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# Effect of homogeneous Fenton combined with electron transfer on the fate of inorganic chlorinated species in synthetic and reclaimed municipal wastewater

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## **Accepted version**

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#### **ABSTRACT**

This study newly investigates in detail the fate of inorganic chlorinated species and potential interference with other inorganic compounds such as phosphate, inorganic carbon and nitrogenous species during the electro-Fenton treatment of synthetic and reclaimed wastewater. A mathematical model was proposed to validate reaction pathways and rate constants of chlorinated species. The comparison of modeling results with experimental data of both synthetic and real solutions was quite good, with root mean square error (RMSE) values less than 0.084. Upon further testing, the results also showed that adding carbonate, phosphate and inorganic nitrogen species did not affect the chlorate and volatile chlorinated species accumulation subsequent to the decay of chloride ions during electro-Fenton. The established pathway in both synthetic and real chlorinated matrices could help to understand and predict the concentration profiles of chlorinated species in wastewater when implementing such electrocatalysis as a complementary treatment. This work also highlights the need to take into account the management of chlorinated intermediates when implementing this technology at larger scale.

**Keywords:** electro-oxidation/reduction; electro-Fenton; kinetic modeling; chlorinated inorganic species; reclaimed wastewater

#### 1. Introduction

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Water is in high demand due to rising global population, rapid urbanization, increased agriculture, and economic growth while, concurrently, water quality is degrading [1]. As a result of these circumstances, providing people access to clean water becomes more and more challenging every day. Wastewater treatment plants (WWTP) are being increasingly contaminated with micropollutants that are released into the waterbodies [2]. This increase, in combination with industrial discharge and agricultural runoff, result in approximately 80% of wastewater returning to the environment without treatment [1]. Categorized into several groups, micropollutants include pharmaceuticals consumed and discharged by humans, metals from industry, or pesticides used in agriculture [2]. Freshwater in Europe is being contaminated by more than 100,000 registered chemicals. The increasing commonality and production of chemicals coupled with an increase in population and demand for clean drinking water pose new challenges for wastewater treatment facilities [3]. The major biological treatment processes currently being employed at most municipal WWTP are unable to fully degrade many of the organic compounds in the effluent stream [2]. The presence of organic micropollutants in drinking water and surface water is causing great concern for the health of humans and aquatic organisms. Even in low concentrations, organic micropollutants may have negative hormonal, carcinogenic and reproductive impacts in human health and otherwise harm the environment [4]. There are opportunities to decrease this quantity of micropollutants and increase the water quality through actions such as the reuse of treated wastewater by implementing complementary advanced physico-chemical treatment technologies [3]. In this study, the water treatment method of electrolysis is investigated using electro-Fenton conditions, an advanced oxidation process for biorecalcitrant organic pollutants removal in wastewater. The electrochemical advanced oxidation processes (EAOPs) have gain increasing interests for their ability to continuously produce hydroxyl radicals (\*OH) using low concentration of chemicals or even no reagents by implementing electrocatalysis [5,6]. OH can react very quickly with biorecalcitrant organic compounds, especially with double C=C bonds, which made them very useful for such water application [7]. EAOPs allow reaching very high degradation and mineralization yields in synthetic or real effluents, as compared to the chemical AOPs [8,9]. Electro-Fenton (EF) has been widely studied due to some advantages compared to chemical Fenton. It allows regenerating ferric ion (Fe<sup>3+</sup>) into Fe<sup>2+</sup> (Eq. 1) and electrogenerating H<sub>2</sub>O<sub>2</sub> in situ (Eq. 2) through reduction reactions at the cathode.

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$$Fe^{3+} + e^{-} \rightarrow Fe^{2+}$$
 (1)

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$$O_2 + 2H^+ + 2e^- \rightarrow H_2O_2$$
 (2)

The combination of  $Fe^{2+}$  and  $H_2O_2$  then permits the production of OH through the Fenton reaction (Eq.

53 <u>3</u>).

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$$Fe^{2+} + H_2O_2 \rightarrow Fe^{3+} + {}^{\bullet}OH + OH^{-}$$
 (3)

Numerous investigations have been performed on the degradation/mineralization kinetics study of single pollutant or with cocktail of pollutants in synthetic solution [10–14] while some investigations have

been performed in real effluents [15–18]. However, one of the disadvantages of the oxidation processes

is the potential to generate harmful by-products, even more harmful than the original pollutants [19,20].

Some efforts have been made to identify and quantify the organic by-products formed during the

electrolysis and assess the ecotoxicity. The fate of the inorganic matrix and its influence on kinetics has

been barely studied, especially in homogeneous Fenton process combined with direct electro-

oxidation/reduction. The concentration profiles of inorganic nitrogen species has been studied in

advanced electro-oxidation conditions [21-26] and more recently in electro-Fenton process combined

with a modeling study [27]. The evolution of concentration of inorganic chlorinated species has been

mainly studied in electro-oxidation process, especially for electro-disinfection purpose [28–36]. Boron-

doped diamond (BDD) is well-known to be a non-active anode that has a strong oxidation power,

allowing not only the generation of 'OH, but also the direct oxidation of chloride ions until perchlorate

69 **[5]**.

The concentration profiles of inorganic chlorinated species in homogeneous Fenton combined with electron transfer using an active anode has never been investigated in detail. For the first time, the reaction mechanisms and kinetic pathways of various chlorinated inorganic compounds including volatile species were investigated and supported by a kinetic model study. The influence of phosphate and carbonate has been also investigated and the comparison with reclaimed municipal wastewater effluent was then examined. Through deeper understanding of the potential by-products that can be

created, this study brings new insights on the redox cycle of inorganic chlorinated species in synthetic and real effluent along with emphasizes on the possible unwanted remaining inorganic species after electrolysis.

#### 2. Experimental

#### 2.1. Chemicals

Sodium hypochlorite (NaOCl), chlorite (NaClO<sub>2</sub>), chlorate (NaClO<sub>3</sub>) and perchlorate (NaClO<sub>4</sub>) were supplied by Sigma-Aldrich (Saint-Quentin-Fallavier, France). Sodium carbonate (NaHCO<sub>3</sub>), sodium hydrogen phosphate (Na<sub>2</sub>HPO<sub>4</sub>) and sodium chloride (NaCl) were provided by VWR International (Fontenay-sous-Bois, France). