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# Coherent interferometric imaging in a random flow

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## Abstract

This paper is concerned with the development of imaging methods to localize sources or reflectors in inhomogeneous *moving* media with acoustic waves that have travelled through them. A typical example is the localization of broadband acoustic sources in a turbulent jet flow for aeroacoustic applications. The proposed algorithms are extensions of Kirchhoff migration (KM) and coherent interferometry (CINT) which have been considered for smooth and randomly inhomogeneous *quiescent* media so far. They are constructed starting from the linearized Euler equations for the acoustic perturbations about a stationary ambient flow. A model problem for the propagation of acoustic waves generated by a fixed point source in an ambient flow with constant velocity is addressed. Based on this result imaging functions are

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proposed to modify the existing KM and CINT functions to account for the ambient flow velocity. They are subsequently tested and compared by numerical simulations in various configurations, including a synthetic turbulent jet representative of the main features encountered in actual jet flows.

*Keywords:* Travel-time migration, Kirchhoff migration, Coherent interferometry, Random flow, Doppler shift.

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## 1. Introduction

This paper is concerned with the problem of localizing acoustic sources or reflectors buried in a randomly heterogeneous moving medium. Our main motivation is the localization of broadband acoustic sources in a turbulent jet flow for aeroacoustic applications [18, 19, 20, 31, 38]. Our main goal is to introduce a wave-based imaging method that can address such a problem. Wave-based imaging has generally two steps. 1) In the first step a data set is collected by an array of sensors. In passive imaging, the goal is to localize sources and the data set consists of the signals transmitted by the sources to be localized and recorded by an array of receivers. In active imaging, the goal is to localize reflectors and the data set consists of the signals transmitted by an array of sources through the medium to be imaged and recorded by an array of receivers. 2) In the second step, the data set is processed to form an image of the medium that is intended to show the positions of the targets (sources or reflectors).

Wave-based imaging has many modalities and applications. In seismic imaging the goal is to estimate the locations of one or more underground sources or reflectors with a passive network of receivers (seismometers) on

the surface of the earth, or the locations of reflective structures from the seismic signals generated by active sources (explosions or air guns) in reflection seismology [6, 25]. The same principle is used in medical ultrasound echography [27], in underwater acoustics (sonar) [28] or in radar [22] for instance.

Imaging sources or reflectors, when performed in a smooth medium, is effective with Kirchhoff migration (KM) [7], when the background propagation velocity is known or can be estimated. The KM imaging technique consists in travel-time migration of the recorded signals, a simplified version of the reverse-time imaging technique where the time-reversed recorded signals are numerically back-propagated by solving a wave equation in a fictitious environment. The waves travel back to their origins (original sources or reflectors) and one can then form an image of them. KM is known to be robust with respect to additive noise, such as measurement noise [1]. This is illustrated for example in [14]. However, KM fails to image in a randomly heterogeneous (cluttered) stationary medium [16]. Indeed, when the medium is cluttered (*i.e.*, when it contains unknown small-scale inhomogeneities), which is generally the case in real-life imaging, travel-time or KM does not work well, because this method in which sources transmit pulses are dependent on clear arrival times. When the medium is cluttered the recorded temporal traces are randomly shifted by the fluctuations of the speed of propagation and they contain long and noisy coda resulting from multiple scattering. The images obtained are then very noisy. Worse they are dependent on the medium, and for two different realizations of the random medium with the same statistical properties we can get two significantly different images.

Contrarily to measurement noise which induces additive independent per-

turbations in the recorded signals, the noise generated by cluttered medium  
 45 in the recorded signals has a complex and correlated structure, which itself  
 generates complex and strong noise in the images formed by KM. For these  
 reasons it is necessary to use imaging methods that are robust with respect  
 to the fluctuations of the medium when it is randomly heterogeneous. In sev-  
 eral studies Borcea and her co-workers [9, 10, 11, 12, 13, 15, 16, 14, 17] have  
 50 introduced a new imaging modality called Coherent INTerferometry (CINT)  
 whose principle is to back-propagate the cross correlations of the recorded  
 signals, and not the signals themselves. In [16] the authors analyze the KM  
 and CINT methods for passive and active arrays of sensors, and quantify  
 their resolution limits and their signal-to-noise ratio (SNR). The resolution  
 55 and statistical fluctuations of the images are analyzed when the ambient en-  
 vironment is random and wave propagation can be modeled mainly by the  
 distortion of the wavefront. KM loses statistical stability at an exponential  
 rate with the propagation distance and leads to unreliable images that change  
 unpredictably with the detailed features of the clutter. Borcea *et al.* [9, 10]  
 60 as well as Chan *et al.* [21] show that CINT imaging statistically stabilizes  
 the images. That is, images have small variance with respect to the random  
 fluctuations of the propagation medium. However, the statistical stability of  
 the CINT method comes at the detriment of some blurring of the images.  
 The trade-off between the resolution and the stability of the CINT imaging  
 65 function can be explicitly quantified [16]. The results obtained so far are  
 very encouraging and this is the reason that motivates us to extend this kind  
 of imaging techniques to heterogeneous flows, *i.e.* random moving media.

More recently, correlation-based imaging have been used to observe fast

moving objects [17, 24]. In these papers, the authors introduce a Doppler  
70 compensation parameter which is used in the imaging function to provide  
the necessary correction of the movement of the object to be observed. In  
our paper we will consider the same compensation mechanism to extend the  
CINT imaging algorithm to moving heterogeneous media such as jet flows.  
One of the most important results is that a sparse configuration of a small  
75 number of uniformly distributed receivers over an area big enough is sufficient  
to create an image with the same resolution as the one obtained with a dense  
set of receivers. It is therefore possible, with a Doppler correction, to obtain  
an image of a fast moving object. This opens very interesting perspectives for  
the objective of imaging through a random flow, which we do in our paper.

80 The rest of the paper is organized as follows. In Sect. 2 a model problem  
of acoustic wave propagation in a flow with constant velocity is addressed,  
starting from the linearized Euler equations with a fixed point source. Imag-  
ing functions for moving cluttered media extending the existing KM and  
CINT functions for quiescent cluttered media are then proposed. They in-  
85 troduce a phase compensation factor accounting for the Doppler shift induced  
by the background flow velocity. The KM and CINT functions for quiescent  
media are reviewed in Sect. 3 for configurations already considered in the  
literature in order to validate our numerical implementation by comparisons  
with the existing results in [10, 11]. Then the proposed imaging functions are  
90 tested in Sect. 4 for moving cluttered media with a random speed of sound  
and either a constant or a randomly perturbed velocity of the background  
flow. They are applied to a numerically generated synthetic jet in Sect. 5,  
where a compensation scheme for refraction of the acoustic waves at the jet

sheared layers is introduced in addition to the Doppler shift compensation.

95 A summary of this research and conclusions are finally drawn in Sect. 6.

## 2. Imaging functions in moving random media

### 2.1. Model problem

We start by considering the problem of computing the pressure field emitted by a point source in an ambient flow with stationary velocity because it  
 100 has relevance to the imaging algorithms considered in the subsequent developments. The Euler equations for mass, momentum, and energy conservation in the compressible flow of an ideal fluid without friction, heat conduction or heat production read:

$$\begin{aligned}\frac{d\rho}{dt} &= -\rho \nabla \cdot \mathbf{v} + m, \\ \frac{d\mathbf{v}}{dt} &= -\frac{1}{\rho} \nabla p, \\ \frac{ds}{dt} &= 0,\end{aligned}\tag{1}$$

where  $\frac{d}{dt} = \partial_t + \mathbf{v} \cdot \nabla$  is the convective derivative with  $\nabla = (\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z})$ ,  
 105  $\mathbf{v}(\mathbf{r}, t)$  is the fluid velocity,  $\rho(\mathbf{r}, t)$  is the density,  $p(\mathbf{r}, t)$  is the (static) fluid pressure,  $s(\mathbf{r}, t)$  is the specific entropy, and  $m(\mathbf{r}, t)$  is a specific mass source per unit time, at the position  $\mathbf{r} = (x, y, z)$  in  $\mathbb{R}^3$  and time  $t$  in  $\mathbb{R}$ . The flow is isentropic (*i.e.* each fluid particle has constant entropy), and by the equation of state  $p = p^\#(\rho, s)$  we have:

$$\frac{dp}{dt} = c^2 \frac{d\rho}{dt}, \quad c^2(\rho, s) = \left. \frac{\partial p^\#}{\partial \rho} \right|_s,\tag{2}$$

110 where  $c$  is the adiabatic speed of sound. For a perfect gas of heat capacity ratio  $\gamma$ , the equation of state  $p\rho^{-\gamma} = C$  along particle paths, where the constant  $C$  may differ for each particle in isentropic flows, yields  $c^2 = \gamma p/\rho$ . The

foregoing Euler equations are linearized about an unperturbed, stationary flow for which the pressure  $p_0(\mathbf{r})$ , velocity  $\mathbf{v}_0(\mathbf{r})$ , and density  $\varrho_0(\mathbf{r})$  do not  
 115 depend on time. They satisfy:

$$\begin{aligned}(\mathbf{v}_0 \cdot \nabla) \varrho_0 &= -\varrho_0 \nabla \cdot \mathbf{v}_0, \\(\mathbf{v}_0 \cdot \nabla) \mathbf{v}_0 &= -\frac{1}{\varrho_0} \nabla p_0, \\(\mathbf{v}_0 \cdot \nabla) p_0 &= c_0^2 (\mathbf{v}_0 \cdot \nabla) \varrho_0,\end{aligned}\tag{3}$$

where  $c_0(\mathbf{r})$  stands for the sound velocity not influenced by the acoustic waves propagating in the actual flow. Linearization consists in considering that the latter is a perturbation  $(p', \mathbf{v}', \varrho')$  of the stationary flow generated by the specific mass  $m$  injected to the fluid:

$$\begin{aligned}p(\mathbf{r}, t) &= p_0(\mathbf{r}) + p'(\mathbf{r}, t), \\ \mathbf{v}(\mathbf{r}, t) &= \mathbf{v}_0(\mathbf{r}) + \mathbf{v}'(\mathbf{r}, t), \\ \varrho(\mathbf{r}, t) &= \varrho_0(\mathbf{r}) + \varrho'(\mathbf{r}, t).\end{aligned}$$

120 The primed quantities  $p'$ ,  $\mathbf{v}'$ , and  $\varrho'$  are the acoustic pressure, velocity, and density, respectively, of which non-linear contributions to the Euler equations (1) are assumed negligible. In other words, these quantities are first-order increments of the zero-th order stationary quantities. They satisfy the following linearized Euler equations (LEE):

$$\begin{aligned}\frac{d\varrho'}{dt} + \nabla \cdot (\varrho_0 \mathbf{v}') + \varrho' \nabla \cdot \mathbf{v}_0 &= m, \\ \frac{d\mathbf{v}'}{dt} + (\mathbf{v}' \cdot \nabla) \mathbf{v}_0 + \frac{1}{\varrho_0} \nabla p' - \frac{\varrho'}{\varrho_0^2} \nabla p_0 &= \mathbf{0},\end{aligned}\tag{4}$$

125 together with the barotropic assumption  $p' = c_0^2 \varrho'$ . Here and from now on the convective derivative is defined as  $\frac{d}{dt} = \partial_t + \mathbf{v}_0 \cdot \nabla$ , *i.e.* the convective derivative within the stationary, ambient flow.

If the ambient quantities are non vanishing constant  $(p_0, \mathbf{v}_0, \varrho_0)$ , which is consistent with Eq. (3), we obtain by taking the convective derivative  $\frac{d}{dt}$  of the first equation in (4) and the divergence  $\nabla \cdot$  of the second equation in (4):

$$\frac{1}{c_0^2} \frac{d^2 p}{dt^2} - \Delta p = \frac{dm}{dt}. \quad (5)$$

Here we have dropped the primes  $(\cdot)'$  for convenience. This is the convected wave equation:

$$\frac{d}{dt} \left( \frac{1}{c_0^2} \frac{dp}{dt} \right) - \varrho_0 \nabla \cdot \left( \frac{1}{\varrho_0} \nabla p \right) = \frac{dm}{dt}$$

first proposed by Blokhintzev [8] for steady irrotational ambient flows. Thus if  $\mathbf{v}_0$  is constant all over the region where the imaging procedure is performed, one can consider a local frame moving at this velocity. The local coordinates  $\mathbf{R}$  and pressure field  $P(\mathbf{R}, t)$  are defined by:

$$\mathbf{R} = \mathbf{r} - \mathbf{v}_0 t, \quad P(\mathbf{R}, t) = p(\mathbf{R} + \mathbf{v}_0 t, t).$$

With this change of variable one notices that  $\partial_t P = \frac{dp}{dt}$  and obtains that in the moving frame:

$$\frac{1}{c_0^2} \frac{\partial^2 P}{\partial t^2} - \Delta P = \frac{\partial \mathcal{M}}{\partial t}, \quad (6)$$

where similarly  $\mathcal{M}(\mathbf{R}, t) = m(\mathbf{R} + \mathbf{v}_0 t, t)$ . This is actually the acoustic wave equation with a vanishing ambient flow velocity.

