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A Core-shell synthesis of $\text{CaCu}_3\text{Ti}_4\text{O}_{12}$ (CCTO) ceramics showing colossal permittivity and low electric losses for application in capacitors

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Abstract

A core-shell synthesis is applied to $\text{CaCu}_3\text{Ti}_4\text{O}_{12}$, a material that shows colossal permittivity. The objective was to test several bulk permittivity of the shell material in order to reach a large capacity of the grain boundaries after sintering. The permittivity is improved with certain shells while the bulk resistivity reaches levels approaching that of commercial grain boundary barrier layer (GBBL) ceramic capacitors. The highest permittivity is confirmed to be related to the highest capacity of grain boundaries. The bulk resistivity is related to that of grain boundaries. If one attaches the more important weight to a high bulk resistivity without need of permittivity larger than 15,000, as in commercial GBBL ceramic capacitors, several samples appear convenient. On the other hand, much higher permittivity can be reached like in CCTO with a shell of TiO_2 but at the expense of dielectric losses, possibly due to oxygen departure from stoichiometry. Thermal post-treatment under various controlled atmosphere have been applied to reduce dielectric losses.

Keywords: colossal permittivity, core-shell, Internal barrier layer capacitance, CCTO, ceramic capacitor

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1. Introduction

The demand for electric vehicles and other technological applications implies an enhanced demand for ceramic capacitors. In addition to capacitors already on the market, promising

trends has supported the research on ceramics showing giant or colossal permittivity [1]. One extensively studies candidate is $\text{CaCu}_3\text{Ti}_4\text{O}_{12}$ [2-10]. Since pioneer works, the search on keywords ($\text{CaCu}_3\text{Ti}_4\text{O}_{12}$ OR CCTO) in the Web of Science returns more than 1700 papers published in peer-reviewed literature (Figure 1). The permittivity of studied samples currently ranges from 10^4 to 10^5 , what constitutes a successful achievement. However, the dielectric losses are generally larger than 2.5 %, which is considered as the upper threshold for commercial capacitors.

The origin of the colossal permittivity has been much debated in the literature. Most recent studies tend to arrive to a consensus that the properties have their origin in the *microstructure* of the ceramics itself. Like in Grain Boundary Barrier Layer (GBBL) similar theory [1], semiconducting grains would play the role of electrodes of the capacitor while grain boundaries carry the permittivity of the capacitor [11]. The system would then consist of as many capacitors in series as the number of grains that pave a line, or a wall of bricks, along the thickness of the sample. Provided that semiconductor grains are conducting enough, the permittivity of the sample may be approximated by [1, 12, 13]

$$\varepsilon = \varepsilon_{gb} A/t \quad (1)$$

ε_{gb} is the permittivity of the *grain boundary*, A is the size of the grain and t is the thickness of the grain boundary. If this Internal Barrier Layer Capacitance (IBLC) model [5] is applicable, the research, therefore, has to be focused not only on grains which has already been extensively studied in the literature, but more importantly on grain boundaries which, by contrast, have been somewhat less studied. Provided they are conducting enough, grains indeed do not play any role in Eq. (1) other than their size A .

A comparison of an undoped CCTO sample sintered 24 hours at 1050°C with a commercial GBBL capacitor has shown that the permittivity of the CCTO sample is currently 4 times higher (Table 1). Electric losses, however, measured via $\tan(\delta) = 0.05$ at 1 kHz are still a bit too high. As a result, the sample resistivity of $1.3 \cdot 10^7$ should be increased for industrial applications in terms of ceramic capacitors. The microscopic reason is the following. The capacitance C_{gb} of the grain boundary reaches $4.5 \cdot 10^{-7} \text{ F.cm}^{-1}$ compared to only $10^{-10} \text{ F.cm}^{-1}$ for the commercial GBBL capacitor. This explains the larger permittivity of CCTO via Eq. (1) rewritten

$$\varepsilon \sim C_{gb} \quad (2)$$

since $C_{gb} \sim \epsilon_{gb}/t$. Conversely, the resistivity R_{gb} of the grain boundary of the GBBL commercial capacitor reaches $10^{10} \Omega\cdot\text{cm}$ whereas that of CCTO does not exceed $8.5 \cdot 10^6 \Omega\cdot\text{cm}$, focusing on the improvement which is needed.

Interesting results in terms of performance of grain boundaries and, therefore, in terms of both high permittivity and high resistivity, have been found when the grain boundary was TiO_2 of crystal structure anatase, as probed by Raman scattering [14]. Anatase indeed is a good insulator. The mechanism by which such grain boundaries were formed during the sintering process, however, is unclear and not yet controlled.

