

# Historical Earthquake Scenarios for the Middle Strand of the North Anatolian Fault Deduced from Archeo-Damage Inventory and Building Deformation Modeling

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## Historical earthquake scenarios for the middle strand of the North Anatolian Fault deduced from archeo-damage inventory and building deformation modeling --Manuscript Draft--

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#### 21 Abstract

The city of Iznik (ancient Nicaea), located on the middle strand of the North Anatolian fault zone 22 23 (MNAF), presents outstanding archeological monuments preserved from the Roman and Ottoman 24 periods (1<sup>st</sup>-15<sup>th</sup> c. AD), bearing deformations which can be linked to past seismic shaking. In order to 25 constrain the date and intensity of these historical earthquakes, a systematic survey of Earthquake Archeological Effects (EAE) is carried out on the city's damaged buildings. Each of the 235 EAE found is 26 27 given a quality ranking and the corresponding damage is classified according to the EMS98 scale. We 28 show that the walls oriented N-S were preferentially damaged, and that most deformations are 29 perpendicular to the walls' axes. The date of postseismic repairs is constrained with available 30 archeological data and new <sup>14</sup>C dating of mortar charcoals. Three damage episodes are evidenced: (1) between the 6<sup>th</sup> and late 8<sup>th</sup> centuries, (2) between the 9<sup>th</sup> and late 11<sup>th</sup> centuries AD, (3) after the late 31 14<sup>th</sup> century AD. The repartition of damage as a function of building vulnerability points toward a global 32 33 intensity VIII on the EMS98 scale. The 3D modeling of a deformed Roman obelisk shows that only 34 earthquakes rupturing the MNAF can account for this deformation. Their magnitude can be bracketed 35 between Mw 6 and 7. Our archeoseismological study complements the historical seismicity catalogue 36 and confirms paleoseismological data, suggesting several destructive earthquakes along the MNAF 37 since the first century AD. We suggest the fault might still have accumulated enough stress to generate 38 a Mw 7+ rupture.

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#### 40 INTRODUCTION

Documenting the calendar of past earthquakes in tectonically active regions is an important step to determine their seismic hazard (Guidoboni and Stucchi, 1993; Bilham et al., 2001). In certain contexts, the knowledge of Holocene earthquakes is the only way to estimate the magnitude range expectable in a given area and the recurrence times between big earthquakes. Paleoseismological trenching allows one to identify the last ruptures in the stratigraphy at a given point of the fault (McCalpin, 2009). Historical seismology has been developed to build earthquake catalogues using written descriptions of seismic events (Ambraseys, 2000, 2002). Whereas palaoseismology is primarily concerned with the source of earthquakes, historical seismology interprets the observable consequences in the form of intensities felt at given locations.

50 Evidence of coseismic deformation found in the stratigraphy of archeological survey sites and on 51 ancient buildings has been increasingly described and used to complement earthquake catalogues 52 and, in some cases, quantitatively constrain earthquakes thanks to numerical modeling (Korzhenkov 53 and Mazor, 1999; Mazor and Korzhenkov, 2001; Hinzen, 2005). Although the interpretation of 54 archeological evidence is delicate because possible traces of earthquakes are rarely unambiguous, 55 this "archeoseismological" approach allows one to document past earthquakes in regions without 56 written archives, which extends the time scale of the catalogue (Karcz and Kafri, 1978). The 57 archeological record may also preserve smaller events that are poorly preserved in classical trenches

58 (Rapp, 1986).

59 In this study, we apply this archeoseimological approach to the city of Iznik (ancient Nicaea), located 3 km north of the active fault segments of the middle strand of the North Anatolian fault (MNAF, Fig. 1). 60 61 Since the beginning of the instrumental period, this fault strand has been characterized by a very low 62 seismicity and deformation rate (Özener et al., 2013; Öztürk et al., 2009). However, various datasets 63 documenting the pre-instrumental seismic activity strongly contrast with this modern quiescence. The historical record of ancient earthquakes having affected Iznik (Fig. 2) contains no less than ten 64 65 destructive earthquakes during the last two millennia (Ambraseys and Finkel, 1991; Ambraseys and 66 Jackson, 1998, 2000; Ambraseys, 2000, 2002, 2009; Guidoboni et al., 1994). The compilation of the 67 paleoseismic trench data along the MNAF suggests the occurrence of at least four Mw 6+ earthquakes during the last two millennia (Barka, 1992, 1993; Dogan, 2010; Ikeda, 1988; Ikeda et al., 1989; Özalp et 68 69 al., 2013; Yoshioka & Kusçu, 1994). Moreover, the region presents several archeological clues 70 suggesting past earthquake occurrence, such as the submerged basilica recently discovered in Iznik Lake (Sahin & Fairchild, 2018), and the numerous traces of deformation and reconstruction on the city's ancient buildings (Benjelloun et al., 2018). Despite this evidence of past earthquakes, more precise data are needed to perform a reliable assessment of seismic hazard for the Iznik region.

The goal of this study is to use the ancient buildings in Iznik and its surroundings as records of past seismicity. The compilation of many traces of potential earthquake damage provides a complementary dataset to historical seismology and paleoseismology in order to discuss the level of seismic activity of the MNAF during the last 2000 years. The dating of several independent buildings affected by earthquake shaking, and their repairs, allows us to complement the earthquake catalogue. The modeling of archeoseismic damage helps to discuss the epicenter location and strength of the earthquakes responsible for the damage observable today in the city.

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#### 82 TECTONIC CONTEXT OF THE STUDY: THE MNAF AND IZNIK'S SEISMIC LANDSCAPE

The study area includes the city of Iznik and its close surroundings, in the southeast of the Marmara Sea (Fig. 1 and 3a). It is located on the middle branch of the North Anatolian fault. The North Anatolian Fault zone (NAFZ) is a major tectonic boundary accommodating the relative motion between the Eurasian and Anatolian plates. It is a 1000-km long, right-lateral strike-slip fault crossing the northern part of Turkey (Sengör, 1979). This fault zone is associated with a significant seismic hazard and with several destructive earthquakes since the beginning of the Common Era (Fig. 2).

In its western termination, the NAFZ is divided into three strands (Fig. 1). The northern strand (NNAF) continues along the strike of the main fault zone and crosses the northern part of the Marmara Sea from Izmit Gulf to Gelibolu Peninsula. This strand was especially involved in the last seismic crisis that occurred as a succession of ruptures migrating westwards, from Erzincan in 1939 to Izmit in 1999 (Stein et al., 1997). The middle strand (MNAF) separates from the NNAF in the Akyazi district, borders on the south two successive basins known as the Geyve-Pamukova Basin and Iznik Lake, reaches the Marmara 95 Sea through Gemlik Gulf and borders the southern shore of the Marmara Sea (Fig. 3a). With a relative 96 horizontal motion estimated around 5 mm/year with GPS (Ergintav et al., 2014), the MNAF shows a 97 deformation rate five times smaller than the NNAF (~20-25 mm/year) (Reilinger et al., 2006). The 98 southern strand (SNAF) separates from the MNAF near Iznik and continues southwestwards to Ulubat 99 and Manyas Lakes (Fig. 1).

In addition to the MNAF, smaller structures around Iznik Lake show morphological evidence of recent activity. North of the lake, two oblique fault zones, the NW-SE striking Orhangazi fault (Fig. 3a) and the ENE-WSW striking Boyalica fault, separate the basement rocks of the Armutlu block and the Quaternary alluvia of the lacustrine plain (Öztürk et al., 2009). A small normal fault zone, the Elbeyli fault, was described east of Iznik, forming a 7 km long scarp at the foot of a marble and schist massif, cross-cutting in the south the eastern section of the Iznik aqueduct (Benjelloun et al., 2018).

106 The natural environment of Iznik presents cumulative expression of Holocene and historical coseismic 107 effects, such as faceted scarps (Fig. 3b), meter scale recent scarplets evidenced on land (Ikeda et al., 108 1989) and in the bathymetry of Iznik Lake (Gastineau et al., 2020 PREPRINT), laterally offset 109 geomorphic markers (Ikeda, 1988; Sipahioglu and Matsuda, 1986; Yoshioka and Kusçu, 1994), and 110 transtensional basins (Dogan et al., 2015). This leads geologists to qualify the city's geological environment as a "seismic landscape", as defined by Michetti et al. (2005). The most prominent 111 112 earthquake source for the Iznik region is the MNAF, which represents a 140 km long dextral fault zone between Akyazi district and Gemlik. A rupture propagating along this whole section would correspond 113 to a Mw 7.6±0.3 earthquake (Wells and Coppersmith, 1994). 114

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#### 116 ARCHEOSEISMOLOGICAL DATA COLLECTION

117 The main principle of an archeoseismological investigation is to look for traces of past earthquake118 deformation in archeological features, which are commonly called Earthquake Archeological Effects

(EAE; Rodriguez-Pascua et al., 2011). These EAE can be located on-fault, when an archeological structure is crossed and deformed by an active fault. However, the most numerous archeoseismic observations are located off-fault and concern buildings which have been deformed because of coseismic ground motion. Finally, we include in EAE the evidence for postseismic reconstructions which serve to repair a building damaged during an earthquake and/or to make it more resistant to future earthquakes.

125 In Iznik and its surroundings, systematic archeoseismic observations were made on the visible ancient 126 remains (Fig. 4 and 5; for the complete list see Tables S2 and S3 in the electronic supplement). We 127 focused our observations on the critical buildings of the city, such as the aqueduct and the defensive 128 walls, which were especially important for its viability and were likely repaired as soon as damaged. 129 The types of inventoried EAE in Iznik include: wall facing collapses, wall warping, wall tilting, cracks, 130 unusual wall offsets, masonry dislocations, block rotations, block corner expulsions, block shifting, 131 damaged arches, dropped keystones, arch collapses, column tilting, expulsion of building corner, and 132 deformed pavement (Kazmér, 2014; Rodriguez-Pascua et al., 2011). To this dataset we also added 133 suspected traces of post-seismic repairs and reconstructions: presumed "seismoresistant" techniques, 134 buttresses, filling of damaged masonry with new materials, partial reconstruction of a damaged 135 building, filling of windows and crenellations, massive reuse of materials taken from older buildings.

136 Each individual observation was given an identification code. This code is composed of a prefix related 137 to the nature or category of building (AQ for the aqueduct, W for the defensive walls, C for the intra 138 muros buildings and O for the obelisk) and a number. For suspected post-seismic repairs and 139 constructions, an R is added at the beginning of the ID. The observations were geolocalized and the 140 nature of the associated deformation or reconstruction was reported. Whenever possible, we 141 measured the azimuth of the damaged wall, and the amount of displacement (lateral shift, vertical 142 drop, angle of tilting). For oriented deformations, we also measured the azimuth (i.e. axis of the 143 deformation, between 0 and 180°) and strike (i.e. direction between 0 and 360°) of the deformation.

144 In the following sections, when referring to the defensive walls, we use the naming conventions of 145 Schneider and Karnapp (1938) and Foss and Winfield (1986). Each tower is numbered from T1 to T114 146 starting from Yenisehir Gate in the south and progressing anti-clockwise (Fig. 6b). Each wall section is 147 numbered according to the adjacent towers (e.g. W1/2 for the wall section between T1 and T2).

148 For each EAE, we used a quality factor between 1 and 3, reflecting the probability of seismic origin of 149 the deformation versus other causes (e.g. anthropic damage, natural decay, soil instability). We assign 150 a quality 1 (good) when the seismic origin is the most probable scenario for the EAE and other 151 processes can be discarded. When the EAE can be associated with one non-seismic process in addition 152 to the seismic scenario, we assign a quality 2 (average). When the seismic origin is dubious because many other processes may be invoked to explain the observed deformation, we assign a quality 3 153 154 (bad). The cases of damage were also classified on a damage scale ranging from 1 to 5 (1 corresponding 155 to very slight damage and 5 to complete destruction) and the buildings investigated were classified on 156 a vulnerability scale (Grünthal & Levret, 2001).

On several EAE, construction material (brick, mortar) was sampled in the original structures and the repairs to constrain the date of damage. Carbonate concretion deposits on the aqueduct formed during potentially coseismic massive leakage episodes were also sampled to date the associated damage.

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#### 163 DESCRIPTION OF THE BUILDINGS STUDIED

#### 164 The Roman obelisk at Elbeyli

6 km north of Iznik, near the village of Elbeyli, stands a Roman obelisk built during the 1<sup>st</sup> century AD
(Fig. 6a and 7). The column is made of five triangular prismatic stones lying on a rectangular pedestal

(Fig. 7). Small offsets between the triangular stones suggest translation and rotation motions probablyduring seismic shaking (Fig. 7b,c).

#### 169 *The aqueduct of Iznik*

170 The remains of two aqueducts are visible in the east of Iznik. One was discovered in 2019 outside of 171 the city walls, north of the graveyard. The other one, much better preserved, enters the city through 172 Lefke gate (Fig. 6). The best-preserved parts of this aqueduct extend along 600 m, starting from the 173 city gate, with an E-W orientation. 1 km east of the city, the aqueduct runs along the southern border of a carbonate massif where its sources are located (Dereköy village, see Fig. 3a for location). The 174 175 aqueduct presents an underground section, 400 m long. The aqueduct of Iznik has only recently been 176 studied in detail by Benjelloun et al. (2018). Using a stratigraphic approach coupled with architectural analogies, they concluded that the earliest phases visible were likely to belong to Justinian's period (6<sup>th</sup> 177 century AD), and identified major restoration works around the 11<sup>th</sup> and 13<sup>th</sup> centuries AD. 178

#### 179 The walls of Iznik

The defensive walls of Iznik are made of two belts surrounding the city (Fig. 6b). They were extensively studied by Schneider and Karnapp (1938) and Foss and Winfield (1986) (the chronology of the fortifications is presented in Fig. S1 in the electronic supplement). The inner belt was first built during the 3<sup>rd</sup> century AD, after Gothic attacks in 256-257. The remains of these early walls can still be seen at several points (Fig. 4b).