The acoustic Green's function  $G_0(\mathbf{R}, \mathbf{R}', t)$  is defined as the solution of the wave equation (6) for a right-hand side  $\partial_t \mathcal{M}(\mathbf{R}, t) \equiv F(\mathbf{R}, t) = \delta(t) \delta(\mathbf{R} - \mathbf{R}')$  with vanishing initial conditions. It reads  $G_0(\mathbf{R}, \mathbf{R}', t) = \mathcal{G}_0(|\mathbf{R} - \mathbf{R}'|, t)$ , where for  $D > 0$ :

$$\mathcal{G}_0(D, t) = \begin{cases} \frac{1}{4\pi D} \delta\left(t - \frac{D}{c_0}\right) & \text{if } t > 0, \\ 0 & \text{if } t \leq 0. \end{cases} \quad (7)$$

The solution of the wave equation (6) for a source  $\mathcal{M}$  with time-dependent spatial compact support  $\Omega_s(t)$  is then:

$$P(\mathbf{R}, t) = \frac{1}{4\pi} \frac{\partial}{\partial t} \int dt' \int_{\Omega_s(t')} \frac{\mathcal{M}(\mathbf{R}', t')}{|\mathbf{R} - \mathbf{R}'|} \delta\left(t - t' - \frac{|\mathbf{R} - \mathbf{R}'|}{c_0}\right) d\mathbf{R}'. \quad (8)$$

We now assume that the source  $m$  is a fixed point source at the position  $\mathbf{r}_s$  in the reference frame, such that  $\mathcal{M}(\mathbf{R}, t) = A(t)\delta(\mathbf{R} - \mathbf{R}_s(t))$  where  $\mathbf{R}_s(t) = \mathbf{r}_s - \mathbf{v}_0 t$ , and  $A$  is its amplitude. Then owing to the identity  $\int Y(t')\delta(X(t'))dt' = \sum_j Y(t_j)|\partial_{t'}X|_{t'=t_j}^{-1}$  where the  $t_j$ 's depend on  $t$  and are the roots of  $X(t') = 0$  (with  $X(t') = t - t' - |\mathbf{R} - \mathbf{R}_s(t')|/c_0$ ), one obtains:

$$P(\mathbf{R}, t) = \frac{1}{4\pi} \frac{\partial}{\partial t} \sum_j \frac{A(t_j)}{||\mathbf{R} - \mathbf{R}_s(t_j)| + \mathbf{M} \cdot (\mathbf{R} - \mathbf{R}_s(t_j))|},$$

where  $\mathbf{M} := \frac{\mathbf{v}_0}{c_0}$  is the Mach number (a vector in the present case) of the ambient flow. The sum is taken over the  $t_j$ 's such that  $c_0(t - t_j) = |\mathbf{R} - \mathbf{R}_s(t_j)|$ , which can not have more than one solution in the subsonic regime  $|\mathbf{M}| < 1$  [33, Chapter 5]. Indeed, if one lets  $\phi(\tau) = |\mathbf{R} - \mathbf{R}_s(\tau)| - c_0(t - \tau)$  then  $\phi'(\tau) = c_0 + \frac{(\mathbf{R} - \mathbf{R}_s(\tau)) \cdot \mathbf{v}_0}{|\mathbf{R} - \mathbf{R}_s(\tau)|} > 0$  in the subsonic regime. Thus  $\phi$  increases monotonically and the situation  $\phi(\tau) = 0$  arises at most once, say  $\tau = t_s$  the time of emission of a sound wave which arrives at the observation point  $\mathbf{R}$  at time  $t$  in the moving frame. Solving for this equation with  $\mathbf{R} = \mathbf{r} - \mathbf{v}_0 t$ , we arrive at:

$$t_s = t - \frac{d}{c_0} \frac{\sqrt{1 - (M \sin \alpha)^2} - M \cos \alpha}{1 - M^2},$$

where  $M d \cos \alpha = \mathbf{M} \cdot (\mathbf{r} - \mathbf{r}_s)$ ; that is,  $M = |\mathbf{M}|$ ,  $d = |\mathbf{r} - \mathbf{r}_s|$  is the distance between the source point  $\mathbf{r}_s$  and the observation point  $\mathbf{r}$  in the reference frame, and  $\alpha$  is the angle between  $\mathbf{v}_0$  and  $\mathbf{r} - \mathbf{r}_s$ . The acoustic

165 pressure in the reference frame finally reads:

$$p(\mathbf{r}, t) = \frac{1}{4\pi d \sqrt{1 - (M \sin \alpha)^2}} A' \left( t - \frac{d}{c_0} \frac{\sqrt{1 - (M \sin \alpha)^2} - M \cos \alpha}{1 - M^2} \right). \quad (9)$$

We will resort to this expression to form imaging functions in moving media in the next sections.

## 2.2. Reverse-time and Kirchhoff migration

We first consider the classical reverse-time (RT) [39] and Kirchhoff mi-  
 170 gration (KM) [7] algorithms to detect and localize sources or reflectors in  
 a homogeneous or weakly heterogeneous medium. We adapt them to the  
 situation of interest for us, namely the localization of such sources or reflec-  
 tors in a random flow. In RT migration [39],  $N$  fixed sensors located at  $\mathbf{r}_r$ ,  
 $1 \leq r \leq N$ , are used to localize a source (passive imaging case) or a reflector  
 175 (active imaging case) at some unknown location  $\mathbf{r}^*$  in the actual (unknown)  
 random flow by back-propagating in a fictitious flow of known characteristics  
 the pressure fields recorded by the sensors.

### 2.2.1. Passive imaging

Let us first consider the case of a quiescent homogeneous medium that is  
 180 a flow with  $\mathbf{v}_0 = \mathbf{0}$  and a constant speed of sound  $c_0$ . Introducing the Fourier  
 and inverse Fourier transforms in the time domain:

$$\widehat{p}(\mathbf{r}, \omega) = \int_{\mathbb{R}} e^{i\omega t} p(\mathbf{r}, t) dt, \quad p(\mathbf{r}, t) = \frac{1}{2\pi} \int_{\mathbb{R}} e^{-i\omega t} \widehat{p}(\mathbf{r}, \omega) d\omega, \quad (10)$$

the time-harmonic Green's function  $\widehat{G}_0(\mathbf{r}, \mathbf{r}', \omega)$  solves the wave equation (6)  
 in the Fourier domain—the Helmholtz equation with point source at  $\mathbf{r}'$ :

$$\frac{\omega^2}{c_0^2} \widehat{G}_0 + \Delta \widehat{G}_0 = -\delta(\mathbf{r} - \mathbf{r}'), \quad (11)$$

together with the Sommerfeld radiation condition at infinity  $|\mathbf{r}| \rightarrow +\infty$ :

$$\left( \hat{\mathbf{r}} \cdot \nabla - i \frac{\omega}{c_0} \right) \hat{G}_0(\mathbf{r}, \mathbf{r}', \omega) = O\left(\frac{1}{|\mathbf{r}|^2}\right), \quad (12)$$

185 where  $\hat{\mathbf{r}} := \frac{\mathbf{r}}{|\mathbf{r}|}$ ; that is,  $\hat{G}_0(\mathbf{r}, \mathbf{r}', \omega) \propto e^{i \frac{\omega}{c_0} |\mathbf{r}|}$  at infinity. It satisfies the reciprocity property  $\hat{G}_0(\mathbf{r}, \mathbf{r}', \omega) = \hat{G}_0(\mathbf{r}', \mathbf{r}, \omega)$  everywhere, and since the ambient medium has a constant speed of sound:

$$\hat{G}_0(\mathbf{r}, \mathbf{r}', \omega) = \hat{\mathcal{G}}_0(|\mathbf{r} - \mathbf{r}'|, \omega) = \frac{e^{i \frac{\omega}{c_0} |\mathbf{r} - \mathbf{r}'|}}{4\pi |\mathbf{r} - \mathbf{r}'|}. \quad (13)$$

Passive imaging is aimed at localizing a source in a quiescent heterogeneous medium of which the actual speed of sound  $c_0(\mathbf{r})$  is instead variable and  
 190 imperfectly known. One starts by recording at the  $N$  sensors the pressure fields emitted by the source  $F(\mathbf{r}, t) = f(t)\delta(\mathbf{r} - \mathbf{r}^*)$ . This yields the dataset  $\{p(\mathbf{r}_r, t); 1 \leq r \leq N\}$  (or its Fourier transforms  $\{\hat{p}(\mathbf{r}_r, \omega); 1 \leq r \leq N\}$ ) constituted by the pressure fields recorded by the sensors located at  $\mathbf{r}_r$ ,  $1 \leq r \leq N$ . They are subsequently time reversed, which amounts of tak-  
 195 ing the conjugates of their Fourier transforms, and back propagated in a fictitious domain of which Green's function is known, namely  $\hat{\mathcal{G}}_0(d, \omega)$ . The RT imaging function  $\mathcal{I}_{\text{RT}}(\mathbf{r}^S)$  is ultimately formed by stacking all the data:

$$\mathcal{I}_{\text{RT}}(\mathbf{r}^S) = \frac{1}{2\pi} \sum_{r=1}^N \int_{\mathbb{R}} \hat{\mathcal{G}}_0(|\mathbf{r}^S - \mathbf{r}_r|, \omega) \overline{\hat{p}(\mathbf{r}_r, \omega)} d\omega. \quad (14)$$

Because the amplitude factor plays no role when one tries to localize sources (or reflectors), the KM function [7] for passive imaging, considering  $\hat{\mathcal{G}}_0(d, \omega) \propto$   
 200  $e^{i \frac{\omega d}{c_0}}$  and replacing the Green's function by this phase term in Eq. (14) above,

reads:

$$\begin{aligned}\mathcal{I}_{\text{KM}}(\mathbf{r}^S) &= \frac{1}{2\pi} \sum_{r=1}^N \int_{\mathbb{R}} e^{i\frac{\omega}{c_0}|\mathbf{r}^S - \mathbf{r}_r|} \overline{\widehat{p}(\mathbf{r}_r, \omega)} d\omega \\ &= \sum_{r=1}^N p\left(\mathbf{r}_r, \frac{|\mathbf{r}^S - \mathbf{r}_r|}{c_0}\right),\end{aligned}\tag{15}$$

so that the source location can be estimated by:

$$\hat{\mathbf{r}}_{\text{so}} = \arg \max_{\mathbf{r}^S \in S} \mathcal{I}_{\text{KM}}(\mathbf{r}^S) \quad \text{in some search region } S.$$

The range resolution of KM is  $c_0/B$ , where  $B$  is the source frequency bandwidth. The cross-range resolution is  $r_c = \lambda_0 L/a$  (Rayleigh resolution formula), where  $a$  is the aperture of the sensor array,  $\lambda_0$  is the source central wavelength, and  $L$  is the distance from the source to the array (range); see Fig. 1 for the typical configuration of imaging sources or reflectors in a two-dimensional quiescent heterogeneous medium with random speed of sound considered in [10]. KM is known to work poorly when the medium is scattering, because the echoes of the sources or reflectors recorded at the array have random time shifts and a lot of delay spread—the coda—induced by the scatterers. However it is very robust with respect to additive measurement noise.

Now in view of the result (9), it is proposed to modify the foregoing imaging function to include a Doppler compensation factor  $\gamma_D(\mathbf{r}, \mathbf{r}', \mathbf{v}_0)$  which compensates the shift of the arrival time induced by the flow when the am-

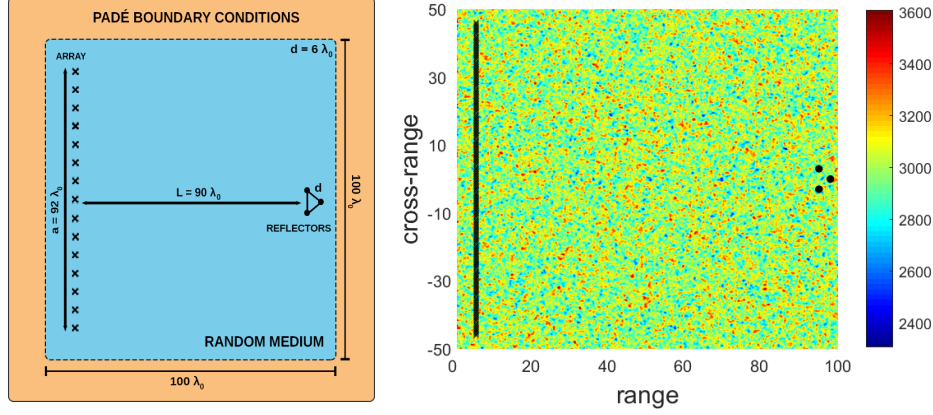


Figure 1: Typical imaging configuration in a quiescent heterogeneous medium with random speed of sound, after [10]. Dimensions are given in units of the central wavelength  $\lambda_0$  of the sources. Left: the locations of the sources (passive case) or reflectors (active case) to be imaged are shown by dots  $\bullet$  and the locations of the transducers are shown by crosses  $\times$ . In active imaging the central transducer is used as a source. Right: typical realization of the random speed of sound  $c_0(\mathbf{r})$  with average  $\underline{c} = 3000$  m/s.

bient medium moves at an average velocity  $\mathbf{v}_0 \neq \mathbf{0}$ :

$$\gamma_D(\mathbf{r}, \mathbf{r}', \mathbf{v}_0) = \left(1 - \left|\frac{\mathbf{v}_0}{c_0}\right|^2\right)^{-1} \left[ \sqrt{1 - \left|\frac{\mathbf{v}_0}{c_0}\right|^2 + \left(\frac{\mathbf{v}_0 \cdot (\mathbf{r} - \mathbf{r}')}{c_0 |\mathbf{r} - \mathbf{r}'|}\right)^2} - \frac{\mathbf{v}_0 \cdot (\mathbf{r} - \mathbf{r}')}{c_0 |\mathbf{r} - \mathbf{r}'|} \right]. \quad (16)$$

The compensated KM imaging function (15) then reads:

$$\mathcal{I}_{\text{KM}}(\mathbf{r}^S) = \sum_{r=1}^N p \left( \mathbf{r}_r, \gamma_D(\mathbf{r}_r, \mathbf{r}^S, \mathbf{v}_0) \frac{|\mathbf{r}_r - \mathbf{r}^S|}{c_0} \right), \quad (17)$$

215 where one observes that  $\gamma_D(\mathbf{r}, \mathbf{r}', \mathbf{0}) = 1$  and the imaging function (15) for a quiescent medium is recovered. Note also that the same Doppler compensation factor has been considered recently in [17, 24] for imaging small fast moving objects revolving around the Earth at low orbits.

