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A swift technique to hydrophobize graphene and increase its mechanical stability and charge carrier density

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Despite the improvement of the quality of CVD grown single-layer graphene on copper substrates, transferring the twodimensional layer without introducing any unintentional defects still poses a challenge. While many approaches focus on optimizing the transfer itself or on necessary post-transfer cleaning steps, we have focused on developing a pre-treatment of the monolayer graphene on copper to improve the quality and reproducibility of the transfer process. By pressing an ethylene-vinyl acetate copolymer foil onto the monolayer graphene on copper using a commercially available vacuum bag sealer graphene is stabilized by the attachment of functional carbon groups. As a result, we are able to transfer graphene without the need of any supporting layer in an all-H₂O wet-chemical transfer step. Despite the general belief that the crumbling of graphene without a support layer in a H₂O environment is caused due to differences in surface energy, we will show that this assumption is false and that this behavior is caused rather by the polar interactions between graphene and water. Suppressing these interactions protects graphene from ripping and results in extremely clean, highly crystalline graphene with a coverage close to 100%.

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INTRODUCTION

ARTICLE

Despite intensive research in graphene since its discovery in 2004, the interest in the two-dimensional (2D) material is still growing^{1–5}. Owing to its exceptional electrical and mechanical properties, its applicability as a membrane or pressure sensor, graphene remains a highly investigated material⁶⁻¹⁵. While initial experiments were mainly performed with exfoliated graphene flakes, the drawbacks of this approach such as low reproducibility and small flake sizes have shifted the focus towards complementary synthesis procedures. In particular, the precondition for every graphene-based industrial application is the feasibility of up-scaling. Driven by this aim, researchers have started focusing on the growth of graphene (Gr) via chemical vapor deposition (CVD). Even though efforts are made towards the direct growth of graphene onto any desired material, copper (Cu) still remains the most used material for CVD growth of graphene¹⁶⁻²¹. However, most applications require the transfer of the 2D layer onto another substrate—a process still posing a challenge. While nearly all transfer techniques discussed in literature focus on optimizing the actual transfer step, we will present a pre-treatment technique of the Gr/Cu, which allows us to perform a polymer-free, wet-chemical transfer of the graphene in an $all-H_2O$ environment²²⁻²⁷. Inspired by the work on reduced graphene oxide (rGO) membranes aiming for homogeneous evenly spaced rGO laminates, we apply a fast and straightforward approach to decorate the graphene with stabilizing functional carbon groups, which strongly increase the stability of our graphene sheet during transfer hence making all polymer-based sacrificial layer redundant.

RESULTS

Surface modifications of graphene

The common transfer method of CVD grown graphene from a Cu surface onto another substrate involves a polymer supporting layer on top of the graphene, e.g., poly(methyl methacrylate) (PMMA), polyvinyl alcohol (PVA), or paraffin acting as a stabilizer and preventing graphene from ripping during the transfer^{28–31}. Dissolving the polymer after the transfer however frequently causes many problems mainly due to polymer residues on the graphene surface, which drastically alter and degrade graphene's properties^{32–34}. So far, every reported transfer or cleaning technique of CVD graphene in order to avoid or remove the polymer support afterwards involves additional chemicals, long-time heating processes or is restricted to certain target materials^{30,35,36}.

In contrast, our pre-treatment of the Gr/Cu involves a flattening step using a commercially available vacuum bag sealing machine with ethylene-vinyl acetate copolymer (EVAC) as the bag material, see Fig. 1 (Supplementary Fig. 1 gives additional characterization information on the bag material). Having flattened the complete Gr/Cu sample, we can place the Gr/Cu on an ammonium persulfate (APS) solution. After etching off the Cu and gradually diluting the APS solution with H₂O, a target substrate can be used to scoop out the graphene sheet. Note that the final transfer is performed in a pure H₂O environment where no supporting layer for stabilization is necessary once the flattening step had been applied. The effect of the flattening already becomes visible when looking at the non-supported graphene layer floating on the APS etching solution, shown in Fig. 2a. While the flattened graphene maintains its rectangular form determined by the shape of the initial Gr/Cu wafer, the non-treated graphene crumbles and rips. The same results are obtained once the graphene sheets have



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Fig. 2 Optical images of regular and pre-treated graphene during and after transfer. a Flattened and regular graphene floating on an APS etching solution. Scale bar is 1 cm. b, c Optical microscopy images of non-flattened and flattened graphene transferred onto Si/SiO₂ substrates. Scale bars are 40 μ m for main images and 500 μ m for insets, respectively.

been transferred, see Fig. 2b for regular graphene and Fig. 2c for flattened graphene, respectively. The latter one shows a perfectly homogeneous coverage over the whole sample. The non-processed graphene, however, not only displays tens of μm^2 -sized uncovered regions, but even the covered parts show poor smoothness and countless wrinkles.

