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Low intrinsic thermal conductivity of Spark Plasma Sintered dense KNbO₃ and NaNbO₃ perovskite ceramics

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Abstract :

The origin of low thermal conductivity in niobium-containing perovskites was investigated. Therefore, dense NaNbO_3 and KNbO_3 ceramics were sintered by spark plasma sintering. The grain size was in the 1 to 10 μm range. NaNbO_3 ceramic has shown a stable thermal conductivity circa $2.6 \text{ W m}^{-1} \text{ K}^{-1}$ from 373 to 1000 K and KNbO_3 , values from 2.5 to a plateau at $1.2 \text{ W m}^{-1} \text{ K}^{-1}$ since 673 K. This value is the lowest thermal conductivity reported for an oxide presenting a perovskite structure. The origin of such low thermal conductivities is indicated to be related with cation deficiency on the A-site of the niobium-containing perovskites.

Keywords : spark plasma sintering ; ceramics ; perovskite ; thermal conductivity

1. INTRODUCTION

Thermoelectric materials can contribute to limit global warming by directly transforming heat into electricity without any emissions (CO₂, other gases, radiations, ...), vibrations or moving parts [1]. Thermoelectric materials potential is evaluated by the thermoelectric figure of merit $ZT = S^2\sigma T/\kappa = PF T/\kappa$, where T is the absolute temperature, S the Seebeck coefficient, σ the electrical conductivity, κ the thermal conductivity and PF the power factor. However, the three parameters, S , σ and κ , are strongly interconnected through more fundamental physical parameters.

Therefore, trying to discover new high ZT thermoelectric materials is a very active research field [2-10] as well as trying to improve ZT values of known materials [11-18]. Gaultois et al. [19] have shown from element abundance and Herfindahl-Hirschman indices for production and reserve criteria that only three families of materials are suitable for mass production: highly conductive transition metal oxides, silicides with low bismuth content, and some half-Heusler compounds.

Oxides are considered as potential thermoelectric materials since 1997, when Terasaki et al. [20] reported a high power factor in Na_xCoO₂. Nowadays, the best reported values for n-type oxides are $ZT = 0.67$ at 773 K [21] in CaMnO₃-based perovskite materials, $ZT = 0.6$ at 1000 K [22] in SrTiO₃-based perovskite materials, and for p-type oxides the best ZT values are exhibited in Ca₃Co₄O₉-based materials ($ZT = 0.74$ at 800 K [23]).

However, one of the main issues of oxides compared to other thermoelectric materials is their relatively high thermal conductivity. Therefore, many routes to reduce their thermal

conductivity have been investigated, such as substitutions by heavier elements, nanostructuring, composites, porosity, microcracking, ... [24-35].

The $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ perovskite is a widely studied lead-free alternative to lead-zirconate-titanates piezoceramics since 2004 [41-45]. However, Delorme et al. [46] have reported promising thermoelectric properties in $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ perovskite sintered by spark plasma sintering (SPS) due to oxygen non-stoichiometry. The most interesting feature is that thermal conductivity is stable from 325 to 1000 K between 3.5 and 4 $\text{W m}^{-1} \text{K}^{-1}$ which is far lower than the values reported in the largely studied SrTiO_3 perovskite (circa 10 $\text{W m}^{-1} \text{K}^{-1}$ at room temperature) [47]. Several phenomena can contribute to such low values. For instance, A-site deficiency in SrTiO_3 perovskite was found to reduce thermal conductivity [47-49]. The volatility of alkali metals is well known and it is difficult to avoid when sintering $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ ceramics [45]. To reach thermal conductivities circa 4 $\text{W m}^{-1} \text{K}^{-1}$ in SrTiO_3 perovskite, it requires almost 20 % vacancies [49]. However, $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_{3-\delta}$ ceramics have shown $(\text{Na}+\text{K})/\text{Nb}$ ratios higher than 0.9 [45]. Moreover, the $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ composition is close to the morphotropic phase boundary that can lead to the formation of domains with A-site cationic heterogeneity [50] that could contribute to reduce thermal conductivity. Finally, ferroelectric domains have also been reported in $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ perovskite [51].

Therefore, in order to investigate the origin of the low thermal conductivity of $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ ceramics, dense KNbO_3 and NaNbO_3 ceramics, representing the end members of the solid solution, have been sintered by Spark Plasma Sintering and characterized. Indeed, it is well known that high density KNbO_3 and NaNbO_3 ceramics are difficult to sinter due to the volatility of the alkali metals at relatively low temperatures [52, 53].