### 2.2.2. Active imaging

220 In active imaging, the network of sensors is used for detecting reflectors. One or several sensors  $\mathbf{r}_s$ ,  $1 \leq s \leq N_s$ , emit signals which are recorded after a round trip to the reflectors. In this context the dataset  $\{p(\mathbf{r}_r, t; \mathbf{r}_s); 1 \leq r \leq N_r, 1 \leq s \leq N_s\}$  (or its Fourier transforms  $\{\hat{p}(\mathbf{r}_r, \omega; \mathbf{r}_s); 1 \leq r \leq N_r, 1 \leq s \leq N_s\}$ ) is constituted by the pressure fields recorded by the sensors located at  $\mathbf{r}_r$ ,  
 225  $1 \leq r \leq N_r$ , when the sensors located at  $\mathbf{r}_s$ ,  $1 \leq s \leq N_s$ , act as active sources one after the other one. The KM function in active imaging is written:

$$\mathcal{I}_{\text{KM}}(\mathbf{r}^R) = \sum_{r=1}^{N_r} \sum_{s=1}^{N_s} p\left(\mathbf{r}_r, \frac{|\mathbf{r}_s - \mathbf{r}^R|}{c_0} + \frac{|\mathbf{r}^R - \mathbf{r}_r|}{c_0}; \mathbf{r}_s\right), \quad (18)$$

and:

$$\hat{\mathbf{r}}_{\text{ref}} = \arg \max_{\mathbf{r}^R \in S} \mathcal{I}_{\text{KM}}(\mathbf{r}^R) \quad \text{in some search region } S \quad (19)$$

is the estimated position of the reflector. As for passive imaging, the foregoing imaging function is modified to include a Doppler compensation factor  $\gamma_D(\mathbf{r}, \mathbf{r}', \mathbf{v}_0)$  when the ambient medium moves at an average velocity  $\mathbf{v}_0 \neq \mathbf{0}$ . In active imaging the KM imaging function (18) now reads:

$$\mathcal{I}_{\text{KM}}(\mathbf{r}^R) = \sum_{r=1}^{N_r} \sum_{s=1}^{N_s} p\left(\mathbf{r}_r, \gamma_D(\mathbf{r}_s, \mathbf{r}^R, \mathbf{v}_0) \frac{|\mathbf{r}_s - \mathbf{r}^R|}{c_0} + \gamma_D(\mathbf{r}^R, \mathbf{r}_r, \mathbf{v}_0) \frac{|\mathbf{r}^R - \mathbf{r}_r|}{c_0}; \mathbf{r}_s\right). \quad (20)$$

The first  $\gamma_D$  compensates the time shift induced by the flow, for the travel between the source to the reflector. The second  $\gamma_D$  compensates this shift  
 230 for the travel between the reflector and the receiver.

### 2.3. Coherent interferometric (CINT) imaging

Coherent interferometric imaging (CINT) [9, 10, 11, 12, 13, 15, 16, 14] of sources or reflectors uses finite-aperture arrays alike to localize in a cluttered

medium a source (passive imaging) or a reflector (active imaging). It consists  
 235 in back propagating selected empirical correlations of the pressure fields,  
 rather than the pressure fields themselves, in a fictitious medium in order to  
 alleviate the statistical instability of KM with clutter. Indeed, forming the  
 correlations enables to partially cancel the incoherent random phase shifts  
 of the signals and thus enhance statistical stability. We refer to Fig. 1 for  
 240 a typical configuration, with a square array  $A = [-\frac{a}{2}, \frac{a}{2}] \times [-\frac{a}{2}, \frac{a}{2}] \times \{0\}$  of  
 $N$  sensors and a target (source or reflector) that is at the position  $(0, 0, L)$ ,  
 where  $L$  is the distance (range) from the array.

### 2.3.1. Passive CINT imaging

The empirical cross-correlation of the recorded pressure fields at the sen-  
 245 sors  $\mathbf{r}_q$  and  $\mathbf{r}_r$ ,  $1 \leq q, r \leq N$ , reads in the Fourier domain:

$$\mathcal{C}_F(\mathbf{r}_q, \mathbf{r}_r, \omega, \omega') = \widehat{p}(\mathbf{r}_q, \omega) \overline{\widehat{p}(\mathbf{r}_r, \omega')}. \quad (21)$$

Then these empirical cross-correlations are back-propagated in a fictitious  
 (*e.g.* homogeneous) medium, of which Green's function is again  $\widehat{\mathcal{G}}_0(d, \omega) \propto$   
 $e^{i\frac{\omega d}{c_0}}$ . Besides, the cross-correlations are computed locally in frequency and  
 space and not over the whole frequency range and for all pairs of sensors.  
 The CINT function for passive imaging in a quiescent medium reads [10]:

$$\begin{aligned} \mathcal{I}_{\text{CINT}}(\mathbf{r}^S; \Omega_d, X_d) = \\ \sum_{\substack{q, r = 1 \\ |\mathbf{r}_q - \mathbf{r}_r| \leq X_d}}^N \iint_{|\omega - \omega'| \leq \Omega_d} \mathcal{C}_F(\mathbf{r}_q, \mathbf{r}_r, \omega, \omega') e^{-i\frac{\omega}{c_0}|\mathbf{r}_q - \mathbf{r}^S| + i\frac{\omega'}{c_0}|\mathbf{r}_r - \mathbf{r}^S|} d\omega d\omega', \end{aligned} \quad (22)$$

such that the source location can be estimated by:

$$\hat{\mathbf{r}}_{\text{so}} = \arg \max_{\mathbf{r}^S \in S} \mathcal{I}_{\text{CINT}}(\mathbf{r}^S; \Omega_d, X_d) \quad \text{in some search region } S.$$

The range resolution of CINT is  $c_0/\Omega_d$  (the usual range resolution formula with the effective bandwidth  $\Omega_d < B$  where  $B$  is the source bandwidth), and its cross-range resolution is  $\lambda_0 L X_d$  (the Rayleigh resolution formula with an effective array diameter  $X_d < a$ ) [10, 11]. Ideally the frequency window  $\Omega_d$  is chosen as the decoherency frequency  $\Omega_c$ , *i.e.* the frequency gap beyond which the frequency components of the recorded pressure fields are no longer correlated. Likewise, the spatial window  $X_d$  is ideally chosen as the decoherency length  $X_c$ , *i.e.* the sensor gap beyond which the recorded pressure fields are no longer correlated. The decoherency parameters  $\Omega_c$  and  $X_c$  depend on the statistical properties of the fluctuations in the random medium, the range  $L$ , and the central frequency. Actually these parameters are not known since the random medium is also unknown, so the CINT parameters  $\Omega_d$  and  $X_d$  have to be determined from the data by the imaging process itself. Alternatively, an optimal set of parameters may be determined by the adaptive algorithm developed in [11].

In view of the result (9), it is proposed to modify the foregoing CINT imaging function (22) for localizing a source to include the Doppler compensation factor (16). The compensated CINT function for passive imaging in a moving medium then reads:

$$\begin{aligned} \mathcal{I}_{\text{CINT}}(\mathbf{r}^S; \Omega_d, X_d) = & \sum_{q, r=1}^N \iint_{\substack{|\omega - \omega'| \leq \Omega_d \\ |\mathbf{r}_q - \mathbf{r}_r| \leq X_d}} \mathcal{C}_F(\mathbf{r}_q, \mathbf{r}_r, \omega, \omega') \\ & \times e^{-i \frac{\omega}{c_0} \gamma_D(\mathbf{r}_q, \mathbf{r}^S, \mathbf{v}_0) |\mathbf{r}_q - \mathbf{r}^S| + i \frac{\omega'}{c_0} \gamma_D(\mathbf{r}_r, \mathbf{r}^S, \mathbf{v}_0) |\mathbf{r}_r - \mathbf{r}^S|} d\omega d\omega'. \quad (23) \end{aligned}$$

**Remark:** The unfiltered, full CINT function (obtained by letting  $X_d, \Omega_d \rightarrow$

$\infty$ ) is:

$$\begin{aligned}
\mathcal{I}_{\text{BF}}(\mathbf{r}^S) &= \sum_{q,r=1}^N \iint_{\mathbb{R}^2} \mathcal{C}_F(\mathbf{r}_q, \mathbf{r}_r, \omega, \omega') \\
&\quad \times e^{-i\frac{\omega}{c_0}\gamma_D(\mathbf{r}_q, \mathbf{r}^S, \mathbf{v}_0)|\mathbf{r}_q - \mathbf{r}^S| + i\frac{\omega'}{c_0}\gamma_D(\mathbf{r}_r, \mathbf{r}^S, \mathbf{v}_0)|\mathbf{r}_r - \mathbf{r}^S|} d\omega d\omega' \\
&= (2\pi)^2 |\mathcal{I}_{\text{KM}}(\mathbf{r}^S)|^2,
\end{aligned} \tag{24}$$

that is, all pairs of sensors and frequencies are summed up in Eq. (23). Thus the same image as with KM (17) is formed. This shows in particular that the full migration of all cross-correlations does not work if the medium is cluttered.

### 2.3.2. Active CINT imaging

CINT imaging can be used to localize reflectors alike. Among the  $N$  transducers of the array  $A$ ,  $N_s$  are used as sources located at  $\mathbf{r}_s$ ,  $1 \leq s \leq N_s$ , and  $N_r$  are used as receivers (sensors) located at  $\mathbf{r}_r$ ,  $1 \leq r \leq N_r$ . The dataset of recorded pressure fields is denoted by  $\{p(\mathbf{r}_r, t; \mathbf{r}_s); 1 \leq r \leq N_r, 1 \leq s \leq N_s\}$ . The CINT function for active imaging in a quiescent medium reads:

$$\begin{aligned}
\mathcal{I}_{\text{CINT}}(\mathbf{r}^R; \Omega_d, X_d) &= \\
&\sum_{\substack{r, r'=1 \\ |\mathbf{r}_r - \mathbf{r}_{r'}| \leq X_d}}^{N_r} \sum_{\substack{s, s'=1 \\ |\mathbf{r}_s - \mathbf{r}_{s'}| \leq X_d}}^{N_s} \iint_{|\omega - \omega'| \leq \Omega_d} \widehat{p}(\mathbf{r}_r, \omega; \mathbf{r}_s) \overline{\widehat{p}(\mathbf{r}_{r'}, \omega'; \mathbf{r}_{s'})} \\
&\quad \times e^{-i\frac{\omega}{c_0}(|\mathbf{r}_r - \mathbf{r}^R| + |\mathbf{r}^R - \mathbf{r}_s|) + i\frac{\omega'}{c_0}(|\mathbf{r}_{r'} - \mathbf{r}^R| + |\mathbf{r}^R - \mathbf{r}_{s'}|)} d\omega d\omega', \tag{25}
\end{aligned}$$

so that the reflector location can be estimated by:

$$\hat{\mathbf{r}}_{\text{ref}} = \arg \max_{\mathbf{r}^S \in S} \mathcal{I}_{\text{CINT}}(\mathbf{r}^S; \Omega_d, X_d) \quad \text{in some search region } S.$$

Along the same lines as in the passive case, we modify the CINT function (25) for active imaging in a moving medium as:

$$\begin{aligned}
\mathcal{I}_{\text{CINT}}(\mathbf{r}^S; \Omega_d, X_d) = & \sum_{\substack{r, r' = 1 \\ |\mathbf{r}_r - \mathbf{r}_{r'}| \leq X_d}}^{N_r} \sum_{\substack{s, s' = 1 \\ |\mathbf{r}_s - \mathbf{r}_{s'}| \leq X_d}}^{N_s} \iint_{|\omega - \omega'| \leq \Omega_d} \widehat{p}(\mathbf{r}_r, \omega; \mathbf{r}_s) \overline{\widehat{p}(\mathbf{r}_{r'}, \omega'; \mathbf{r}_{s'})} \\
& \times e^{-i \frac{\omega}{c_0} (\gamma_D(\mathbf{r}_r, \mathbf{r}^S, \mathbf{v}_0) |\mathbf{r}_r - \mathbf{r}^S| + \gamma_D(\mathbf{r}^S, \mathbf{r}_s, \mathbf{v}_0) |\mathbf{r}^S - \mathbf{r}_s|)} \\
& \times e^{+i \frac{\omega'}{c_0} (\gamma_D(\mathbf{r}_{r'}, \mathbf{r}^S, \mathbf{v}_0) |\mathbf{r}_{r'} - \mathbf{r}^S| + \gamma_D(\mathbf{r}^S, \mathbf{r}_{s'}, \mathbf{v}_0) |\mathbf{r}^S - \mathbf{r}_{s'}|)} d\omega d\omega'. \quad (26)
\end{aligned}$$

### 3. Imaging in a quiescent random medium

In this section the imaging algorithms outlined in Sect. 2 are first applied  
to the case of a quiescent random medium. The same two-dimensional con-  
270 figuration as in [10, 11] and shown in Fig. 1 is considered in order to validate  
the numerical solver used throughout the simulations for both motionless  
and moving media. The array data  $\{p(\mathbf{r}_r, t); 1 \leq r \leq N\}$  of recorded pres-  
sure fields is generated numerically using the computer code SPACE [23, 34]  
275 for computational fluid dynamics (CFD) and computational aero-acoustics  
(CAA). It solves the Euler equations (1) and LEE (4) written as first-order  
symmetric systems by the nodal discontinuous Galerkin (DG) finite-element  
method [26], using flux splitting techniques and an explicit Runge-Kutta  
time-integration scheme. In the typical configuration of Fig. 1 the propaga-  
280 tion medium is considered to be infinite in all directions, thus non-reflective,  
Padé boundary conditions [30] surround the computational domain for the  
numerical simulations. This absorbing layer allows to limit the numerical

echo induced by the boundaries of the finite-element mesh. All computations are performed using the parallel scalar cluster of ONERA [32]. This  
285 cluster has a total of 17,360 cores for a peak performance of 667 Tflop/s. The post-processing of all results is done using Matlab<sup>©</sup>. The imaging functions are normalized and their range is  $[0, 1]$ . In addition, in order to compare the results obtained by the KM and CINT algorithms, the CINT imaging function  $|\mathcal{I}_{\text{CINT}}|$  and the squared KM imaging function  $|\mathcal{I}_{\text{KM}}|^2$  are formed  
290 because  $|\mathcal{I}_{\text{CINT}}| \propto |\mathcal{I}_{\text{KM}}|^2$  as we have seen in (24).