How to control the grain boundaries of CCTO to enhance their resistivity? One way which has been little exploited about CCTO up to now is the core-shell approach. The grains of CCTO are embedded in a shell of an insulating ceramic and then sintered with the hypothesis that the chosen shell will become the grain boundary. Several shell materials and several core-shell processes have been experimented in this study. The purpose is to check which one gives the highest permittivity associated with the highest resistivity.

2. Experimental

The CCTO grains have been synthesized by mixing stoichiometric amounts of CaCO_3 , CuO and TiO_2 powders via ball-milling media in ethanol during 24 h. The resulted mixing has to be calcined at 950°C for 24 h. The average size of CCTO particles can be evaluated by a Malvern zetasizer using dynamic light scattering. Typical value is about one micrometer. For comparison, the CCTO powder was also functionalized by PVP or by PEG. To functionalize CCTO, the powder was dispersed in ethanol and then 10 %wt of PVP or PEG was added and mixed during 24h. Using an ultrasonic bath, the synthesis of core-shell noted CCTO@ Al_2O_3 [15] was promoted by sol-gel reaction. The amount of aluminum isopropoxide precursor solution (0.15 g of aluminum isopropoxide dissolved in 45 milliliters of ethanol) was calculated from the average size of CCTO particles to obtain an alumina nanocoating of 20 nanometers. Then, 5 grams of CCTO or CCTO-PVP or CCTO-PEG powder was dispersed in 420 milliliters of ethanol which has to be added in the precursor solution. It is then sonicated during 20 minutes. 50 mL of H_2O /ethanol mixture (1:5 (v/v)) has to be added. In this case, the final mixture is ultrasonicated during 2 hours. Also, the CCTO@ SiO_2 core-shell was synthesized from CCTO particles by a Stöber modified process. SiO_2 has the advantage to be

insulating, which is important for a capacitor by avoiding electric leakage. It also shows a good conformal shell around the core. The thickness of the shell in addition may be easily controlled. The CCTO powder was firstly dispersed in a mixed solution of ethanol/H₂O/ammonia (75/23.5/1.5 %vol). The solution was agitated at room temperature during one hour. Then tetraethyl orthosilicate (TEOS) was added slowly under magnetic stirring. The amount of TEOS was calculated from the average size CCTO particles (~1 μm) to obtain a silica nanocoating of 20 nm. The sol-gel technique was also used to synthesize CCTO@TiO₂ core-shell. The CCTO particles were firstly mixed with absolute ethanol and the solution was placed in an iced bath. Then, the titanium butoxide (TBOT) was added and the solution was mixed during 20 minutes under vigorous stirring. Secondly, a mixed solution of ethanol/H₂O/ammonia (75/23.5/1.5 %vol) was added to the first one and the resulted solution was agitated during 4 hours.

All the as-formed based CCTO core-shell powder are collected by centrifugation (305 RCF-5min). The nanocoating powder has to be washed several times with ethanol and dried overnight at 60°C.

After the collection of the CCTO@SiO₂ core-shell powder, a double core-shell of SiO₂ and Al₂O₃ noted CCTO@SiO₂@Al₂O₃ was synthesized. The same process of CCTO@Al₂O₃ was done but in the beginning instead of using CCTO, the CCTO@SiO₂ powder was dispersed.

All the pellets are then sintered at 1050°C during 5 h except for the CCTO@TiO₂ pellet which is sintered during 24 h. A post-annealing treatment under oxygen atmosphere was realized on CCTO@Al₂O₃ pellet at 500°C during 12 h.

The sintered pellets have been analyzed using X-ray diffraction (Bruker D8) with Cu Kα a radiation of wavelength ~ 1.5418 Å. The dielectric and complex impedance data were measured in a frequency range from 100 Hz to 10 MHz at ambient temperature using an Agilent 4294A impedance analyzer. The data were fitted with the RC element model and the four parameters R_g , C_g , R_{gb} , C_{gb} were extracted as shown in more details by De Almeida-Didry *et al.* [16].

Results and discussion

An example of fit of a two RC elements model, one for the grains and one for the grain boundaries, to experimental data of CCTO@TiO₂ is shown in Figure 2. Two distinct semi-circles are expected, each being associated with a distinct dielectric process, one corresponding to ceramic grains (observed at high frequencies) and the other to grain boundaries. The permittivity and loss tangent of this core-shell sample compared to undoped CCTO and to a commercial GBBL capacitor manufactured by Johansen is shown in Figure 3. Results for each studied sample have been similarly fitted with two RC elements. The dielectric behavior of CCTO ceramics has a Debye-like relaxation with a steep decrease in dielectric constant at the frequency where the dielectric loss tangent displays a relaxation peak. The Debye-like relaxation can be explained by the Maxwell–Wagner relaxation at the interfaces between the grains and their boundaries [17-20]. Results for the grain boundaries which are of main interest in this study are reported in Table 1. Results for the grains are less accurate since the profiles of Figure 2 are mainly related to grain boundaries.