After an Arab attack in 727, the walls were partly rebuilt by Leo III (717-741). These reconstructions mainly affected the eastern and southern parts. Another important reconstruction campaign followed in 858 under Michael III, especially affecting the eastern and southern sides. After a period of peace, the 10<sup>th</sup> and 11<sup>th</sup> century saw the walls damaged on several occasions, until the city was taken by the Turks in the end of the 11<sup>th</sup> century. In 1097, the city was given back to the Byzantine ruler Alexios I Komnenos, who carried out a few reconstructions (Fig. 4a). The last major reconstructions occurred during the Lascaris and Palaeologue periods in the 13<sup>th</sup> century (Fig. 4c), with the addition of the outer walls during the reign of John III Doukas Vatatzes (1222-1254 AD). Since 2018, important restoring works have been carried out on the defensive walls, erasing most of the traces of previous damage and reconstruction phases. Our observations on the walls were done before the beginning of these works.

#### 196 Intra muros buildings

197 We inventoried several deformations and possible "seismoresistant" techniques in the Iznik theater (Fig. 6b), built during the 2<sup>nd</sup> century AD, and spoiled significantly as a quarry in later periods. 198 Deformations were also described in Aya Sofia, a church built by Justinian in the 6<sup>th</sup> century AD, 199 restored in the 9<sup>th</sup>, 11<sup>th</sup>, and 13<sup>th</sup> centuries, and converted into a mosque by Orhan shortly after the 200 201 Ottoman conquest of 1331 (Brounoff, 1925; Schneider, 1943). We also found deformations and 202 technical innovations potentially related to earthquakes in several Ottoman buildings: Yesilcamii 203 mosque built in the late 14<sup>th</sup> century (Fig. 4e), Mahmut Celebi mosque built in 1442, and Murat II 204 hamam built in the first half of the 15<sup>th</sup> century (Fig. 4d). Other traces of damage were encountered 205 on a few Ottoman tombstones located in Candarli Hayrettin Pasa mausoleum.

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#### 207 DAMAGE INVENTORY

### 208 Location of the damage

We inventoried 235 cases of damage (Fig. 5). The observations are especially dense on the inner walls (almost 4 observations every 100 m in average) and the outer walls seem much less affected (less than 1 observation every 100 m on average). The damage observed is in general regularly distributed all along the inner walls. In some areas the density of observations is much lower. This can be the case when the remains have disappeared, such as in west of the city. In other areas, the dense vegetation or the presence of private areas near the walls prevented the survey, such as in the northeastern
section between towers 46 and 50, and in the southwestern section between towers 95 and 104.

## 216 Azimuth of the damaged walls

217 The relative repartition of the different wall orientations was compared to the relative number of EAE 218 found in these different wall azimuth ranges, no matter the azimuth of the deformation (Fig. 8a). The 219 results do not change significantly when data of lower qualities are included. If all the walls were 220 affected in the same way whatever their azimuth, the relative amount of EAE and the orientations 221 should present similar distributions. This is the case for the E-W and NW-SE oriented walls that show 222 a correspondence between the relative amounts of EAE and the lengths of the walls affected. By 223 contrast, we can see that the N-S oriented walls bear much more EAE than what could be expected 224 from their length: they contain a third of the walls' EAE whereas they represent only 12.7% of the total 225 wall length. Conversely, the NE-SW oriented walls are underrepresented in terms of EAE.

#### 226 Oriented deformations

105 of our observations present an oriented pattern (e. g. azimuth of collapse or expulsion). Most of the oriented deformations show a strong correlation with the wall azimuth (Fig. 8b): they are either perpendicular to the wall (out-of-plane) or parallel (in-plane). A clear, dominant, N-S azimuth appears, representing 30% of the observations (Fig 8c). This actually mirrors the greater length of walls oriented E-W (Fig. 8a). For almost all the azimuth ranges, deformations exist in both directions, but the deformations oriented NE-SW are characterized by an exclusive NE strike of the damage.

233 Time constraints on the deformations

The earliest EAE are found almost all around the inner walls and in the theater (Fig. 5b). The later sections of the walls were also affected by several deformations. The aqueduct shows a significant number of EAE from all periods. EAE from the Ottoman period were found especially intra muros on the mosques and the bathhouse. It is expected that older buildings display a larger amount of damage compared to more recent ones because they are more likely to accumulate damage from several
deformation episodes. As mentioned in the previous section, the amount of EAE seems much smaller
on the outer walls built in the 13<sup>th</sup> century, which is coherent with the fact that it is one of the latest
buildings of the Byzantine period.

The repairs were mainly dated relying on the age of the repaired structure and the technique used in the repair. We could find repairs for all the major construction periods of the city, from the 9<sup>th</sup> century to the Ottoman times (for the list, see Table S3 in the electronic supplement). For the earlier periods, we could only find possible seismoresistant techniques of construction in the theater with the use of polygonal imbricated ashlars (Garduño-Monroy et al., 2012; Hinzen and Montabert, 2017).

We were also able to date with <sup>14</sup>C four charcoal samples from mortar filling the dismantled ashlars of tower T57 base and one sample from the new masonry covering the rotated blocks of Istanbul Gate (Fig. 4f, see Fig. 6b for locations). The ages obtained point toward repairs following a deformation episode in the late 11th or early 12th centuries (Table 1). Finally, we tried to date the organic fraction of carbonate concretions sampled on the aqueduct wall, but we obtained a very recent age. The link between the external concretions and historical earthquakes is therefore unlikely.

253 Combining the ages of the affected walls and their repairs, we obtain many time ranges of different 254 widths constraining one or several events (Table 2). The narrower, distinct time intervals obtained for possible earthquakes are (1) 527-787, (2) 858-1097, and (3) after the late 14<sup>th</sup> century AD. The first 255 256 interval corresponds to several good quality EAE but located in Aya Sofya only. The second interval is constrained by one intermediate and one bad quality EAE in the walls, but also matches the <sup>14</sup>C ages 257 258 of the sampled postseismic repairs. It is then probable that the associated damage observed on 259 Istanbul Gate and tower T57 belongs to this episode. The third interval is documented by one good 260 and two intermediate quality EAE in the walls. We can also mention a wider interval, between 730 and 261 1254 AD, including 12 good quality EAE that might belong to the two precedent intervals. Finally, the 262 Ottoman period presents 17 EAE, mostly of good quality, collected on four different buildings. The 263 earliest building, Yesilcamii, was built in 1378 AD, but the EAE observed on Celebi camii indicate a
264 deformation occurring after 1442 AD.

#### 265 Vulnerability analysis and estimation of local intensity

266 The investigated buildings were classified into three vulnerability classes A, B and C following the EMS-267 98 framework (Grünthal & Levret, 2001). Class A includes the most vulnerable buildings, which use 268 rough rubble stones and a mortar of average quality. Class B includes the buildings using carefully cut 269 stones or terracottas, and a mortar of good quality. Class C includes more resistant buildings using 270 large ashlar. When the building presented visible defaults or weaknesses in its construction, we lowered its vulnerability class by one rank (e.g. A instead of B). For each vulnerability class, we 271 272 computed the ratio of the total number of damage of a given grade observed over the length of the 273 walls considered (Fig. 9a). The damage repartition is quite similar for classes B and C with a maximum 274 for grade 2 (moderate) and limited damage for higher grades. The buildings of class A appear less 275 affected by individual cases of damage on their total length, but are characterized by a higher severity 276 of the damage, with a maximum for grade 3 (important non-structural damage and moderate 277 structural damage).

278 The assessment of building damage following an earthquake makes it possible to derive a local 279 intensity reflecting the severity of ground shaking. For that, the damage distributions obtained for 280 different building vulnerability classes is compared to empirical relationships (damage probability 281 matrices, DPM) linking, for a given intensity, the probability that buildings are affected by damage of 282 different grades (Fig. 9b; Riedel, 2015). In modern postseismic damage surveys, each building is given 283 one grade of damage. In our case, the number of individual buildings that could be surveyed is too low, 284 and long linear buildings like the defensive walls and the aqueduct cannot be considered "individual 285 buildings". Therefore, we chose to assign a damage grade to each EAE and to consider the ratio of EAE 286 per linear meter of wall. It is difficult to directly compare our damage ratios with the DPMs because

our counting method should be first calibrated with modern earthquakes, but we can still obtainqualitative estimates of intensity.

289 For vulnerability class A, we obtain a flat distribution for quality 1 EAE (Fig. 9a). When lower qualities 290 are included, we observe a larger peak for grade 3 damage and a significant representation of grade 1 291 damage. The grade 3 damage peak points toward a VII-VIII intensity, but our grade 1 damage is 292 overrepresented compared to the DPM in this range. For vulnerability class B, the obtained distribution 293 is more regular and insensitive to EAE quality, with a maximum for grade 2 followed by a progressive 294 decrease for bigger grades. This distribution is most compatible with an intensity VIII. For vulnerability 295 class C, we obtain a similar distribution to class B, with a clear maximum for grade 2 and much lower 296 ratios for the other grades. This suggests a VIII-IX intensity, with an overrepresentation of grade 4 297 damage compared to the DPM in this range. As a result, a minimal intensity VIII seems to account best 298 for the three damage distributions (Fig. 9b).

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#### 300 MODELING OF THE DEFORMATION OF THE OBELISK

301 The obelisk located north of Iznik was chosen to test numerically whether an earthquake rupturing the 302 MNAF is able to cause the displacement of the blocks, as is observed today. The constituting elements 303 of the obelisk were measured in order to build a 3D model of the obelisk (for the geometry of the 304 model, see Fig. S2 in the electronic supplement). The numerical model was built using a non-linear 305 transient finite-element analysis (Baillet et al., 2005). The marble blocks were assigned a Young 306 modulus of 50 GPa, a Poisson's ratio of 0.2 and a density of 2.7. Two values of Coulomb friction 307 coefficient between each block were tested at 0.5 and 0.7. We selected as input five three-component 308 ground acceleration signals, recorded during four real strike-slip earthquakes (for the list and 309 characteristics of these earthquakes, see Table S5 in the electronic supplement). The range of 310 magnitude of these earthquakes is Mw 5.9-7.3. The signals were selected so that the distance between 311 the recording station and the epicentre was in the same range as the distance between the obelisk and the closest MNAF segments (5-20 km) and with a similar site effect category (site class C in Eurocode-8). The acceleration signals were converted into displacement signals with two integrations. Before each integration, we subtracted the mean and the trend to prevent a drift of the signals, and smoothed the high-frequency peaks with a 4-order bandpass Butterworth between 0.1 and 20 Hz. The signals were eventually resampled to the 0.5e-5 s time step of the numerical modeling approach. They were then imposed at the base surface of the obelisk. In a second set of simulations, we applied the earthquake signals twice in a row to reproduce examples of cumulative deformation (Fig. 10).

Most of the energy of the seismic signals is focused below 1 Hz for the Düzce earthquake and 4 Hz for the others. The modal analysis of the modeled structure shows two main resonance frequencies at 7.8 and 7.84 Hz in flexional modes. The third mode corresponds to a frequency over 30 Hz, which is not excited by the selected seismic signals.

323 The obelisk collapses only for the signal of Mw 7.3 Düzce earthquake (Table 3). For the other signals, 324 the obelisk still shows irreversible relative displacement between blocks. The most significant values 325 of displacement between adjacent blocks are obtained for the Mw 6.1 Azores Islands and Mw 5.9 326 Kyllini signals. At the end of the single-event simulations, these values are slightly lower than the 327 centimeter offsets observed on the field. The relative rotations obtained between adjacent blocks are 328 less than 1° and hardly reproduce the actual rotation component, clearly visible on the monument. At 329 the end of the double-event simulations, the obelisk remains standing for all events but Düzce, and 330 shows a cumulative deformation, which is twice the deformation of the single-event simulations. The 331 final values obtained for two Azores Islands events better reproduce the field observations.

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#### 336 Discussion

#### 337 Local intensity and associated earthquakes

338 Our intensity estimation can be impacted by two biases. (1) Contrary to postseismic surveys, we did 339 not study a representative sample of the buildings that used to stand in Iznik in ancient and medieval 340 times. It is probable that the buildings still visible today are among the most resistant, and that the 341 more vulnerable buildings have disappeared and were replaced by modern constructions. The 342 empirical damage distributions suggest that the heaviest structural damage is concentrated on these 343 vulnerable buildings, while the more resistant buildings tend to mainly bear slighter damage (Fig. 9b). 344 Therefore, the successive cycles of repairs and reconstructions will tend to erase the traces of the 345 heaviest damage (grades 4 and 5), while the slighter damage will be preferentially preserved. This 346 selection bias will lead to underestimation of the intensity felt in Iznik during past earthquakes. This 347 means that we constrain a minimal intensity. (2) Our damage dataset results from the cumulative 348 effects of several earthquakes, and our qualitative comparison with the DPMs relies on the assumption 349 that these earthquakes produced similar damage distributions. This seems to be the case as the 350 obtained damage distributions are close to the empirical DPMs (Fig. 9). We can also assume that the 351 final curve will mostly reflect the bigger events, which leave most traces of damage. Our vulnerability 352 analysis may thus only constrain a minimal intensity, around VIII, for the biggest ruptures suffered in 353 Iznik in the last two millennia.