### 3.1. Model setup for numerical simulations

The setup for numerical validation is shown in Fig. 1 where dimensions are given in terms of the central wavelength  $\lambda_0$ . The horizontal axis is the range and the vertical axis along which the array is aligned is the cross-range.  
295 This array contains  $N = 185$  transducers at a distance  $\lambda_0/2$  from each other, with an aperture  $a = 92\lambda_0$ . The object to be imaged is at a range  $L = 90\lambda_0$  and zero cross-range, and it is either constituted by three sources (two at the forefront  $6\lambda_0$  apart from each other and one in the rear at  $3\lambda_0$  from the others) emitting the same signals  $t \mapsto f(t)$  simultaneously in the passive  
300 configuration, or three non penetrable disks of radius  $\lambda_0/2$  centered at the same points with homogeneous Neumann boundary conditions in the active configuration. In this latter case, the central transducer of the array emits the probing pulse  $t \mapsto f(t)$  and all other transducers and this one are used as receivers. The pulse is (the derivative of a Gaussian):

$$f(t) = -\omega_0^2 t e^{-\frac{1}{2}\omega_0^2 t^2}, \quad (27)$$

305 where  $\omega_0 = 2\pi f_0$  is the central (angular) frequency such that  $\lambda_0 = \underline{c}/f_0$  and  $\underline{c}$  is the average speed of sound. We choose  $f_0 = 1$  kHz as in [10]. For this central frequency, the bandwidth of the signal is  $[0.6, 1.3]$  kHz. All array data in the bandwidth  $[0, 1.5]$  kHz have been subsequently post-processed to build the KM and CINT imaging functions.

310 To simulate the KM and CINT imaging processes in clutter, we consider a quiescent random medium with  $\mathbf{v}_0 = \mathbf{0}$ ,  $\varrho_0 = \text{constant}$ , and a random speed of sound  $c_0(\mathbf{r}) = \underline{c}(1 + \sigma\mu(\mathbf{r}))$ , where  $\underline{c} = \text{constant}$  is the average value,  $\sigma$  is the relative standard deviation, and  $(\mu(\mathbf{r}), \mathbf{r} \in \mathbb{R}^2)$  is a homogeneous (stationary), mean-zero second-order random process. A Gaussian covariance  
315 model is chosen for that process, namely:

$$\mathcal{R}_\mu(\mathbf{r}, \mathbf{r}') := \mathbb{E} \{ \mu(\mathbf{r}) \mu(\mathbf{r}') \} = \exp \left[ -\frac{1}{2} \left( \frac{|\mathbf{r} - \mathbf{r}'|}{\ell_c} \right)^2 \right], \quad (28)$$

corresponding to smooth samples. Here  $\mathbb{E} \{ \cdot \}$  stands for the mathematical expectation, and  $\ell_c$  is the correlation length of the random fluctuations  $\mu$  of the speed of sound. These fluctuations are simulated by a random Fourier series of the stationary process  $\mu(\mathbf{r})$ ; see for example [35, 37]. A typical  
320 realization of the random speed of sound is shown in Fig. 1 for a correlation length  $\ell_c$  which is one-half the central wavelength  $\lambda_0$  for the sources, and a standard deviation  $\sigma = 3\%$ . The cluttered medium in Fig. 1 and subsequent simulations corresponds to an average speed of sound  $\underline{c} = 3000$  m/s and wavelength  $\lambda_0 = 3$  m at the central frequency  $f_0 = 1$  kHz. The correlation  
325 length is  $\ell_c = \lambda_0/2 = 1.5$  m. This is a delicate and interesting situation to deal with, since this wavelength is *a priori* required to image objects of its size and the clutter in which they are embedded has also the same characteristic

length.

The same mesh is used for all our DG simulations in this section and the  
330 subsequent Sect. 4 where a moving random medium is considered. It consists  
in triangular and quadrangular elements with 3 and 4 vertices respectively,  
and includes about  $1.7 \times 10^5$  vertices and  $1.8 \times 10^5$  elements. Fig. 2 shows a  
zoom on the mesh around the three reflectors to be imaged in the active con-  
figuration. For the central frequency  $f_0 = 1000$  Hz and the average speed of  
335 sound  $\underline{c} = 3000$  m/s, this corresponds to about 5 to 10 nodes per wavelength  
in the most refined area. We use a mixed finite element mesh with refined  
elements of polynomial interpolation order 2 close to the reflectors (shown  
in blue on Fig. 2) and coarser elements of polynomial interpolation order 5  
far from the reflectors (shown in red on Fig. 2) to evade possible numerical  
340 instabilities for a moving random medium. In [10], a piecewise polynomial  
interpolation of degree 1 on regular four-node quadrilateral elements with  
30 nodes per wavelength has been considered, as well as a mixed finite el-  
ement method for spatial integration and perfectly matched layers (PML)  
[5] to surround the computational domain. They also used a second-order  
345 leapfrog scheme [3, 4] for temporal integration, while we use a second-order  
Runge-Kutta explicit scheme [23, 34]. Some differences will thus be observed  
in the resolution of the results obtained here compared to those obtained in  
[10]. However, the DG method considered in this research for the simula-  
tions allows to increase the order of the mesh and polynomial interpolation  
350 straightforwardly.

Numerically generated data recorded at the array are shown in Fig. 3  
for the active configuration (localization of reflectors). The central sensor of

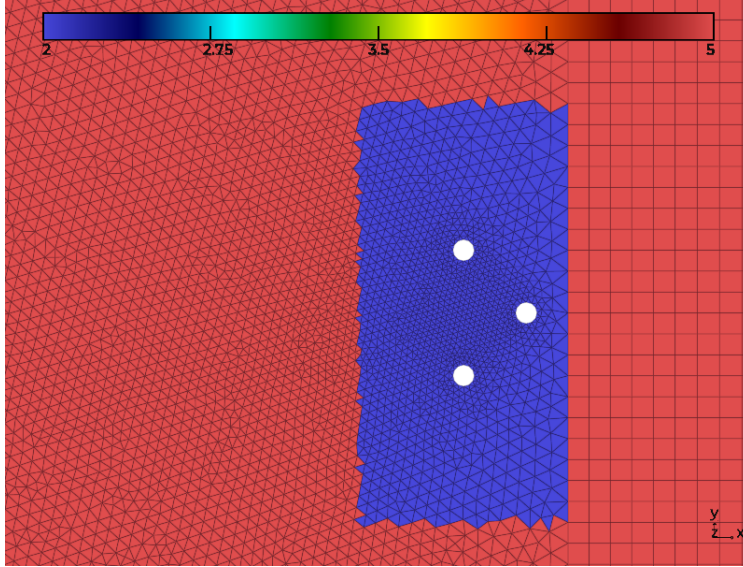


Figure 2: Mesh used for the validation of the KM and CINT imaging functions in a motionless and moving random medium. Zoom around the three reflectors to be imaged in the active case. The blue elements have polynomial interpolation order 2 and the red elements have polynomial interpolation order 5.

the array is used as a source, and all the sensors of the array are used as  
as receivers. In the active configuration wavefronts have travelled twice the  
355 distance from the array to the reflectors before being recorded. We clearly  
distinguish the echoes of the signal for each reflector in the homogeneous  
case (Fig. 3, left). In addition, the signals are symmetric with respect to the  
central receiver. The effects of the heterogeneity of the speed of sound in  
the random medium are clearly visible on these time traces (Fig. 3, right).  
360 It is much more difficult to distinguish the wavefronts and the echoes of the  
three reflectors since the signals are noisy. The causes of this noise are the  
multiple scattering of acoustic waves on the inhomogeneities present in the  
random medium. Even if the typical amplitude of the inhomogeneities is

weak ( $\sigma \ll 1$ ), the range  $L$  is large with respect to  $\lambda_0$  and  $\ell_c$  and there are  
 365 significant multiple scattering effects. In addition, the noise will be different  
 from one realization of the medium to another.

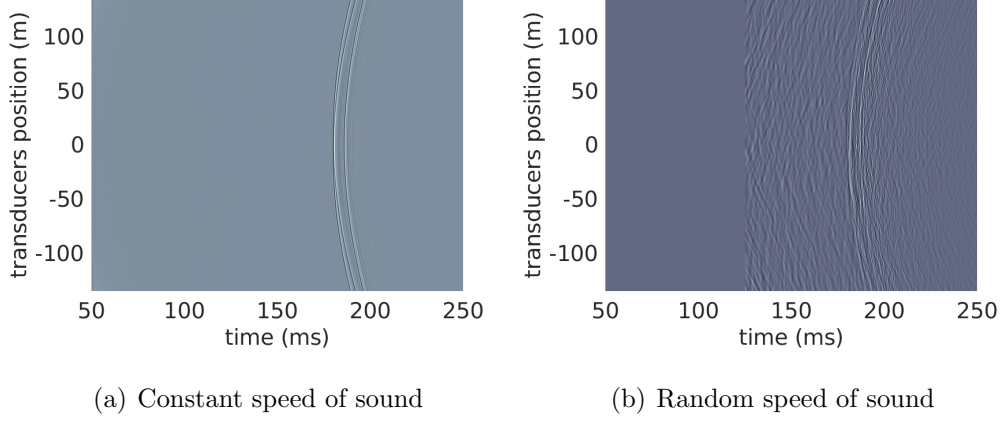


Figure 3: Active imaging in a quiescent medium in the configuration of Fig. 1. (a) Time traces recorded at the receivers for a constant speed of sound  $\underline{c} = 3000$  m/s. (b) Time traces recorded at the receivers for a random speed of sound with average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . The horizontal axis is time (in ms) and the vertical axis is the array transducer location (in m).

### 3.2. Active imaging

We first consider the localization of three reflectors using the KM imaging function (18) and the CINT imaging function (25) with  $N_r = N = 185$  and  
 370  $N_s = 1$ . The search domain is a square of size  $20\lambda_0 \times 20\lambda_0$  centered around  $(90\lambda_0, 0)$ . The results obtained for the (square) KM image in a homogeneous medium with constant speed of sound are shown in Fig. 4 for a pixel size of  $\lambda_0/2$ . The three reflectors are actually found in the middle of the search region and their positions are precisely localized by the brightest pixels of

375 the KM imaging function. This result validates both the efficiency of KM active imaging in homogeneous media, and the ability of our code to correctly simulate acoustic wave propagation with negligible numerical dispersion.

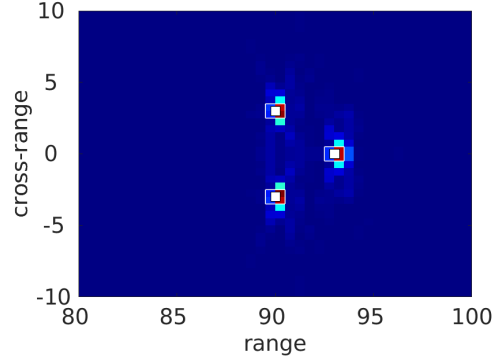


Figure 4: KM active imaging in a quiescent medium in the configuration of Fig. 1 with a constant speed of sound  $\underline{c} = 3000$  m/s. The reflectors to be localized are shown by white squares. Range and cross-range dimensions are in units of  $\lambda_0$ .

