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**Late Pleistocene slip rate of the central Haiyuan fault constrained
from OSL, ^{14}C , and cosmogenic isotope dating and high resolution
topography**

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ABSTRACT: The Haiyuan fault is a major left-lateral active fault of the India-Asia collision zone. While the 1000 km-long fault between Hala Lake in the west to Liupan Shan in the east accommodates eastward displacement of northeast Tibet relative to the Gobi-Alashan to the north, the amount of slip accumulated and its slip-rate remain debated. We revisit the site of Daqing (or Sangedun at 102.7°E in Gaudemer et al., 1995), to better constrain the long-term slip-rate of the Haiyuan fault in its central part. We used terrestrial LiDAR to build a high-resolution DEM and Unmanned Aerial Vehicle to build an aerial photomosaic with ~0.1 m resolution to survey the offset terraces, their geomorphology and the fault trace. We refine the geomorphological interpretation of the site, measure riser offsets and determine their relation to terrace formation. The well constrained age of the highest terrace T3 at 13.7 ± 1.5 ka determined from the combination of surface and sub-surface OSL, ^{14}C , and terrestrial in situ ^{10}Be cosmogenic nuclide dating, associated with the maximum lower terrace riser offset of 88 m yield a minimum slip-rate of 6.4 ± 1.2 mm/yr over the late Pleistocene. The age of the intermediate terrace (T2) is bracketed between 8.0 ka (^{14}C) and 12 ka (^{10}Be). The ages and vertical offsets of the 2 highest terraces is used to infer the age of T2' offset vertically 5-7 m at 5.4 ± 1 ka. Its 29 ± 2 m offset is consistent with a rate of 6.5 mm/yr. Given the vertical offset youngest terrace T1 of 1.3 ± 0.2 m its age is estimated at 1.2 ± 0.2 ka in agreement with the youngest surface exposure age. Overall, a slip rate of 5-8 mm/yr fits all offset and age data at the Daqing site. The smallest offset of a gully incised into T1 of 6.0 ± 0.5 m is potentially associated with the most recent slip event that occurred in the last millennia.

Keywords: Haiyuan fault, northern Tibetan plateau, slip rate, LiDAR, cosmogenic nuclide dating

48

49 INTRODUCTION

50 How strain is distributed in the Tibetan-Himalayan orogen is important to
51 understand how continental orogens deform ([Tapponnier and Molnar, 1977](#); [England](#)
52 [and Molnar, 1997](#)). The Haiyuan left-lateral strike-slip fault, whose eastern part
53 ruptured in 1920 for a length of about 220 km ([Deng et al., 1984](#)), is a major strike
54 slip fault at the northeastern margin of the Tibetan Plateau. This fault plays an
55 important role in accommodating eastward extrusion of the northern Tibet plateau
56 relative to the Gobi-Alashan to the north ([Tapponnier and Molnar, 1977](#); [Burchfiel et](#)
57 [al., 1991](#); [Gaudemer et al., 1995](#); [Tapponnier et al., 2001a](#)).

58 Overall decadal geodetic and millennial geological recent slip-rate studies mostly
59 agree to a rate of 4-10 mm/yr, implying that the Haiyuam fault is the major active
60 fault at the rim of Tibet at this longitude ([Li et al., 2009](#); [Daout et al., 2016](#); [Jiang et](#)
61 [al., 2017](#)). However, higher slip rates have been documented ([Gaudemer et al., 1995](#);
62 [Zhang et al., 1988](#); [Lasserre et al., 1999, 2002](#)). Because it has been suggested that the
63 fault slip rate might vary over time., thus, it is valuable to find multiple slip-rate
64 constraints at a single site to constrain possible temporal slip-rate variations (e.g., [Sieh](#)
65 [and Jahns, 1981](#); [van der Woerd et al., 1998, 2002](#); [Lasserre et al., 1999](#); [Li et al.,](#)
66 [2009](#); [Jiang et al., 2017](#); [Mattrau et al., 2019](#)).

67 Terrace risers have commonly been used as markers of fault displacement to
68 constrain slip rates along strike slip faults (e.g., [Lensen, 1968](#); [Weldon & Sieh, 1985](#);
69 [Berryman et al., 1990](#); [Knuepfer, 1992](#); [Van der Woerd et al., 1998, 2002](#); [McGill et](#)
70 [al., 2013](#)). However, terrace risers can be seldom directly dated. One may infer
71 displacement started to be recorded at the time of upper terrace abandonment or upon
72 abandonment of the lower terrace ([Van der Woerd et al., 2002](#); [Mériaux et al., 2004,](#)
73 [2005](#); [Cowgill, 2007](#); [Zhang et al., 2007](#)). In general, upper terrace age yields a
74 minimum slip rate, while the lower terrace age a maximum slip rate. Ideally, when

75 terrace ages are not too different a combination of upper and lower age constraints
76 may be used to bracket the riser age (Mériaux et al., 2005; Cowgill, 2007).

77 The precision of a late Quaternary slip rate depends upon displacement
78 accumulation and its uncertainty as well as the reliability of the corresponding dating
79 (Cowgill et al., 2007, 2009; Gold et al., 2009; Le Béon et al., 2012; Sieh, 1981; Van
80 der Woerd et al., 1998, 2006; Weldon & Sieh, 1984; Zhang et al., 2007). Across the
81 Qilian Shan-Hexi Corridor, loess covers late Quaternary surface broadly. Researchers
82 have often used optically stimulated luminescence (OSL) or radiocarbon ages of
83 materials collected within the basal loess to date the end of terrace emplacement (e.g.
84 Li et al., 2009; Jiang et al., 2017; Liu et al., 2018). Several studies indicate that loess
85 deposition started just prior to the Holocene in this area (~13-10 ka) (Küstera et al.,
86 2006; Stokesa et al., 2003). Thus, loess deposition age is a minimum age for terraces
87 formed before the Holocene. Because terraces capped by loess are usually formed of
88 coarse gravels, if one could correct for the shielding effect due to loess, in situ
89 cosmogenic nuclides should be an optimal dating method, ideally complemented by
90 OSL and ^{14}C dating of loess capping materials (e.g., Perrineau et al., 2011; Hetzel et
91 al., 2004; Hetzel, 2013).

92 High-resolution topographic data make it possible to image subtle landforms and
93 deformation features due to active tectonics, and to make reproducible and precise
94 measurements, improving understanding of rupture history and slip along faults (e.g.
95 Zielke et al., 2010, 2015). Satellite or aerial photography offers two-dimensional
96 imagery which is often used to trace fault line and look for offset markers (e.g.,
97 Tapponnier and Molnar, 1977; Peltzer et al., 1989; Meyer et al., 1998; Lasserre et al.,
98 1999; Klinger et al., 2011; Middleton et al., 2016). Studies have applied Airborne
99 Laser Scanning (ALS) data to map fault-zone features (e.g., Hudnut et al., 2002;
100 Oskin et al., 2007; Arrowsmith and Zielke, 2009; Liu-Zeng et al., 2013), to survey
101 coseismic surface ruptures (Oskin et al., 2012; Clark et al., 2017; Langridge et al.,
102 2018) or to determine paleo-earthquake slip distributions (Zielke et al. 2010, 2012;

Thackray et al., 2013; Chen et al., 2015). Recently, this technique has also been used to measure the most recent rupture traces along the eastern Haiyuan fault (Chen et al., 2014, 2018; Ren et al., 2015).

Based on new imagery and field investigation, we revisit the Daqing site (also named Sangedun site in the study of Gaudemer et al., 1995), a location with multiple marker offsets, to reassess the slip rate of the Haiyuan Fault. We constrain the slip rate at this site with new offset measurements and a combination of absolute age dating approaches.

GEOLOGIC SETTING

The Haiyuan fault extends for ~1000 km from Hala Hu within the Qilian Shan in the west to the Liupan Shan in the east (e.g., Deng et al.1984; Tapponnier and Molnar, 1977; Deng et al.1984; Burchfiel et al., 1989; Gaudemer et al., 1995; Lasserre et al., 1999; Zhang et al., 1988a, b). Thermochronological data indicate that the Haiyuan fault initiated along its western section, then perhaps propagated eastward to the Liupan Shan area (Zheng et al., 2006; Duvall et al., 2013). The fault is characterized by left-lateral strike slip with oblique-slip components along some strands. Six major sections are distinguished, which are separated by left step-overs or branches. These sections, from west to east, are Halahu, Lenglongling, Jinqiang He, Maomao Shan, Haiyuan, and Liupan Shan sections (sections 1 to 6, respectively, in Figure 1). The Gulang-Zhongwei fault branches off the Haiyuan fault near the junction of Lenglongling and Jinqiang He sections, and turns back towards the Haiyuan fault east of 106°E. Large historical earthquakes, such as 1709 Zhongwei M7.5, 1920 Haiyuan Mw7.8-8.3 and Gulang 1927 M8.0 earthquakes, ruptured these two faults, which raises concern about seismic hazard on the faults.

Numerous field studies along the Haiyuan fault have been carried out during the last 30 years. For instance, paleoseismic investigations along the Haiyuan (e.g. Zhang et al., 1988; Ran et al., 1997; Xiang et al., 1998; Min et al., 2001; Liu-Zeng et al.,

2015) and Maomao Shan (e.g. Yuan et al., 1998; Liu-Zeng et al., 2007) sections show that earthquakes can rupture single or several sections together, and cluster temporally (Zhang et al., 2003). Magnitude 6 to 7 earthquakes were also evidenced in trenches with high-resolution deposition sequences (Liu-Zeng et al., 2015). Six events were revealed on the Lenglongling section, and the most recent event may be the Gulang M8.0 earthquake in 1927 (Guo et al., 2019).

Geological slip rates determined along the Haiyuan fault differ greatly between different studies, from a few mm/yr to more than 1 cm/yr (Table S1), which are due to different dating methods and slip reconstruction models. Lasserre et al. (2002) estimated the slip rate of the Lenglongling segment to be 19 ± 5 mm/yr according to the study of a dated offset moraine. However, He et al. (2000) argued for a lower slip rate along the Lenglongling segment of $3.3 \sim 4.1$ mm/yr during the late Quaternary, although without dating constraints. Recently, Jiang et al. (2017) investigated the eastern section of the Lenglongling segment and estimated a left-lateral slip rate of 6.6 ± 0.3 mm/yr during the Holocene by ^{14}C and OSL dating. Lasserre et al. (1999) determined a slip rate of 12 ± 4 mm/yr along Maomao Shan segment. While Yuan et al. (1998) estimated lower slip rates on the Maomao Shan segment to be 4.1-5.4 mm/yr. Yao et al. (2019) recently reassessed the estimation of Lasserre et al. (1999) with a slip rate for the Haiyuan fault between 5 and 8.9 mm/yr over the late Pleistocene - Holocene. Liu et al. (2018) also estimate a low slip rate of 4.3 ± 0.16 mm/yr from four offset terraces on the Laohu Shan segment. The Haiyuan segment, which ruptured in 1920 during a magnitude Ms8.0 (Richter, 1958), was assigned a slip rate of 8 ± 2 mm/yr by Zhang et al. (1988). Li et al. (2009) updated this value to $\sim 4.5 \pm 1$ mm/yr by dating offset alluvial terraces. Matrau et al. (2019) constrained a minimum slip rate of 3.2 ± 0.2 mm/yr along the main strand of the Hasi Shan restraining bend along the western section of the 1920 Haiyuan earthquake rupture. Further east, the slip rate decreases to about 1~3 mm/yr along the Liupanshan segment (Xiang et al., 1999).