With an epicentre located on the fault segments 3 km south of the city on the MNAF segments, an intensity VIII in Iznik can be produced by a Mw 6+ earthquake (Erdik et al., 1985). The deformations observed on the obelisk suggest magnitudes over 6, probably between 6 and 7, in the case of events rupturing the same segments south of Iznik, in agreement with the vulnerability analysis. However, the modeling also shows that a stronger earthquake near Iznik would have destroyed the obelisk. We may therefore rule out the occurrence of this kind of Mw 7+ event during the historical period for the fault segments close to Iznik.

#### 362 Historical seismicity scenarios

The vulnerability analysis and obelisk modeling argue for a significant seismogenic potential of the MNAF. In this section, we discuss the deformation episodes identified by archeoseismology and examine together independent evidence gathered from the historical seismicity catalogues and paleoseismic trenching studies.

## 367 Possible deformations before the 6<sup>th</sup> century AD

Although it was not possible to find repairs anterior to the 8<sup>th</sup> century AD, a part of the EAE affecting 368 369 the older buildings of Iznik may have been caused by earlier earthquakes. The historical catalogue 370 includes six events with damage reported in Nicaea (Fig. 2). Three events were attributed to the MNAF, 371 in 29-32 AD, 121 AD and 368 AD. The magnitudes estimated are around 7 and it seems that the 121 372 AD event was the strongest, possibly of M~7.4. While the first two events are said to have caused 373 partial destruction in Iznik, the 368 AD event is said to have caused complete destruction. This last 374 description is likely exaggerated as several buildings from this period, such as the theater and the 3<sup>rd</sup> 375 century walls, are still standing today.

376 We also need to examine the possibility that Nicaea was affected by earthquakes rupturing the NNAF. 377 Historical descriptions do include such occurrences, e. g. in 358 AD, 362 AD and 478 AD with 378 magnitudes estimated between 6.8 and 7.4, but the precise nature and severity of the destruction 379 caused are difficult to determine (Fig. 2). A Mw 7.5 earthquake rupturing the fault segments crossing 380 Izmit Gulf may produce an intensity VIII in Iznik (Erdik et al., 1985). However, during the 1999 Mw 7.6 381 Izmit earthquake, intensities VI were reported in the Iznik area and the local seismic station recorded a peak horizontal acceleration of 0.12g only (Celebi et al., 2000). Accordingly, the damage in Iznik was 382 383 slight: the chimneys of some houses fell down or were bent and a very small part of the defensive walls collapsed (pers. comm. Cengiz Celik). Therefore, the earthquakes rupturing the NNAF are unlikely to
 account for a significant part of our damage dataset.

## 386 The 527-787 AD episode

387 This period of time is associated with two historical earthquakes, both of them located on the NNAF 388 (Fig. 2). In 554 AD, a Ms~7 earthquake severely affected Constantinople and Nicomedia (Izmit). Partial 389 damage is reported in Iznik, but by one source only. In 740 AD, a major Ms 7.1 event affected the 390 eastern part of the Marmara Sea and it is reported that "a single church survived" in Iznik which was 391 totally destroyed. For the same reasons as exposed above, this testimony cannot be taken literally. But given that no other earthquake is known in the region, the EAE associated to this episode may result 392 393 from these earthquakes. It should be emphasized that our constraints for this episode are scarce and 394 limited to one building only.

#### 395 The 858-1097 episode

Iznik was affected by war damage during this period of time. In the late 10<sup>th</sup> century, the Byzantine general Bardas Skleros led a wide-scale rebellion in Asia Minor. In 978, he besieged Iznik and some parts of the walls, especially the tower T106 in the southwest were heavily damaged (Holmes, 2005). One century later, the city was temporarily seized by the Turks and was attacked by the Crusaders in 1097 AD. Most fights happened around the southern gate, damaging the walls and destroying tower T106 (Cahen, 1948; Foss, 1996; Norwich, 1993).

Our evidence for this deformation episode includes good quality EAE and rebuilding on tower T57 and Istanbul Gate in the northern section. The rebuilding closely postdates the only historical earthquake documented in Iznik for this time interval, in 1065 AD. With a magnitude estimated at 6.8, it caused widespread damage to churches, the city walls, and numerous houses. No other locality seems to have been damaged, which suggests a local event rupturing the MNAF. Sediment cores recently sampled in the southeastern part of Iznik Lake corroborate the occurrence of a seismic event rupturing the fault

segments south of Iznik during the 11<sup>th</sup> century AD (Gastineau et al., 2020 PREPRINT). We can consider
that our EAE dataset most probably includes the archeological signature of this event.

410 The Ottoman episode (after 1330 AD)

The traces of earthquake damage found on several Ottoman buildings indicate that Iznik was affected by at least one significant earthquake since the 14<sup>th</sup> century AD. Three different scenarios can be proposed.

414 (1) This damage may have resulted from earthquakes rupturing the NNAF. Several historical 415 earthquakes with damage reported at Iznik are known (Fig. 2). In 1754 AD, a strong Ms 7 earthquake 416 affected the region of Izmit on the NNAF, destroying a few houses in Iznik, apparently without 417 casualties. In 1878 and 1893 AD, two smaller earthquakes in the same area of the NNAF caused slight 418 damage in Iznik, but with much lower magnitudes, between 5 and 6. Finally, in 1894 AD, a Ms 7.3 419 earthquake ruptured the Izmit Gulf faults and caused liquefaction and landslides in the epicentral 420 region and widespread destruction between Istanbul, Gemlik and Sapanca. The effects in Iznik are not 421 well known.

422 (2) Another source of damage comes from a cluster of earthquakes that affected the SNAF and MNAF 423 west of Iznik in the second half of the 19<sup>th</sup> century (Fig. 2). Most of the activity extended between Bursa 424 and Gemlik, but it seems that some ruptures were also located closer to Iznik, probably along the faults 425 bordering the southern shore of Iznik Lake. The biggest earthquakes happened in the Bursa region and 426 did not affect the area east of Gemlik significantly. The other events correspond to much smaller 427 earthquakes, with magnitudes under 6. Only slight damage is mentioned in Iznik on March 3, 1893 AD.

(3) Interestingly, the Ottoman episode matches the paleoseismic evidence of two contemporary ruptures (Fig. 2), sometime between the 12<sup>th</sup> and 18<sup>th</sup> century AD in Gemlik (Özalp et al., 2013), and sometime between the 14<sup>th</sup> and 18<sup>th</sup> century AD in the west of Mekece (Ikeda, 1988). It can thus be proposed that the Ottoman damage in Iznik was caused by one or several earthquakes rupturing the

MNAF segments between the 14<sup>th</sup> and 18<sup>th</sup> centuries AD. The trench data do not constrain the 432 magnitudes of these events, but the obelisk modeling argues against a Mw 7+ earthquake south of 433 Iznik, which suggests more moderate and/or distant events. The historical catalogues do not present 434 any mention of Iznik between the 12<sup>th</sup> and 18<sup>th</sup> centuries AD, but it can be questioned whether this 435 436 reflects a true period of seismic quiescence for the Iznik region. It is known that at the end of the 13<sup>th</sup> 437 centuries, Iznik suffered significant emigration because of the Ottoman conquests in Anatolia, so much 438 so that after the city was conquered, in 1331 AD, it was described as a ruined city only inhabited by 439 few people (Ibn Batuta, 2012). The city eventually lost its political and strategic importance, which 440 might explain why it disappeared from the archives of past seismicity. In comparison, important 441 centers like Bursa or Gemlik continued to suffer damage from repeated earthquakes, such as in 1419 442 AD. During this period of time, the historical catalogue also includes events which were felt in Istanbul 443 but with too little information to precisely locate the epicenter, e.g. in July 1402 and January 1656 AD 444 (Ambraseys, 2009).

445

#### 446 **CONCLUSION**

447 Using an archeoseismological approach, we identified 235 traces of possible earthquake damage in 448 Iznik, and more than 100 of them can be attributed to seismic shaking with high confidence. The 449 different walls of the city, depending on their orientation or their age, show different patterns of 450 damage. The damage was more severe for N-S oriented walls, while NE-SW walls show less 451 deformation. The older constructions are also more affected than more recent walls. Three distinct 452 episodes of earthquake damage were identified, two before the Ottoman conquest of 1331 AD, and one after. The dating of several repairs associated with earthquake damage enabled us to constrain 453 454 the time of occurrence of two individual events, between 527 and 787 AD, and between 858 and 1097 455 AD. While the latter event may correspond to the 1065 earthquake described by ancient sources, the 456 two others can be accounted for by different earthquake scenarios. We have estimated that the 457 damage observed corresponds to a minimal intensity VIII, most compatible with ruptures along the MNAF segments of magnitudes above 6. The modeling of an obelisk a few kilometres north of Iznik 458 also suggests magnitudes over 6, but is incompatible with a stronger, Mw 7+ rupture along the MNAF 459 460 segments south of Iznik. This last result implies that the fault segments south of Iznik have not known 461 a big rupture for nearly two millenia, which corresponds to several meters of accumulated stress. This 462 study shows that in favourable contexts, archeoseismology can be used complementarily with 463 historical seismology and paleoseismology to refine past earthquake scenarios and contribute to a 464 better seismic hazard assessment.

465

#### 466 Data and Resources

467 The bathymetric map of Marmara was made available by the EMODnet Bathymetry project, (https://www.emodnet.eu/bathymetry), using the EMODnet Bathymetry portal (EMODnet 468 469 Bathymetry Consortium EMODnet (2016): Digital Bathymetry (DTM), http://doi.org/10.12770/c7b53704-999d-4721-b1a3-04ec60c87238) funded by the European 470 471 Commission Directorate General for Maritime Affairs and Fisheries. The large-scale topography of the 472 study area was obtained from the Shuttle Radar Topography Mission 1 Arc-Second Global (DOI: 473 /10.5066/F7PR7TFT). The bathymetry of Iznik Lake was provided by and can be obtained from the 474 Turkish General Directorate of Hydraulic Works (DSI). The raw acceleration signals can be obtained 475 from the Engineering Strong Motion Database (https://doi.org/10.13127/ESM.2; Luzi et al., 2020). The EAE photos, the 3D displacement signals used as input for the obelisk modeling and the complete 476 477 output file can be obtained on the Zenodo repository at https://zenodo.org/record/3966773. The 478 maps of Figures 5 and 6 are from Google Earth satellite imagery. The diagrams of Figures 8 and 9 were 479 prepared using the Matplotlib 3.3.0 package for Python (https://matplotlib.org/; Hunter, 2007). 480 Supplemental Material for this article includes the lists of mentioned historical earthquakes and EAE, additional information on the walls chronology and obelisk model, and the complete data of wallorientations.

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- **Table 1:** Sample list and radiocarbon dating in Iznik. The dating was done by the LMC14/LSCE. The
- ages were calibrated with the Oxcal 4.2 program (Bronk Ramsey, 2009) using the IntCal13 calibration
- 683 (Reimer et al., 2013).

Name	Location	Туре	Carbon analyzed (mg)	%modern carbon	<sup>14</sup> C date (yr BP)	<sup>14</sup> C calibrated age AD
W5a1	Repair mortar on T57	charcoal	1.38	88.84716	950±30	1024-1155
W5b1	Repair mortar on T57	charcoal	1.25	89.00717	935±30	1026-1162
W5b2	Repair mortar on T57	charcoal	1.33	89.42842	900±30	1039-1210
W5a2	Repair mortar on T57	charcoal	0.09*	87.31807	1090±70	769-1046*
IZAQC2	Aqueduct concretion	tufa	0.79	102.37583	Posterior to	1950
W61b	Reconstruction Istanbul Kapi	charcoal	1.51	89.36830	905±30	1037-1207

\*due to the very low carbon content, this age result has a low confidence level

Terminus post quem	Terminus ante quem	Q1*	Q1+Q2†	Q1+Q2+Q3‡
2nd c.	858	1	1	1
2nd c.	1330	1	1	1
3rd c.	858	5	5	5
3rd c.	1254	6	9	9
3rd c.	1185	2	2	2
3rd c.	1065	0	0	1
3rd c.	1097	11	15	16
3rd c.	1254	7	8	9
3rd c.	1330	0	2	2
527	787	3	3	3
730	1254	12	13	13
858	1097	0	1	2
858	1222	1	1	1
858	1254	0	1	1
858	1330	0	2	2

**Table 2:** EAE constrained by post-seismic repairs, separated by quality categories.

\*Quality rank 1 (good). †Quality rank 2 (average). ‡Quality rank 3 (bad).

684	Table 3: Maximum displacements (in mm)	and rotations (in °) obtaine	ed between adjacent blocks.
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Earthquake (station)		ve displacement m)	Maximum relative rotation (°)	
	Friction 0.5	Friction 0.7	Friction 0.5	Friction 0.7
Düzce		Colla	apse	
Azores Islands	7	7	0.5	0.6
Patti Gulf (PTT1)	1.36	1.3	0.085	0.037
Patti Gulf (MLZ)	0	0	0	0
Kyllini	3	3	0.2	0.19

685

#### 687 List of Figure Captions

688 **Figure 1:** Morphology and geometry of the NAFZ in the Marmara region. The active fault segments,

drawn in black, were taken from Emre et al. (2011) and Benjelloun et al. (2018). The Mw>6.5

690 ruptures during the 20<sup>th</sup> century are shown in colors (Hubert-Ferrari et al., 2000; Pondard et al.,

691 2007). The main cities are located with dots. NNAF, MNAF and SNAF: northern, middle and southern692 branches of the NAF.