CCTO@TiO₂

The highest permittivity, 870,000, is found for the sample CCTO@TiO₂. Figure 4 compares the XRD diagram of undoped CCTO with that of a sample of CCTO@TiO₂. Additional peaks which are characteristic of TiO₂ crystalized with the rutile crystal structure are displayed in the latest samples. Table 1 shows that this highest permittivity is related to the highest C_{gb} . Among all the shells experimented in this study, rutile single crystal shows the highest permittivity averaged over the three main axes of $(\epsilon_{//} + 2 \epsilon_{\perp})/3 = 108$ [21]. Rutile single crystal treated under reducing atmosphere becomes conductor [22]. It is possible, therefore, that the rutile grain boundary would have become slightly conducting, what would explain the lowest R_{gb} found among all studied samples in Table 1. As a result, the bulk resistivity of the sample is also the lowest among all studied samples.

CCTO@SiO₂

An oxide which remains a good insulator independently of thermal treatments contrary to TiO_2 is SiO_2 . As a result, it has been used as the dielectric material of capacitors integrated to silicon chips for decades. It has also been used as a gate of transistors for decades. Several thicknesses of SiO_2 shells have been experimented. Best results are reported in Table 1. The resistivity, $\tan(\delta)$ and R_{gb} unfortunately are not improved with respect to undoped CCTO. The permittivity is even found lower. Table 1 shows that this is related to the C_{gb} which is found 10 times lower than that of undoped CCTO. This is presumably related to the low permittivity, only 4, of bulk SiO_2 .

CCTO@Al₂O₃

Table 1 shows that the sample CCTO@Al₂O₃ shows a higher permittivity than undoped CCTO while the bulk resistivity is slightly improved. No parameter appears obviously responsible for this improvement. Conversely, considerable improvement is found to be obtained by the procedure of functionalization. With PolyEthyleneGlycol (PEG), the permittivity reaches 130,000 without significant losses measured via $\tan(\delta)$. In addition, the bulk resistivity is multiplied by 3 with respect to undoped CCTO. The bulk resistivity is even multiplied by 15 with respect to undoped CCTO with the functionalization by PolyVinylPyrrolidone (PVP), while the permittivity is found 27 % higher than that of undoped CCTO. The mechanisms which allowed such progresses have to be further studied. The functionalization favors the conformal shell. Since the organic species disappeared during the sintering process, the effect is assumed to be mechanical.

A post-annealing of core-shell samples under oxygen at 500°C during 12 hours increases the bulk resistivity up to 1.9 GΩ.cm, a value that becomes comparable with that of a commercial GBBL capacitor (Table 1). The permittivity however appears reduced with respect to that of the non-post-annealed sample. It still amounts to 17,000, a value higher than for the GBBL capacitor. The drop of permittivity is related to the drop of C_{gb} in Table 1.

CCTO@SiO₂@Al₂O₃

The core-shell microstructure of CCTO@SiO₂@Al₂O₃ observed by TEM is shown in Figure 5. Both distinct shells of SiO₂ and Al₂O₃ are observed in the picture. After sintering, the bulk

resistivity reaches $5 \cdot 10^9 \Omega \cdot \text{cm}$, not far from the $10^{10} \Omega \cdot \text{cm}$ of the Johanson GBBL capacitor. The permittivity nevertheless appears 11 % higher, ranking this double shell and associated process as a good challenger of GBBL capacitors.

CCTO@SiO₂@TiO₂

It was tempting to check whether a double shell combining good insulator like SiO₂ and an oxide showing a large bulk permittivity like TiO₂ rutile would improve the properties. The resistivity reaches $5.2 \cdot 10^8 \Omega \cdot \text{cm}$, but this is not the best result of the studied series of table 1. In addition, the permittivity is found poor. Compared to the other samples of the series, the microstructure is heterogeneous and shows SiO₂ aggregates as observed in the figure 6 that can explain the disappointing results. Grains are also smaller, what is a disadvantage in Eq. 1.