In order to evaluate the success of the transfer method presented here in terms of quality and coverage, we will compare the pre-flattened graphene with conventionally transferred graphene supported by a PMMA layer (in the following referred to as PMMA graphene) after transfer onto a SiO₂ substrate. For this, we have performed Raman mappings. By plotting the intensity ratio of graphene's Raman active defect(D)-mode and graphite(G)-mode, we can visualize the density of defects in graphene. Raman measurements indeed confirm an extremely low-defect density with an average A_D/A_G intensity ratio of ~0.04 for the flattened graphene compared to an intensity ratio of ~0.2 for the PMMA-assisted graphene transfer as shown in Fig. 3a, b (note that neither of the samples have undergone any additional ethanol rinsing, heat treatment or similar). Supplementary Fig. 2 presents representative Raman spectra of graphene for both transfer techniques. Aside from a highly crystalline graphene layer, we observe a considerably high charge-carrier density in graphene induced by charge transfer as can be derived from the peak



Fig. 3 Raman spectroscopy maping of graphene transferred with and without PMMA. Intensity ratios of D- and G-mode of a PMMAtransferred and b flattened graphene. Raman shift of graphene's Gmode is presented in c and d for PMMA-transferred and flattened graphene, respectively. Neither of the samples had been treated by any means after the transfer. After scooping graphene out of the H₂O with a SiO₂/Si wafer, the samples were left to dry under ambient conditions. Scale bars for **a**-**d** are 500 µm.

position of the G-mode in the Raman mappings, see Fig. 3c, d for PMMA-transferred graphene and flattened graphene, respectively. Even though PMMA is known as a strong p-dopant for graphene, the flattened graphene displays an even higher level of doping, most likely originating from the two oxygen atoms present in the side group (acetate) which will promote a charge transfer due to oxygen's strong electronegativity and presumably facilitated by the intimate contact at the interface between the rubbery EVAC and graphene and the weaker bond (C–O) between polymer main chain and side group (acetate), compared to glassy PMMA with a C–C bond to the side group (methyl ester); see also the mass spectroscopy results of surface analysis below. Comparing the Raman shift of the G-mode (and I_{2D}/I_{G} intensity ratio, see Supplementary Fig. 3) of the flattened graphene with the work



Fig. 4 AFM images of graphene transferred with and without PMMA. AFM images of transferred CVD graphene onto SiO₂ substrates with **a**, **c** and without **b**, **d** PMMA support. Graphene supported with PMMA during the transfer shows high density of nm-sized polymer residues after dissolving the PMMA layer, whereas the flattened graphene is nearly free of any contaminations. Note the different scale bars in **c** and **d**, underlining the huge improvement in cleanliness. The bright spots in **b** and **d** are no polymer residues from the flattening foil but overlapping graphene parts or wrinkles resulting from the drying process after scooping out graphene with a target wafer. Scale bar is 5 μ m for **a**, **b**, 1 μ m for **c**, and 2.5 μ m for **d**.

of Bruna et al.³⁷, we can conclude that both transferred samples exhibit a p-doped behavior with a charge carrier concentration of $\sim 5 \times 10^{12}$ cm⁻² for the PMMA-transferred and 1.5×10^{13} cm⁻² for the flattened graphene³⁷. The combination of an extremely low-defect density and a high level of charge carriers in graphene is expected to be beneficial for a high charge-carrier mobility. The flattening step thus proves to be an effective and gentle way for doping graphene.

In addition to an extremely low-defect density, another advantage of a polymer-free transfer is the avoidance of persistent polymer residues on the graphene surface after dissolving the support layer. Numerous cleaning procedures of polymer contaminated graphene have been presented in literature. However, despite time-consuming cleaning steps, polymer residues are almost impossible to remove completely. This in turn causes a downgraded electrical performance of graphene, an uncontrollable and inhomogeneous doping level or makes it simply useless for atomic force microscopy (AFM), and in particular transmission electron microscopy (TEM) measurements, which typically demand a high degree of cleanliness^{32,34,35,38,39}. Figure 4 presents AFM measurements of graphene transferred with (a, c) and without (b, d) PMMA support. While Fig. 4a, c display numerous nanometer sized PMMA leftovers, we obtain large areas of perfectly clean graphene surface for flattened graphene in Fig. 4b, d.