2. MATERIALS AND METHODS

KNbO_3 and NaNbO_3 samples were synthesised from K_2CO_3 (Chempur, $\geq 99\%$ purity), Na_2CO_3 (Chempur, $\geq 99.9\%$ purity) and Nb_2O_5 (Chempur, $\geq 99.9\%$ purity) precursors. The precursors were heated at 200°C for 4 h and then stoichiometric amounts of the precursors were mixed for 5 min at 400 rpm in an agate planetary ball mill (Retsch PM 100). The powders were then heated at 830°C for 12 h at a rate of $2^\circ\text{C}/\text{min}$, in an alumina crucible and slowly cooled down to room temperature.

Sintering was performed by Spark Plasma Sintering (Syntex 515 S of the SPS Platform Ile-de-France). The synthesised powders were placed in a 15 mm diameter graphite die. A graphite foil was placed between the samples and the different parts of the die. Experiments were performed in argon atmosphere. NaNbO_3 sample was first sintered using conditions close to the ones reported by Wada et al. [52]: 1200°C and 50 MPa. However, the experiment was stopped circa 1045°C as a liquid phase appeared. Therefore, both NaNbO_3 and KNbO_3 ceramics were sintered using the cycle developed for $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_{3-\delta}$ ceramics [46]: a pressure of 50 MPa was applied whereas the temperature was raised at $100^\circ\text{C}/\text{min}$ up to 920°C for 5 minutes. Then the samples were cooled down to room temperature at $100^\circ\text{C}/\text{min}$.

Graphite foils used during the SPS process were removed by polishing. The pellets were cut into $2.8 \times 2.8 \times 13$ and $6 \times 6 \times 1$ mm parallelepipeds with a diamond wire saw for electrical and thermal properties measurements, respectively.

Weight and dimensions of the samples used for thermoelectric characterization were used to calculate apparent density of the samples.

Resistivity and Seebeck coefficient were measured simultaneously in a ZEM III equipment (ULVAC Technologies) from 1000 to 325 K. The laser flash diffusivity technique (Netzsch LFA 457) from 373 to 1000 K under vacuum after graphite coating was used to measure thermal diffusivity. Each sample was measured three times at each temperature. The specific heat capacity (c_p) was measured by differential scanning calorimetry (Netzsch STA 449 F3 Jupiter) from 330 to 1000 K, with a heating rate of 20 K.min⁻¹ in platinum crucibles and in nitrogen atmosphere.

Powder X-ray diffraction (XRD) patterns have been recorded at room temperature on a BRUKER D8 Advance $\theta/2\theta$ diffractometer (Cu-K α radiation, at 40 kV and 40 mA) with a Linxeye detector from 20 to 80°(2 θ) with a step of 0.02° and a counting time of 0.5 s per step.

Samples were first gold coated and then observed by scanning electron microscopy (SEM - Tescan Mira 3 field emission microscope coupled with an Energy Dispersive Spectrometer EDS Oxford INCA X-Act).

3. RESULTS AND DISCUSSION

After sintering, the two pellets are greyish, NaNbO₃ being darker than KNbO₃.

Figure 1 exhibits the XRD patterns measured on the ceramic pellets after sintering by SPS. All the peaks can be attributed to the KNbO_3 (PDF 01-071-0946) and NaNbO_3 (PDF 00-033-1270) compounds.

The relative densities calculated from the theoretical value given by PDF cards are high and similar, 96 and 97 % for KNbO_3 and NaNbO_3 , respectively. The value for NaNbO_3 is consistent with the recent results reported by Gouget et al. [54]: indeed, they achieved densities of at least 94 % for samples sintered by SPS at 900°C and 100 MPa during 5 minutes.

Temperature dependence of the thermal conductivity of the $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$, KNbO_3 and NaNbO_3 ceramics sintered by SPS, from 373 to 1000 K is shown in Figure 2. As already reported [46], thermal conductivity of $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ ceramic is stable ($3.5\text{-}4 \text{ W m}^{-1} \text{ K}^{-1}$) over the whole temperature range and lower than the thermal conductivity of conventionally studied SrTiO_3 perovskite [47]. NaNbO_3 ceramic presents a similar behaviour, i.e. stable over the whole temperature range, but a lower thermal conductivity value circa $2.6 \text{ W m}^{-1} \text{ K}^{-1}$. KNbO_3 ceramic presents a different behaviour, similar to SrTiO_3 one. The highest thermal conductivity is observed around room temperature and decreases until it reaches a plateau. The value at 373 K is below $2.5 \text{ W m}^{-1} \text{ K}^{-1}$ and the plateau value ($1.2 \text{ W m}^{-1} \text{ K}^{-1}$) is reached at 673 K. As far as the authors know, this is the lowest thermal conductivity reported for an oxide presenting a perovskite structure. Moreover, this value is lower than the thermal conductivity of oxides used as thermal barriers, like yttrium-stabilized zirconia or pyrochlores [55].

The three niobium-containing perovskites exhibit low thermal conductivity values. Therefore, it excludes the possibility that the origin of low thermal conductivity values in $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ ceramics could be related to composition heterogeneities due to the vicinity of the morphotropic phase boundary. Indeed, pure poles as KNbO_3 and NaNbO_3 cannot present such domains.

An influence of the different crystallographic structures has been ruled out by Delorme et al. [46]. Indeed, in $\text{K}_{0.5}\text{Na}_{0.5}\text{NbO}_3$, thermal conductivity remains similar whereas the perovskite is orthorhombic, tetragonal and cubic at room temperature, 450 K and 700 K, respectively. Similarly, no significant thermal conductivity change related to phase transitions can be observed in NaNbO_3 and KNbO_3 .

Another possibility could be nanosized grains [27, 35, 37]. However, SEM observations (figure 3) show that both KNbO_3 and NaNbO_3 ceramics exhibit micrometer-sized grains. According to Bah et al. [45], $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ ceramics sintered by SPS exhibits micrometer-sized grains too. Therefore, the low thermal conductivities of niobium-containing perovskite are not related to nanograins. However, EDS measurements show that $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$, KNbO_3 and NaNbO_3 ceramics present a common feature : they all present a cation deficiency on the A-site of the perovskite. A decrease in the thermal conductivity due to A-site deficiency has already been reported for SrTiO_3 perovskite [47-49]. However, the thermal conductivity values obtained in niobium-containing perovskites are lower than those obtained in SrTiO_3 even with higher deficiency. Indeed, the $(\text{Na}+\text{K})/\text{Nb}$ ratio is circa 0.97, 0.91 and 0.96 for $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$, KNbO_3 and NaNbO_3 , respectively. It appears that the lower the $(\text{Na}+\text{K})/\text{Nb}$ ratio, the lower the thermal conductivity. Therefore, one can conclude that the A-

deficiency is responsible for the low thermal conductivity measured in niobium-containing perovskites.

Such low thermal conductivities make KNbO_3 and NaNbO_3 ceramics potentially attractive for thermal barrier applications. However, for such application, an absence of phase transition in the targeted temperature range and chemical inertness is requested [56-58].

The thermal diffusivity and c_p values measured circa room temperature on the SPS-sintered KNbO_3 ceramics are consistent with the values reported for single crystals by Hofmeister [59]. Figure 4 exhibits the temperature dependence of apparent specific heat capacity values of KNbO_3 and NaNbO_3 ceramics from 330 to 1000 K. For KNbO_3 , two peaks can be observed at circa 486 and 693 K, corresponding to orthorhombic-tetragonal and tetragonal-cubic phase transitions, respectively [59, 60]. Temperature-resolved XRD studies should allow determining whether these phase transitions are associated with the volume changes that could be detrimental for thermal barrier application.

NaNbO_3 cannot probably be used for thermal barrier application as it is well known to present many phase transitions [54, 61-63]. Figure 4 shows that for NaNbO_3 , at least six peaks can be observed at 352 (with a shoulder after the peak), 554 (with a shoulder prior the peak), 612, 730, 790, 850 with a shoulder around 920 K, respectively. However, discussing the correlation between peaks and phase transitions in NaNbO_3 is far beyond this communication's aim.

Finally, thermoelectric properties have been measured. Indeed, according to the thermoelectric figure of merit $ZT = S^2\sigma T/\kappa$, ceramics with low thermal conductivity can

present promising thermoelectric properties as reported for $(K_{0.5}Na_{0.5})NbO_{3-\delta}$ ceramics [46]. Theoretical study [64] has shown that $NaNbO_3$ and in a larger extent $KNbO_3$ could present high thermoelectric properties, if appropriately doped (i.e. controlled oxygen stoichiometry and divalent substitution on the of alkali metal site). Unfortunately, it was impossible to measure the electrical conductivity and Seebeck coefficient of $KNbO_3$ ceramic in ZEM3. Indeed, the 2.8 x 2.8 x 13 mm bar broke when clamped between the ZEM3 electrodes, suggesting that $KNbO_3$ is a fragile material. For $NaNbO_3$ ceramic, the properties were only measurable at 1000 K. The Seebeck coefficient value is $-688 \mu V K^{-1}$, indicating a n-type material. This value is similar to the one reported for $(K_{0.5}Na_{0.5})NbO_{3-\delta}$ ceramics [46]. Unfortunately, the electrical conductivity is limited at $16 S m^{-1}$, which is about one fifth of the value reported for $(K_{0.5}Na_{0.5})NbO_{3-\delta}$ ceramics [46]. It will be necessary to optimize the power factor by doping and control of the oxygen stoichiometry to estimate the real potential of niobium-containing perovskites as thermoelectric materials.

4. CONCLUSION

Dense $NaNbO_3$ and $KNbO_3$ ceramics were obtained by spark plasma sintering. After sintering, the two pellets are greyish, indicating an oxygen deficiency as $(K_{0.5}Na_{0.5})NbO_{3-\delta}$ when sintered under the similar conditions. The grain size was in the 1 to 10 μm range. Both $NaNbO_3$ and $KNbO_3$ ceramics present low thermal conductivity: circa $2.6 W m^{-1} K^{-1}$ and stable from 373 to 1000 K for $NaNbO_3$ and from 2.5 to $1.2 W m^{-1} K^{-1}$ since 673 K for $KNbO_3$. This value is the lowest thermal conductivity reported for an oxide presenting a perovskite structure and is lower than the thermal conductivity of oxides used as thermal barriers, like yttrium-stabilized zirconia or pyrochlores. The origin of such low thermal conductivities is

indicated to be related with cation deficiency on the A-site of the perovskite. Indeed, the (Na+K)/Nb ratio is circa 0.97, 0.91 and 0.96 for $(K_{0.5}Na_{0.5})NbO_3$, $KNbO_3$ and $NaNbO_3$, respectively. Applications in the field of thermal barriers or as thermoelectric materials could be expected. However, one would require the absence of phase transitions with important volume changes and the other, optimizing the electrical properties by controlling the charge carrier concentration by doping or controlled oxygen deficiency, respectively.

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FIGURE CAPTION

Figure 1: XRD patterns of the a) KNbO_3 ceramic and b) NaNbO_3 ceramic.

Figure 2: Temperature dependence of the thermal conductivity of $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ (○), NaNbO_3 (●) and KNbO_3 (●) ceramics.

Figure 3: SEM images of a) NaNbO_3 and b) KNbO_3 ceramics.

Figure 4: Temperature dependence of apparent specific heat capacity of a) KNbO_3 and b) NaNbO_3 ceramics.

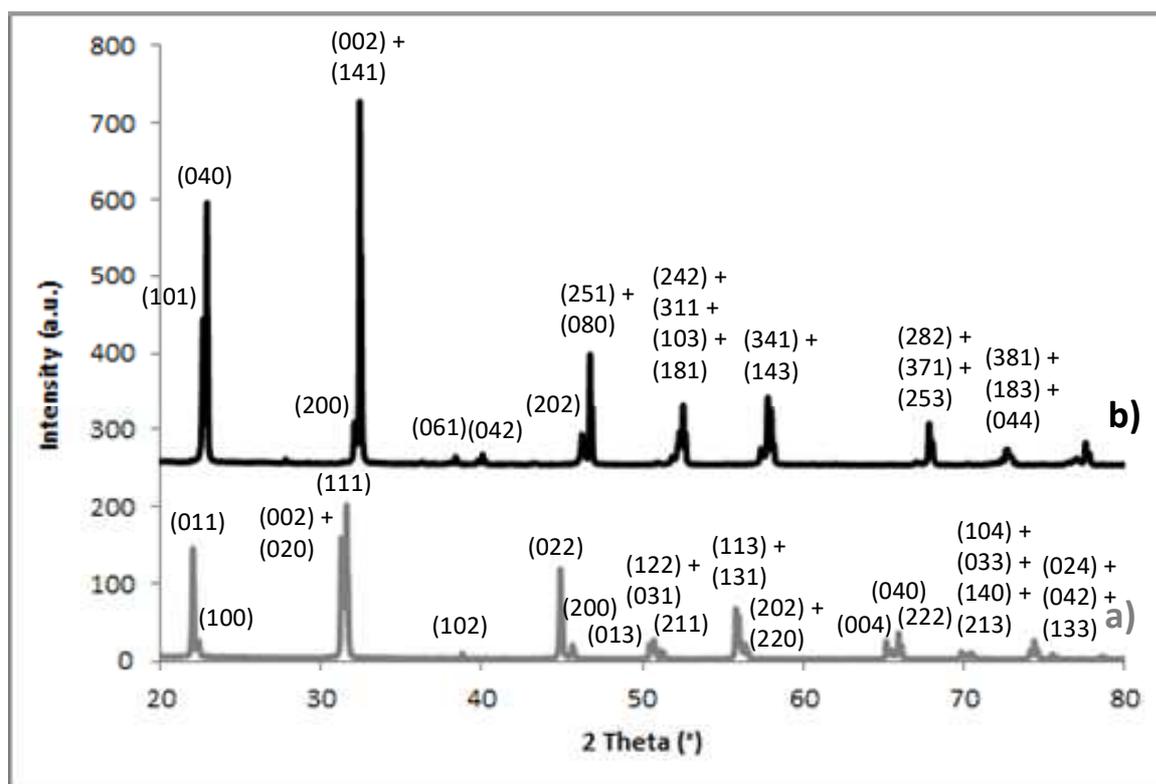


Figure 1

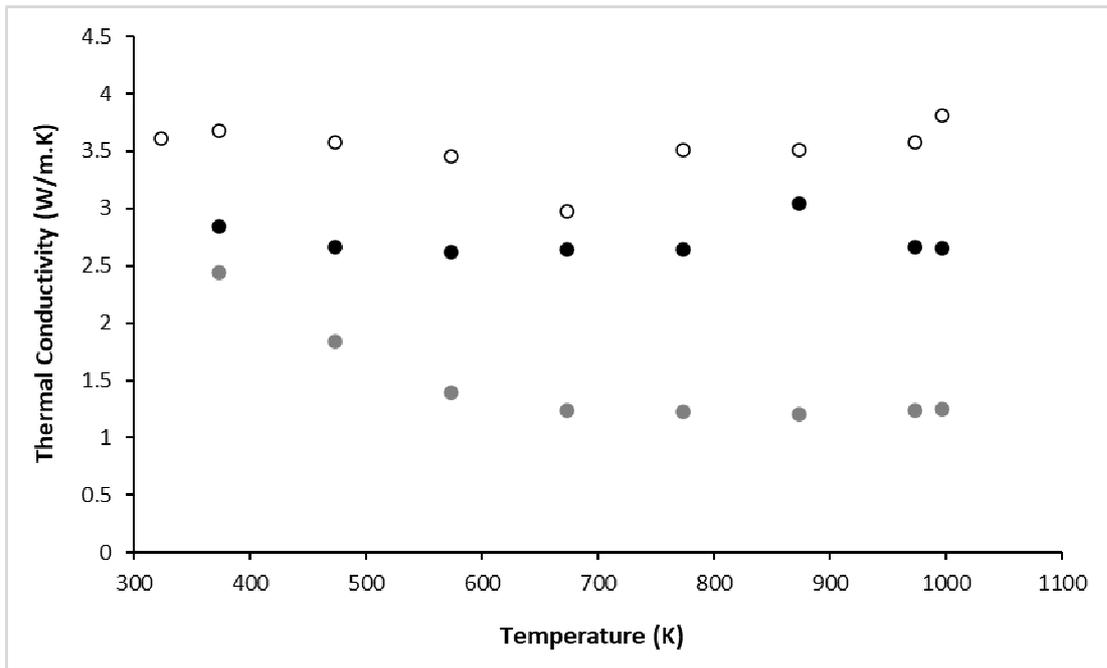
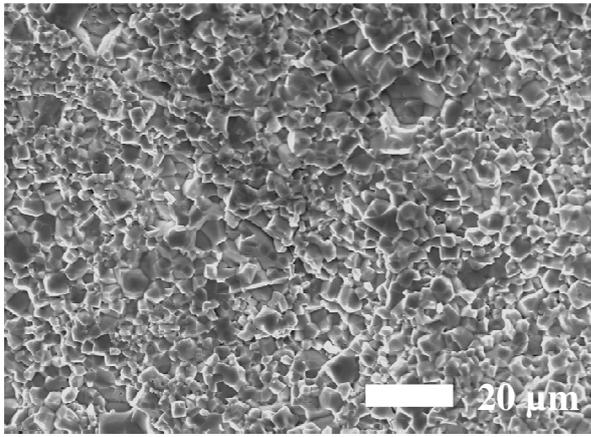
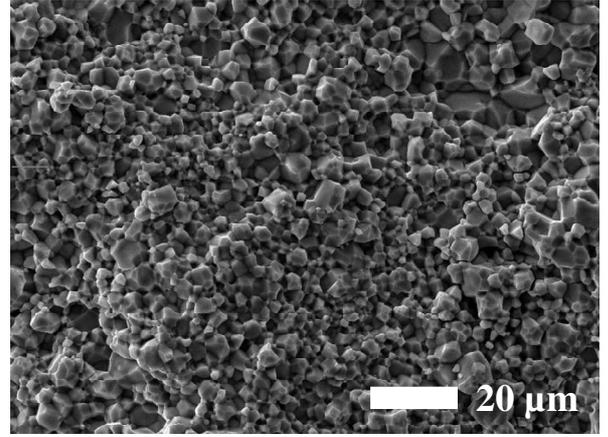