The Jinqiang He section (3) (named after the name of the Jinqiang river) and the Maomao Shan section (4) are linked across a 6 km left step by a N45°E-striking and east dipping normal fault, which bounds the Tianzhu half-graben or pull-apart basin to the west (Gaudemer et al., 1995; Figure 2). There is no evidence of large earthquake during at least the past eight centuries along these two fault sections, which are considered as “the Tianzhu seismic gap” (Gaudemer et al., 1995; Liu-Zeng et al., 2007). The fault offsets alluvial fans and ridges along the northern side of the Jinqiang He valley, then steps to the north at the Tianzhu pull-apart basin with mostly a large normal component before veering eastward to resume a N110°E strike. The southern rim of the Tianzhu basin is limited by a minor fault strand (Figure 2) with no evidence of faulting during the Holocene.

The site of Daqing (or Sangedun site in Gaudemer et al., 1995; Tapponnier et al., 2001b) is located along the eastern part of the Jinqiang section, north of the Daqing village (Figure 1). A stream that flows down from a high catchment (elevation >4000 m asl) and perpendicular to the main fault has abandoned a set of 3 main terrace levels along its west bank (Figure 2). These terraces are cut and offset by the fault. Based on fieldwork, aerial-photo interpretation, and topographic leveling with a theodolite, Gaudemer et al. (1995) determined the horizontal and vertical offsets of the three main terrace levels to be 143 m, 89 m, 35 m and 18 m, 11 m, and 4 m, respectively. Assigning an abandonment age of 13.5 ± 2 ka to the highest terrace based on the assumption that it was deposited and abandoned during the wetter and warmer period following the last late glacial maximum, they proposed a slip-rate of 11 ± 4 mm/yr. However, more recent slip rates determined in a range of 100 km from the Daqing site, respectively westward and eastward along the Jinqiang and Maomoshan sections, are much lower and range from 1.8 to 4.8 mm/yr based on soil sequence comparison (Yuan et al., 1998). The slip rate determined for a similar period of time (10-25 ka) by Yao et al. (2019) is 5 to 9 mm/yr at Songshan (a site located at a

distance of ~80 km to the east). Thus, the slip-rate of the central Haiyuan fault along the Jinqiang He section remains arguable.

LEVELING AND GEOCHRONOLOGY METHODS

Terrestrial LiDAR (TLS) was used to generate a detailed scan of the landscape of the Daqing site. We used a Riegl VZ-1000, with an effective scan range of ~1400 m and a precision of ~5 mm. Three successive scans were needed to cover all the studied area. A Trimble real-time kinematic (RTK) Global Position system (GPS) surveyed each scanning base position and elevation. These positions were used to register the different point cloud datasets together. Even though TLS scans the landscape with a rate of more than one hundred thousand points per second, some places may remain hidden due to topographic roughness. In addition to TLS, we used a small drone equipped with a fixed focus camera to capture aerial imagery vertically and obliquely to generate an ortho-photo mosaic of the site by structure from motion techniques (Figures 3 and 4). We projected the DEM derived from points cloud of TLS in the same coordinates of the ortho-photo.

At the Daqing site, large boulders armor the surface of the terraces, some of them are partially buried into the subsurface. Rock samples for terrestrial cosmogenic nuclide dating were collected from the top of blocks using chisel and hammer (Figure 4 and 5). In addition, a pit was dug into the highest terrace (T3) for sub-surface sampling (Figure 6). The upper 1.1 m of the profile consists of 80 cm thick dark brown to black soil topping a 30 cm silty (loess) layer mixed with gravels. From these upper layers we sampled 2 radiocarbon samples at 62 and 77 cm depths, and 2 OSL samples at 82 and 104 cm depths (Tables 1 and 2). In the lower conglomeratic part of the profile, we collected 8 samples of amalgamated gravels and pebbles down to 3 m depth for cosmogenic isotope dating. All sample locations were recorded using a portable GPS and elevations was adjusted with the topography data from the TLS (Figure 5).

Radiocarbon samples were analyzed by Beta Analytic with accelerator mass spectrometry (AMS) and calibrated using Calib 7.1 (Stuiver et al., 1993) (Table 1). The two OSL samples were processed and analyzed following Aitken (1998) and Lu et al. (2007). Coarse-grained quartz was purified from samples through chemical separation using 30% H₂O₂, 10% HCl, and 40% HF, and magnetic separation. The ratio of Infra-red Stimulated Luminescence (IRSL) to Blue Light Stimulated Luminescence (BLSL) has been checked to be lower than 45% to make sure the quartz is clean. A Risø TL/OSL-DA-20 reader was used for irradiation, heating and luminescence measurements (Table 2 and Figure 7). All dose rates were calculated by the central age model (Galbraith et al., 2012). The samples analyzed for ¹⁰Be cosmogenic nuclide were pre-processed at the Key Laboratory of Crustal Dynamics, China Earthquake Administration. We crushed the gravels and pebbles, purified the 250-500 µm fraction with acid leaches to obtain pure quartz, then dissolved about 30 g of quartz to which 0.25 mg of Beryllium-9 standard solution was added with hydrofluoric acid. We isolated beryllium hydroxide (BeOH₂) using cation exchange chromatography, which was then heated to 700°C to form beryllium oxide (BeO). Final targets were prepared at the Cosmogenic isotope Laboratory of Institut de Physique du Globe de Strasbourg (CNRS, University of Strasbourg) and sent to the ASTER-AMS facility of Centre Européen de Recherche et d'Enseignement des Géosciences de l'Environnement (Aix-en-Provence, France) for measurement (Table 3).

RESULTS

Accumulated slip determination

Combining the DEM with a resolution of ~0.1 m computed from point clouds acquired by TLS, the kinematic GPS topographic profiles, and the aerial orthophoto mosaic acquired by UAV, we produce a geomorphic map of the Daqing site (Figures 3 and 4). Overall, our mapping and leveling are consistent with previous

interpretation of the site by Gaudemer et al. (1995). Three main terrace levels are abandoned and preserved on the right bank of the Daqing stream. These are offset both horizontally and vertically due to oblique fault slip. The trace of the main Haiyuan fault can be clearly followed along the steepest part of the topographic scarp trending N110°E. The fault trace, as noted by Gaudemer et al. (1995), is marked by roughly aligned large blocks visible in the active stream bed that are clearly visible on the aerial photo (Figure 3).

The terrace levels are well defined and separated by steeply sloping risers (Figure 4). The terrace surfaces slope 14° to 8° from oldest to youngest (Figures 4 and 8) reflecting progressive incision and slope lowering of fan shape deposits (Figure 8). The highest terrace level T3 is present to the west and cut by the fault visible at the base of a 15 m-high scarp. The intermediate terrace level is subdivided into older higher standing ridges (T2) dotted with large outcropping blocks and incised by channels at a lower level (T2'). Another sub-level terrace T2'' is locally distinguished upstream. The lowest terrace level T1 stands a few meters above the active river bed. At places, gullying and riser-slope instabilities have added some disturbance to the overall simple geomorphological setting. The height and width of the fault scarp are larger on the older terraces than the younger terraces, due to additional accumulated deformation and progressive degradation of the steep fault scarp (Figures 4) (e.g., Tapponnier et al., 1990; Zinke et al., 2015). In addition, due to relative vertical motion on the fault, terrace separation and riser heights upstream are much larger than downstream with no marked changes in average slopes of the terraces (Figure 8).

Because of lateral stream erosion and local degradation of terrace risers, terrace edges are not linear features, especially upstream of the fault, which makes it difficult to reconstruct their geometry prior of being offset. Downstream risers T3/T2' and T2/T1 are curved near the fault trace (Figure 4), which suggests that displacement of the risers started to accumulate before the lower terrace levels were completely abandoned.

We bracket higher and lower displacement values by fitting far-field riser edges (more than 200 meters-long away from fault trace) and near-field riser edges (few tens of meters long from fault trace) across the fault. Risers slope toward the river bed, so offsets related to riser top and bottom are also specified, especially offsets of curved risers nearby fault trace (Figure 9). All measurements are shown in Table 4. It is worth pointing out that the far field displacements of riser tops ($D_{\#u}$) may be related to the abandonment of the adjacent upper terrace, while near-field displacements (e.g. d_{3u} , d_{3l} , d_{2u} , d_{2l}) (Figure 9F) are more closely related to the adjacent lower terrace and regarded as a minimal offset value for the upper adjacent terrace (e.g., Gold et al., 2011a).

For terrace riser T3/T2', the crest of the upstream riser may be fit in two ways. First option is that piercing line fits tangentially two convex bumps close to the fault. The second option is a piercing line fit to the concave curve between those two convex bumps, similar to Gaudemer et al. (1995). Downstream, the top edge of the riser is smoothed near the fault zone because of erosion when T2 or T2' were active. Therefore, we locate the piercing line away from this erosion area. Bottom piercing lines of riser T3/T2' are almost parallel to the top. Correlating piercing riser crest lines from upstream and downstream of fault, the displacement of the crest is 82 ± 3 to 94 ± 3 m, or 88 ± 9 m. 94 ± 3 m is similar to the measurement of 101.5 m obtained by Gaudemer et al. (1995). Piercing lines at base of riser constrain an offset of 72 ± 3 m. Considering the different possibilities, displacement of T3/T2' ranges from 72 ± 3 to 88 ± 9 m. The near field displacements by fitting bent riser crest (d_{3u}) and bottom (d_{3l}) are similar 25 ± 2 - 28 ± 2 m or 26 ± 2 m (Figure 4, Table 4).

Riser T2/T1 is almost linear with exception of a small bump outward upstream and erosion near the fault. We neglect this minor curve, which does not affect much the maximum slip estimate. Downstream, piercing lines along riser crest and bottom are not exactly parallel because of diffusion of the riser. The cumulated slip of riser T2/T1 ranges from 27 ± 2 m to 35 ± 2 m or 31 ± 4 m. This value is similar to the offset

of the western edge of T2 (or riser T2/T2') of 29 ± 2 m. The near field displacement of the bent riser T2/T1 along the fault is 6.5 ± 1 m (d2u and d2l, Figure 4, Table 4).

Riser T1/T0 does not preserve lateral slip, even though T1 and T0 were likely ruptured in the past (Figures 4 and 10). A small stream incising the inner T1 surface, however, was offset by 6.0 ± 0.5 m (Figure 10A), which is similar with d2u and d2l.

Total displacements of terraces, however, are larger than the offsets of lower risers and smaller than upper risers because of probable lateral erosion when lower terraces were active. Therefore, 88 ± 9 m can be defined as the lower bound for offset of T3, the offset of T2 is between 72 ± 3 m and 35 ± 2 , the horizontal offset of T1 is 6.5 ± 1 m. For T2', the offsets of its west and east edges are 28 ± 2 m and 29 ± 2 m respectively (Figure 4). Thus, its offset is well constrained to be 29 ± 2 m.

In addition to left lateral slip, the Haiyuan fault exhibits a vertical component of slip at this site. We used a dGPS survey to measure the throw along the riser crests to take into account the apparent vertical offset due to displacement of obliquely sloping terrace surfaces (e.g., Rodgers and Little, 2006; Chevalier et al., 2016). Therefore, scarp height of 15 ± 2 m (Sc3) across T3 as measured from the profiles (Figure 8) may be larger than the real throw. The scarp height measured along the swath profile in the middle of terrace T3 (19 ± 2 m) is even larger than on the edge (15 ± 2 m) (Figure 4 and 7) since the terrace slopes toward the west (see details in Gaudemer et al., 1995). The maximum slope direction of terrace T3 on both side of the fault makes an angle of $\sim 4.2^\circ$ with a perpendicular to the fault trace. Taking this angle and assuming 94 ± 3 m is the total offset of T3, the measured vertical slip of 19 ± 2 m (Vi) is corrected to 13 ± 2 m (Vr) (e.g., Gaudemer et al., 1995; Figure 8), which is close to the value found on the terrace edge (15 ± 2 m). Maximum slopes of terrace T2 across the fault are similar and perpendicular to fault trace, so that no correction is needed for T2 and its vertical throw is 10 ± 1 m (Sc2) (Figure 8).

The slopes of T1 are similar upstream and downstream, both from dGPS measurements and a swath profile through the LiDAR DEM. The height of the fault

scarp across T1 is 1.3 ± 0.2 m (Figure 8). This value is smaller than the vertical displacement of ~ 4.1 m across T1 estimated by Gaudemer et al. (1995).

Five topographic profiles parallel to the Haiyuan fault (Figures 3 and 8) illustrate how riser heights change across the fault scarp (Table 4). Riser T3/T2' is 15-19 m high upstream, but less than 2 m downstream. Height of riser T2/T1 is also larger upstream (12-13 m) than downstream (~ 7.5 m). T1 is ~ 6 m high above the active bed upstream, and only ~ 2.5 m high downstream.

Terrace ages

To constrain the age of abandonment of T3 we dug a 3 m-deep pit in the downstream tread of terrace T3 (Figure 3). The upper 1.1 m of the profile exhibits a 30 cm sandy-loessic layer overlain by an 80 cm-thick black silty soil, which developed from the loess including some coarse sand. Below 1.1 m depth, the profile penetrates the conglomeratic terrace deposit made of blocks, cobbles, gravels and sand. Two OSL samples from the loess layer yield ages of 12.2 and 8.7 ka, in stratigraphic order (Figure 4 and Table 2). Two radiocarbon samples from the lower part of the soil give ages of 7.7 and 7.6 ka, also in stratigraphic order (Figure 4, Table 2). Whether the loessic layer is of eolian origin or reworked loess in over bank deposits cannot be confirmed. In any case, the 1.1 m top of the terrace indicates deposits of low energy incompatible with the presence of an active stream and thus indicates that the underlying conglomerate has been abandoned prior to deposition of these upper layers, i.e., prior to 12.2 ka. To better constrain the age of abandonment of the terrace, we modeled the Beryllium-10 concentration with depth for 8 amalgamated gravel-pebble samples collected in the conglomeratic terrace deposit (Table 3). To take into account the shielding effect of the loess and soil we propose 3 end-member models (Figure 11A, B, C). The first one (model 1) is a maximum shielding or maximum age model, where despite some knowledge of the loess and soil ages, we consider that loess and soil were deposited immediately after the abandonment of conglomerate T3 was abandoned. Considering the respective density for sandy-loess

of 2.0 and soil of 1.2, the best fit of the ^{10}Be data is obtained with an exposure age of 21.6 ± 4.6 ka (t_{1-1}) (Figure 11). Clearly, given the age of the lowermost OSL sample of 12.2 ka, this age is not realistic and is too old. A second model (model 2) takes into account the oldest ages of the sandy-loess and soil deposit as the moment when these layers were deposited. This model has thus 3 exposure phases, a first one corresponding to the abandonment of the conglomerate without shielding (between t_{2-1} and t_{2-2}), a second one, with 30 cm of sandy-loess shielding starting at 12.2 ka (t_{2-2}), and a third one, with the additional 80 cm of soil shielding starting at 7.7 ka (t_{2-3}). The sandy-loess and soil layers are supposed to deposit instantaneously. Model 2 gives a time of exposure of the conglomerate without shielding of 2.7 ka, thus an abandonment age of 14.9 ka (t_{2-1}). A third model (model 3), is similar to model 2 but instead of considering an instantaneous deposition of the sandy-loess and soil layers, it considers progressive deposition of the shielding layers, the 30 cm of loess between 12.2 ka and 7.6 ka, (6.5 cm/ka) and the 80 cm-thick soil development between 7.6 ka until today (10.5 cm/ka). Model 3 is a minimum shielding model or minimum age model and gives an abandonment age of 13.7 ka (t_{3-1}). The results of the two latter models are similar within error bars, and we thus suggest an abandonment age for T3 of 13.7 ± 1.5 ka.

For terraces T2 and T1, we collected surface samples, mostly pieces of the top of large boulders from the surface of the terraces. 7 samples were collected on T2, all on the part of the terrace located downstream from the fault (Figure 4, Table 3). 6 samples were collected on T1, 3 north of the fault and 3 south of the fault (Figure 4, Table 3). The exposure ages of T1 and T2 were calculated using the CRONUS calculator (Balco et al., 2008) with the time-dependent Lal (1991) / Stone (2000) scaling scheme for spallation (Table 3). Ages of T1 range from 1 to 14 ka with an average of 9.0 ± 1.4 ka. Ages of T2 range from 10 to 39 ka with an average of 16.6 ± 3.0 ka. Both age distributions on T2 and T1 indicate a large scatter in the data, with overlapping values between terraces (Figure 9), that may be related to unevenly

distributed and large inheritance among the boulders and/or variable erosion affecting the protruding large boulders at the surface of the terraces. Such ^{10}Be concentration scatter is a common feature of boulders originating from small size high-mountain glacier catchments where accumulation and transport vary with climate changes (e.g. Putkonen & Swanson, 2003; Heimsath & McGlynn, 2008; Heyman et al., 2011). Boulders may have sat at various depths in moraines upstream at high elevation during a large part of the Pleistocene, before being transported episodically thanks to increased moist periods and during brief flash floods. Unlike large catchments with deep valley fill, most of the conglomeratic material composing the fan and terraces at the outlet of the upper valley across the fault zone were probably never buried deep enough to be shielded completely from cosmic rays. The deepest gravels in the T3 depth profile have concentrations representing about 20 to 30% of the surface samples, which represent a significant amount of inherited ^{10}Be acquired upstream. This amount of inheritance may be indicative of the intermittent stream dynamics and evidence of sediment accumulation in the catchment. Inheritance may be distributed differently in amalgamated gravels and large blocks, as their mode of transport and residence time in the catchment differ greatly (e.g. Benedetti and Van der Woerd, 2014; Carretier et al., 2015). Alternatively, the youngest boulder ages may correspond to samples with minimal inheritance and thus closest to the true surface age (e.g., Le Dortz et al., 2011; Owen et al., 2011), yielding 11.8 ± 1.1 ka for T2 and 1.2 ± 0.1 ka for T1 (Figure 9). Additional age constraints for T2 may be given by the age of the overlying soil determined by radiocarbon dating (Liang et al., 2018). The concordant ages of 8.0-8.7 ka obtained in two soil pits upstream and downstream in T2 indicate that T2 must have been abandoned at that time. Thus, the abandonment age of T2 must have occurred sometime between 8.0 and 11.8 ± 1.1 ka.

Slip rate

The difference between far field and near field offsets of the T3/T2 and T2/T1 risers indicates incomplete riser refreshing during lower level occupation. Near field displacements of d3u, d3l, d2u and d2l exist. Furthermore d3u and d3l are similar to the displacement of riser T2/T1 (D2u, D2l), and d2u and d2l are similar with the stream offset Ds (Table 4). Therefore, offsets of risers T3/T2 and T2/T1 started to accumulate before the lower terraces were abandoned (Figure 11). In addition, the riser T3/T2 may have been further modified by incision of channel T2' at its base and within level T2. The timing of abandonment of T2' is loosely constrained as occurring after abandonment of T2 (i.e., 8-12 ka) and before deposition of T1 (i.e., 1.2 ka).

Dividing the average cumulative displacement of the crest of the T3/T2 riser of 88 ± 9 m by the abandonment age of T3 of 13.7 ± 1.5 ka yields a minimum left-lateral slip rate of 6.4 ± 1.2 mm/yr (5.2-7.9 mm/yr). The cumulative displacement of the base of the T3/T2 riser of 72 ± 3 m may correspond to the emplacement of T2 at $8.0-11.8 \pm 1.1$ ka and yields a maximum slip rate of 7.3 ± 2.0 mm/yr (5.3-9.4 mm/yr). The T2/T1 riser offset of 35 ± 2 m at crest or 27 ± 2 m at base, similar to the T2' channel offset of 29 ± 2 m, remains unconstrained in the absence of ages for T2'.

Fault scarp heights across T3 and T2 and corresponding ages may be used to estimate the vertical slip rate. For T3, dividing the throw of profile C-C' of 15 ± 2 m by its abandonment age of 13.7 ± 1.5 ka yields a vertical slip rate of 1.1 ± 0.3 mm/yr. For T2, dividing the throw of profile B-B' of 10 ± 1 m by its abandonment age of $8.0-11.8 \pm 1.1$ ka yields a similar vertical slip rates of 0.7-1.4 mm/yr. The average vertical slip rate is 1.1 ± 0.3 mm/yr (Figure 12).

Given the vertical offsets of T2' of 5-7 m, and assuming a constant vertical slip rate of 1.1 ± 0.3 mm/yr, the age of T2' may be estimated to be about 5.4 ± 1 ka. Similarly, the age of T1 offset 1.3 ± 0.2 m may be estimated at about 1.2 ± 0.2 ka, concordant with the youngest surface exposure age.

Relating these less well constrained and indirectly determined ages for T2' and T1, with the corresponding offsets of T2' of 29 ± 2 m and T1 of 6.5 m, yields rates of 5.3 ± 1.5 mm/yr and 5.4 ± 1.3 mm/yr, respectively.

DISCUSSION

Variability in slip rate determination

Geologic fault slip rate reflects the long-term fault behavior, it is thus a basic datum for understanding strain accommodation through a system of faults, and also one of the most important indicators for earthquake potential of a fault. Considerable efforts have been devoted to determining the slip rate on active faults within the Tibetan Plateau. Geologic determination of fault slip rate is simple in principle but is subject to considerable uncertainty. The difficulty lies in the fact that the duration of offset accumulation is often approximated by a surrogate age. For instance, terrace risers are commonly used as offset features in slip rate determination of faults in northern Tibet, including the Haiyuan, the Altyn Tagh and the Kunlun faults (e.g. Cowgill et al., 2009; Kirby et al., 2007; Lasserre et al., 1999; Mériaux et al., 2004, 2005, 2012; Van der Woerd et al., 1998, 2000; Meyer et al., 1996; Peltzer et al., 1988). They are erosive features, which likely form diachronously, starting to record offset sometime after the abandonment of the upper terrace and before the abandonment of the lower terrace (e.g., Ryerson et al., 2006). The abandonment age of the upper terrace surface provides the maximum age of slip accumulation, thus the lower bound of the true slip rate. Accordingly, the lower terrace surface age represents the minimum age of slip accumulation and thus the upper bound of the slip rate.

The difference in geologic slip rate on the Haiyuan fault stems mainly from this uncertainty of using upper terrace surface versus lower terrace surface age as the surrogate for the true offset age of the terrace riser. Lasserre et al. (2002) reported 12 ± 4 mm/yr on the eastern Maomao Shan (Laohu Shan) sections of the Haiyuan fault. They used the lower terrace age, i.e., the minimum age for offset accumulation, thus

provided an upper bound for the slip rate. On the other hand, much lower slip rates were reported, 3.3-6.6 mm/yr on the Lenglongling section (He et al., 2000, 2010; Jiang et al., 2017), and 4.1-5.8 mm/yr on the Laohu Shan section (Yuan et al., 1998), respectively. These lower rates are based on the scenario of using the upper terrace surface age for slip accumulation, and thus provide the lower bound of the slip rate. As shown in the summary of Table S1, studies along the Haiyuan fault showing slip rate less than 5 mm/yr are mainly based on an upper terrace reconstruction. In a few cases both the upper and lower terraces were dated (Li et al., 2009; Zheng et al., 2013). If the lower terrace reconstruction scenario is considered, an upper bound in the range of 4.5-22 mm/yr is implied, even though this upper bound is not mentioned in these studies (Table S1). An objective evaluation of these two previous studies show that these studies sampled the loess cover (either OSL or 14C dating) of the upper terrace surface, which postdated the abandonment of the terrace surface. The implication is that even though the upper terrace constrains the maximum age of offset accumulation, the loess cover shifts the age to be younger. Eventually, considering these factors, many slip rate determinations should have larger uncertainty than reported. It is tempting to favor the lower bound estimates for the Haiyuan fault, as it is closer to the geodetic rates from GPS velocity field of 4-5 mm/yr (Li et al., 2009) or from InSAR data of 4-8 mm/yr (Cavalié et al., 2008; Jolivet et al., 2012; Daout et al., 2016), as in the case of the Altyn Tagh fault (Cowgill, 2007; Zhang et al., 2007; Gold et al., 2009, 2011a). However, high GPS loading rate of 8.6 mm/yr was also reported on the Haiyuan fault (Gan et al., 2007), as well as high rate from InSAR of 8.6 ± 1.5 mm/yr along the central section (Daout et al., 2016). These data remind us that the current GPS field is not targeted for optimal determination of fault loading rate, because GPS sites are still sparse, and thus the strain rate across the fault must be estimated by collapsing all measurements within a wide (often 100 km wide) swath. When doing so, the effects of fault geometry changes along strike are

not taken into account, which could be important for explaining the considerable lateral and gradual variation in the regional GPS velocity field.

Strictly speaking, the true slip rate of the Haiyuan fault should lie between the ranges of upper and lower bounds. It is helpful to resolve the variability to explicitly distinguish the lower and upper bounds when reporting the rate. At the Daqing site in this study, the upper and the lower bounds of the slip rate constrained by T3/T2 terrace riser are remarkably similar, 6.4 mm/yr and 7.3 mm/yr. This is because the ages of T3 (13.7 ka) and T2 (8.0-11.8 ka) might be relatively close in time.

T2/T1 terrace riser, on the other hand, provides a much larger uncertainty and looser constraint on the slip rate (3.3-23.5 mm/yr) when neglecting T2' ([Figure 12B](#)). The contrast in slip rate bracketed by T3/T2 and T2/T1 at the same site highlights again that one should not favor the upper or the lower terrace reconstruction scenarios, without additional information. If we use the upper terrace age as the offset age, the offset of T3/T2 riser suggests a slip rate of 6.4 mm/yr (since 13.7 ka), whereas the offset of T2/T1 riser suggests 3.3 mm/yr (since 8.0-11.8 ka), almost two times lower. This difference at the same site could be interpreted as a temporal change in slip rate, as suggested elsewhere in some previous studies ([Gold et al., 2017](#); [Liu et al., 2018](#)). In reality, the rates given are simply the lower bound, rather than the true slip rate. The difference is a good indication of variable initiation time of riser offset record after the abandonment of the upper terrace, thus the uncertainty in slip rate determination, rather than an indication of temporal change in slip behavior. In fact, the comparison between short term and long term slip rate for a number of large strike-slip faults all over the world also shows that the slip rate is not changing significantly through time ([Cowgill et al., 2009](#); [Meade et al., 2013](#); [Tong et al., 2014](#)).

The assumption of uniform slip rate over time implies that the slip vector should be temporally stable. Thus, the ratio of vertical and horizontal offsets is also consistent on each terrace. The vertical offset of 15 ± 2 m and the minimum horizontal offset of 88 ± 9 m on T3 imply a maximum ratio of 0.17 ± 0.04 . The ratios are

0.21±0.05 and 0.2±0.05 on T2' and T1, respectively. We constrain an average ratio of 0.16±0.01 consistent with the range of ratios for the three terraces.

The ratio of 0.125±0.025 estimated by Gaudemer et al. (1995) is a little smaller than the average ratio of 0.16±0.01 (Figure 13). This is due to a larger total horizontal displacement of the upper terrace (T3, 145 m) estimated from the assumption of lower terrace reconstruction. As we discuss above, the horizontal offset of the upper riser can only define an upper bound of the displacement of the lower terrace, suggesting that the ratio of 0.125±0.025 is in the low range.

Furthermore, when combining the ratio of 0.16±0.01 and the vertical offset of 10±1m on T2, we can estimate the total displacement of T2 to about 63±10m, which is much larger than the riser T2/T1 offset (35±2 m) and similar to the minimum offset of T3/T2 (72±2 m).

Following the assumption of a temporally stable deformation rate, we summarize the measured offsets versus corresponding ages (Figure 14), and propose a broadly uniform strike slip rate of 5-8 mm/yr. The tightly constrained age of T3 and the far field offset of the lower riser (solid rectangle) have much more weight in the determination of the rate than other less well determined data (dashed rectangles).

Our investigation at the Daqing site shows that incomplete riser refreshment and slip accumulation before the lower terrace abandonment can also occur on the unprotected side of the river bank. A terrace riser on the left bank of a river across a left-lateral fault would be on the protected side, i.e., continuous left-lateral slip would move the downstream section of the riser away from the stream center and be less frequently refreshed, thus more likely to record offset before the abandonment of the lower terrace abandonment (e.g., Cowgill, 2007). At the same time, if a terrace riser on the right bank was developed, left-lateral slip on the fault would move the downstream part of the riser toward the center and in alignment with the upstream channel. This configuration would favor more frequent riser refreshment and obliteration of offset before the abandonment of the lower terrace (e.g., Van der

Woerd et al., 1998; Tapponnier et al., 2001). However, our offset measurements and dating of sequentially abandoned terrace surfaces suggests that right-bank terrace riser on a left-lateral fault, i.e., erosive side, is also subject to incomplete riser refreshment and partial preservation of offset before the abandonment of the lower terrace. The lower terrace reconstruction may not be a safe assumption even for this favorable riser-offset configuration. The obliquity in slip vector and the accumulation of vertical displacement inducing strong incision in the upstream terrace deposits (Figure 8) may increase channeling upstream and less erosion downstream. The terrace riser development and preservation remain complex processes, including diachroneity and different age of riser sections on opposite sides of the fault related to fluvial erosion and riser degradation (e.g., [Harkins and Kirby, 2008](#); [Gold et al., 2009, 2011b](#)).

Earthquake rupture implication

The youngest exposure age on terrace T1 is 1.1 ± 0.1 ka, which implies that the age of the most recent rupture at this site should be younger than 1.1 ± 0.1 ka, but may be older than eight centuries (Gaudemer et al., 1995). Trenching by Yuan et al. (1997) indicated three events on the Jinqiang He section near our site with the most recent event around 1000 a B.P. This result may give some clue about the latest rupture, even though details about the trench interpretations are lacking. The two older events presented might rupture both the Jianqiang He and western part of the Maomao Shan sections around ~ 1800 ka B.P. and ~ 4000 yr B.P. The Lenglongling section, west of our site, has a mean event recurrence interval of 1430 ± 140 a during the Holocene ([Jiang et al., 2017](#)) or 1640 ± 570 a ([Guo et al., 2019](#)). To the east of our site, the Laohu Shan section seemingly ruptures every ~ 1000 a ([Yuan et al., 1997](#); [Liu-Zeng et al., 2007](#)). If T1 and T0 experienced only one rupturing event with the scarp on T0 being almost completely eroded, the offset of $\sim 6.0 \pm 0.5$ m of the abandoned stream channel present on T1 may preserve the last coseismic lateral slip. Using the slip rate of 5-8 mm/yr and this coseismic offset, the average recurrence

interval would be 1100 ± 300 a, consistent with other studies. We speculate the Jinqiang He section has similar rupture history with recurrence interval of 1000-1500 a and the most recent rupture about 1000 a.

The Jinqiang He section, called Tianzhu seismic gap by Gaudemer et al. (1995), is about 55 km long. If this section ruptured entirely, the magnitude could reach M_w 7.4 to 7.7 according to empirical relationship between magnitude, surface rupture length and average displacement, respectively, for strike slip faults (Wells and Coppersmith, 1994). It is likely that a rupture on the Jinqiang He section could breach the Tianzhu stepover and propagate to the western part of the Maomao Shan section. The rupture length would reach ~ 120 km, and the maximum magnitude would be M_w 7.8 (Wells and Coppersmith, 1994). The Jinqiang He and adjacent sections could be ripe for rupturing in a future great earthquake. Precise seismic risk assessment demands that further detailed paleoseismical investigations be carried out to define a more accurate rupture history along the central Haiyuan fault.

CONCLUSION

High resolution topography data derived from the terrestrial LiDAR enable us to investigate offset features of the Haiyuan fault in detail. Based on T1, T2 and T3 terraces mapped carefully from topography data, we use local fitting piercing lines to estimate the range of displacement for T3/T2 to be 88 ± 9 m at the crest and 72 ± 3 m at the base, and for T2/T1 to be 27 ± 2 - 35 ± 2 m. Maximum vertical throw for T3, T2 and T2' is 15 ± 2 m, 10 ± 1 m and 6 ± 1 m respectively. The vertical motion on T1 was also estimated to be 1.3 ± 0.2 m. The total strike displacement of T3 is larger than 88 ± 9 m, T2 is between 72 ± 3 m and 35 ± 2 m, or 63 ± 10 m derived from relationship of vertical and horizontal offset. The channel T2' incised in T2 is horizontally offset 29 ± 2 m. The horizontally offset small stream on T1 and near field offset of riser T2/T1 indicate the total strike displacement of T1 is 6.5 ± 1 m. The offset of 6.0 ± 0.5 m of the small stream may be associated with the most recent slip event. Terrestrial

Cosmogenic nuclides dating, combined with ^{14}C and OSL dating, were used to constrain the age of T3 at 13.7 ± 1.5 ka. These data suggest a slip rate of 6.6 ± 1.4 mm/yr since 15 ka. T2 and T1, are less well constrained at $8.0\text{--}11.8 \pm 1.1$ ka and 1.1 ± 0.1 ka, respectively. Assuming a constant vertical to horizontal ratio, the age of T2' may be inferred at 5.4 ± 1 ka. The slip rate of 5-8 mm/yr is broadly consistent with all data. This slip rate is similar to the recent reassessment of the slip rate (5.0-8.9 mm/yr) near Songshan (Yao et al., 2019).

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Table 1. Radiocarbon dates table

Sample	Lab ^a	Depth (m)	Fraction Modern	±	D ¹⁴ C (‰)	±	¹⁴ C Age (B.P.)	±	2σ calibrated age (B.P.) ^b
HGD-C14-01	414950	0.77	0.4236	0.0016	-576.4	1.6	6900	30	Cal 7790 - 7675
HGD-C14-02	414951	0.62	0.4414	0.0016	-558.6	1.6	6570	30	Cal 7555 - 7545

a: All sample were AMS dated at Beta Analytic; b: Calibration with Calib 7.1 (Stuiver et al., 1998), did not include probability distribution of range < 0.1.

Table 2. Quartz OSL ages on T3

Sample No	Lab. no ^a	Depth(m)	Water content ^b (%)	U(ppm)	Th(ppm)	K(%)	Cosmic dose rate(Gy/ka)	grain size (μm)	Dose rate ^c (Gy/ka)	Equivalent Age ^e dose ^d (Gy) (ka)
HGDOSL-1502	15-64	0.82	2.6	2.71±0.1	14.4±0.39	2.18±0.06	0.32±0.02	90-125	4.06±0.15	35.3±1.3 8.7±0.5
HGDOSL-1501	15-63	1.04	8.04	2.45±0.1	12.8±0.36	2.12±0.06	0.31±0.02	90-125	3.61±0.13	44.2±0.8 12.2±0.5

a: All samples were processed at Zhejiang Zhongke Institute of Luminescence Testing Technology;

b: The measured water content;

c: The concentrations of U, Th and K were measured by neutron activation analysis at the China institute of atomic energy;

d: All De values conform to normal distribution;

e: All De values were calculated by the central age model (Galbraith et al., 2012).