Conclusion

The core-shell approach applied to CCTO is shown to give results that compares favorably with commercial GBBL capacitor. The permittivity is improved while the bulk resistivity reaches levels comparable to commercial ceramic capacitors. The highest permittivity values are confirmed to be related to the high capacity of grain boundaries. The bulk resistivity is related to that of grain boundaries. This study shows that one may play with the bulk permittivity of the shell to try to reach large C_{gb} . However the possible departure of oxygen stoichiometry gives a limitation as observed in TiO₂ rutile grain boundary. If one attaches the more important weight to the bulk resistivity without need of permittivity larger than 15,000, several samples appear convenient. On the other hand, much higher permittivity can be reached like in CCTO@TiO₂ but at the expense of dielectric losses. Thermal post-treatment under various oxidizing or reducing atmosphere have to be developed to solve the problem of dielectric losses like in the example of CCTO@Al₂O₃ post-annealed at 550°C under oxygen.

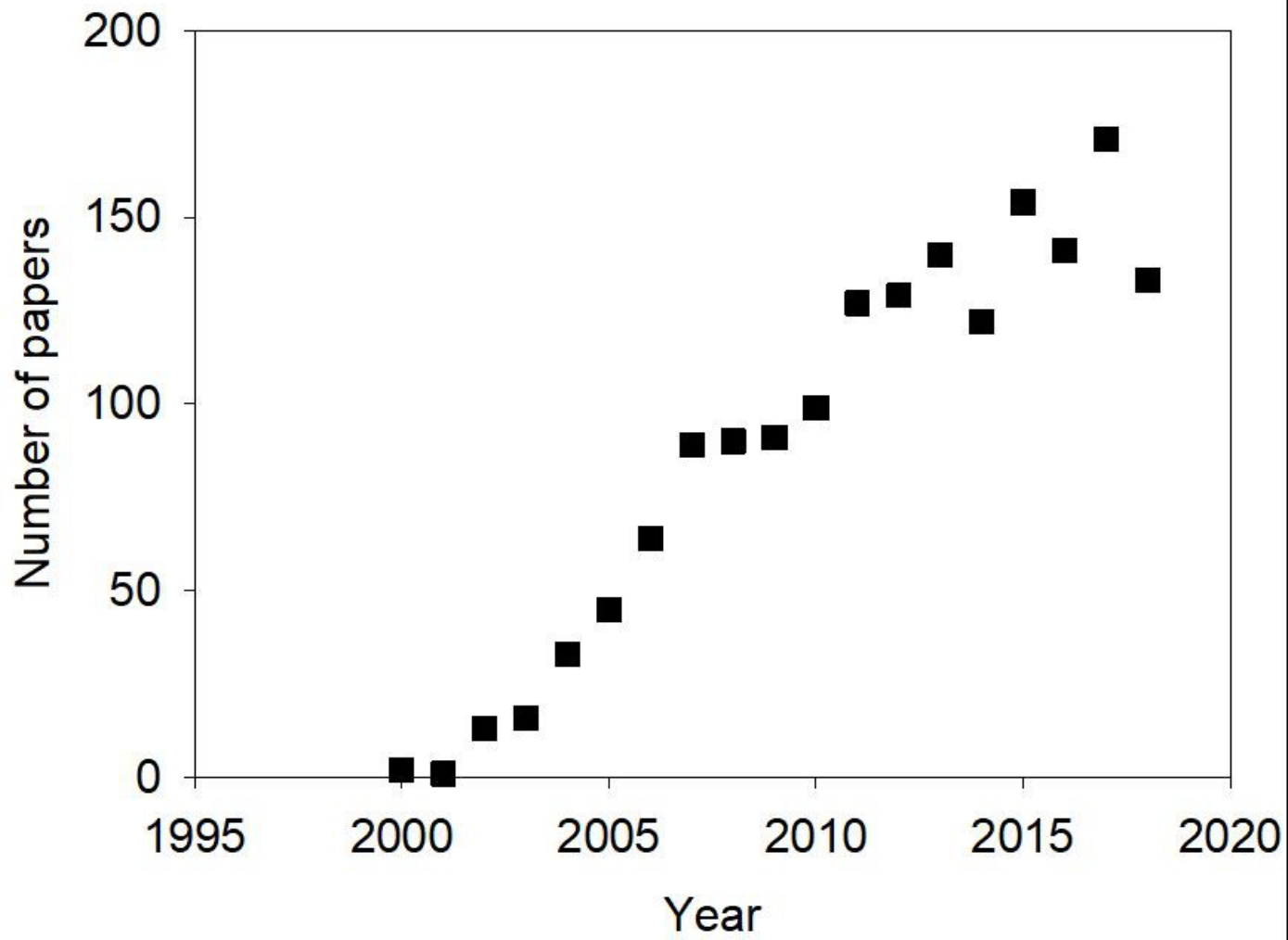
Acknowledgements

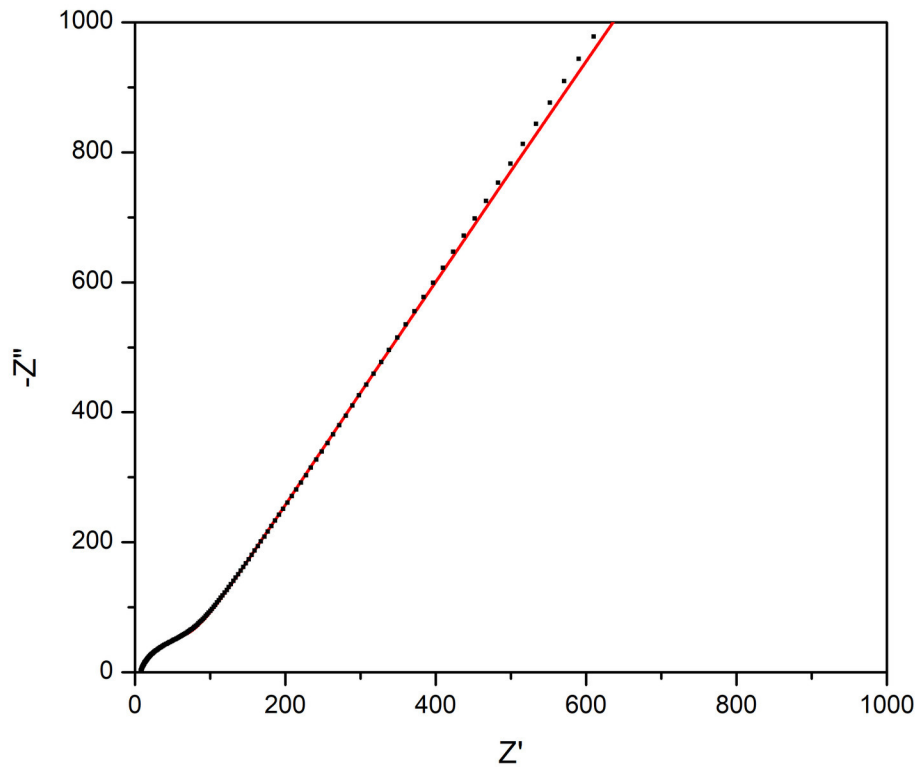
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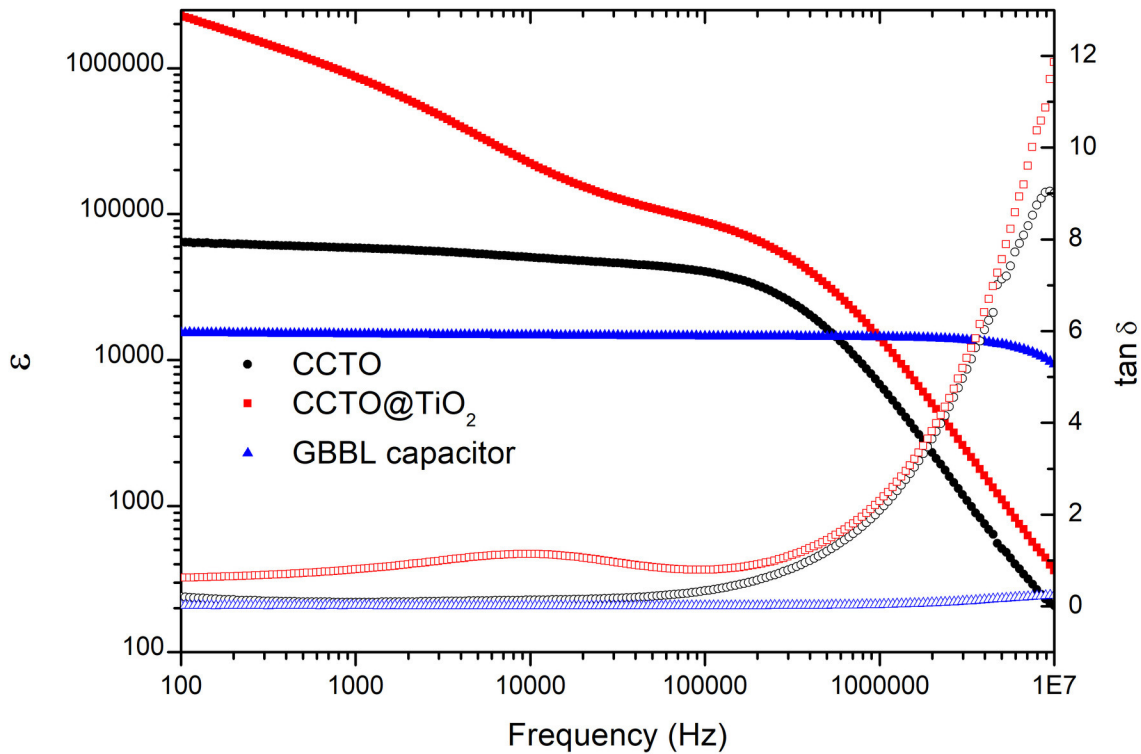
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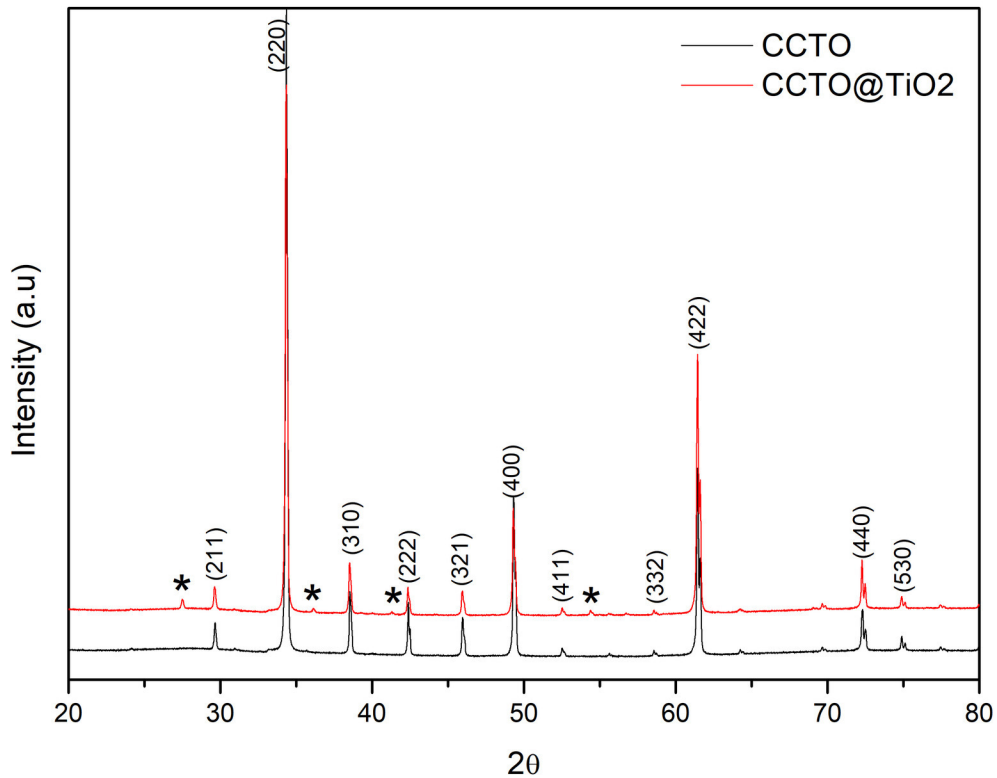
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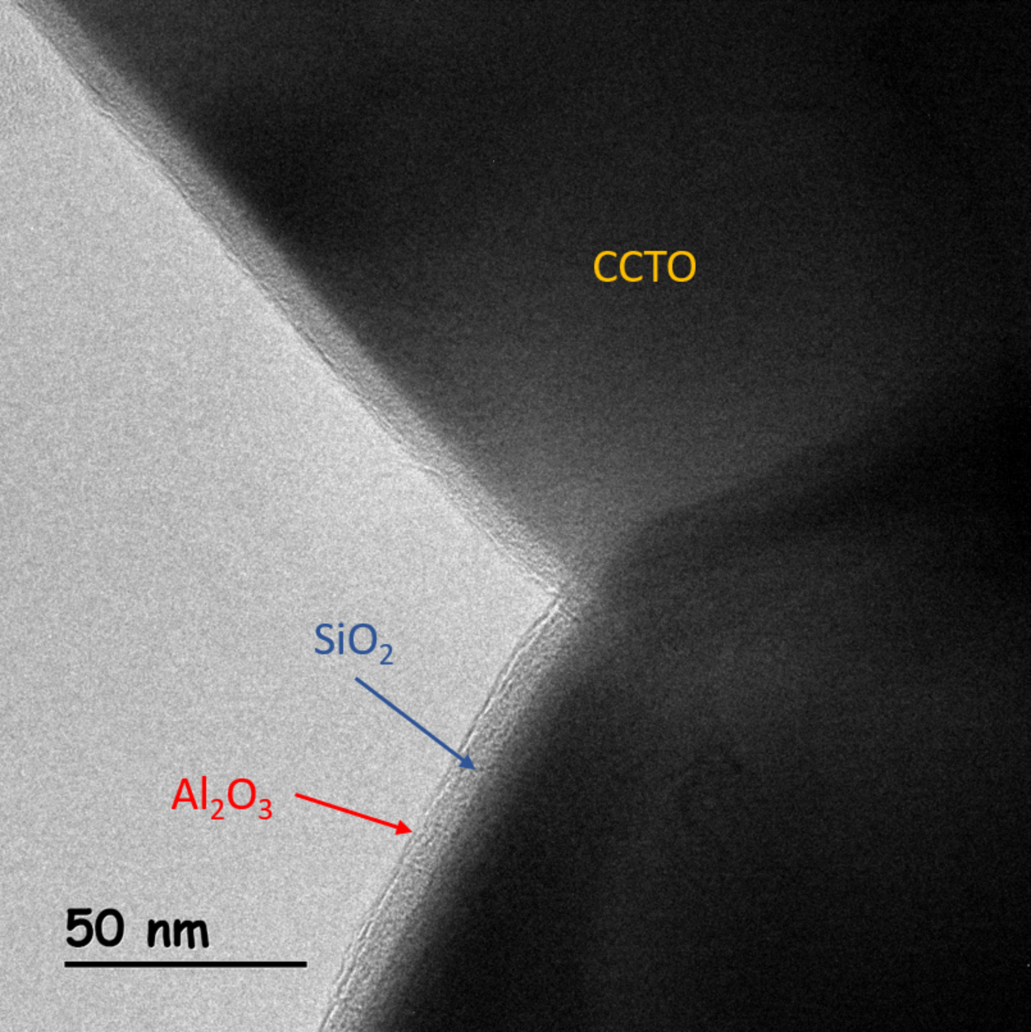


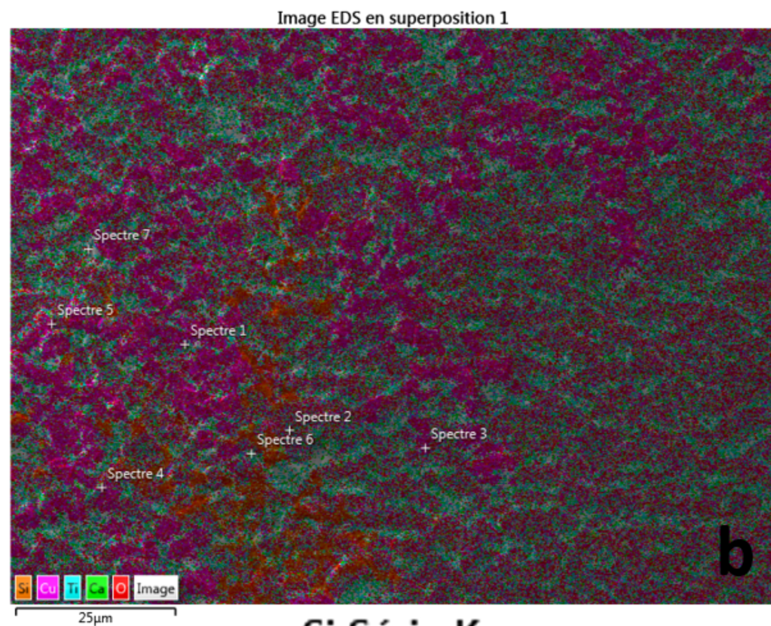
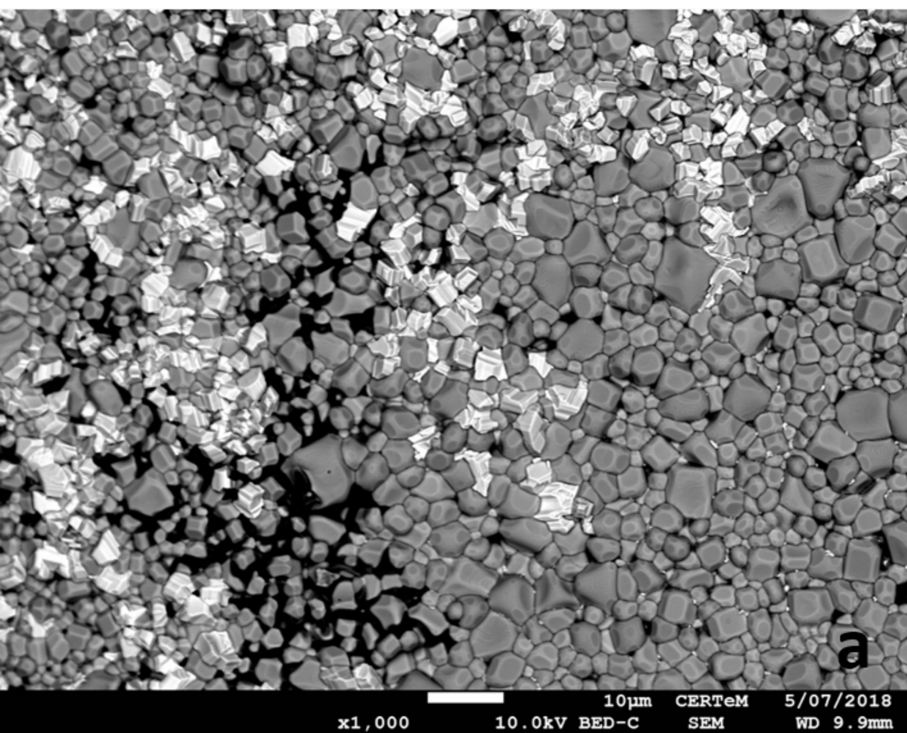
CCTO