693

Figure 2: Chronological frieze of Nicaea's history. The colors show the main historical periods of the city: Roman (blue), Seljuk and Ottoman Turk (green) and Lascarid (yellow). The red stars correspond to historical earthquakes having damaged the city according to historical descriptions, and the white stars indicate the historical events for which the reality or amount of seismic damage is uncertain (for the complete list, see Table S1 in the electronic supplement). The two bars under the frieze refer to earthquakes identified in paleoseismological trenches done on the MNAF.

700

Figure 3: Field examples of active faulting in the vicinity of Iznik. (a) Shaded DEM of the MNAF
region, with the locations of the field photograph. The MNAF segments are mapped in red, and other
active faults in black. The lines in the lake correspond to a 5-m interval bathymetry (see Data and
Resources). The fault traces in Iznik Lake are taken from Gastineau et al. (2020 PREPRINT). (b)
Triangular facets (black arrows) at the southeast corner of Iznik lake. The vertical faulting component
of the MNAF is more visible in the landscape in the vicinity of Iznik Lake.

707

Figure 4: Examples of EAE in Iznik. The white arrows indicate the deformation azimuth and strike. The
quality category and identifier are indicated on each picture. (a) Tilted base of the defensive wall, the
upper part collapsed and was rebuilt in a very distinct masonry. (b) Conjugated cracks in a vaulted

711	passage of the inner defensive walls. (c) Tower T97, showing a simple terracotta structure from the
712	early 13 <sup>th</sup> century. The crenellations (black dotted line) were blocked (red arrows) during the
713	following reign of John Vatatzes (1222-1254 AD). (d) Arch with imbricated ashlars, bearing traces of
714	damage and posterior cementation on Murat II hamam (early 15 <sup>th</sup> c. AD). (e) Dropped central ashlars
715	on an arch of Yesilcamii mosque (late 14 <sup>th</sup> c. AD). The damaged arches were later reinforced with
716	transversal iron bars, then wood beams. (f) Pushed and rotated ashlars of the inner Istanbul Gate;
717	note the posterior rebuilding in masonry (red arrows). (g) Collapse in the northwestern section of the
718	inner defensive walls.

Figure 5: Inventory and locations of the EAE in Iznik, classified by quality (a) and by age of the wallaffected (b).

722

Figure 6: (a) Satellite image of Iznik surroundings with the active faults drawn in red and the main aqueduct in yellow. (b) Simplified map of Iznik. The historical city is delimited by a double belt of defensive walls and used to be supplied with water by two aqueducts in the east. The other buildings investigated and mentioned in the text are drawn in grey. The numbers refer to the nomenclature of the towers used in the text, following Foss and Winfield (1986).

728

Figure 7: (a) General view of the obelisk near Elbeyli village. See Fig. 6a for location. (b, c) Detailed
views of rotated and offset blocks. The red arrows point to the parts of the pictures where the
deformation is most visible.

732

733 Figure 8: (a) Comparison between the relative distribution of wall length (bars) and quality 1 EAE 734 (line) for different wall azimuths. The percentages in length and EAE were computed on the total wall 735 length and total number of EAE of quality 1, respectively. For the other qualities, see Table S4 in the 736 electronic supplement. (b) Azimuths of the damage plotted against the azimuths of the wall affected. 737 Note the general correlations between the two values. This correlation is linear for the in-plane 738 deformations (i.e. parallel to the wall) and affine with a ±90 shift for the out-of-plane deformations 739 (i.e. perpendicular to the wall). (c) Rose diagrams of the azimuths of damage observed in Iznik (118 740 EAE). Note the prominent N-S azimuths.

741

742 Figure 9: (a) Distribution of the damage of various grades for the three vulnerability classes of 743 buildings in Iznik. (b) Quantitative translations of the EMS98 damage classification according to 744 vulnerability class and macroseismic intensity, adapted from Riedel (2015). The vulnerability class A 745 to C correspond to the buildings studied in Iznik that use terra cotta, rubble and ashlar. The 746 probability distributions of the different damage grades are shown with different colors. For each 747 vulnerability class, we try to find the intensity which best replicates our observed damage 748 distribution (reported on the graphs as vertical bars). For example, for our vulnerability B buildings, 749 we observe a majority of D2 damage. This is compatible with an intensity VII or VIII. Then, the fact 750 that we have much more D3 than D1 damage rather suggests an intensity VIII.

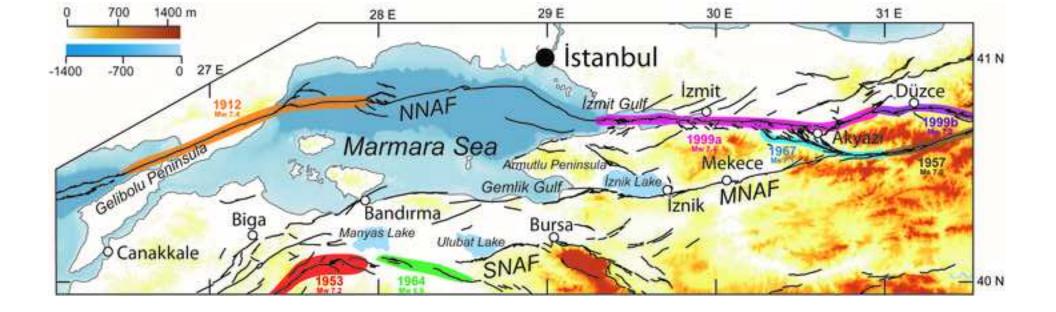
751

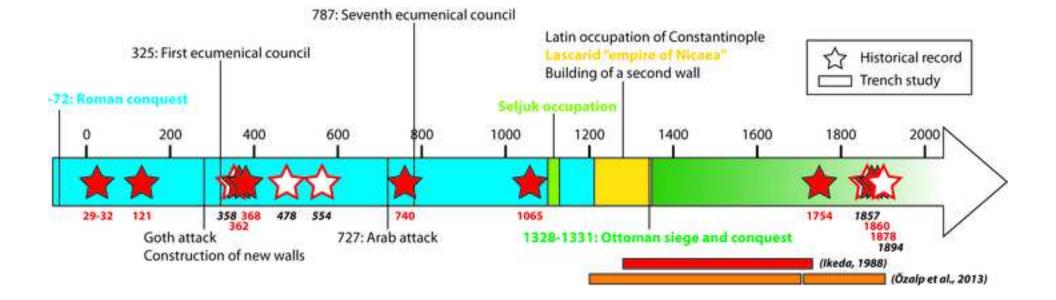
Figure 10: Modeled N displacement (a), E displacement (b), and rotational displacement (c) of the
obelisk for the two-event simulation of the Mw 6.1 Azores Islands earthquake. The blocks are
numbered from base to top.