Let us now address the reason for the enhanced mechanical stability and improved quality of the graphene once it has been modified by our approach. Arguing that the copper itself has been



Fig. 5 SEM images of regular and flattened Gr/Cu as well as analysis of transfer success rate and Gr/Cu-water contact angle as a function of flattening time. SEM images of a regular and b flattened Gr/Cu. Scale bars are 250 µm for main images and 100 µm for insets. c Dependency of the relative success of transfer and contact angle on flattening time of Gr/Cu. Error bars represent standard deviations.

flattened on a microscopic scale, hence providing a more uniform and smoother surface for the graphene is highly unlikely. SEM images shown in Fig. 5a, b of regular and flattened CVD graphene on Cu, respectively, reveal no observable differences in terms of the smoothness of the Cu substrate (aside from a reduced dirt particle density for the flattened Gr/Cu). It is much more plausible that the very surface of graphene itself has been altered by our approach. In order to draw conclusions about the flattening step, the success rate in transfer, and the flattening time, we studied how graphene behaves during the transfer when varying the flattening time, the result of which is presented in Fig. 5c. We found that there is a clear dependency of the transfer success rate (corresponding to graphene not ripping/crumbling) and the flattening time. While we were practically never able to successfully transfer non-flattened graphene, we obtained a success rate of 100% after just one day of flattening. Relating this observation with the change of the contact angle of a water droplet on the Gr/Cu surface, also shown in Fig. 5c, we can draw two important conclusions: (i) both the transfer success rate and the contact angle have their lowest values for non-treated Gr/Cu with values of 0 and 89.1°, respectively. After 1 day of flattening, the success rate and the contact angle have increased displaying values of 1 and 93.1°. (ii) Neither of the two values change when we further increase the flattening time indicating that the responsible mechanism during the flattening step has converged. Since a large contact angle between a water droplet and a surface typically indicates hydrophobic properties of the surface, we can conclude that the flattening increases the hydrophobicity of the graphene. A saturation of the contact angle most likely results from the fact that once the majority of graphene's surface has been decorated with adsorbates, additional molecules are less

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likely to attach to graphene as nearly all free adsorption sites have already been filled. Even if additional layers of adsorbates would remain on graphene's surface, the contact angle is not expected to change any more as it is predominantly governed by the layers in direct contact.

DISCUSSION

To further address this observation, we performed X-ray photoelectron spectroscopy (XPS) measurements to confirm the presence of additional adsorbates on graphene's surface. Owing to the surface sensitivity of XPS, the data we obtained can be correlated with surface modifications. Again, we have varied the flattening time from 0 s to 2 days as shown in Fig. 6a, b. The data reveals that initially almost all of the carbon present on the sample is sp²-hybridized. This is of no surprise since the electrons of pristine graphene form sp²-hybridized orbitals. With increasing flattening time, we observed a growing amount of sp³-hybridized as well as C-O bound carbon, which we explain by additional adventitious carbon from the EVAC-foil as a result of the flattening step. Supplementary Figs. 4 and 5 show additional XPS data of flattened Gr/Cu. To estimate the amount of carbon residues on graphene after flattening, we compared the carbon signal originating from graphene to the overall carbon intensity, as presented in Fig. 6d for EVAC and various other materials. Despite the direct contact to the EVAC-foil, graphene still contributes 48% to the total C signal after being in contact with the foil for two days, which is a similar value when using other polymer-based materials or aluminum. Interestingly, similarly processed Gr/Cu samples flattened with a polycarbonate (PC) foil sometimes also allow successful transfers comparable to the EVAC-flattened samples. Notably, the XPS spectra of EVAC- and PC-flattened Gr/ Cu are almost identical (Supplementary Fig. 6). Despite this, all other Gr/Cu samples flattened with, e.g., polyethylene terephthalate (PET), aluminum or simply old Gr/Cu sample not only show a



Fig. 6 XPS analysis of flattened graphene as well as evolution of sp²- and sp³- hybridized intensity ratio as a function of flattening time. XPS measurements of Gr/Cu samples that have been flattened before with various materials. **a**, **b** With increasing flattening time of the EVAC-foil additional carbon residues are deposited on graphene. **c** XPS spectrum of Gr/Cu after two days of flattening using a polyethylene terephthalate (PET) foil. **d** Intensity ratio of carbon signal originating from graphene compared to the total carbon signal for differently treated Gr/Cu samples as a function of time.

signal of hydrophilic adsorbates, e.g., COOH groups, on graphene as presented for PET-flattened Gr/Cu in Fig. 6c, but also displayed the same ripping/crumbling behavior during the transfer as nontreated Gr/Cu.