Table 3. Analytical data of ^{10}Be at Daqing site on the Haiyuan fault

Samples	Mass quartz (g)	Be Carrier (mg)	Latitude (N)	Longitude (E)	Altitude (m)	Depth (cm)	Thickness (cm)	Sample type	$^{10}\text{Be}/^9\text{Be}$	$^{10}\text{Be}/^9\text{Be}$ error (%)	$^{10}\text{Be} \pm \text{error}$ (atom/g)	Exposure age \pm uncert (yr)
T1 surface												
HGD14-08	30.107	0.2461	37.259544	102.696663	3441	0	2.5	boulders	1.11247E-12	3.1680	608254 \pm 19269	13344 \pm 1205
HGD14-09	26.9599	0.2699	37.259254	102.696609	3432	0	2.5	boulders	5.23986E-13	3.0904	350879 \pm 10843	7705 \pm 693
HGD14-10	25.7075	0.241	37.259041	102.696503	3426	0	2.5	boulders	7.61713E-13	3.1744	477641 \pm 15162	10529 \pm 951
HGD14-16	30.0079	0.2458	37.256313	102.695001	3369	0	2.5	boulders	3.02524E-13	3.1761	165752 \pm 5264	3956 \pm 357
HGD14-22	29.8354	0.25	37.256969	102.695702	3389	0	2.5	boulders	6.77539E-13	3.1746	379748 \pm 12055	8594 \pm 776
HGD14-23	29.972	0.2517	37.257381	102.695984	3393	0	2.5	boulders	8.62754E-14	3.5217	48462 \pm 1706	1165 \pm 106
T2 surface												
HGD14-18	30.0132	0.2901	37.255253	102.694336	3351	0	2.5	boulders	1.11507E-12	3.0821	720924 \pm 22219	16489 \pm 1486
HGD14-19	24.5073	0.2253	33.255444	102.69445	3354	0	2.5	boulders	1.41835E-12	3.4983	872173 \pm 30511	21606 \pm 1982
HGD14-20	30.0075	0.2495	2m south of 19			0	2.5	boulders	2.79689E-12	1.9939	1555499 \pm 31016	36437 \pm 3185
HGD14-25	30.0081	0.2555	37.256226	102.694389	3371	0	2.5	boulders	1.37277E-12	3.0506	781814 \pm 23850	17590 \pm 1584
HGD14-26	25.0845	0.2432	37.257112	102.69458	3388	0	2.5	boulders	1.23744E-12	3.0546	802483 \pm 24512	17877 \pm 1610
HGD14-27	30.0488	0.2546	37.257439	102.694618	3391	0	2.5	boulders	9.21578E-13	3.1078	522297 \pm 16232	11788 \pm 1062
HGD14-28	30.0016	0.253	37.257252	102.69455	3393	0	2.5	boulders	1.12670E-12	3.1186	635531 \pm 19820	14360 \pm 1295
T3 depth profile												
HGDT3-01	31.4296	0.2592	37.257061	102.693886	3389	85	5	gravel	1.30104E-12	2.4296	717695 \pm 17436	See model
HGDT3-02	29.9764	0.2484	37.257061	102.693886	3389	100	5	gravel	2.05011E-12	2.6603	1136327 \pm 30229	/

HGDT3-03	25.1784	0.2563	37.257061	102.693886	3389	115	5	gravel	8.73919E-13	3.1803	595039 ± 18923	/
HGDT3-04	32.0859	0.2514	37.257061	102.693886	3389	145	5	gravel	7.71630E-13	3.2954	404402 ± 13326	/
HGDT3-05	30.1135	0.2566	37.257061	102.693886	3389	175	5	gravel	5.80584E-13	3.0688	330913 ± 10154	/
HGDT3-06	29.3054	0.254	37.257061	102.693886	3389	205	5	gravel	6.24376E-13	3.0946	361981 ± 11201	/
HGDT3-07	30.0178	0.2501	37.257061	102.693886	3389	245	5	gravel	6.97878E-13	3.5702	388926 ± 13885	/
HGDT3-08	30.041	0.2549	37.257061	102.693886	3389	285	5	gravel	4.62999E-13	3.2264	262778 ± 8478	/

Note: All samples were taken chemical process at the Key Laboratory of Crustal Dynamics, China Earthquake Administration and AMS measurement at Centre de Recherche et d'Enseignement de Géosciences de l'Environnement (CEREGE) of France. Scaling scheme for spallation: Time-dependent Lal (1991) / Stone (2000), ages calculated with the CRONUS 2.3 calculator (<http://hess.ess.washington.edu/>), density of sample is assigned simply with 2.7 g/cm³, erosion rate is zero.

Table 4. Terrace displacement and geometry measurement

	Marker	Parameter	Value/m	error/m	Note
Horizontal Offset	Stream	Ds	6.0	0.5	
		D2u	35	2	
	T2/T1	D2l	27	2	
		d2u	6.5	1	
		d2l	6.5	1	
	T3/T2	D3u	94	3	
			82	3	
		D3l	72	3	
		d3u	25	2	
		d3l	28	2	
	T2'	D2'	29	2	
		West bank	28	2	
Vertical offset	T1 tread interior	Sc1	1.3	0.2	
	T2' interior		5.7	1	
	T2' outer		6.4	1	
	T2 tread interior	Sc2	9	1	
	T2 tread outer		10	1	
	T3 tread interior	Sc3	19	2	
	T3 tread outer		15	2	
Width	T1 tread	W1u	61	4	upstream
	T1 tread	W1l	34	2	downstream
	T2'		42	2	upstream
	T2'		42	2	downstream
	T2 tread	W2u	135	5	upstream
	T2 tread	W2l	89	3	downstream
Height	T1-T0 tread	R1u	6	1	upstream
		R1d	2.5	0.5	downstream
	T2-T1 tread	R2u	16-17	1	There is a bump at upstream of T2 tread
		R2d	7.5	1	downstream
	T3-T2 tread	R3u	10-15	1	There is a bump at upstream of T2 tread
		R3d	1.4-1.7	0.3	downstream

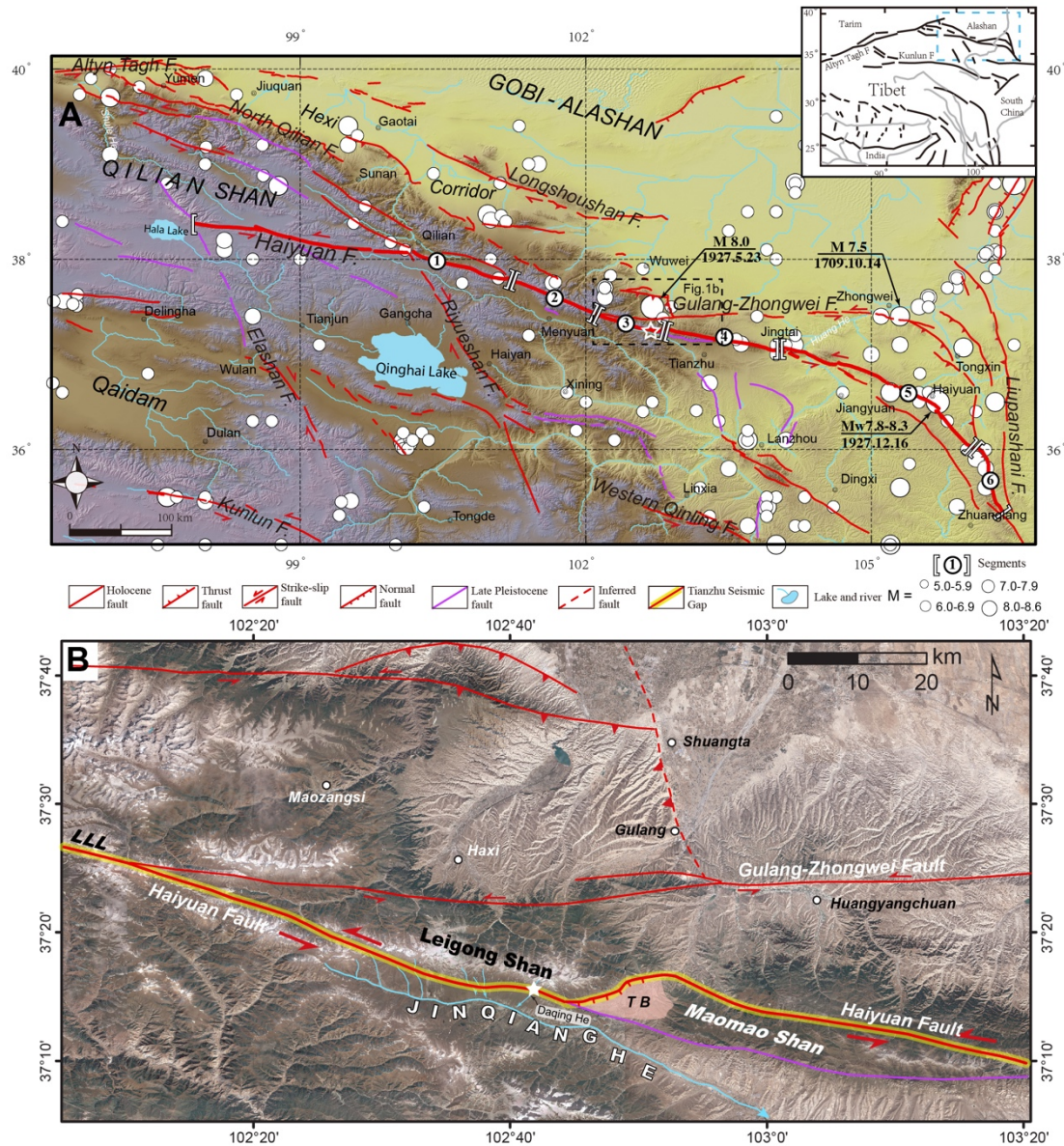


Figure 1. (A) Active faults map of northeastern Tibetan Plateau. Seismicity from B.C. 780 to A.D. 2006, Historical earthquake from Division of Earthquake Monitoring and Prediction, State Seismologic Bureau (1995), instrumental seismicity from China Earthquake Networks Center (<http://www.cenc.ac.cn/>). White star indicates study site, dashed box is figure 1B. Haiyuan fault is subdivided into six sections (1): Halahu, (2): Lenglongling, (3): Jinqiang He, (4): Maomao Shan, (5): Haiyuan, (6): Liupan Shan. Inset is location of map in tectonic frame of Tibetan Plateau. (B) Active faults along Jinqiang He section that extends from Lenglongling-Gulang-Jinqiang (LGH) faults triple junction to the west, to Tianzhu pull-apart basin (TB) to the east, left-stepping to Maomao Shan section. Jinqiang He Valley is fed mostly by north-south tributaries that are cut by Haiyuan fault and flowing down from Leigong Shan. LLL: Lenglongling.

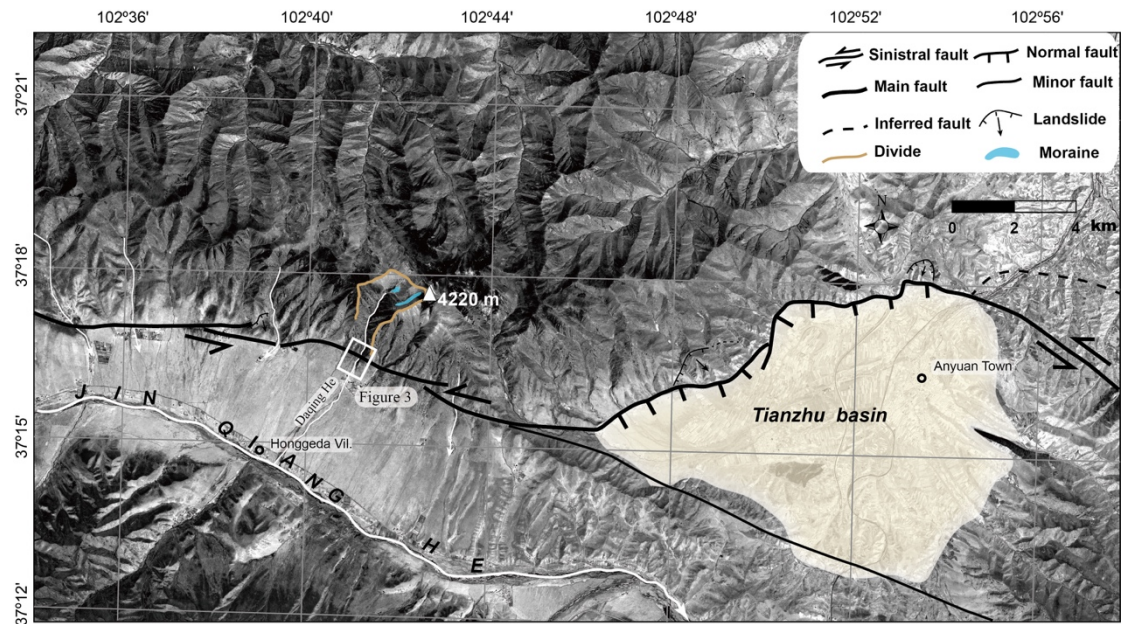


Figure 2. GF-1 satellite imagery (pixel ~2m) of Haiyuan fault near Daqing site (white rectangle) upstream from Honggeda village. Light shading delimits Tianzhu basin.

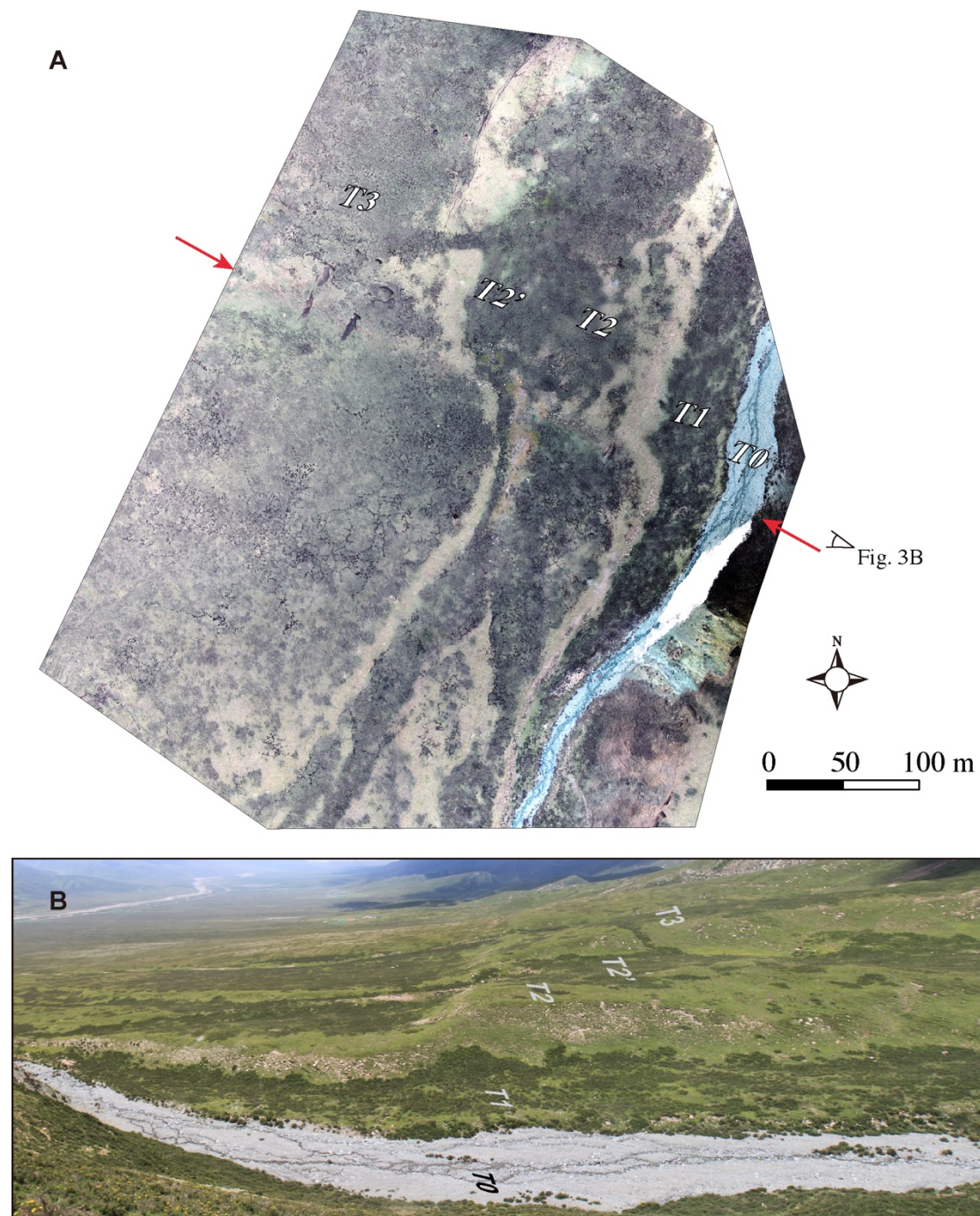


Figure 3. (A) Unmanned aerial vehicle (UAV) derived photo mosaic with ~0.2m resolution. Fault trace is clear across stream bed T0 and terraces T1 to T3 west of it. Red arrows point to the fault trace. (B) West looking panoramic field view of faulted terraces at Daqing site.

Surface sample numbers abbreviated without prefix “HGD14-”. Purple lines are piercing lines for horizontal slip measurement. (B) Hill shading and (C) slope map of DEM highlighting terrace surface morphology, distinct terrace risers and fault scarp.

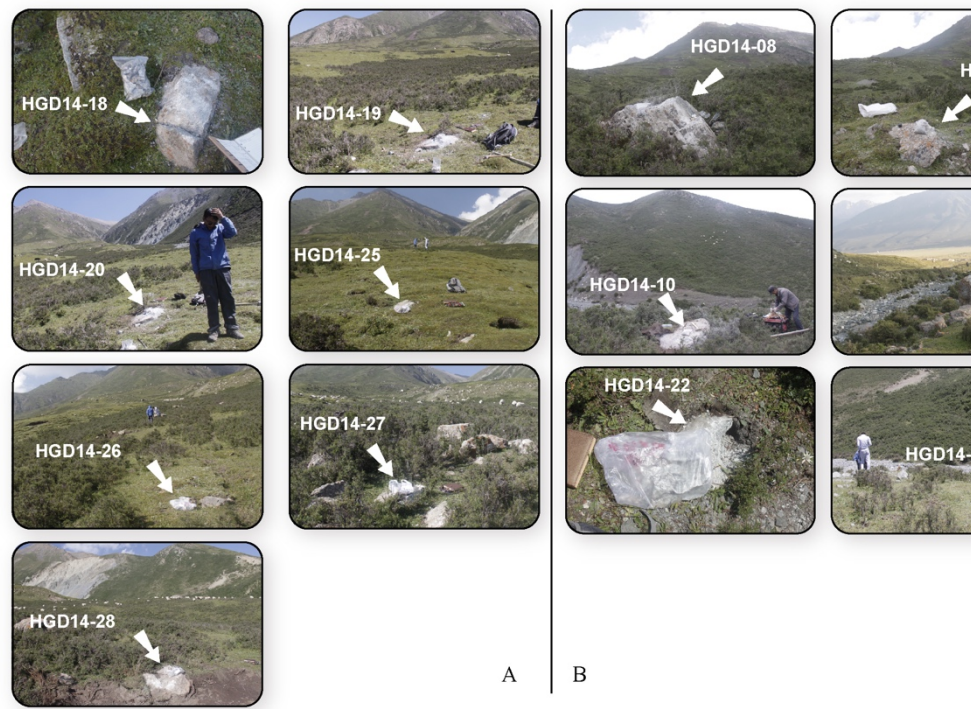


Figure 5. Field photographs of surface samples for cosmogenic dating with sample numbers on T2 (A) and T1 (B). White arrows point to boulders where samples were collected from.

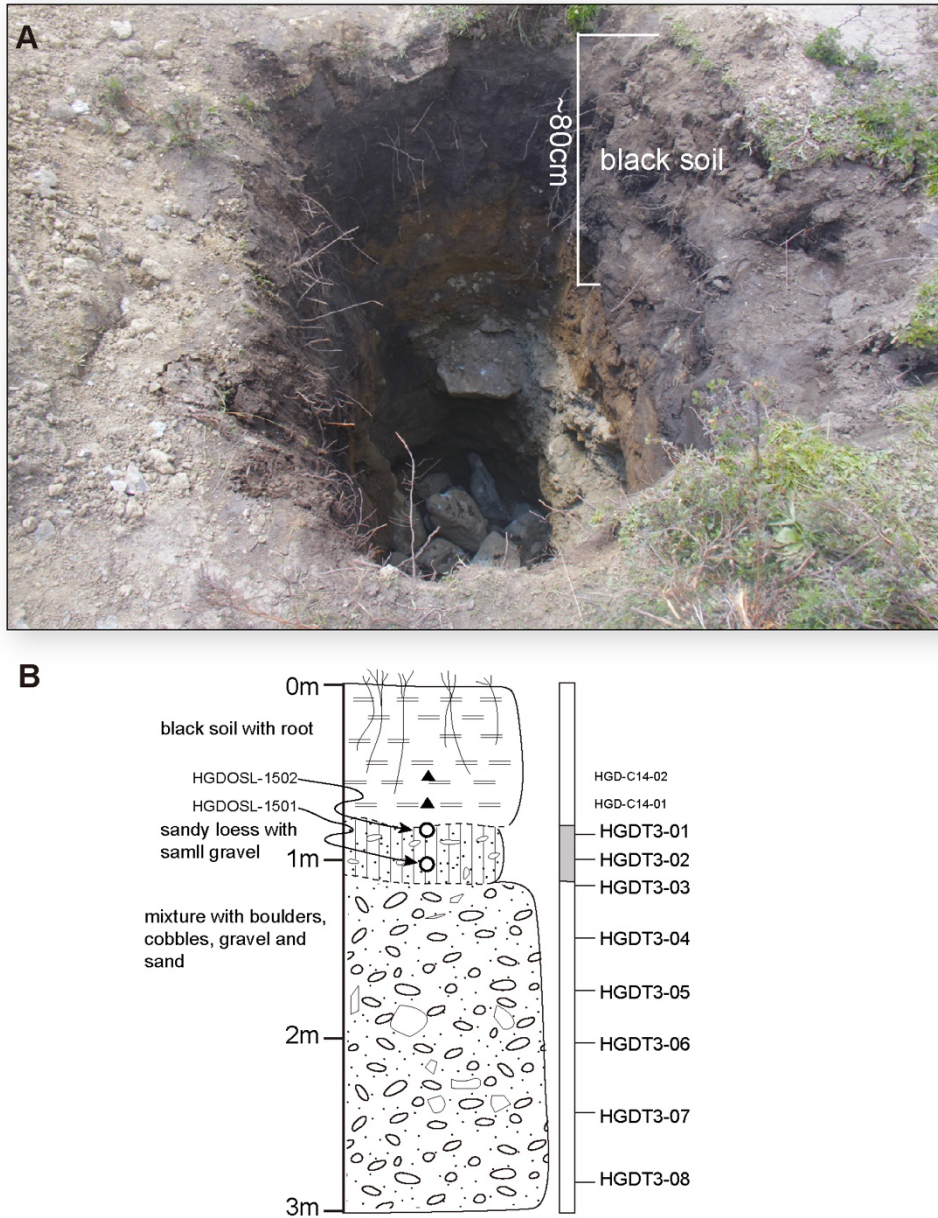


Figure 6. (A) Sampling pit on T3. (B) Stratigraphic description of pit. Eight sand and gravel samples were collected from below ~80 cm to ~3 m depth for cosmogenic isotope dating. Open circles are sandy loess samples for OSL dating, solid triangles are black soil samples for ^{14}C dating.