755

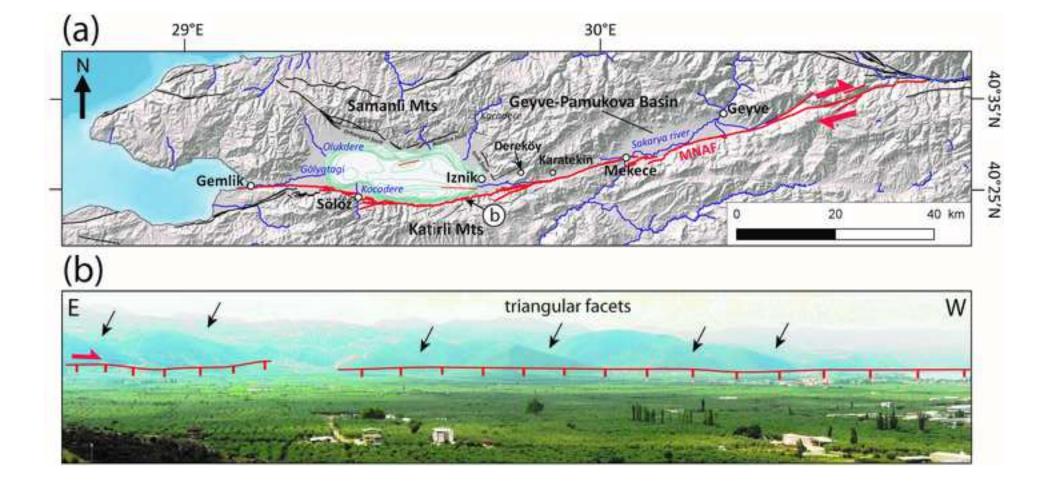
756

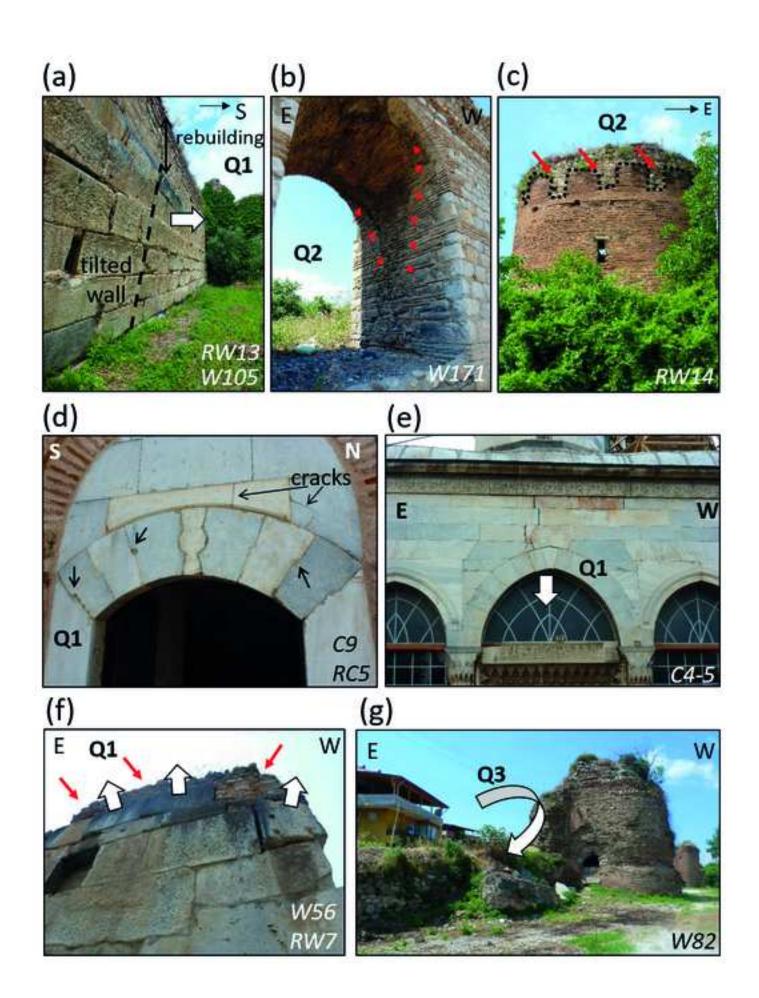




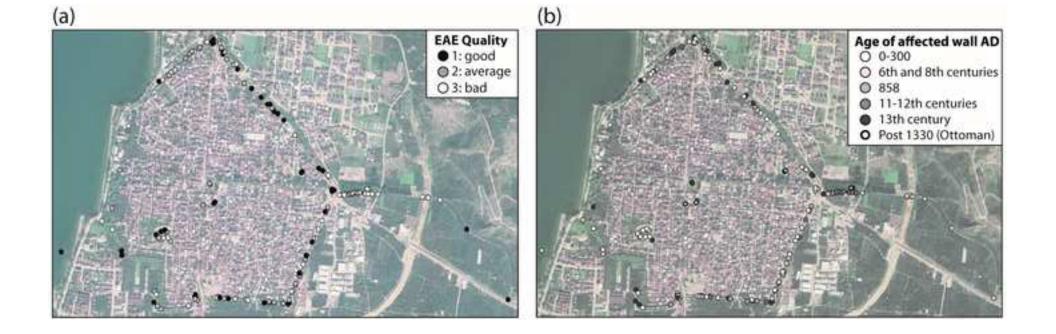




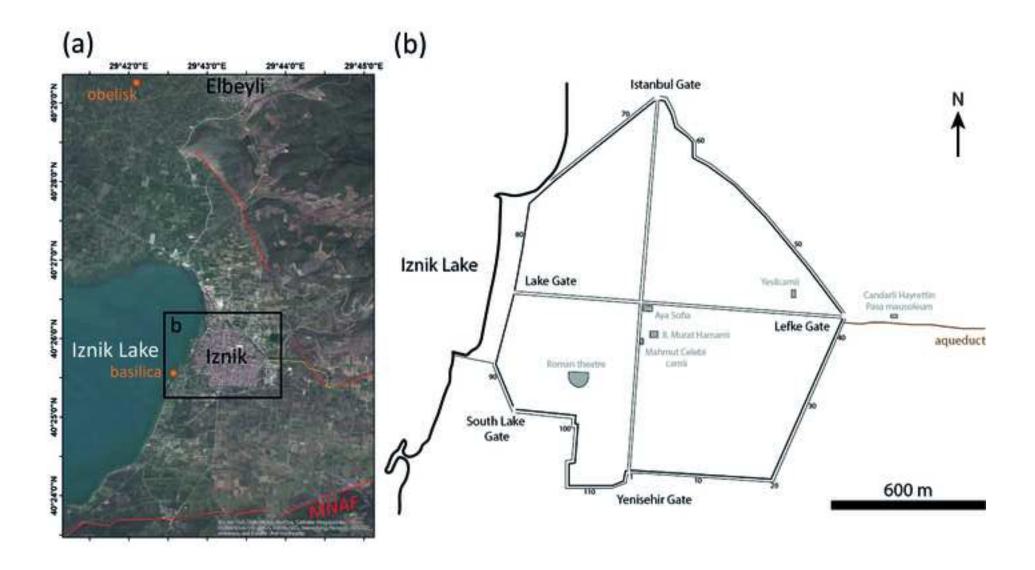


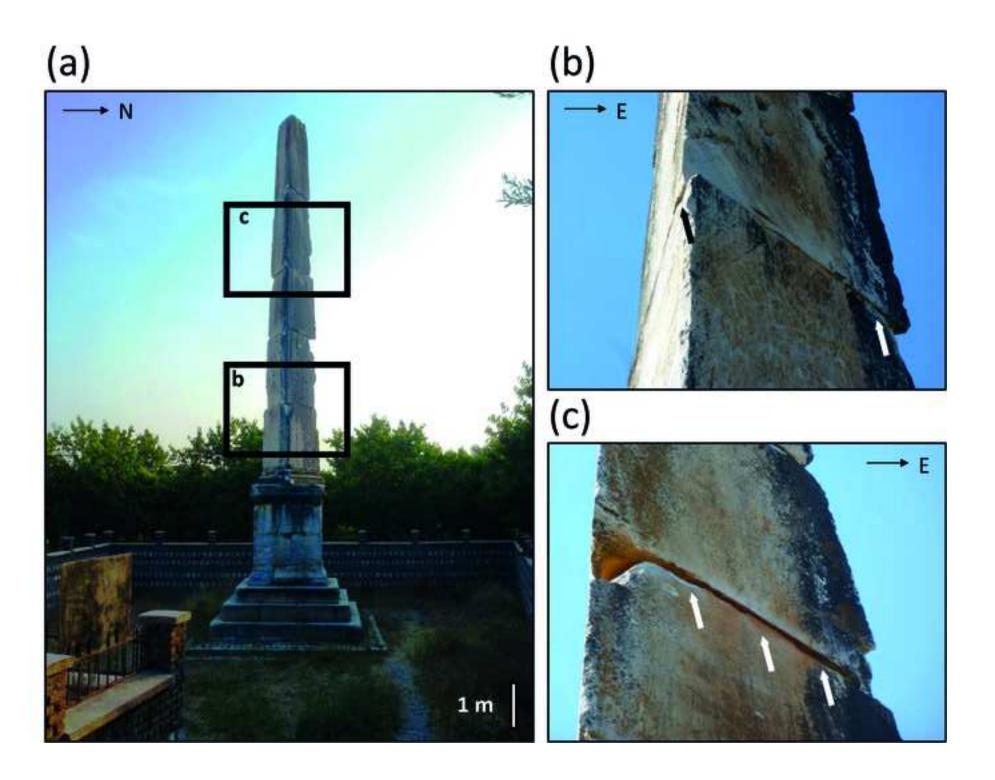


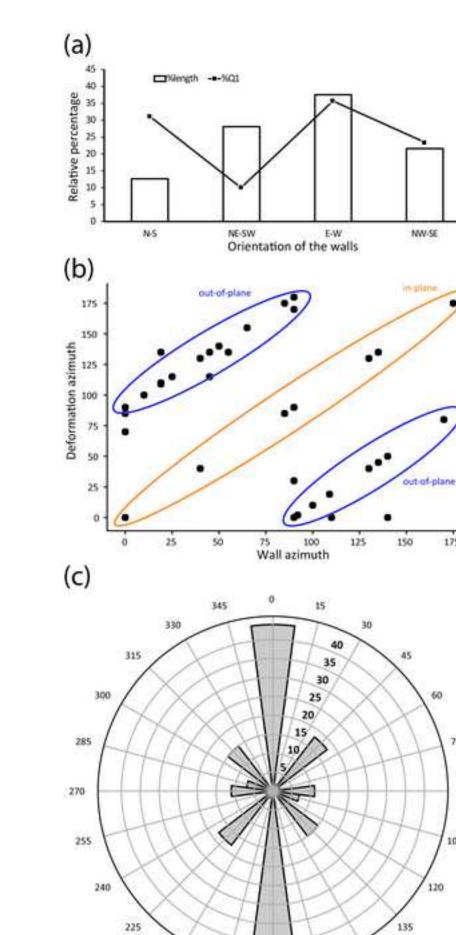


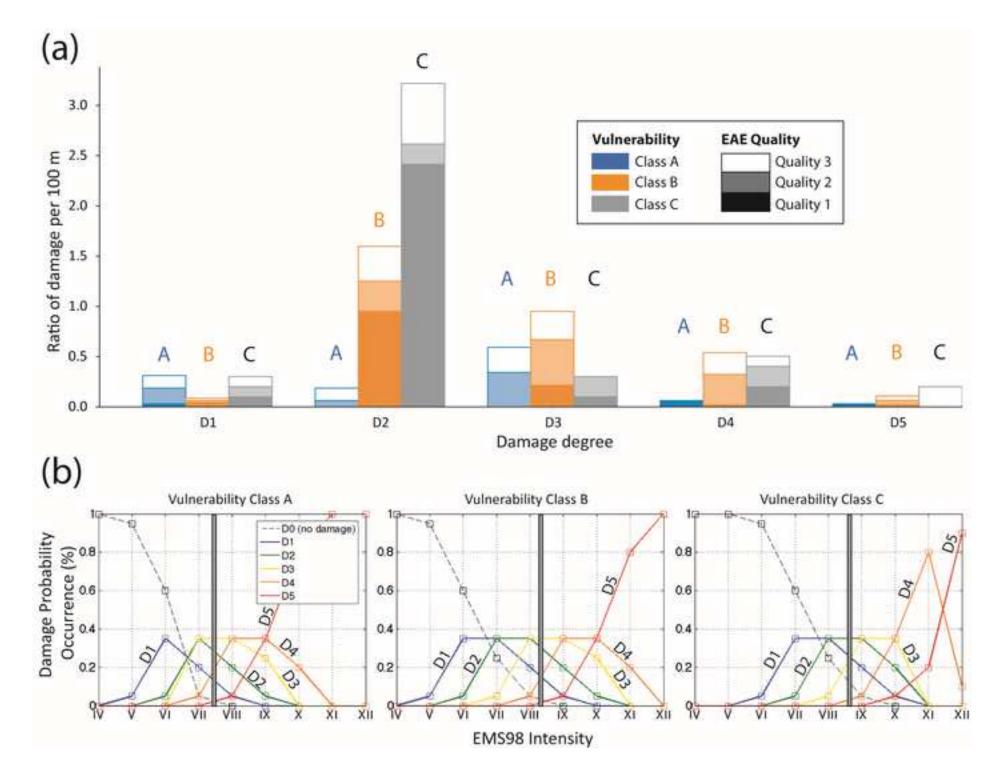


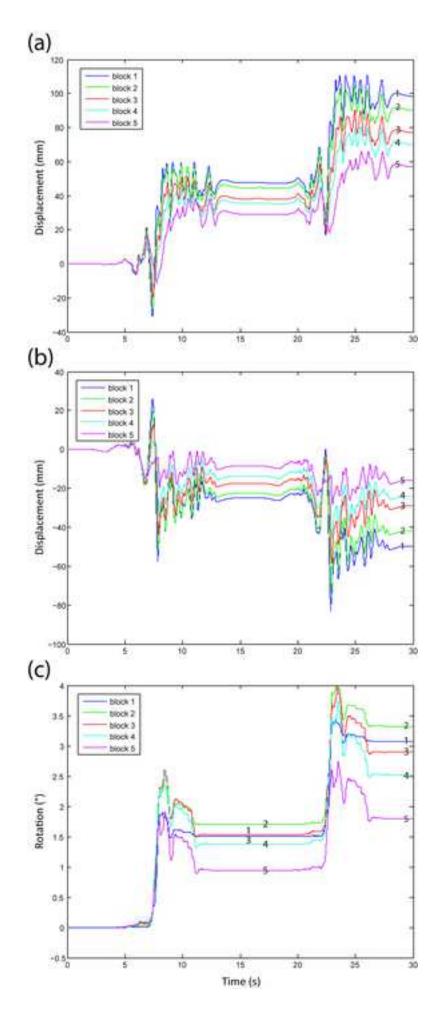












## Historical earthquake scenarios for the middle strand of the North Anatolian Fault deduced from

## archeo-damage inventory and building deformation modeling

Yacine Benjelloun, Julia de Sigoyer, Hélène Dessales, Laurent Baillet, Philippe Guéguen, Mustafa Sahin

## **Supplemental Material**

**Table S1:** Catalogue of earthquakes with effects in Iznik and neighbouring areas. Ms=surface wave magnitude. For the magnitude and epicentre location, we provide the different ranges found among the references.

**Table S2:** Description of the damage EAE observed in Iznik area.

Table S3: Description of the repair EAE observed in Iznik area.

**Table S4:** Length of walls and EAE of different qualities for each wall orientation range. The percentages in length and EAE were computed on the total wall length and total number of EAE in each quality class respectively.

Table S5: Characteristics of the earthquake used for the simulations on the obelisk.

**Figure S1:** Summary of the construction history of Iznik walls, after Schneider and Karnapp (1938) and Foss and Winfield (1986). After the construction of the walls in the 3<sup>rd</sup> century AD, the successive interventions and restoration works are drawn in color. The state of the walls preceding each intervention is drawn in grey.

**Figure S2:** (a) Drawing of Iznik obelisk with the dimensions and arrangement of the different blocks as measured on the field. The western face is given as an example on the left. (b) 3D mesh of the obelisk used for numerical modeling. (c, d) First and second main vibration modes for eigen frequencies of 7.8 and 7.84 Hz respectively. The initial shape of the obelisk is drawn in black, and the distribution of motion in color.

<u>±</u>

Date AD	Affected localities	Effects in Nicaea/Iznik	Estimated Ms
29-32	Bithynia, Nicaea	Most houses destroyed, tax exemptions for damaged cities in Asia Minor and imperial donations for repairs Great part of the city destroyed, publicly	6-7
12	Bithynia, Nicomedia, Nicaea, 1 probably Aoria	funded reconstruction, rebuilding of the fortifications	7.4, 7+
35	Bithynia, Nicomedia, Nicaea, 8 Perinthus, Constantinople	Destruction ? (severity unknown)	7.4, 7+
36	Nicomedia, Nicaea, 2 Constantinople	"a good part of the city was destroyed"	6-7, 6.8+
36	8 Bithynia, Nicaea Bithynia, Nicomedia,	Complete destruction, "sea wave" (one source)	6-7, 6.8
47	Helenoupolis, 8 Constantinople, Nicaea	Damage ?, sea/lake wave	7.3, 7+
55	Constantinople, Nicomedia, 4 Nicaea Eastern part of Marmara, Bithynia, Nicomedia, Praenetos (Karamursel),	Partly damaged ? (one source only) Complete destruction, "a single church	7, 6-7
74	0 Nicaea, Constantinople	survived"	7.1, 7+
106	5 Nicaea	Almost complete destruction, Widespread damage on churches, the city walls and numerous houses	6.8
2 Sep 1754	Izmit, Istanbul, Geyve, Bursa, Izmir (felt) Gemlik, Yalova, Bursa, Iznik (felt), Izmit (felt), Istanbul	A few houses ruined, no casualties	7, 7+
17 Sep 1857	(felt)	Felt Panic, collapse of a few walls, no serious	5-6
7 June 1860	Bursa, Istanbul (felt)	damage	5-6
Nov 1860	Prusa (felt), Iznik (felt) Lake Sapança, Izmit, Labinia, Esme, Adapazari, Akyazi, Bursa, Geyve, Iznik, Istanbul	Several shocks occurring over a month	<5?
19 Apr 1878	(felt) Iznik, Yenisehir (felt), Istanbul	Slight damage	5.5-6.1
3 March 1893	(felt)	Slight damage on a few buildings	<5?

	Adapazari, Istanbul, Sapanca,	
	Izmit, Karamursel, Hersek,	
	Yalova, Karaköy, Katirli,	
	Gemlik, Mudanya, Iznik,	
10 Jul 1894	Pendik, Bandirma, Bursa	Dan

Damage? (lack of details)

## References

1=Ambraseys (2002) 2=Ambraseys (2009) 3=Guidoboni et al. (1994) 4=Ambraseys and Finkel (1991) 5=Ambraseys (2000) 6=Ambraseys and Jackson (1998)

Lat Lon	Quality of epicenter location	NAF strand involved
40.5 30.4-30.5	poorly constrained	Middle (close to NAF junction?)
40.5 30.1	well constrained	Middle
40.7 30.2	e well constrained	North
40.7 29.8-30.2	well constrained	North
40.5 29.5-30.5	well constrained	Middle
40.7 29.8	8 very well constrained	North
40.7-40.8 29.5-29.8	well constrained	North
40.7 27.7-29.6	well constrained	North
40.4 30	) not given	Middle
40.7-40.8 29-30.1	poorly constrained	North
40.4 29.2	2 well constrained	Middle
40.3 29.3	8 not given	South?
	not given	unknown
40.7 30.2	2 not given	North
	not given	Middle?

40.7 27.5-29.6 very well constrained

North

Sources

Phlegon (Olympiads, 2nd c. AD), Eusebius (Hist, 2-3rd c. AD), Hieron. (Hist, 4-5th c. AD), Orosius (early fifth century)	1, 2, 3	
Eusebius (Hist, 2-3rd c. AD), Hieron. (Hist, 4-5th c. AD)	1, 2, 3, 4	
Sozomen (5th c. AD)	1, 2, 3	
Ammianus Marcellinus (4th c. AD), John of Nikiu (7th c.)	1, 2, 4	
Idatius (Cons. Const., 5th c. AD), Socrates Scholasticus (5th c), Hieron. (Hist., 4-5th c. AD), John of Nikiu (7th c) and others	1, 2, 3, 4	
One late source	1, 2, 3	
Vit. Sym. lun (6th-7th c AD)	1, 2, 3, 6	
Theophanes (8-9th), Michael Syrianus	1, 2, 3, 4	
Attaliates (11th), Scylitzes (from public records?)	1,2	
BC Misc. PD (contemporaneous)	1, 2, 4	
Perrey (1860)		2
Perrey (1862c, 1875a), Schmiddt (1879)		2
Perrey (1862c)		2
Schmidt (1879)	1, 2, 4, 5	
Rebeur-Paschwitz (1895)		2

contemporaneous

<u>±</u>

# Damage EAE dataset

EAE ID	Ν	E	Location
AQ1	40.428672	29.729736	Arch N face
AQ2	40.428716	29.729896	Arch N face
AQ3	40.428716	29.730155	Wall N face
AQ5	40.428731	29.730457	Arch N face
AQ6	40.428781	29.730702	Wall N face
AQ7	40.428773	29.730776	Wall N face
AQ8	40.428767	29.730858	Wall N face
AQ9	40.428764	29.730921	Wall N face
AQ48	40.428764	29.730921	Arch N face
AQ10	40.428788	29.731086	Wall N face
AQ11	40.428739	29.731444	Wall N face
AQ12	40.42874	29.731493	Wall N face
AQ13	40.428713	29.731968	Wall N face
AQ14	40.428737	29.731699	Wall N face
AQ16	40.428705	29.732405	Wall N face
AQ17	40.428555	29.7356	Wall N face
AQ18	40.428524	29.736018	Wall N face
AQ19	40.428779	29.730635	Wall S face
AQ20	40.428719	29.730503	Wall S face
AQ22	40.428662	29.72996	Wall S face
AQ25	40.4286833	29.7302505	Wall S face
AQ28	40.42872	29.730365	Wall N face
AQ33	40.428713	29.730347	Wall N face
AQ34	40.428717	29.73037	Wall N face
AQ37	40.428742	29.73052	Wall N face
AQ38	40.428746	29.730554	Wall N face
AQ44	40.428405	29.736874	Reinforcement brick structure
AQ45	40.428655	29.729618	Arch
AQ46	40.4269	29.7388	Underground section
AQ47	40.4233	29.7418	Underground section
W1	40.4296	29.728884	Outer wall 45/46, outer facing
W2	40.429676	29.728791	Outer wall, outer facing
W3	40.429913	29.728396	Inner wall, T46 base
W4	40.429913	29.728396	Inner wall, T46 base
W5	40.429913	29.728396	Inner wall, T46 base
W6	40.429913	29.728396	Inner wall, T46 base
W7	40.429913	29.728396	Inner wall, T46 base
W8	40.429913	29.728396	Inner wall, T46 base
W9	40.429913	29.728396	Inner wall, T46
W10	40.430041	29.728097	W46-47
W11	40.431735		Isolated ashlar wall section
W12	40.431735		Isolated ashlar wall section
W13	40.431735	29.726386	Isolated ashlar wall section
W15	40.431735	29.726386	Isolated ashlar wall section

W16	40.431735	
W17	40.432509	29.725585 W52/53
W18	40.432822	29.725154 T53 base
W19	40.432822	29.725154 T53 base
W20	40.433132	29.724737 T54
W21	40.432959	29.724893 W53/54
W22	40.432959	29.724893 W53/54
W23	40.432959	29.724893 W53/54
W24	40.433132	29.724737 T54 base
W26	40.433321	29.724417 W54/55 inner wall
W27	40.433324	29.724601 W54/55 outer wall
W28	40.433731	29.724092 W55/56 outer wall
W29	40.433686	29.723945 W55/56 inner wall
W30	40.434126	29.723269 T57
W31	40.434126	29.723269 T57 base
W32	40.434126	
W33	40.434126	
W34	40.434126	29.723269 T57 base
W36	40.434126	
W37	40.434126	
W38	40.434126	
W39	40.434126	29.723269 T57 base
W40	40.434126	29.723269 T57 base
W41	40.434402	
W42	40.434402	29.722751 T58 central part
W43	40.434402	29.722751 T58 eastern western part
W44	40.435115	29.722236 W59/60
W46	40.435342	29.721959 T61
W48	40.435383	
W50	40.435628	
W51	40.435894	29.721191 W63/64
W52	40.436003	29.721319 Outer wall in front of T64
W53	40.436131	29.721105 W64/65
W55	40.436225	29.721108 W64/65 and T65
W56	40.436454	29.72052 Istanbul Gate, inner door
W57	40.436427	29.720472 Istanbul Gate, inner door, inner facing
W58	40.436477	29.720354 Istanbul Gate, inner door, outer facing
W59	40.436448	29.720308 Istanbul Gate, inner door
W60	40.43647	29.720394 Istanbul Gate, inner door, outer facing
W60 W61	40.436576	29.720927 T66
W62	40.436576	29.720927 T66
W63	40.436576	29.720927 T66
W64	40.436376	29.720927 100 29.720995 W65/66
W65	40.436742	29.720384 Istanbul Gate, outer wall, west tower
W65 W66	40.436742	29.720384 Tstanbur Gate, outer wan, west tower 29.720384 T68
W67	40.436742	29.720364 108 29.720047 W68/69 outer facing
W68	40.436235	29.719516 W69/70 outer wall

W	59	40.436235	29.719516	W69/70 inner wall, outer facing
W	71	40.436235	29.719516	W69/70 inner wall, outer facing
W	72	40.436235	29.719516	W69/70 inner wall, outer facing
W	195	40.436027	29.71912	Т70
W	74	40.436042	29.718953	W70/71 outer wall, inner facing
W	75	40.435916	29.718792	W70/71 outer wall, inner facing
W	76	40.435916	29.718792	W70/71 outer wall, inner facing
W	77	40.436042	29.718953	W70/71 outer wall, inner facing
W	78	40.43568	29.718494	T71
W	79	40.43568	29.718494	T71
W	30	40.43568	29.718494	T71
W	32	40.435075	29.717725	W72/73 inner wall
W	83	40.434984	29.717525	W72/73 inner wall
W	34	40.434931	29.717425	Т73
W	85	40.434811	29.717285	W73/74
W	37	40.434563	29.71684	T74
W	38	40.434563	29.71684	Т74
W	39	40.434494	29.716566	W74/75 outer wall
W	91	40.432208	29.71437	W80/84
W	92	40.429951	29.713724	T84
W	94	40.427988	29.713183	Т88
W	95	40.427319	29.712449	W98/lake
W	97	40.426883	29.713197	-
W	98	40.425862	29.71382	Т92
W	99	40.425793	29.713872	South Lake Gate, N side, inner face
W	100	40.425793		South Lake Gate, N side, inner face
W	102	40.425567	29.713889	Т94
W	192	40.425567	29.713889	W94/95
W	103	40.425567	29.713889	W94/95
W	104	40.425567	29.713889	W94/95
W	105	40.425567	29.713889	W94/95
W	107	40.423719	29.716242	Corner of outer wall in front of T104
W	108	40.423556	29.716381	W104/105
W	109	40.423151	29.716195	W105/106 outer wall, outer facing
W	110	40.422964	29.716464	T106
W	111	40.422805	29.71671	T107
W	112	40.422977	29.718715	T113
W	113	40.42347	29.719166	Yenisehir central Gate, inner facing
W	114	40.42347	29.719166	Yenisehir central Gate, inner facing
W	115	40.42347	29.719166	Yenisehir central Gate, inner facing
W	116	40.423557	29.719208	Yenisehir inner Gate
W	117	40.423458	29.719218	Yenisehir central Gate, inner facing
W	118	40.423436	29.719221	Yenisehir central Gate
W	119	40.423419	29.719221	Yenisehir central Gate, outer facing
W	120	40.423419	29.719221	Yenisehir central Gate, inner facing
W	121	40.423256	29.719346	Outer wall in front of T1
W	122	40.423256	29.719346	Outer wall in front of T1

W190	40.423256	29.719346	T1
W191	40.423256	29.719346	T1
W183	40.423324	29.719195	Yenisehir outer Gate
W123	40.423444	29.720843	W4/5, inner wall, inner facing
W124	40.423412	29.720966	W5/6, inner wall, inner facing
W125	40.423396	29.721499	W6/7, inner wall, inner facing
W126	40.423397	29.720636	Τ4
W127	40.423384	29.720794	W4/5, inner wall, outer facing
W128	40.423376	29.720968	Τ5
W130	40.423355	29.721288	Тб
W131	40.423355	29.72157	T7 west corner
W132	40.423324	29.722092	W8/9
W133	40.423324	29.722092	W8/9
W134	40.423291	29.722828	W10/11
W135	40.423267	29.722987	T113
W136	40.423121	29.724184	T15
W137	40.423122	29.724185	
W138	40.423163	29.724557	T16
W139	40.423164	29.724558	T16
W140	40.423147		
W141	40.423148	29.724881	
W142	40.423109	29.725546	
W143	40.42311	29.725547	
W192	40.42311		-
W144	40.423073	29.725906	T20
W145	40.423122	29.725974	
W146	40.423285	29.725959	-
W147	40.42366	29.726168	•
W148	40.423768	29.726252	W22/23
W196	40.424062	29.726438	T23
W150	40.424114	29.726442	W23/24
W151	40.424634	29.726782	
W152	40.424528	29.726733	-
W153	40.424529	29.726734	-
W158	40.424693	29.726793	-
W159	40.425094	29.726994	-
W160	40.425358	29.727153	-
W162	40.428028	29.728775	
W163	40.428029	29.728776	
W164	40.427785	29.728624	
W165	40.427786	29.728625	T38
W166	40.427334	29.728366	
W168	40.426912	29.728086	
W194	40.426912	29.728086	
W193	40.426421	29.727916	
W170	40.427809		T38, inner face
W171	40.42646	29.727753	T33, inner face

W172	40.426255	29.727625 T32, inner face
W173	40.425552	29.727225 T29, inner face
W175	40.425552	29.727225 W26/27, inner face
W176	40.425552	29.727225 W26/27, inner face
W177	40.424649	29.726709 T26, inner face
W178	40.424649	29.726709 W26/25, inner face
W180	40.423714	29.726154 T21, inner face
W180	40.423212	29.724522 T16, inner face
W182	40.423212	29.724522 T16, inner face
W184	40.436644	29.720502 Istanbul central Gate
W185	40.428902	29.729214 Lefke central Gate
W186	40.42885	29.729057 Lefke Gate western area
W187	40.42885	29.729057 Lefke Gate western area
W189	40.428959	29.729073 Lefke Gate western area
W189	40.428959	29.729073 Lefke Gate western area
C1	40.429817	29.726843 Yesilcamii, west wall
C2	40.429817	29.726843 Yesilcamii, west wall
C4	40.429861	29.726921 Yesilcamii, north wall
C5	40.429861	29.726921 Yesilcamii, north wall
C48	40.429861	29.726921 Yesilcamii, north wall
C6	40.429001	29.719755 Celebi Camii, north wall
C8	40.428146	29.719755 Celebi Camii, north wall
C9	40.428306	29.720615 II. Murhat Hamami, east wall
C10	40.42822	29.720528 II. Murhat Hamami, south wall
C11	40.429246	29.720232 Aya Sofya, north wall, inner facing
C12	40.429253	29.720228 Aya Sofya, NE room
C15	40.429213	29.720259 Aya Sofya, NE wall of nave
C17	40.429253	29.720228 Aya Sofya, NE room
C48	40.426283	29.717399 Terracotta building next to theater
C18	40.42645	29.716512 Theater, southern side
C19	40.42652	29.716529 Theater, entry corridor
C21	40.426367	29.71674 Theater, corridor wall
C23	40.426524	29.716357 Theater, western side
C24	40.426624	29.716357 Theater, western side
C25	40.426468	29.717228 Theater, SE side
C28	40.426468	29.717228 Theater, S corridor
C29	40.426786	29.716731 Theater scene, outer western vault
C32	40.426786	29.716731 Theater scene, inner western vault
C33	40.426774	29.717086 Theater scene, inner western vault
C35	40.426774	29.7169 Theater, inner corridor
C36	40.426463	29.716554 Theater, S side
C37	40.420403	29.717116 Theater, NE side
C39	40.426794	29.716992 Theater, NE side
C39 C40	40.428866	29.731713 Candarli Hayretin Pasa, east room
C40 C41	40.428964	29.731713 Candarli Hayretin Pasa, east room
C41 C42	40.428964	29.731713 Candarli Hayretin Pasa, east room
C42 C46	40.428964	29.731616 Candarli Hayretin Pasa, west room
C40	40.420303	25.751010 Candani Hayretiii Fasa, west 10011

C47	40.428969	29.731616 Candarli Hayretin Pasa, west room
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01 40.487589 29.701961 Obelisk

B1 40.42575 29.7095 Lake basilica

Important sinter deposit90Collapsed facing900Collapsed facing900Sinter deposit900Sinter deposit900Collapse facing900Large and deep collapse900Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900Thick sinter deposit900
Collapsed facing900Sinter deposit9090Sinter deposit9090Collapse facing900Large and deep collapse900Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Sinter deposit90Sinter deposit90Collapse facing90Large and deep collapse900Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Sinter deposit90Collapse facing90Large and deep collapse900Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Collapse facing90Large and deep collapse900Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Large and deep collapse900Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Sinter deposit and collapse900Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Collapsed facing900Large and deep collapse900Collapsed facing + sinter deposit900
Large and deep collapse900Collapsed facing + sinter deposit900
Collapsed facing + sinter deposit900
Thick sinter deposit90
General wall warping northward 90 0
Thick sinter deposit 90
Collapsed facing 90 0
Wall warping southward900
Wall warping northward900
Sinter deposit 90
Tilted wall 90 0
Sinter deposit 90
Sinter deposit 90
Sinter deposit 90
Top of wall warping northward900
Tilted wall900
Tilted wall900
General wall warping northward 90 0
Destruction of top of structure 90
Damaged keystone 90
Vertical offset
Vertical offset
Collapsed part between cracks 135
Significant crack at junction between tower and wall 135
Expulsion of block corners, cracks070
In-plane offset blocks 0 0
In-plane offset blocks 135 135
Out-of-plane offset blocks13545
In-plane offset blocks 135 135
Out-of-plane offset blocks13545
Cracks in terracotta masonry 135
Expulsed block corners 135
Anticlockwise block rotation + apparent offset10010
In-plane offset blocks 90 90
Dropped ashalrs 90
Anticlockwise block rotation 88