As a next step, we performed secondary ion-mass spectroscopy (ToF-SIMS) measurements to further understand the nature of the C-based material on graphene's surface after having used EVAC for the flattening step. Figure 7 presents the results from this analysis. We observed a significant difference between treated and non-treated Gr/Cu for the mass of 59. After irradiating the Gr/ Cu sample with Bi³⁺ ions and detecting the ejected material of the sample after ion impact, we observed negatively charged acetate aroups being emitted from the surface, hence contributing with a total mass-charge ratio of 59 to this peak. While the flattened Gr/ Cu sample shows a large signal at this particular mass compared to the signal in its close surrounding, the non-flattened sample shows no such striking feature. The presence of this peak at mass 59 for the flattened Gr/Cu sample can be linked directly to the flattening step, since the foil used for the flattening of the Gr/Cu shows the exact same signature, see Fig. 7b. Although, it is worth noting that during the flattening process no continuous polymer film of the foil is peeled off and attached to the graphene as we also observed EVAC-foil characteristic groups not being present on the flattened Gr/Cu. It is rather the presence of additional fragments of the EVAC foil including the characteristic acetate group which stick to graphene (Supplementary Fig. 7). With this observation, we can roughly estimate the coverage of these adsorbates. Since we could not observe any fingerprint of the acetate in the XPS measurements (e.g. a signal from C = O, which is present in the acetate) after using the EVAC-foil, but only witnessed their presence in the far more sensitive (ppb) ToF-SIMS measurements, we can deduce the density of the acetate groups to lie below 0.2 monolayer which corresponds to the sensitivity of the XPS.

A possible explanation for the increase of the mechanical stability after the EVAC-flattening step is based on lowering the difference in surface energy of graphene and the etching solution. If the difference in surface energy is small enough graphene would retain its shape allowing a successful transfer. In case of a large difference in surface energies between graphene and the etching solution, the system is expected to minimize its energy by reducing the surface area of graphene causing it to crumble. To test our hypothesis, we probed the contact angle of calibrated liquids with flattened and regular CVD graphene on copper. Generally, the interactions between a liquid and a solid depend on the chemical structure of the adsorbate and adsorbent and can be divided into polar and dispersive interactions. Polar interactions arise due to permanent or dipole-induced interactions, hence, strongly depend on the chemical structure of the investigated materials. Dispersive interactions on the contrary are caused by fluctuating electron densities and therefore are always present regardless of the chemical nature^{40,41}. Both the polar σ^{p} and dispersive σ^{d} interactions contribute to the total surface energy σ of a liquid (subscript L) or solid (subscript S) and can be correlated according to the Owens-Wendt equation as:

$$\frac{\sigma_{\rm L}(\cos\theta + 1)}{2\sqrt{\sigma_{\rm L}^{\rm d}}} = \frac{\sqrt{\sigma_{\rm S}^{\rm p}}\sqrt{\sigma_{\rm L}^{\rm p}}}{\sqrt{\sigma_{\rm L}^{\rm d}}} + \sqrt{\sigma_{\rm S}^{\rm d}}$$
(1)

By probing the contact angles θ of well characterized test liquids with graphene, we are able to observe variations in both the polar and dispersive interactions. As shown in Fig. 8, the flattening step surprisingly does not increase but decreases the surface energy of the Gr/Cu surface from 40.6 mJ cm⁻² to 37.8 mJ cm⁻² for PET-flattened and 34.5 mJ cm⁻² for EVAC-flattened Gr/Cu, respectively, meaning that the difference in surface energy with respect to water ($\sigma_{water} \sim 72.8 \text{ mJ cm}^{-2}$) even increases. We