The results obtained for the (square) KM images and CINT images in a random medium are shown in Fig. 5 for two different realizations of the random speed of sound with the same average and standard deviation. The  
 380 ineffectiveness of the KM imaging algorithm is apparent in that we observe noisy images that are different from one realization of the medium to another, and are thus statistically unstable. Indeed the KM algorithm back-propagates all the noise contained in the signals recorded by the receivers, but this noise is not canceled by the Green's function  $\hat{\mathcal{G}}_0$  of the homogeneous  
 385 ambient medium playing here the role of a fictitious medium. We do not get sharp peaks around the positions of the three different reflectors as in the case of an homogeneous medium. The random phases present in the signals in the Fourier domain are not satisfactorily compensated by back-propagation (the

390 complex conjugates of the Fourier Green's functions), contrary to what is  
 done when empirical cross-correlations instead of the signals themselves are  
 back-propagated. Using the CINT algorithm, we can cancel some parts of  
 the random phases present in the signals recorded at the receivers and arising  
 from the multiple scattering of the acoustic waves on the inhomogeneities of  
 395 the medium. The influence of the realization of the random medium can  
 be mitigated as can be seen on Fig. 5 where CINT images are relatively  
 stable and free of noise. Nevertheless the cross-range and range resolutions  
 are slightly altered, as expected. The peaks centered at each reflector are  
 rather blurry here, as a result of the smoothing of images induced by the  
 400 CINT algorithm. Forming good images is based on a trade-off between the  
 smoothing necessary to compensate the noise, and the blurring that it im-  
 plies. This trade-off is obtained by a relevant choice of the parameters  $\Omega_d$   
 and  $X_d$  of the CINT imaging function (25). The choice of an optimal de-  
 coherency frequency  $\Omega_d$  contributes to enhance range resolution, while the  
 405 choice of an optimal decoherency length  $X_d$  contributes to enhance cross-  
 range resolution. In Fig. 5 the “optimal” choice  $\Omega_d = 0.1B$  and  $X_d = 0.8a$   
 for a stable image with the least blurring has been found incrementally by  
 successive tests. However an optimal set of parameters can be obtained using  
 the adaptive algorithm of [11], which uses an optimization criterion based on  
 410 the quality of the image as it is formed. We postpone this perspective to  
 future works, and consider again that the achieved resolution validates the  
 CINT algorithm in quiescent media for its extension to moving media in the  
 next Sect. 4.

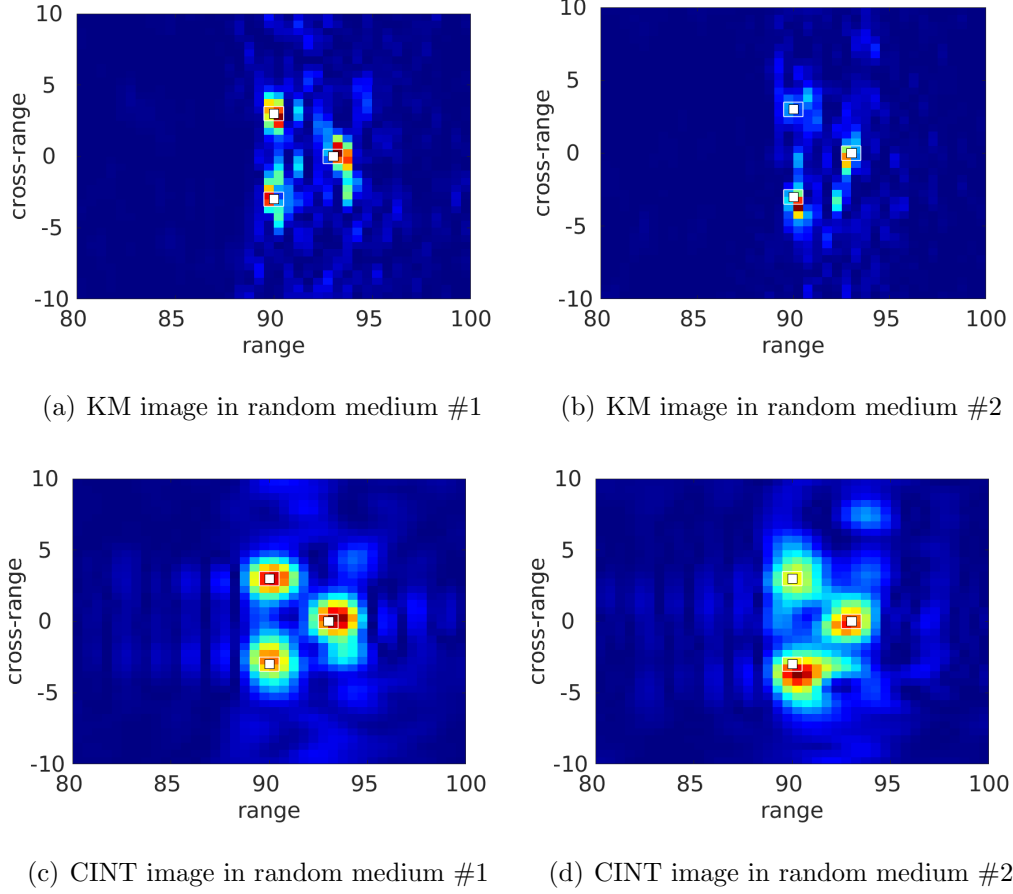


Figure 5: Active imaging in a quiescent medium in the configuration of Fig. 1 with a random speed of sound of average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . Comparison of KM and CINT images for two realizations of the random medium: (a) Squared KM image for the first realization of the medium; (b) Squared KM image for the second realization of the medium; (c) CINT image for the first realization of the medium; (d) CINT image for the second realization of the medium. The CINT parameters  $\Omega_d = 0.1B$  and  $X_d = 0.8a$  are used for both media. The reflectors to be localized are shown by white squares  $\square$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

### 3.3. Passive imaging

415 We now turn to the localization of three sources using the KM imaging function (15) and the CINT imaging function (22) with  $N = 185$ . In passive configuration, we note that the KM algorithm is able to find the sources, so there is little interest using the CINT algorithm to the extent that much less time is required to produce an image by the former algorithm. We see on 420 Fig. 6 that both imaging functions find the three sources with a good resolution. Indeed in the passive setup the signal emitted by the sources travels through the random medium only once, which is not enough to be sufficiently scattered and put at fault the KM algorithm. Higher levels of randomness (standard deviation  $\sigma$ ) yield noisier signals which could invalidate this ob- 425 servation. We also may observe that the localization of the rear source at range  $93\lambda_0$  is less precise than that of the forefront sources at range  $90\lambda_0$ . In [10] though the rear source was at  $6\lambda_0$  from the forefront sources, a slightly more favorable situation than the present one. In the next section we will only consider the active imaging configuration to illustrate the interests of 430 the CINT algorithm compared to the KM algorithm.

## 4. Imaging in a moving random medium

In this section, we consider again the configuration depicted in Fig. 1 where the ambient medium is now moving at the velocity  $\mathbf{v}_0$  which may be either uniform, or randomly perturbed around its average uniform value. We 435 first assume that the speed of sound is constant in order to highlight the role of the Doppler compensation factor (16) for the KM and CINT imaging algorithms in the moving medium. The speed of sound is also randomly

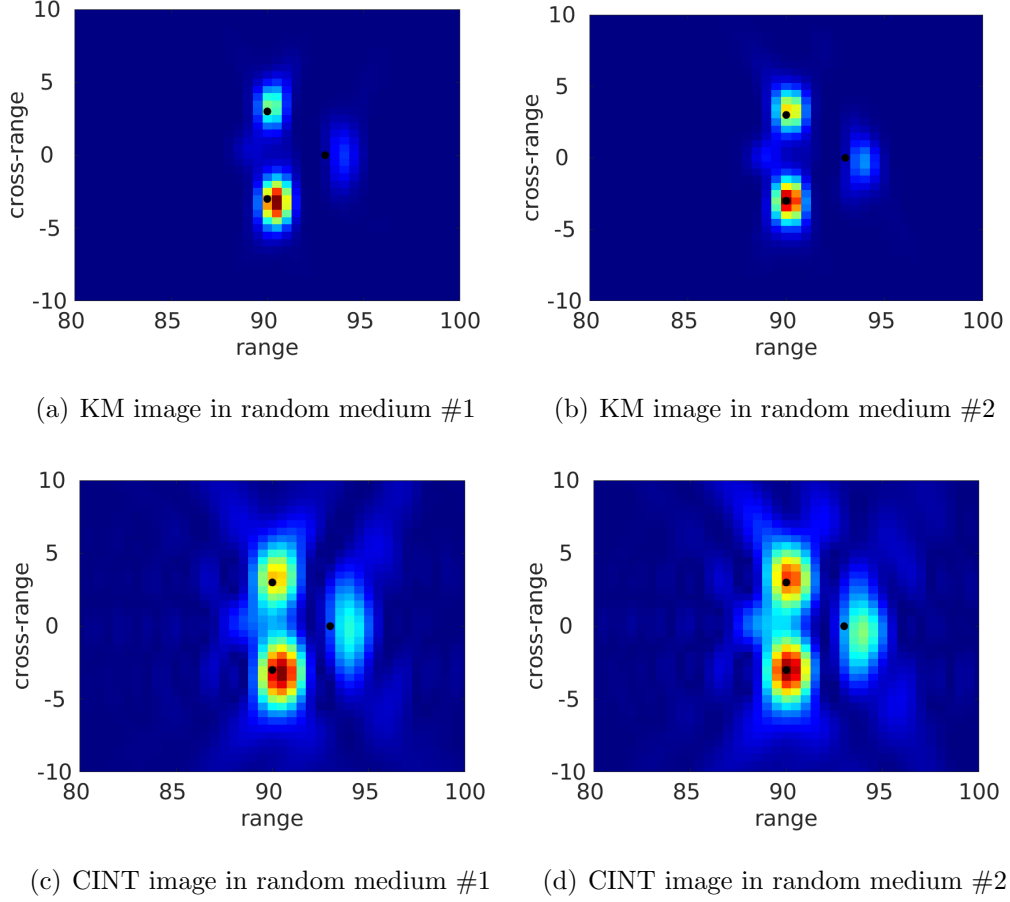


Figure 6: Passive imaging in a quiescent medium in the configuration of Fig. 1 with a random speed of sound of average  $\bar{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . Comparison of KM and CINT images for two realizations of the random medium: (a) Squared KM image for the first realization of the medium; (b) Squared KM image for the second realization of the medium; (c) CINT image for the first realization of the medium; (d) CINT image for the second realization of the medium. The CINT parameters  $\Omega_d = 0.25B$  and  $X_d = 0.85a$  are used for both media. The sources to be localized are shown by dots  $\bullet$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

perturbed around its average value, as in the foregoing section. We note that the average speed of sound considered here is unchanged from the previous  
440 section where it is  $\underline{c} = 3000$  m/s. This value rather corresponds to solid media and is unrealistic for aeroacoustic applications, however it is kept here for comparison purposes. In Sect. 5 more realistic speed of sound and jet velocity are chosen.

#### 4.1. Active imaging in a random medium moving at constant velocity

445 The ambient medium is moving at a constant velocity  $\mathbf{v}_0 = \underline{c} \times (0, M)$  in the cross-range upward direction with Mach number  $M = 0.3$  and average speed of sound  $\underline{c} = 3000$  m/s. We use the KM imaging function (20) and CINT imaging function (26) with  $N_r = N = 185$  and  $N_s = 1$  to localize the three fixed reflectors in Fig. 1 (active configuration). The central transducer  
450 of the array is again used as the single source with the emitted signal equal to (27). Numerically generated data recorded at the array are shown in Fig. 7 for either a constant or a random speed of sound. Because the ambient medium is now moving upward in the cross-range direction, we note that the symmetry with respect to the transducer used as a source is lost compared to  
455 Fig. 3. We thus understand that this phenomenon has to be compensated by a correction factor in our imaging functions. This is the role of the Doppler compensation factor  $\gamma_D$  of Eq. (16). In Fig. 7, the different echoes of the signal on the reflectors are still observable. Thus if the compensation factor is correct, we should be able to localize each reflector at least for a constant  
460 speed of sound.

In order to highlight the role of the Doppler compensation factor, we compare in Fig. 8 the KM imaging function (18) (without  $\gamma_D$ , left) with

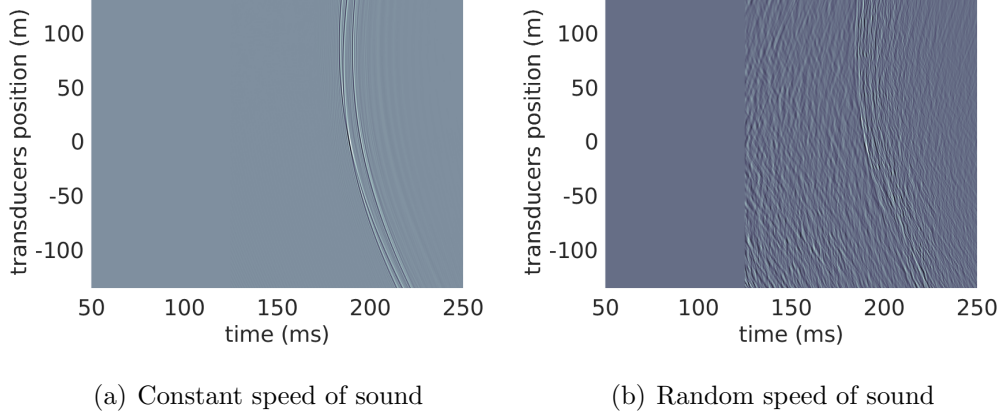


Figure 7: Active imaging in a moving medium in the configuration of Fig. 1 with constant velocity  $M = 0.3$  in the cross-range upward direction. (a) Time traces recorded at the receivers for a constant speed of sound  $\underline{c} = 3000$  m/s. (b) Time traces recorded at the receivers for a random speed of sound with average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . The horizontal axis is time (in ms) and the vertical axis is the array transducer location (in m).

the KM imaging function (20) (with  $\gamma_D$ , right). The moving medium has a constant speed of sound and the search domain is a square of size  $20\lambda_0 \times 20\lambda_0$  centered around  $(90\lambda_0, 0)$ . When  $\gamma_D$  is ignored, the positions of the three reflectors cannot be identified at all since the signals are back-propagated in a fictitious medium at rest. Conversely, when  $\gamma_D$  is taken into account in the KM imaging function, these positions can be identified relatively well. Nevertheless, we notice that there is a slight shift for the top reflector. There can be several explanations: discretization errors (mesh, solver), imperfect reflections of the waves on the reflectors and/or imperfect absorption on the edges of the computational domain, or most likely errors induced in the model by the compensation factor  $\gamma_D$  which is only a first-order corrector. From

now on,  $\gamma_D$  will be considered to form all KM and CINT images.

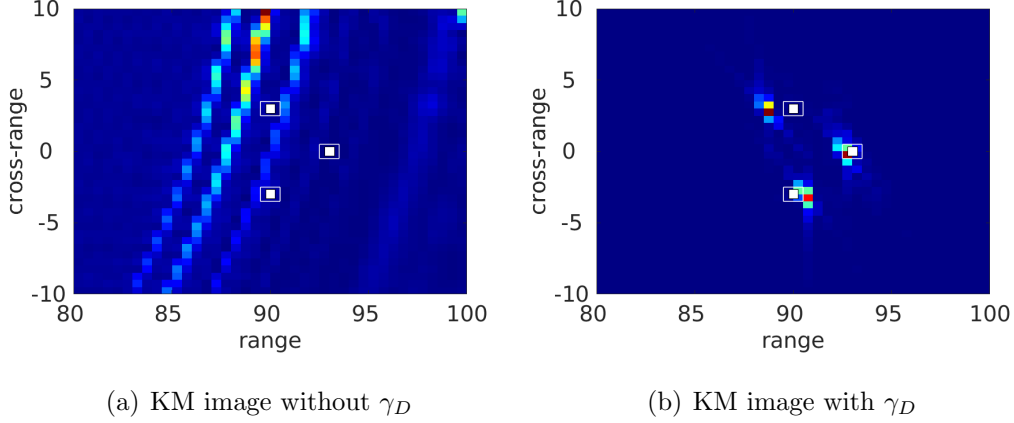


Figure 8: KM active imaging in a moving medium in the configuration of Fig. 1 with constant velocity  $M = 0.3$  in the cross-range upward direction and constant speed of sound  $\underline{c} = 3000$  m/s. Influence of the Doppler compensation factor  $\gamma_D$ : (a) KM image (18) without  $\gamma_D$ ; (b) KM image (20) with  $\gamma_D$ . The reflectors to be localized are shown by white squares  $\square$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

475 Now the ambient medium moving at the constant velocity  $M = 0.3$  in the cross-range upward direction has a random speed of sound with average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . The KM imaging function for two realizations of the medium is shown in Fig. 9. As in Fig. 5, we observe noisy images that differ from one realization to another. We thus form the  
480 CINT imaging function (26) from the signals recorded by the receivers. The "optimal" choice of  $\Omega_d$  and  $X_d$  is found incrementally by successive tests as in the previous experiments of Sect. 3. The results can be seen in Fig. 9 alike. We show the results obtained with two realizations of the random medium and we observe the same behaviors as in Sect. 3: the KM algorithm  
485 is statistically unstable while the CINT algorithm is statistically stable. For

the KM function of Fig. 9 (top), we have difficulties finding the positions of the three reflectors since the image is noisy. For the CINT function of Fig. 9 (bottom), the positions of the three reflectors appear much more clearly. The uncertainties present on the image obtained by the KM algorithm have  
490 practically vanished. Nevertheless, we have some blurring that comes from the smoothing induced by the CINT algorithm, as expected. These images could be improved by the adaptive algorithm of [11] though.

#### 4.2. Active imaging in a random medium moving at random velocity

The ambient medium is now moving at a random velocity  $\mathbf{v}_0 = \underline{c} \times$   
495  $(\sigma\mu_1(\mathbf{r}), M(1+\sigma\mu_2(\mathbf{r})))$  in the cross-range upward direction with Mach number  $M = 0.3$ ,  $\underline{c} = 3000$  m/s, and  $\sigma = 3\%$ . The disturbances  $(\mu_1(\mathbf{r}), \mathbf{r} \in \mathbb{R}^2)$  and  $(\mu_2(\mathbf{r}), \mathbf{r} \in \mathbb{R}^2)$  are stationary, mean-zero and independent second-order random processes. Gaussian covariance functions (28) are chosen for both of them with identical correlation lengths. These perturbations are simu-  
500 lated by random Fourier series of stationary processes [35, 37]. We note that this random ambient velocity  $\mathbf{v}_0$  does not necessarily solve the ambient flow equations (3) and the covariance functions of its turbulent components do not fulfill the necessary condition stated in [2, 29, 36]. This simplified model is a first attempt to take into account turbulent phenomena with the KM  
505 and CINT imaging algorithms. More realistic models shall be envisaged in future works.

Numerically generated data recorded at the array are shown in Fig. 10 for either a constant or a random speed of sound. Again, the symmetry with respect to the transducer used as a source—the central one—is lost. Compared  
510 to the moving medium with constant velocity, we observe here echoes fairly

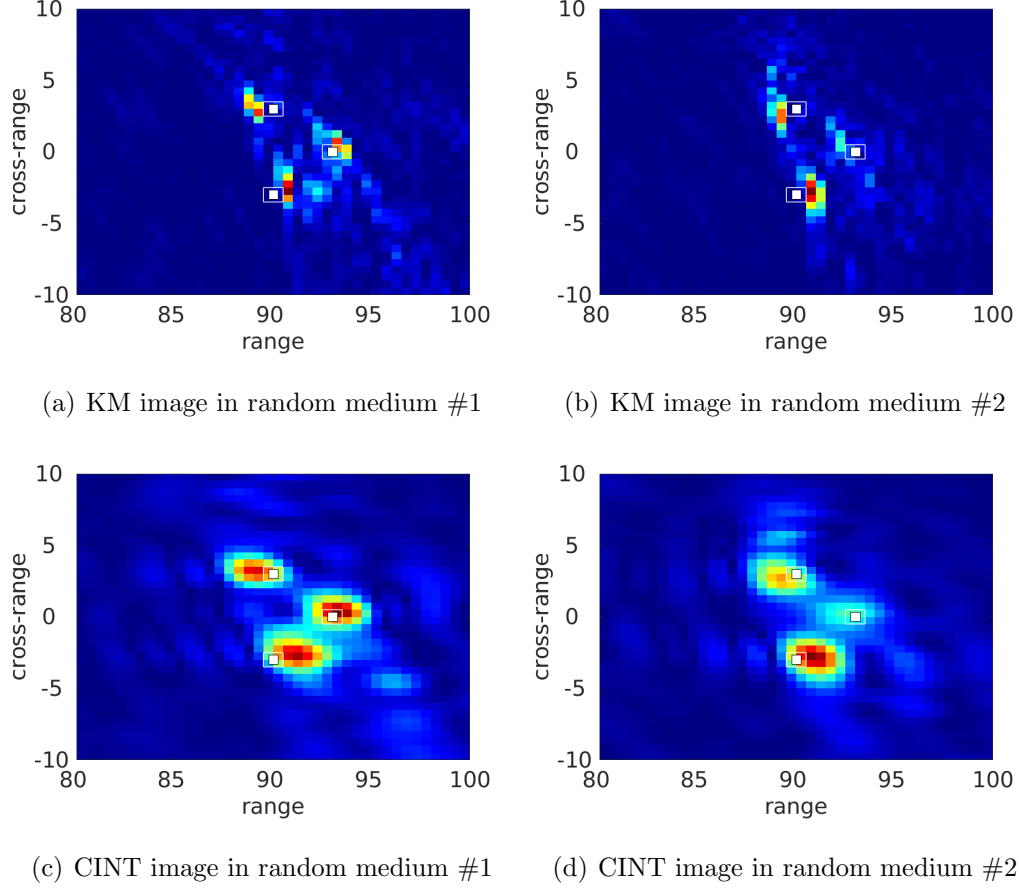


Figure 9: Active imaging in a moving medium in the configuration of Fig. 1 with constant velocity  $M = 0.3$  in the cross-range upward direction and random speed of sound with average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . Comparison of KM and CINT images for two realizations of the random medium: (a) Squared KM image for the first realization of the medium; (b) Squared KM image for the second realization of the medium; (c) CINT image for the first realization of the medium; (d) CINT image for the second realization of the medium. The CINT parameters  $\Omega_d = B/12$  and  $X_d = 0.9a$  are used for both media. The reflectors to be localized are shown by white squares  $\square$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

close to the echoes in Fig. 7 but noisier. This is induced by the velocity of the ambient medium which is now random. Thus, the waves propagating in this medium will also be noisier. Even in the presence of this noise, we still see the different fronts representing the echoes of the signal on the three reflectors.

515 The role of the Doppler compensation factor  $\gamma_D$  is also highlighted in Fig. 11. Here the KM imaging function (18) (without  $\gamma_D$ , left) and the KM imaging function (20) (with  $\gamma_D$ , right) for one realization of the random velocity  $\mathbf{v}_0$  of the ambient medium are shown. The compensation factor is computed for the average velocity  $\underline{c} \times (0, M)$  of the ambient medium. The search domain

520 is again a square of size  $20\lambda_0 \times 20\lambda_0$  centered around  $(90\lambda_0, 0)$ . The KM algorithm accounting for the Doppler compensation factor works well for this configuration (constant speed of sound) even if the ambient velocity is random.

Images obtained by the KM algorithm for two realizations of the ambient

525 medium with random velocity and random speed of sound are shown in Fig. 12. Again, we observe the statistical instability of the KM functions, since the positions of the reflectors can not be determine unambiguously for any realization of the medium. We thus form the CINT imaging function (26) from the signals recorded by the receivers. The "optimal" choice of  $\Omega_d$  and

530  $X_d$  is found incrementally by successive tests as in the previous experiments. The results can be seen in Fig. 12 alike. We show the results obtained with two realizations of the medium and we can make the same observations as in Sect. 3. Using the KM function (Fig. 12, top), the positions of the three reflectors can not be distinguished. On the other hand, using the

535 CINT function (Fig. 12, bottom), the positions of the three reflectors can be

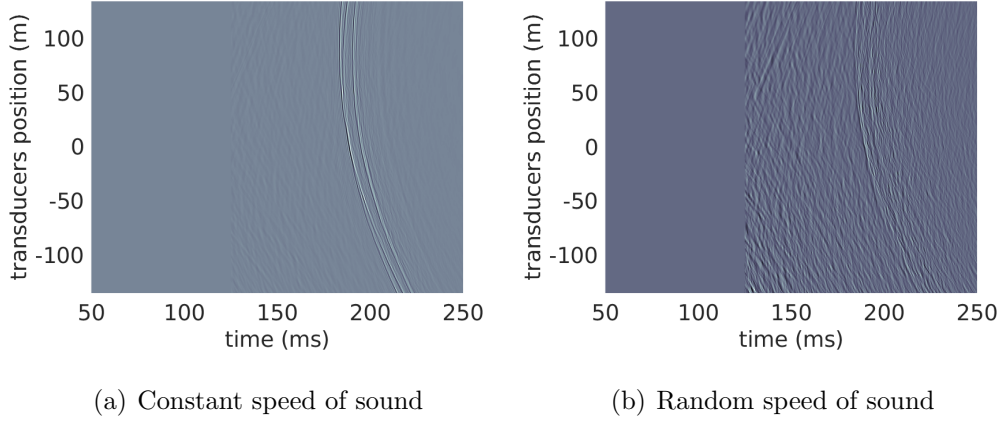


Figure 10: Active imaging in a moving medium in the configuration of Fig. 1 with random velocity with average  $M = 0.3$  in the cross-range upward direction. (a) Time traces recorded at the receivers for a constant speed of sound  $\underline{c} = 3000$  m/s. (b) Time traces recorded at the receivers for a random speed of sound with average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . The horizontal axis is time (in s) and the vertical axis is the array transducer location (in m).

distinguished much more easily. Two issues are worth noticing though. First, a loss in resolution due to smoothing is observed. Second, slight offsets of the positions of the reflectors (of the order of a few pixels) are observed. This phenomenon can be explained by the fact that the Doppler compensation  
540 factor  $\gamma_D$  is a first order correction term, and to a lesser extent by the possible spurious reflections of the waves on the boundaries of the numerical domain.