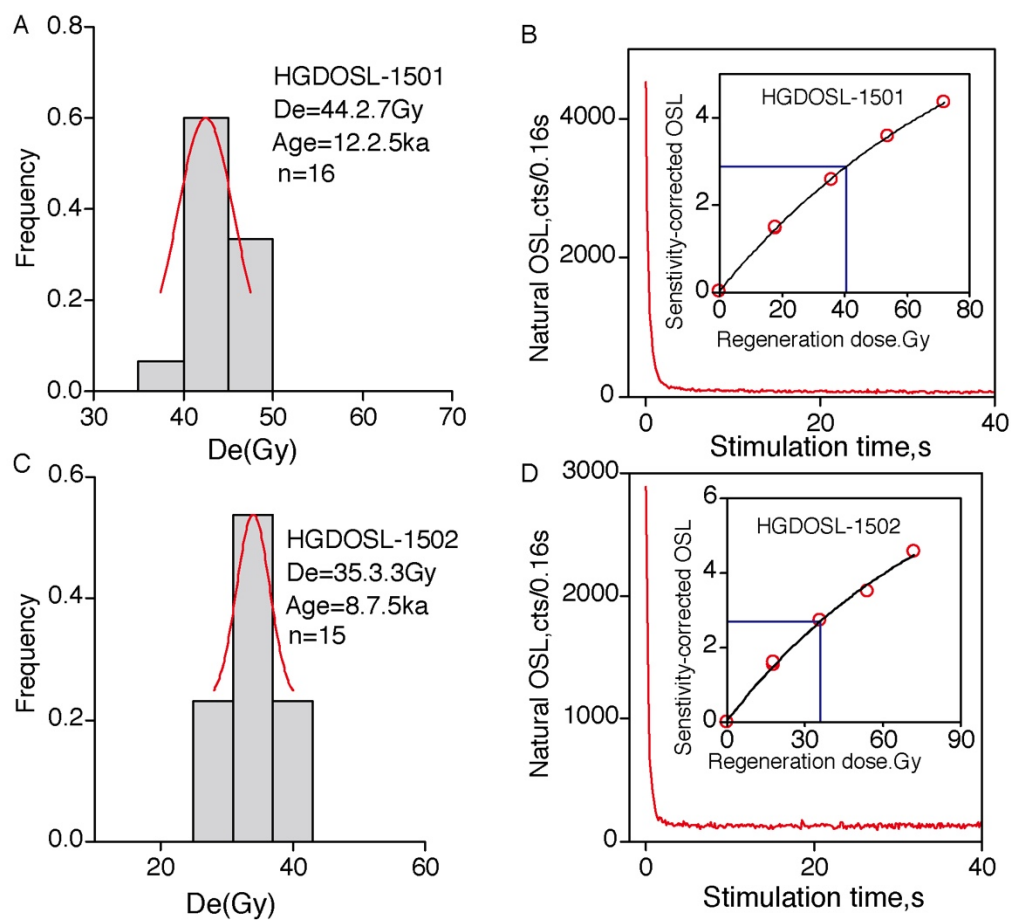


Figure 7. The De distributions, natural OSL decay curve and growth curves for samples HGDOSL-1501 (A and B) and HGDOSL-1502 (C and D).

offset of sloping surface. V_r , corrected vertical offset, is function of V_i vertical throw measurement from perpendicular to fault profile C1-C1', h is horizontal offset of terrace, α is angle between maximum slope direction and perpendicular to fault (about 4.2°) (see also Gaudemer et al., 1995).

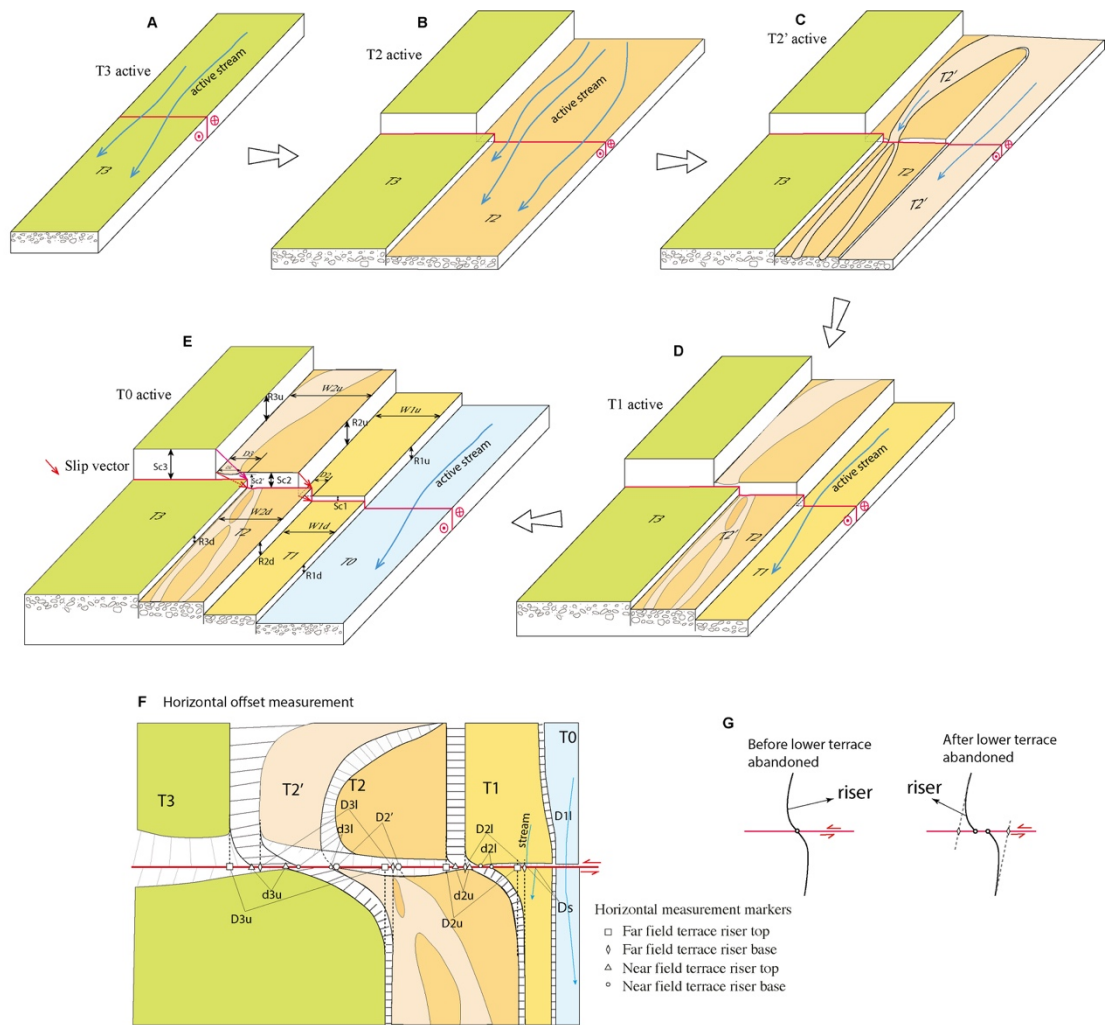


Figure 9. Offset terraces reconstruction. (A)-(E) are diagrams of different stages during river downcutting, lateral erosion and displacement accumulation. Simplified risers are vertical. (F) sketch of offset terraces at our Daqing site. All measurement results are shown in Table 4. (G) shows how near field (d_{3u} , d_{3l} , d_{2u} and d_{2l}) and far field displacements are related.

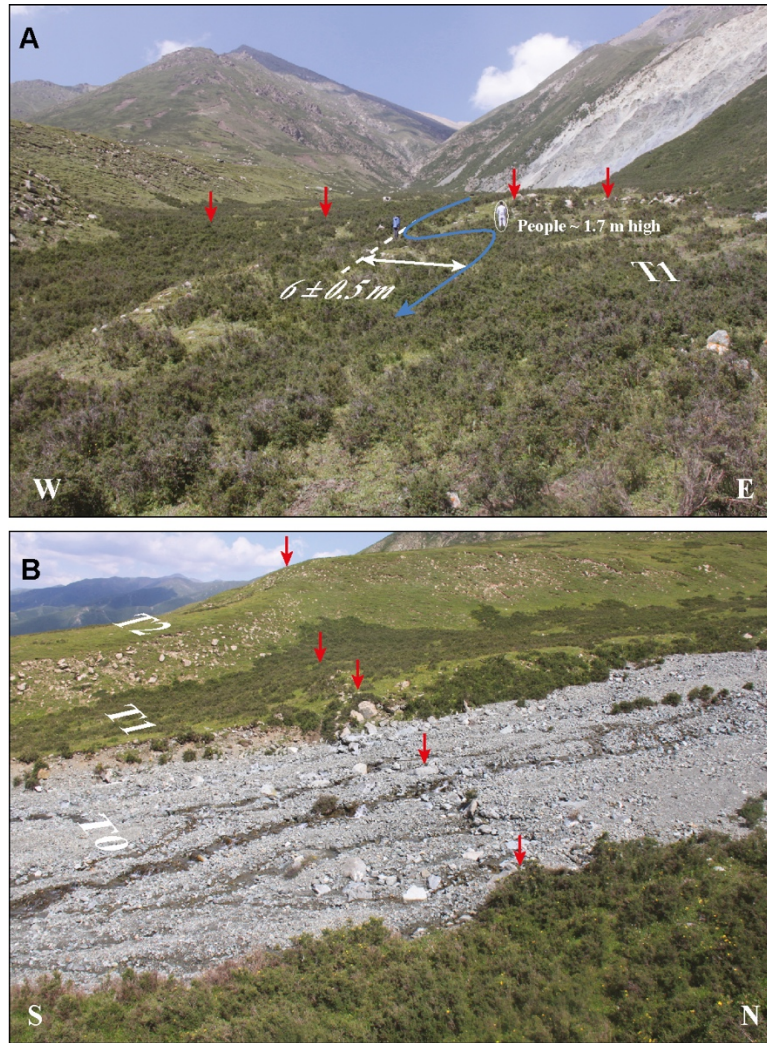


Figure 10. Field details of fault trace at Daqing site. (A) Small stream offset on terrace T1. Red arrows indicate top of fault scarp across T1. (B) Oblique view showing fault trace across T0, T1 and T2.