Fig. 7 ToF-SIMS analysis and surface modifications of regular and flattened Gr/Cu. ToF-SIMS measurement of a 1-day-flattened and nonflattened Gr/Cu and b bare EVAC-flattening foil. The data shows the negatively charged ion spectrum of the ToF-SIMS measurements.





can therefore rule out that it is the difference in surface tension, which causes the graphene to rip as often stated in literature^{27,42,43}. Rather, we believe the reason for the increased mechanical stability during transfer to be due to the suppression of the polar interactions with the water molecules in the etching solution. While σ^d decreases by only 8% for PET-flattened and 14% for EVAC-flattened Gr/Cu, respectively, compared to non-treated samples, σ^p is reduced by 29% after PET- and 76% after EVAC-foil treatment. Considering that the polar part constitutes almost 2/3 of water's total surface energy, the flattening step seems to suppress the polar-polar interactions of the floating graphene sheet on the etching solution, hence preventing the graphene from tearing apart⁴⁴. Supplementary Fig. 8 presents individual measurements of the contact angle for water, diiodmethane, and glycerol as test liquids.

ethylene-vinyl acetate copolymer foil against the graphene (done with a regular commercially available vacuum bag sealing machine used for groceries, vegetables, etc.). The foil remains being pressed against the graphene for a minimum of 24 h. Afterwards, the Cu of the Gr/Cu wafer is etched off in an ammonium persulfate solution (7 g dissolved in 200 ml Dl H₂O). The etching solution is diluted by Dl water and the graphene can be scooped out with the target material.

Flattening of Gr/Cu and sample preparation

polar interaction.

METHODS

Raman spectroscopy/AFM/XPS

Raman spectroscopy measurements have been performed using a Renishaw InVia Raman spectroscope with a 532 nm laser. In order to avoid heating effects, the laser power was kept below 100 μ W.

In conclusion, we have developed a fast, inexpensive, and scalable way to increase the mechanical stability of graphene by

flattening the Gr/Cu prior to the transfer using a regular EVAC-foil

and a vacuum bag sealing machine. In addition to an extremely

low-defect density and a considerably cleaner graphene surface due to the absence of any polymer support during the transfer,

our technique may as well be used for intentional doping of

graphene, as well as for increasing its hydrophobicity. We attribute

the improvement of graphene's properties in terms of mechanical stability during wet-chemical transfer to the suppression of polar-

Applying the flattening step of the Gr/Cu wafer using the ethylene-vinyl

acetate copolymer foil is crucial for a successful polymer-free transfer. First,

the Gr/Cu wafer (single-layer Gr/Cu from Graphenea, Spain) is placed onto a solid and smooth plate and covered by the ethylene-vinyl copolymer foil.

The covered wafer including the plate are then placed into a regular plastic

bag used for vacuum sealing. The vacuum sealing process presses the

AFM measurements were performed under ambient conditions with a Bruker Dimension FastScan microscope using the PeakForce Tapping mode.

XPS measurements were performed using the VersaProbe II microscope (UlvacPhi) with a monochromatic AI K-alpha source under a 45° angle with respect to the samples surface.

Contact-angle measurements

Contact angles were measured using a Contact-Angle System OCA 15EC (DataPhysics Instruments GmbH, Filderstadt, Germany). First, a 2 µl droplet was formed using an automatic dispenser unit. The sessile droplet was then formed by slowly approaching the substrate to the needle and removing it again after the droplet had contacted the samples surface. All test liquid measurements were carried out under ambient conditions.

ToF-SIMS measurements

ToF-SIMS data were obtained using an IONTOF ToF-SIMS 5 with a LMIG Bi^{3+} source operated at 30 kV. To avoid charging effects, we measured with a constantly running electron flood gun.

DATA AVAILABILITY

The datasets generated during and/or analyzed during the current study are available from the corresponding author on reasonable request. All data generated or analyzed during this study are included in this published article (and its Supplementary Information).

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AUTHOR CONTRIBUTIONS

E.P., T.F., A.H., R.J., H.L., and A.B. contributed AFM, SEM. and FT-IR measurements to this work. ToF-SIMS measurements were performed and interpreted by T.H., M.H., L.S., and L.B. Contact-angle measurements were done and interpreted by J.S., A.W., and M. U. XPS measurements were performed and interpreted by U.H. L.M. and M.S. performed Raman measurements, developed the idea of this work, and wrote the manuscript.

COMPETING INTERESTS

The authors declare no competing interests.

ADDITIONAL INFORMATION

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