## 5. Passive imaging through a synthetic turbulent jet flow

In this section we finally aim at imaging sources through a synthetic turbulent jet flow using the KM and CINT algorithms. A sketch of the  
545 configuration considered here is shown in Fig. 13. This case study is inspired

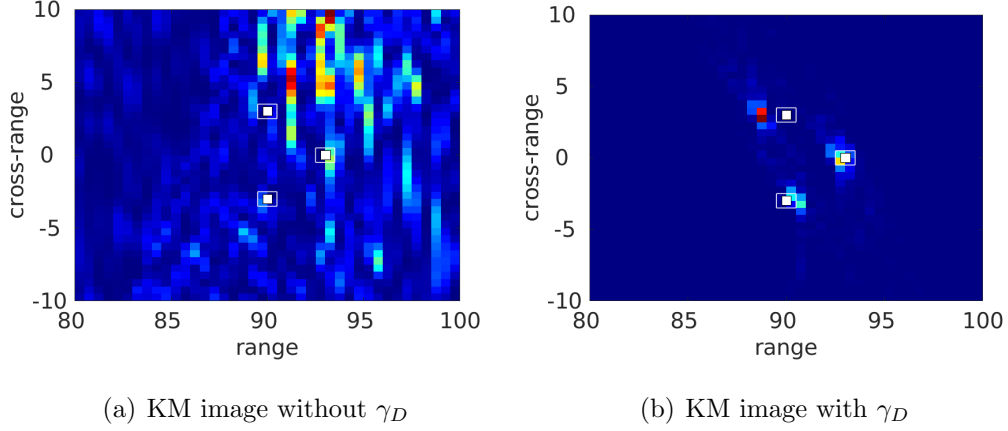


Figure 11: KM active imaging in a moving medium in the configuration of Fig. 1 with random velocity with average  $M = 0.3$  in the cross-range upward direction and constant speed of sound  $c = 3000$  m/s. Influence of the Doppler compensation factor  $\gamma_D$ : (a) KM image (18) without  $\gamma_D$ ; (b) KM image (20) with  $\gamma_D$ . The reflectors to be localized are shown by white squares  $\square$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

by the experiments conducted by Candel *et al.* in the seventies [18, 19, 20] at the low speed open wind tunnel of the Von Kármán institute, and more recently by Kröber *et al.* [31] at the Aeroacoustic Wind Tunnel Braunschweig (AWB) facility, and by Sijtsma *et al.* [38] at the DNW (the German-Dutch  
550 Wind Tunnels) PLST wind tunnel. The jet inflow boundary conditions on the left side of Fig. 13 yield two sub-domains with average ambient flow velocities  $|\mathbf{v}_0| = U_1 = 100$  m/s and  $|\mathbf{v}_0| = U_2 = 50$  m/s, respectively, with turbulent shear layers in between. Our goal is to image point sources lying in the first medium with an array of sensors placed in the second medium—that  
555 is, a passive imaging configuration in the terminology used in the foregoing sections.

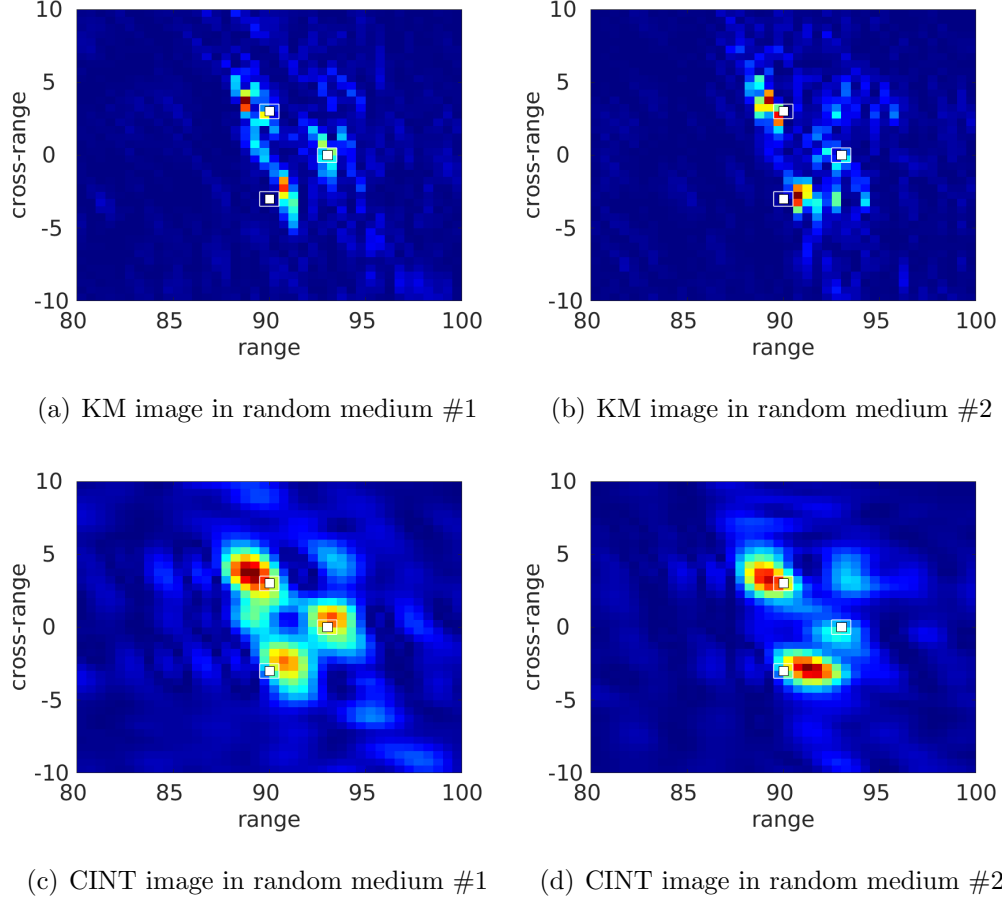


Figure 12: Active imaging in a moving medium in the configuration of Fig. 1 with random velocity with average  $M = 0.3$  in the cross-range upward direction and random speed of sound with average  $\underline{c} = 3000$  m/s and standard deviation  $\sigma = 3\%$ . Comparison of KM and CINT images for two realizations of the random medium: (a) Squared KM image for the first realization of the medium; (b) Squared KM image for the second realization of the medium; (c) CINT image for the first realization of the medium; (d) CINT image for the second realization of the medium. The CINT parameters  $\Omega_d = 0.09B$  and  $X_d = 0.9a$  are used for both media. The reflectors to be localized are shown by white squares  $\square$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

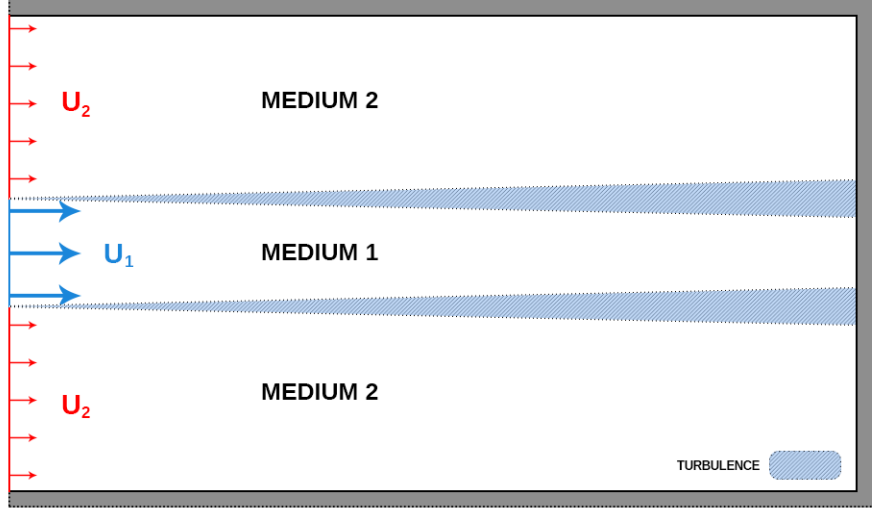


Figure 13: Synthetic jet flow configuration:  non-reflection Padé boundary conditions; — jet inflow boundary condition for the central zone with  $U_1 = 100$  m/s; — jet inflow boundary condition outside the central zone with  $U_2 = 50$  m/s.

### 5.1. Synthetic jet model

The data for this generic jet configuration are synthesized numerically in two steps as follows:

- 560 • First, we simulate the ambient shear flow by solving the Euler equations (1) using the DG solver SPACE [23, 34]; this is the CFD step. In order to generate turbulence, viscosity phenomenon must be present. By definition, Euler equations are applicable to adiabatic and inviscid flows. Nevertheless, some viscosity is actually generated by the numerical scheme. At first, we will use this numerical viscosity to simulate  
565 the turbulent shear layers.
- Second, we simulate the propagation of acoustic waves in the ambient

flow obtained in the CFD step by solving the linearized Euler equations (4) using again the DG solver SPACE [23, 34]; this is the CAA step. In a first approximation, we will consider that the acoustic phenomena are much faster than the fluidic phenomena. As a result, the ambient flow will be considered as "frozen" (time independent). The flow obtained at the last time increment of the CFD step will be used as the carrier (ambient) flow for the CAA step.

Of course the ambient flow obtained by the foregoing computation is poorly resolved and cannot be considered as a realistic jet flow. We are actually not interested in computing precisely the turbulent structures for this jet configuration. Our aim is rather to test the KM and CINT imaging algorithms in such a heterogeneous medium. The turbulent layers as resolved by the present numerical scheme are sufficient to exhibit and discuss the main features of these algorithms. These complex structures will play the role of the "clutter" of the idealized experiments of Sect. 3 and Sect. 4.

### 5.2. Imaging setup

A parameterization of the imaging setup for the synthetic jet flow of Fig. 13 is shown in Fig. 14. We seek to determine the positions of three point sources of which emitted signals go through a turbulent shear layer. All sources emit the same signal given by Eq. (27). The central frequency is here  $f_0 = 50$  kHz. The fluid studied is the air defined by an average speed of sound  $\underline{c} = 340$  m/s at the temperature  $T = 20^\circ\text{C}$ . This corresponds to a wavelength  $\lambda_0 = 6.8 \cdot 10^{-3}$  m. The remote array contains  $N = 45$  sensors at a distance  $\lambda_0/2$  from each other (a very dense array).

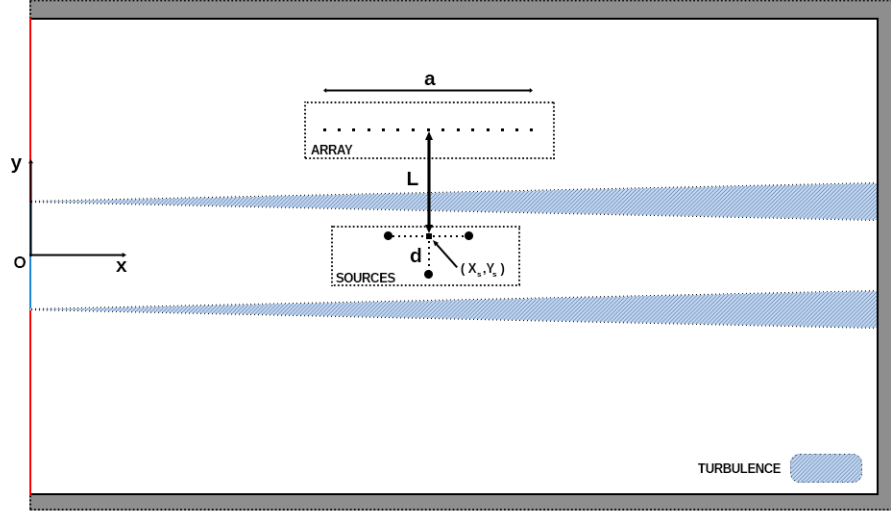


Figure 14: Synthetic jet flow configuration: imaging setup.  $a$  is the aperture of the sensors array,  $L$  is the distance between the central sensor and the mid-point  $(X_s, Y_s)$  of the two upper sources which are  $d$  apart, and the lower source is also at the distance  $d$  from the upper sources.

### 5.3. Flow computation

The same mesh is used for both the CFD and CAA steps. It is constructed so that there are 30 elements per wavelength  $\lambda_0$  (the central wavelength of the source) for a mesh size of  $100\lambda_0 \times 100\lambda_0$ . We thus have  $3000 \times 3000$  elements, that is a total of  $9 \cdot 10^6$  elements. The mesh is regular and constituted by four-node quadrilateral elements. The base flow computed in the CFD step is shown in Fig. 15. As a first approximation, we will consider it as frozen and use it as the ambient flow for testing the KM and CINT imaging algorithms.

We first notice the development of a turbulent shear layer at the interfaces between the parts of the jet having different inflow velocities. This turbulent layer arises from the inflow velocity difference: 100 m/s for the first medium

located between  $-10\lambda_0$  and  $10\lambda_0$  along the range axis  $y$  (the first medium), and 50 m/s elsewhere (the second medium).

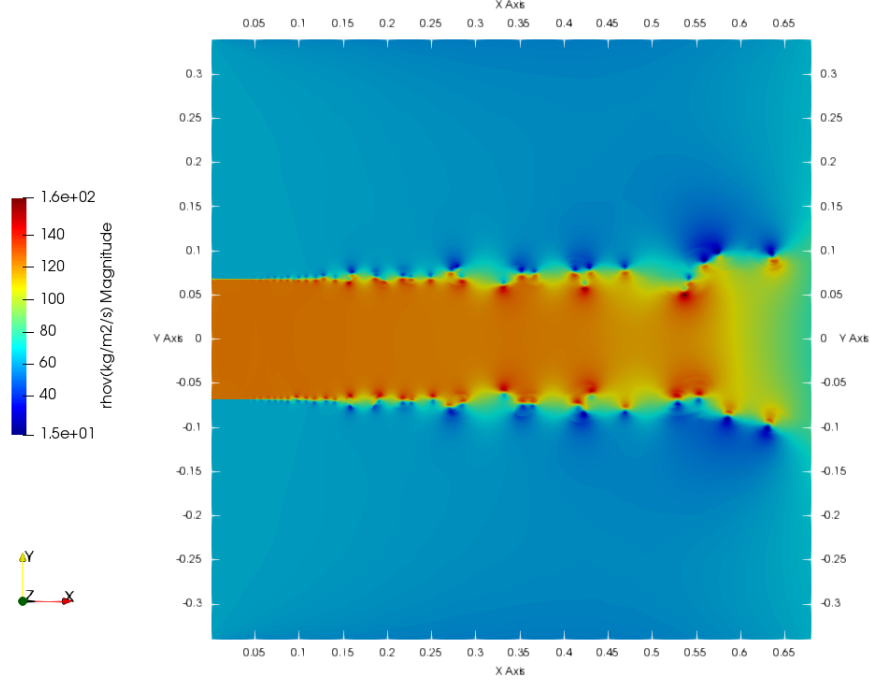


Figure 15: Base flow obtained by solving the Euler equations (CFD step) using a DG finite element method for spatial discretization and a Runge-Kutta method for time discretization for the synthetic jet configuration of Fig. 13. The color gradient displays the norm of the momentum  $|\rho v|$ .