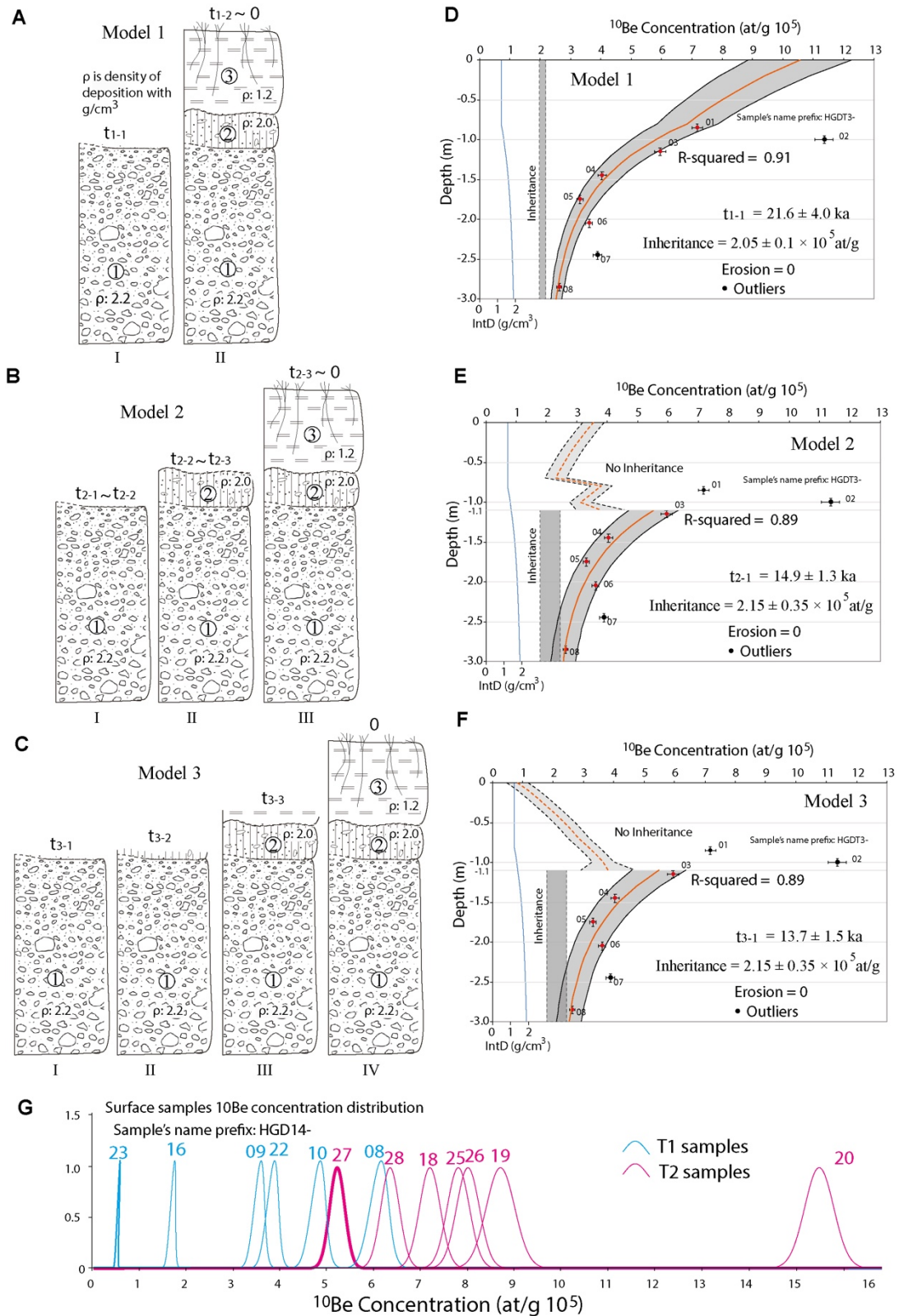


Figure 11. Exposure age constraints at Daqing site. (A), (B) and (C) are proposed end-member models of T3 depth profile. t_{1-1} , t_{2-1} and t_{3-1} are abandonment ages. (A and D) model 1: loess and soil are deposited immediately after T3 conglomerate, t_{1-1} equals to t_{1-2} . Maximum age is 21.6 ka (t_{1-1}) with R-squared of 0.91. (B and E) model 2: three exposure stages: conglomerate without shielding (t_{2-1} - t_{2-2}), sandy-loess

shielding ($t_{2-2} - t_{2-3}$), and soil shielding ($t_{2-3} - 0$) in (B). Sandy-loess and soil are instantaneous deposits. Exposure age of 14.9 ka (t_{2-1}) with R-squared of 0.89. (C and F) model 3: progressive deposition of upper sandy-loess and soil layers. Model gives minimum age of 13.7 ka with R-squared of 0.89. Black circles are outliers not considered in modeling. More realistic model 3 takes into account OSL and 14C dates. t_{2-2} , t_{2-3} , t_{3-2} , and t_{3-3} are constrained by dates of sandy-loess and soil. (G) ^{10}Be concentrations of surface samples of T1 and T2.

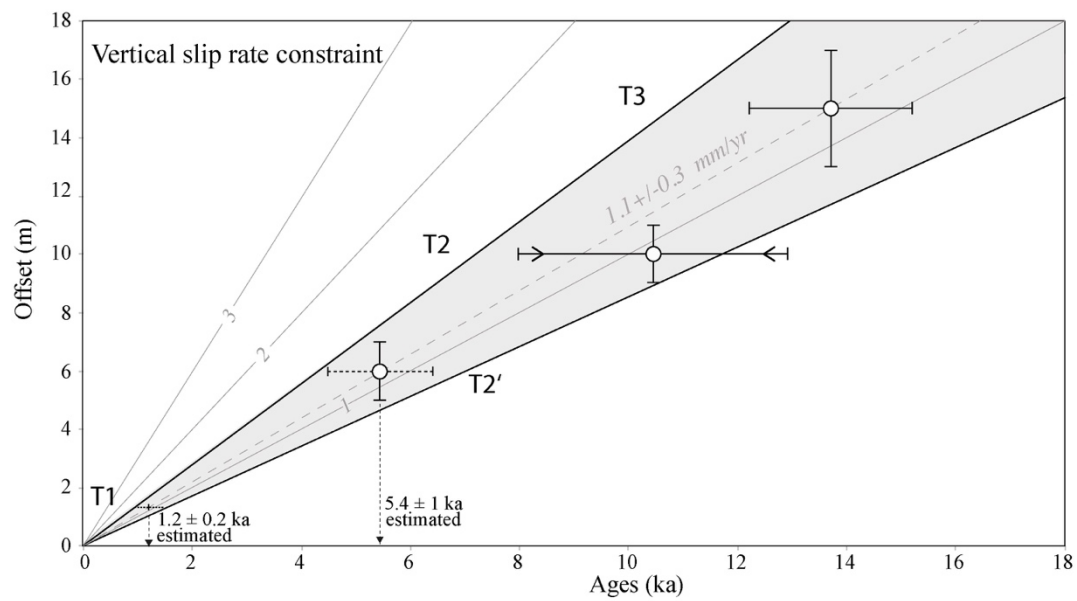


Figure 12. Vertical slip rate determination based on data from T3 and T2 at Daqing site on the Haiyuan fault. Oblique lines are slip rates in mm/yr. Gray shaded area is preferred range of slip value with a mean of 1.1 mm/yr. Combining this mean vertical slip rate and the vertical offsets of T2' and T1, their ages are estimated at 5.4 ka and 1.2 ka, respectively.

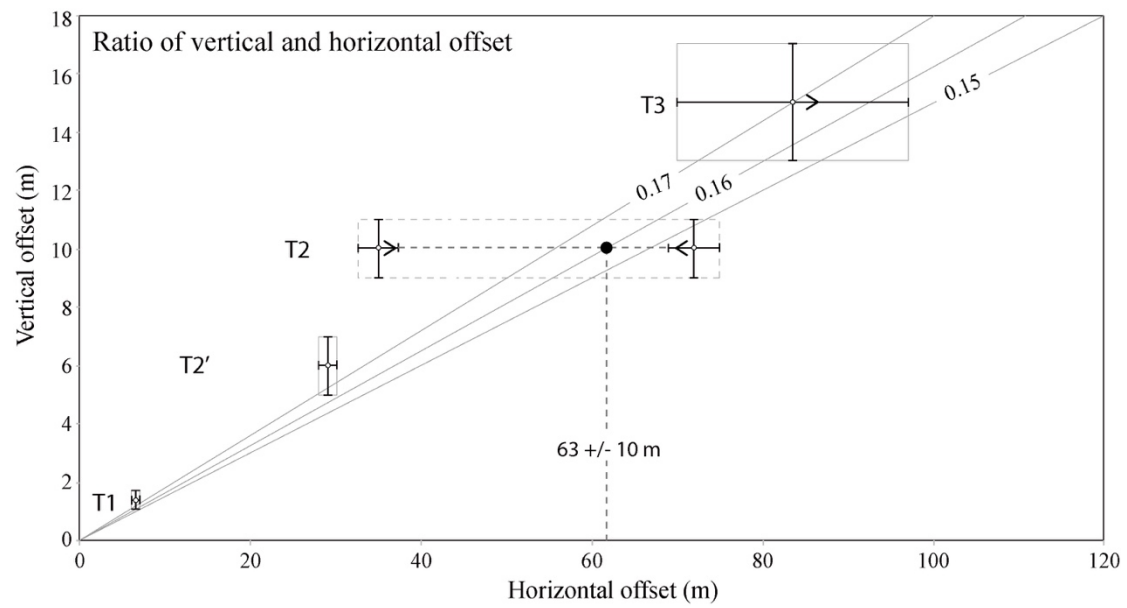


Figure 13. Ratio of vertical to horizontal offsets. T3 with a minimum horizontal offset. Best estimated ration is 0.16 ± 0.01 by T3, T2' and T1. Because of, lateral erosion and river bed incision, vertical offset may accumulate earlier than the horizontal displacement of lower risers. Total horizontal offset of T2 might be estimated at 63 m based on average ratio.

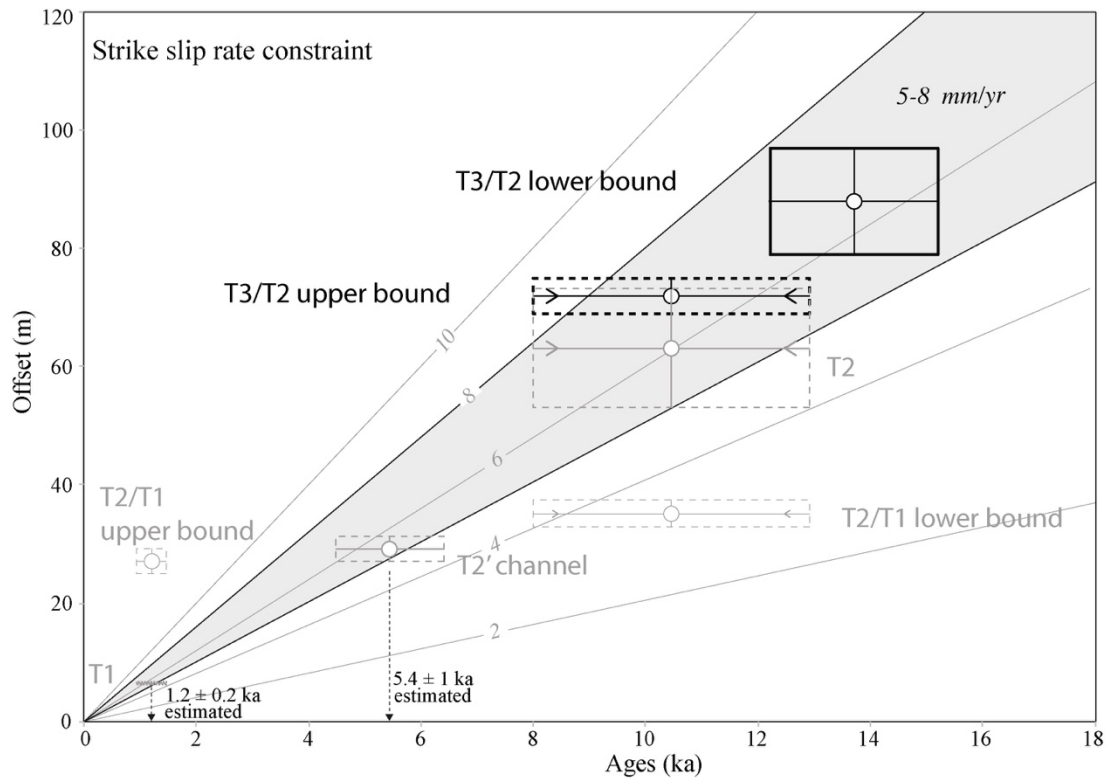


Figure 14. Strike slip rate determination at Daqing site. Oblique lines are slip rates contour with unit in mm/yr. Dashed rectangles represent weak data envelopes, but Solid rectangle is best determined rate, dashed rectangles are based on estimated data. Gray shaded area is preferred range of rates of between 5 and 8 mm/yr.