Figure 2



a)



b)

Figure 3

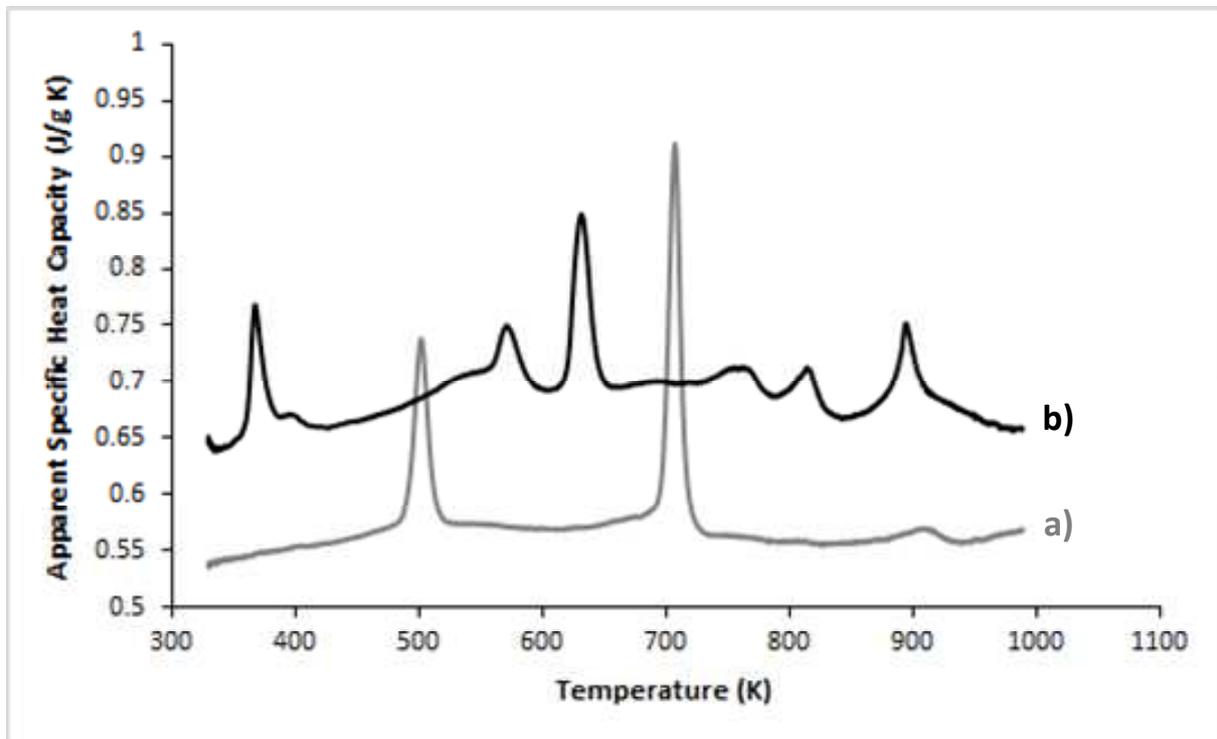


Figure 4