#### 605 5.4. Refraction compensation mechanism

In addition to the Doppler compensation factor  $\gamma_D$  of Eq. (16) which accounts for the convection effects, we must consider the fact that the acoustic waves generated by the source in the first medium will travel through media possibly with different speeds of sound; see Fig. 16. Therefore we introduce

610 a refraction compensation mechanism in the imaging functions introduced in Sect. 2. In this context the KM passive imaging function (17) and CINT passive imaging function (23) take the form:

$$\mathcal{I}_{\text{KM}}(\mathbf{r}^S) = \sum_{r=1}^N p(\mathbf{r}_r, \gamma_{D_1}(\mathbf{r}^S, \mathbf{r}_{\mathcal{O}}, U_1 \hat{\mathbf{e}}_x) T_1 + \gamma_{D_2}(\mathbf{r}_{\mathcal{O}}, \mathbf{r}_r, U_2 \hat{\mathbf{e}}_x) T_2) , \quad (29)$$

and:

$$\begin{aligned} \mathcal{I}_{\text{CINT}}(\mathbf{r}^S; \Omega_d, X_d) = & \sum_{\substack{q, r=1 \\ |\mathbf{r}_q - \mathbf{r}_r| \leq X_d}}^N \iint_{|\omega - \omega'| \leq \Omega_d} \mathcal{C}_F(\mathbf{r}_q, \mathbf{r}_r, \omega, \omega') \\ & \times e^{-i\omega(\gamma_{D_1}(\mathbf{r}^S, \mathbf{r}_{\mathcal{O}}, U_1 \hat{\mathbf{e}}_x) T_1 + \gamma_{D_2}(\mathbf{r}_{\mathcal{O}}, \mathbf{r}_q, U_2 \hat{\mathbf{e}}_x) T_2)} \\ & \times e^{i\omega'(\gamma_{D_1}(\mathbf{r}^S, \mathbf{r}_{\mathcal{O}'}, U_1 \hat{\mathbf{e}}_x) T'_1 + \gamma_{D_2}(\mathbf{r}_{\mathcal{O}'}, \mathbf{r}_r, U_2 \hat{\mathbf{e}}_x) T'_2)} d\omega d\omega' , \quad (30) \end{aligned}$$

respectively, where  $\hat{\mathbf{e}}_x$  is the unit vector along the (horizontal) direction of the ambient flow. The Doppler compensation factors  $\gamma_{D_1}$  and  $\gamma_{D_2}$  are calculated  
 615 as in (16) with speeds of sound  $c_1$  and  $c_2$  for the two media. Referring to Fig. 16 where  $\alpha$  is the angle of the incident wave,  $\beta$  the angle of the refracted wave, and  $\mathcal{O}$  is the point of the interface between both media where the wave is refracted, then the travel times within the first and second media are  $T_1 = a_1/c_1$  and  $T_2 = a_2/c_2$ , respectively, where  $a_1 = l_1/\cos \alpha = |\mathbf{r}^S - \mathbf{r}_{\mathcal{O}}|$   
 620 and  $a_2 = l_2/\cos \beta = |\mathbf{r}_{\mathcal{O}} - \mathbf{r}_q|$ , respectively (likewise,  $T'_1 = a'_1/c_1$  and  $T'_2 = a'_2/c_2$  with  $a'_1 = |\mathbf{r}^S - \mathbf{r}_{\mathcal{O}'}|$  and  $a'_2 = |\mathbf{r}_{\mathcal{O}'} - \mathbf{r}_r|$ ). It is important to note that in this refraction compensation mechanism only the phase (travel times) is significant for localizing the source, and not the amplitude. This is the reason why no amplitude reflection/transmission coefficient is required in  
 625 the imaging functions.

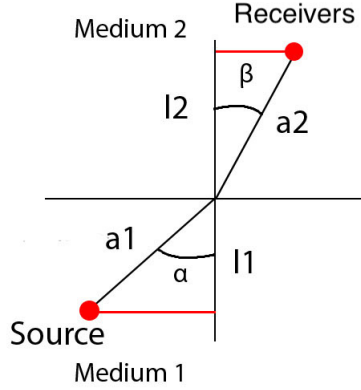


Figure 16: Refracted acoustic wave at the interface between two media with speeds of sound  $c_1$  and  $c_2$ :  $\alpha$  is the angle of the incident wave,  $\beta$  is the angle of the refracted wave. The interface is the mean shear layer between the first and second media in Fig. 13.

### 5.5. Imaging of the sources

We thus aim at determining the positions of the three sources. The size of the search window is  $10\lambda_0 \times 10\lambda_0$  centered around the mid-point  $(X_s, Y_s)$  of the upper sources. A pixel being of size  $2\lambda_0/5$ , this corresponds to a window  
630 of  $25 \times 25$  pixels. The parameters defining the imaging setup are gathered in Tab. 1. The results obtained with the KM and CINT imaging algorithms are shown in Fig. 17. Again, we acknowledge that the jet flow used is ideal and does not reflect reality but we obtain the desired mechanisms with the proposed simulation. The influence of the Doppler compensation factor  $\gamma_D$  is  
635 clearly seen. Without this factor the positions of the sources are significantly shifted, however using the proposed compensated imaging functions their positions are recovered with a satisfactory precision. We observe that the refraction compensation mechanism does not have any significant influence on the result. This was predictable since the speeds of sound of the two

$f_0$	$X_s$	$Y_s$	$d$	$L$	$a$
50 kHz	$12\lambda_0$	0	$3\lambda_0$	$20\lambda_0$	$22\lambda_0$

Table 1: Imaging parameters for localization of three sources through a synthetic turbulent jet.

media are identical and equal to  $\underline{c}$ . Furthermore the distance between the sources and the receivers is small, which leads to weak refraction of the waves. However in cases where strong refraction is likely to happen it is expected that this mechanism will become of prime importance.

## 6. Summary and conclusions

In this paper we consider array imaging techniques for moving cluttered media extending the methods that have already been developed for quiescent cluttered media in [10, 11]. Our aim is to apply them to classical experiments in jet flow aero-acoustics in order to localize sources through a turbulent jet, as applicable to aircraft noise characterization for example.

After introducing a model problem and recalling the principles of two imaging algorithms for motionless media, namely Kirchhoff migration (KM) and Coherent Interferometry (CINT), we propose in Sect. 2 a suitable form of these functions for moving media by introducing a Doppler compensation factor for the travel times of the array data. Accounting for this compensation it is possible to perform imaging through a heterogeneous (random) flow by simulating the back-propagation of the recorded signals in a fictitious moving ambient medium. This has the effect to partially cancel out the random time (or phase in the Fourier domain) shifts that the signals have

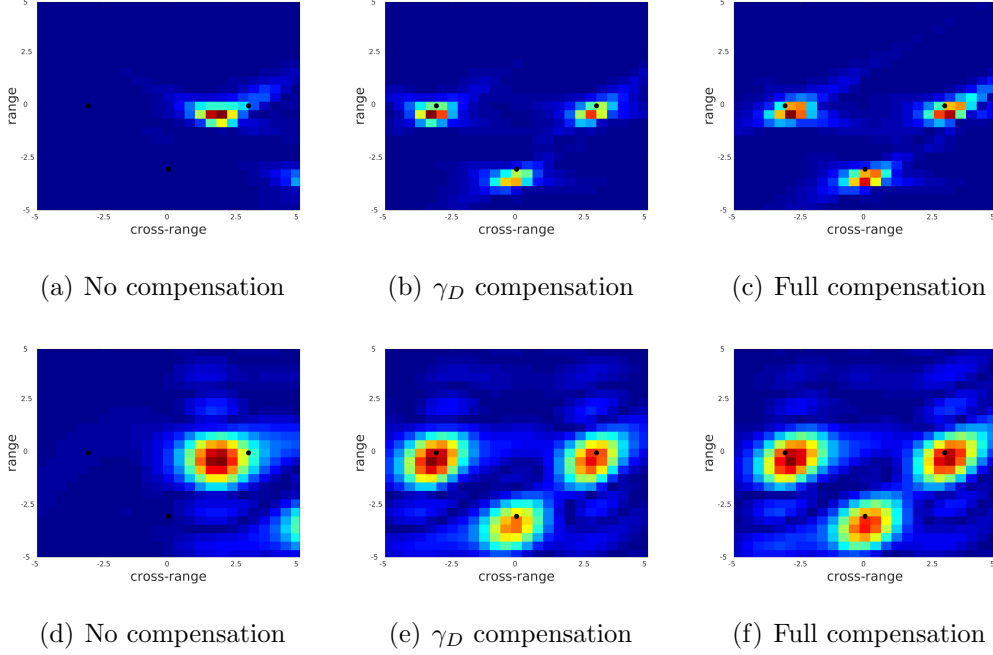


Figure 17: Passive imaging of three sources through a synthetic turbulent jet flow. Influence of the Doppler compensation factor  $\gamma_D$  and refraction compensation mechanism on KM (top) and CINT (bottom) imaging functions: (a) KM image without any compensation; (b) KM image with Doppler compensation factor  $\gamma_D$ ; (c) KM image with Doppler compensation factor  $\gamma_D$  and refraction compensation mechanism. (d) CINT image without any compensation; (e) CINT image with Doppler compensation factor  $\gamma_D$ ; (f) CINT image with Doppler compensation factor  $\gamma_D$  and refraction compensation mechanism.  $\Omega_d = 0.3B$  and  $X_d = 0.5a$  for all images. The source locations are shown by dots  $\bullet$ . Range and cross-range dimensions are in units of  $\lambda_0$ .

undergone when passing through the random flow.

660 In Sect. 3 array imaging in quiescent homogeneous and random media is first introduced in order to validate the numerical tools used to generate the array data by comparisons with the existing results in [10]. Passive and active configurations are studied in order to localize either sources or

reflectors, respectively, by the KM and CINT imaging functions. It is seen  
665 that in the passive configuration both algorithms can efficiently localize the  
sources. Indeed, the waves travel once in the cluttered medium and are  
weakly scattered by the latter so that KM and CINT are equally effective.  
In the active configuration the waves first go to the reflectors and then go back  
to the receivers, thus propagating back and forth in the cluttered medium.  
670 Consequently the array data are noisier. The strength of CINT images lies in  
the fact that they are statistically stable, which is not the case of KM images.  
The former are however blurred compared to the latter as a result of the  
smoothing that must be applied in order to obtain clear images. The trade-off  
between stabilization and blurring is driven by the decoherency parameters  
675 which localize the array data in space and frequency. They depend on the  
random medium and are therefore unknown *a priori*. They are found here  
incrementally by successive tests, though an adaptive method to determine  
them optimally is developed in [11]. We also note that CINT works well if  
significant coherence remains in the data, so that the clutter needs not be too  
680 strong. In other words, the range  $L$  must be comparable to or smaller than  
the transport mean free path that characterizes the onset of wave diffusion,  
a regime where interferometric imaging cannot work. We have observed in  
our numerical experiments that perturbations  $\sigma$  of up to about 7 to 10%  
could be handled by the CINT imaging algorithm in both passive and active  
685 configurations. The latter is however much more demanding computationally  
than the KM algorithm.

In Sect. 4 the KM and CINT imaging algorithms are implemented and  
tested in the active configuration for a heterogeneous medium with random

speed of sound and moving with either a uniform or a randomly perturbed  
690 velocity. The relevance of the Doppler compensation factor is highlighted.  
Such correction notwithstanding, the KM imaging function is put at fault in  
both situations (uniform and random velocity). The three sources considered  
in these numerical experiments are however correctly localized by the CINT  
imaging function for a suitable choice of the decoherency parameters.

695 In Sect. 5 numerical tests of the KM and CINT imaging algorithms are  
finally performed to localize sources through a synthetic turbulent jet flow  
computed by CFD. Doppler compensation and refraction compensation at  
the interface between the jet layers, are implemented. In this experiment both  
the KM and CINT imaging functions yield accurate images of the sources.  
700 Also the refraction compensation mechanism has only a marginal influence  
compared to the Doppler compensation factor, which remains essential for the  
proper reconstruction of the images. These observations are explained by the  
jet configuration considered here. The different layers have the same average  
speed of sound, and the clutter induced by the sheared layers is mild. In  
705 other configurations with fully developed turbulent layers and heterogeneous  
speeds of sound refraction effects may be of prime importance, and KM  
imaging may be less effective than CINT imaging. Such jet configurations  
and other applications in moving random media should be considered in  
future works.

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