Out-of-plane offset adjacent blocks	92	2
Expulsed block corners + out-of-plane shift	130	40
Expulsed block corners	130	
Expulsed block corner + in-plane offset	40	40
Facing collapse + cracks in core		
Out-of-plane block shift	130	40
Cracks in block	130	
Expulsed block corners	130	
Lower part of tower base is shifted outward	130	40
Significant crack with no vertical offset	130	
Crack	130	
Collapsed arch keystone	120	
Significant crack with no vertical offset	130	
Cracks	130	40
In-plane offset blocks	40	40
In-plane offset blocks	40	40
In-plane offset blocks	130 130	130 40
Out-of-plane offset blocks In-plane offset blocks	130	40 130
In-plane offset blocks	130	130
Out-of-plane offset blocks	130	40
In-plane offset blocks	40	40
Out-of-plane offset blocks	40	130
Cracks and structural collapse		100
Multiple cracks		
Crack and facing collapse		
Tilted ashlar	0	90
Destruction of superstructure		
Sinistral offset of wall	130	40
Significant crack and lower facing collapse	140	
Expulsed block corner + crack	170	
Out-of-plane arch distorsion	170	80
Expulsed block corners	170	
Significant structural collapse		
Out-of-plane block shift	90	180
Out-of-plane shift + tilting	90	180
Anticlockwise block rotation	90	
Column collapse	90	30
Out-of-plane ashlar shift and rotation	90	0
General tilting	140	0
Facing collapse under window	140	50
Facing collapse under window	50	140
Superstructure collapse	140	50
Vault collapse Facing collapse	0	85
Cracks + collapse	53	60
Wall offset	55	
wan onset	55	

Clockwise block rotation	55	
Significant crack + tilted masonry	55	
Superstructure collapse	55	135
Slight damage on blocks	55	
Partial out-of-plane facing expulsion	45	135
Offset and tilted arch	50	140
Oblique parallele cracks	45	
Tilted wall	45	135
Slightly expusled angle	135	135
Partial collapse		
Collapsed blocks	135	45
Total destruction	45	135
Superstructure collapse	45	135
Facing collapse	45	115
Crack visible from both sides of wall	45	
Crack	45	45
Collapse of western angle	135	45
Collapsed keystones on two successive arches Widespread destruction	50	
Parallel cracks		
Small crack initiated at window	10	
Apparent wall offsets	90	
Crack initiated at window	150	
Crack through beam holes	100	
Anticlockwise block rotation + expulsed block corner	0	
Block shifts + cracks	90	90
Expulsed block corner	0	
Expulsed block corner	90	
Block rotations	90	
Warped masonry + offset	90	0
Ashlar phase tilted southward + warping	90	0
Outward corner expulsion		
Collapsed blocks		
Facing collapse	0	90
Destruction of eastern part + cracks at window		
Partial destruction of superstructure		
Partial collapse around window	65	155
Collapsed blocks	90	0
Block expulsion	90	
Clockwise block rotation	90	
Block shift + rotation	96 90	0
Shifted arch keystone Shifted arch keystone	90	0
Damaged keystone	90	0
Expulsed block corners	90	
Dropped central arch	90	
Southward tilting	90	170
	50	1/0

Collapsed facing under window	0	
Collapsed facing at window	0	
Damaged keystones	90	
Large vertical crack	90	
Large vertical crack with offset layers	90	
Two "conjugated cracks" crossing arch	90	
Large structural collapse	90	0
Cracks and facing collapse	90	0
Expulsed block corner	0	0
Sub-horizontal crack at base	135	
Anti-clockwise block rotation	90	
Cracks	90	
Facing collapse	90	0
Partial collapse	90	0
Total destruction		-
Partial destruction of superstructure	0	90
Out-of-plane shift + tilting	110	0
Crack	0	
Crack	0	
Crack at base	0	
Crack	0	
Out-of-plane shift of window frame	90	0
Large crack with general shift of superstructure		45
Collapse of superstructure	90	0
Large vertical fissure		
Large vertical fissure + expulsion of upper fragment	10	100
Clockwise block rotation	19	
Partial collapse	19	110
Block and facing collapse	19	110
Slight damage on superstructure		
Cracked ashlar	19	
Large facing collapse	19	
Anticlockwise block rotation	19	
Out-of-plane shift	19	109
Large facing collapse	19	109
Superstructure collapse	19	109
Block collapse	19	109
Large crack and outward tilting	109	19
Large crack + facing collapse	109	
Large vertical crack	109	
Large vertical crack	19	
Large collapse + tension crack in superstructure	109	
Destroyed facing		
Crack	109	
Crack and facing collapse		
Large vertical, penetrative crack	19	
Two cracks, slight deformation of masonry	19	

Two vertical cracks	19	
Vertical crack	19	
Cracked and slightly dislodged block + facing collapse	19	
Cracked and shifted ashlar	19	135
Damaged arch + facing collapse	19	
Vertical crack, penetrative through masonry and base ashlar	19	
Left-lateral wall offset + slight wall warping	19	
Right-lateral offset of upper facing	90	0
Damaged arch keystone	90	
Shifted voussoir	90	
Large cracks and damaged voussoirs	0	
Lintel shift	0	0
Collapsed block	90	0
Shifted block	0	0
Shifted blocks	90	90
Dropped keystone	175	
In-plane offset blocks	175	175
Dropped and shifted keystones	85	175
In-plane offset blocks	85	85
Damaged voussoirs	85	
Shifted block	85	175
Cracked column capital		
Damaged voussoirs	175	
Damaged voussoirs	85	
Clockwise block rotation		
Deformed pavement		
Dislodged blocks	90	
Partial collapse of vaults	90	
Collapsed keystones	2	10
Collapsed block	130	40
Dropped vault block		
Multiple cracks in block		
Expulsed block corners	0	00
Out-of-plane block shift	0	90 115
Shifted keystone and voussoirs	25	115
Dropped vault block	0	00
Shifted keystone and voussoirs	0 0	90
Cracked keystone Out-of-plane block shift	0	90
Dropped vault block	0	50
Destroyed arch	90	
Collapsed block	90	0
Shifted stair block	90	0
Cracked gravestone	0	0
Cracks + corner expulsion	U	
Horizontal crak of gravestone base		
Horizontal cracks	0	
	U	

Vertical crack + slight shift Shifted and rotated blocks Destruction

Deformation strike	Other measurement	Terminus post quem	Terminus ante quem
		1208	
C		527	
C	)	527	
		1097	
		1097	
		1097	
C		1097	
C	1	527	
0		1097 1097	
C		527	
L. L.		1097	
		1097	
		1097	
C		527	
		527	
		527	
		527	
180	)	527	
		527	
		527	
		1097	
		527	
	dip 80S	527	
		1097	
		1097	
		527	
		1208	
	offset >50 cm	527	
	offset >50 cm	527	
		1222	
		1222	
		3rd c.	1254
	offset 5.5 cm	3rd c.	1254
4 -	offset 4-4.5 cm	3rd c.	1254
45	offset 5-9 cm offset 2.5-3 cm	3rd c.	1254
4	offset 2.5-3 cm	3rd c.	1254
40	UIISEL 2.J UII	3rd c. 3rd c.	1254 1254
		3rd c.	1204
	rotation 10°; offset 8-10cm	3rd c.	
	offset 5-9 cm	3rd c.	
	drop 6 cm	3rd c.	
	rotation 4°	3rd c.	

	offset 3-4 cm each	3rd c.		
40	shift 3 cm	3rd c.		
		3rd c.		
		3rd c.		
			858	
40			730	
			730	
			730	
40			858	
			730	
			1222	
			1222	
		3rd c.		
		3rd c.		
	shift 2 cm	3rd c.		1097
	shift 4 cm	3rd c.		1097
	shift 15 cm and 4 cm	3rd c.		1097
40	shift 3.5 cm	3rd c.		1097
	shift 3 cm	3rd c.		
	shift 3-4 cm	3rd c.		
40	shift 4 cm; dip 5-10°	3rd c.		
24.0	shift 2.5-3.5 cm	3rd c.		
310	shift 4 cm	3rd c.	1200	
	crack plane N060 dip 70E		1260	
	crack plane N040 dip 60		1260	
00	crack dip > 80E dip 5°	3rd c.	1260	
90	up 5	Siu c.	1208	
	offset 15 cm		1208	
		3rd c.	1222	
		3rd c.		
	keystone offset 6 cm	510 0.	1222	
			858	
			858	
180	shift 5 cm	3rd c.		
180	shift 6 cm; tilt 5°	3rd c.		
	max rotation 20°	3rd c.		1185
30		3rd c.		
0		3rd c.		1185
0			858	
50			858	
140			858	
50			858	
			1222	
265			1208	
		3rd c.		
	dextral offset 10 cm		1222	

		1143	
	3rd c.		
315		1143	
		730	
135		1222	
dextral offset 20 cm		1222	
crack dip 45° NE		1222	
dip 85° NW		1222	
315		730	
		730	
45		730	
315		730	
315		1143	
295	3rd c.		
crack dip 70W	3rd c.		
crack plane azimuth 165	3rd c.		
225	3rd c.		
225	Sid C.	4000	
		1222	
	3rd c.		
	3rd c.		1330
		1260	
left-lateral offset 40 cm		730	
	3rd c.		
creek plane 020 (EM			
crack plane 030 65W	3rd c.		
rotation 6°	3rd c.		1254
shifts 1-11cm	3rd c.		1254
		730	1254
		730	1254
		730	1254
		1208	1201
			4054
tilt 10°		730	1254
		1222	
	3rd c.		
		1222	
		1208	
	3rd c.		
166	Siuc.	050	
155	- ·	858	
0	2nd c.		
	2nd c.		
rotation 8°	2nd c.		
rotation 5°	2nd c.		
0 horizontal shift + slight drop	2nd c.		
180	2nd c.		
	2nd c.		
	2nd c.		
		1222	
170		1222	

			858	
			858	
			1222	
		3rd c.		
		3rd c.		
	crack plane 90, dip 60°		1208	
180		3rd c.	1200	
180		3rd c.		
	shear plane NE-SW		858	
	plane azimuth NE-SW, dip 20N	3rd c.		
			1143	
	dip 35-40°	3rd c.		
180		3rd c.		
180		510 0.	1222	
100				
			858	
90			1208	
180	shift 6 cm; tilt 5°		858	1
	dip 50 NW		1208	
	dip 45 S		1208	
	dip 55 S		858	
	dip 50 S		858	
180			1208	
			1208	
180	1		1065	
	dextral offset		1222	
100	dextral offset		1222	
			730	
110				
110			730	
110			730	
			1222	
			730	
			1208	
			730	
109			730	
109			730	
109			730	
109			730	
19			858	
	crack dip 55 N		858	
	crack dip 70 S	3rd c.		
	crack dip 80 N	3rd c.		
	crack dip 70 N	514 61	1065	
		ع امعا	1002	
		3rd c.		
	crack dip 60°	3rd c.		
			1065	
		3rd c.		1
	crack dip 80°	3rd c.		1
	- 1			

crack dip 80°	3rd c.		858
slight vertical shift in masonry	3rd c.		1065
125	3rd c.		
135	3rd c. 3rd c.		
	3rd c.		858
offset 30-40 cm	3rd c.		070
01361 30-40 Cm	3rd c.		1065
	3rd c.		1005
	2nd c.		858
	2nd c.		
180	3rd c.		1254
180	3rd c.		858
0	3rd c.		
270	3rd c.		
		1378	
175		1378	
175		1378	
		1378	
		1378	
355		1442	
		1442	
		1421	
		1421	
rotation 5°		527	787
		1260	
		527	787
		1260	
220	2nd c.	1208	
220	2nd c. 2nd c.		
	2nd c. 2nd c.		
	2nd c. 2nd c.		
270	2nd c.		
tilt 5-10°; vertical shift 2.5-5 cm	2nd c.		
	2nd c.		
90 tilt 6°; drop 1-2 cm	2nd c.		
	2nd c.		
270	2nd c.		
	2nd c.		
	2nd c.		
0	2nd c.		
0	2nd c.		
		1387	
		1387	
		1387	
		1387	

left-lateral

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Vulnerability class	Damage grade Non-seismic causing processes?	Quality rank Ref (if other study)
В	3 Recent, natural decay	3 Benjelloun et al. (2018)
В	3 Recent, natural decay	3 Benjelloun et al. (2018)
А	3 War damage	2 Benjelloun et al. (2018)
А	2 Recent, natural decay	3 Benjelloun et al. (2018)
А	2 Recent, natural decay	3 Benjelloun et al. (2018)
А	3 War damage	2 Benjelloun et al. (2018)
А	3 War damage	2 Benjelloun et al. (2018)
А	3 War damage	2 Benjelloun et al. (2018)
А	3 War damage	2 Benjelloun et al. (2018)
А	3 War damage	2 Benjelloun et al. (2018)
А	3 Recent, natural decay	3 Benjelloun et al. (2018)
А	3 Recent, natural decay	3 Benjelloun et al. (2018)
А	1 Soil instability, original construction	3 Benjelloun et al. (2018)
А	2 Recent, natural decay	3 Benjelloun et al. (2018)
А	3 Man-made damage, natural decay	3 Benjelloun et al. (2018)
А	1 Original construction	3 Benjelloun et al. (2018)
А	1 Original construction	3 Benjelloun et al. (2018)
А	2 Recent, natural decay	3 Benjelloun et al. (2018)
А	1 Soil instability	2 Benjelloun et al. (2018)
А	3 Recent, natural decay	3 Benjelloun et al. (2018)
В	2 Recent, natural decay	3 Benjelloun et al. (2018)
А	3 Recent, natural decay	3 Benjelloun et al. (2018)
А	1	1 Benjelloun et al. (2018)
А	1 Soil instability	2 Benjelloun et al. (2018)
А	1 Soil instability	2 Benjelloun et al. (2018)
А	1 Original construction	2 Benjelloun et al. (2018)
В	4 Man-made damage	3 Benjelloun et al. (2018)
В	2 Recent, vehicles traffic	3 Benjelloun et al. (2018)
В	1	1 Benjelloun et al. (2018)
В	1	1 Benjelloun et al. (2018)
Α	3 Original construction, natural decay	3
А	3 Foundation failure, soil instability	3
В	2	1
В	2	1
В	2	1
В	2	1
В	2	1
В	2	1
В	3	1
В	2	1
С	2 Dubious context, man-made	3
С	2 Dubious context, man-made	3
С	2 Dubious context, man-made	3
С	2 Dubious context, man-made	3

