOA plane with backward ray tracing method; its area is $S_p(\Omega_n)$. After atmospheric RT modelling, rays through $\Sigma_{BOA}(\Omega_n)$ along direction Ω_n illuminates the scene. $P_{ray}(x, y, z)$ (**x**) is the source point of an incident ray, on the scene top or scene window. $P_{OP}(x, y, z)$ (**x**) is the projection on OP of $P_{ray}(x, y, z)$ along incident direction Ω_n .

964

Figure 11. Ray projection on OP. a) The red triangle gives rise to a ray along direction r (red arrow) that reaches the scene top. The green triangle is its projection onto OP. P is the projection on OP of a corner l_0 of the red triangle. d is the distance $||P - l_0||$. P_0 is the highest

point of OP. b) Parallel projection for the orthographic camera and perspective projection for
the perspective camera. c) Nadir view of the projected triangle on OP and its break-down into
four polygons.

971

Figure 12. Projection processes for simulating images. Parallel projection along direction Ω_n for satellite (orthographic) camera (a), and perspective projection along local viewing direction for pinhole camera (b) and pushbroom camera (c).

975

976 Figure 13. Projection processes for simulating fisheye images. First, pixel on OP is projected 977 onto a unit sphere. Then, it is spread on the sensor plane with Lambert azimuthal equal-area 978 projection method that projects a point (x, y, z) of the unit sphere onto the sensor plane at point 979 (X, Y, Z). θ_{max} is the maximum viewing zenith angle.

980

Figure 14. DART simulations with the new infinite slope mode. Solo slope. Same legend asFigure 7.

983

Figure 15. DART simulations with the new infinite slope mode. Solo slope plus a cherry tree.Same legend as Figure 8.

986

Figure 16. Absolute relative error of DART energy flux images (*i.e.*, $\sum_{z} W(i, j, z)$ (W) per pixel

(*i*, *j*)) simulated with the initial infinite slope mode. a) Solo slope. b) Solo slope with a cherry
tree.

990

Figure 17. The rugged slope. a) 3D view. b) slope map (unit °). c) 9 duplications of the rugged

992 slope (a) with respect to the continuity of slopes and altitudes. 51

Figure 18. DART simulated satellite images of the rugged slope (experimental scene) with the initial (a, b) and new (d, e) infinite slope modes. The reflectance profile of near infrared band (0.87 μ m) in the solar plane are computed for 3 different z-scale factors ($F_z = 0.8$, 1.0 and 1.2). Figure 19. Tree spatial distribution in the experimental (a) and reference (b) scene. c) Nadir

righte 19. The spatial distribution in the experimental (a) and reference (b) seene. c) Fudal
colour composite satellite image of the reference scene simulated with the new infinite slope
mode. Its central red square outlines the "reference experimental scene". d) NIR BRF in the
solar plane for "experimental scene + initial infinite slope mode" (-), "experimental scene +
new infinite slope mode" (-) and "reference experimental scene + new infinite slope mode" (. Scatter plots of pixel NIR nadir radiance for "Initial - Reference" (e) and "New - Reference"
(f).