SiO_2

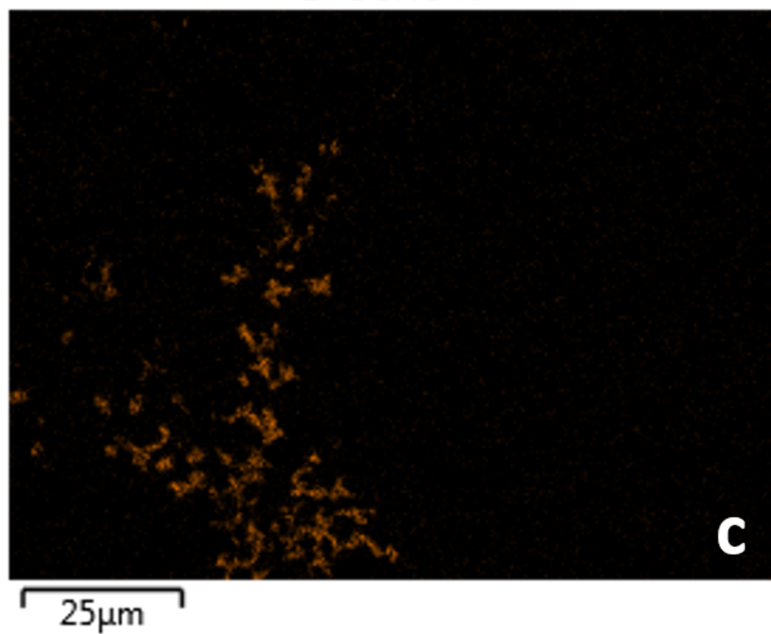
Al_2O_3

50 nm





Si Série K



	ϵ at 1 kHz	$\tan(\delta)$ at 1 kHz	Bulk resistivity ($\Omega\cdot\text{cm}$)	C_{gb} (F. cm^{-1})	R_{gb} ($\Omega\cdot\text{cm}$)
Undoped CCTO-24 h	62,000	0.05	$1.3 \cdot 10^7$	$4.5 \cdot 10^{-7}$	$8.5 \cdot 10^6$
CCTO@Al ₂ O ₃	91,000	0.06	$1.5 \cdot 10^7$	$5.5 \cdot 10^{-8}$	$1.2 \cdot 10^6$
CCTO@Al ₂ O ₃ +PEG	130,000	0.07	$3.9 \cdot 10^7$	$4.2 \cdot 10^{-8}$	10^8
CCTO@Al ₂ O ₃ +PVP	78,600	0.08	$1.9 \cdot 10^8$	$2.25 \cdot 10^{-8}$	$1.8 \cdot 10^7$
CCTO@Al ₂ O ₃ +O ₂ 500°C	17,000	0.09	$1.9 \cdot 10^9$	$9 \cdot 10^{-9}$	$4 \cdot 10^7$
CCTO@SiO ₂	38,000	0.096	$1.1 \cdot 10^7$	$3.5 \cdot 10^{-8}$	$9 \cdot 10^5$
CCTO@SiO ₂ @Al ₂ O ₃	16,700	0.098	$5 \cdot 10^9$	$2.9 \cdot 10^{-9}$	$3 \cdot 10^7$
CCTO@TiO ₂	870,000	0.8	$2 \cdot 10^6$	$1.06 \cdot 10^{-5}$	$8.8 \cdot 10^4$
CCTO@SiO ₂ @TiO ₂	4,700	0.17	$5.2 \cdot 10^8$	$1.5 \cdot 10^{-8}$	$1.5 \cdot 10^6$
Johanson GBBL	15,000	0.01	10^{10}	10^{-10}	10^{10}

Table 1 – A comparison of properties of undoped CCTO, core-shell samples and commercial GBBL capacitor.