С	2 Dubious context, man-made	3
В	2	1
В	2	1
В	2	1
В	4 War damage	2
В	2	1
В	2 Wardamaga	
	2 War damage	2
В	2	1
В	2 Original construction	2
_		
В	3	1
В	3	1
В	3 Man-made damage	2
В	3	1
В	2 War damage	2
В	2	1
В	2	1
В	2	1
В	2	1
В	2	1
В	2	1
В	2	1
_		
В	2	1
В	2	1
В	4 Natural decay	2
	-	
В	2 Natural decay	2
В	4 Natural decay	2
В	2	1
В	5 War damage	2
А	1 Original construction	3
В	4 War damage	2
_		
В	2	1
А	3 Vegetation	2
В	2	1
В	3 War damage	2
С	2	1
С	2	1
C	2	1
С	5 Dubious context, natural decay	3
С	2	1
В	2 Foundation failure, soil instability	3
В	3 War damage	2
В	3 War damage	2
В	5 War damage	2
А	4	1
В	4 Natural decay	2
	-	
В	3 War damage, natural decay	3
В	2 Original construction	3

В	2	1
В	3 War damage	2
В	3 War damage	2
С	1 War damage, natural decay	3
A	3 Original construction	2
A	3 Foundation failure, soil instability	3
A	2 Natural decay	2
A	1 Soil instability	2
С	2	1
С	4 War damage, natural decay	3
С	2 War damage	2
С	5 War damage, natural decay	3
В	4 War damage, natural decay	3
В	4 War damage, natural decay	3
В	3 War damage	2
В	3 War damage	2
В	4 War damage, natural decay	3
A	4	1
В	5 Dubious context	3
В	4 Natural decay	2
В	2 Natural decay	2
C	2 Original construction	3
В	2 War damage, natural decay	3
В	2 War damage, natural decay	3
В	2	1
В	2	1
C	2	1
C	2	1
C	2	1
В	1 Original construction	2
C	1	1
A	3 Natural decay	2
В	2 War damage, natural decay	3
A	5	1
В	4 Natural decay	2
В	4 Natural decay	2
В	3 War damage, natural decay	3
С	4 War damage	2
С	4	1
С	2	1
C	2	1
C	2	1
C	2	1
C	4	1
C	2	1
A	3 Soil instability	2
A	2 Soil instability	2

B4 War damageB4 War damageA3 Natural decayB3 Original constructionB3 Natural decayB4 War damage, natural decayB4 War damage, natural decayB2B3 War damage, natural decayB2B3 War damageB2B3 War damageB2B3 War damageB2B4 War damage, natural decayB2B4 Natural decayB2B3 Natural decayB2B3 Natural decayB2B3 Natural decayB2B4C3 Natural decayB2B4B4B4B4B4B3B2B3B3B2B4B4B4B4B2B3B2B4B4B2B3B2B4B2B3B2B4B2B2B2B3B2		
A3 Natural decayB3 Var damageB3 Original constructionB3 Natural decayB4 War damage, natural decayB4 War damage, natural decayB2B3 War damageB2B3 War damageB4 War damage, natural decayB2B3 War damageB4 War damage, natural decayB5 Dubious contextB4 Natural decayB2B3 Natural decayB2B3 Natural decayB2B3 Natural decayB2B3 Natural decayB2B3 Natural decayC3 Natural decayB2B3 Natural decayC3 Natural decayB2 War damageB3 War damageB4 War damageB3 War damageB2 War damageB2 War damageB2 War damageB2 War damageB2 War damageB3 Natural decayB2 War damageB3 Natural decayB3 Natural decayB3 Natural decayB3 War damage, natural decayB3 War damageB3 War damageB3 Natural decay, war damageB3 War damage, natural decayB </td <td>4 War damage</td> <td>2</td>	4 War damage	2
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	4 War damage, natural decay	3
B 3 War damage, natural decay	3 War damage, natural decay	3
	3 War damage, natural decay	3
В 3		1
B 2 Natural decay		2
		2

В	3	1
В	3	1
В	2	1
В	2	1
В	3 Natural decay	2
В	3	1
В	1 Original construction	3
В	2 Dubious context	3
В	3 Natural decay	2
C	2	1
C	2	1
C	4 Natural decay	2
C	3	1
C	2	1
C	2	1
C	2	1
C	2	1
C	2	1
C	2	1
C	2	1
C	2	1
C	2 Natural decay	2
В	2	1
В	2	1
В	2	1
В	2 Soil instability	2
В	2	1
В	3 Natural decay	2
В	3 Natural decay	2
В	3 Man-made	2
В	2 Natural decay, original construction	3
В	2 Natural decay	2
В	2	1
В	2	1
В	2	1
В	2 Natural decay, original construction	3
В	2	1
В	2	1
В	2	1
В	2 Natural decay, original construction	3
В	3 Man-made	2
B	2 Man-made	2
В	2	1
B	2 Dubious context	3
В	2 Dubious context	3
B	3 Dubious context	3
В	3 Dubious context	3

В	2 Dubious context	3
C	2	1
В	5	1

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## **Reconstruction EAE dataset**

RC1         40.426492         29.716886 Theater, inner corridor           RC2         40.429246         29.720232 Aya Sofya, N inner wall	Reinforcement Repair Repair
RC2 40.429246 29.720232 Ava Sofva, N inner wall	•
	Repair
RC3 40.429213 29.720259 Aya Sofya, NE wall of nave	
RC4 40.429213 29.720259 Aya Sofya, N wall	Reinforcement
RC5 40.428306 29.720615 II. Murhat Hamami, east door	Reinforcement
RC8 40.42822 29.720528 II. Murhat Hamami, south door	Reinforcement
RC11 40.429817 29.726843 Yesilcamii, nort door	Reinforcement
RW2 40.42885 29.729057 Lefke Gate, SW area	Reinforcement
RW5 40.429913 29.728396 T46	Repair
RW6 40.434126 29.723269 T57 base	Repair
RW7 40.436477 29.720354 Istanbul inner Gate	Reconstruction
RW8 40.436235 29.719516 Outer wall in front of T61, inner fa	cing Repair
RW10 40.429951 29.713724 T84	Reconstruction
RW11 40.428476 29.713401 W87/88	Reinforcement
RW12 40.425793 29.713872 South Lake Gate	Reconstruction
RW13 40.425554 28.714165 W94/95	Reconstruction
RW14 40.425462 29.715602 T97	Reinforcement
RW18 40.423714 29.726154 T21, inner wall, inner facing	Repair
RW19 40.423212 29.724522 T16, inner wall, inner facing	Reconstruction
RAQ1 40.428735 29.730474 Close to arch 8, northern facing	Reconstruction
RAQ3 40.428728 29.731783 Aqueduct, northern facing	Reinforcement
RAQ4 40.42871 29.732231 Aqueduct, northern facing	Reconstruction
RAQ5 40.428702 29.732815 Aqueduct, northern facing	Reinforcement
RAQ7 40.4287 29.732951 Aqueduct, northern facing	Reinforcement
RAQ8 40.428403 29.736874 Aqueduct, northern facing	Reinforcement
RAQ9 40.428667 29.729747 Arch 7, southern facing	Reinforcement

Description	Date range	Ref (if other study)
Imbricated, polygonal bocks	2nd c.	
Pink mortar sealing	8th c.	
Terracotta and white mortar sealing	8th c.	
Walled windows	13th c. ?	
Seismoresistant technique on arch	Early 15th c.	
Seismoresistant technique on arch	Early 15th c.	
Seismoresistant technique on arch	Late 14th c.	
Walled opening	12-13th c.	
Light pink mortar on crack	12-13th c.	
Thicker terracotta masonry	12-13th c.	
Mixed terracotta+rubble masonry	1143-1180	
Bright mortar on wall offset	Early 13th c.	
Mixed terracotta+rubble masonry	Late 13th c.	
Buttress	Late 12th c.	
Terracotta masonry with yellowish pink mortar	Early 13th c.?	
Mixed terracotta+rubble masonry	12-13th c.	
Mixed terracotta+rubble masonry	1222-1330	
Mortar on wall offset		
Very similar style to surrounding walls		
Limestone and travertine rubble + marble spoils	Early 11th c.	Benjelloun et al. (2018)
Walled arch	6th-11th c.	Benjelloun et al. (2018)
Mixed materials (terracottas, spoils)	11th c.	Benjelloun et al. (2018)
Walled arch	6th-11th c.	Benjelloun et al. (2018)
Walled arch	6th-11th c.	Benjelloun et al. (2018)
Buttress-like brick structure	6th-11th c.	Benjelloun et al. (2018)
New travertine facing over terracotta	6th-11th c.	Benjelloun et al. (2018)

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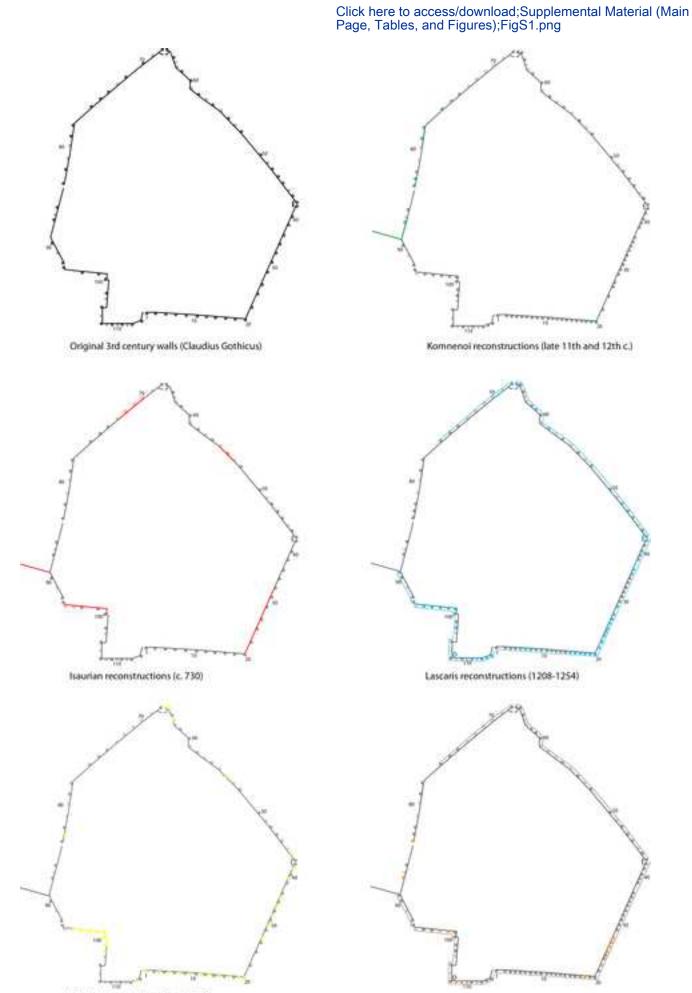
Orientation	Length (m)	% Length	Q1	%Q1	Q1+Q2	%Q1+Q2
N-S	1124	12.7	25	30.8	45	31.3
NE-SW	2478	28.1	8	9.9	16	11.1
E-W	3319	37.6	29	35.8	54	37.5
NW-SE	1912	21.6	19	23.5	29	20.1

Q1+Q2+Q3	%Q1+Q2+Q3
53	26.5
24	12
88	44
35	17.5

<u>±</u>

Name	Date	Event location (lat;lon)	Event depth (km)	Moment magnitude	Station code	Station location (lat;lon)
Düzce	11/12/1999	40.81;31.19	10.4	7.3	8101	40.84;31.15
Azores Islands	7/9/1998	38.61;-28.57	10	6.1	HOR	38.53;-28.63
Patti Gulf	4/15/1978	38.27;15.11	22	6.0	MLZ	38.23;15.24
Patti Gulf	4/15/1978	38.27;15.11	22	6.0	PTT1	38.15;14.97
Kyllini	10/16/1988	37.93;20.92	25	5.9	ZAK1	37.79;20.90

Epicentral distance (km)	
5.3	
10.7	
12.5	
18.3	
15.7	



Michael III reconstructions (c. 858

Palaeologue reconstructions (1254-1331)

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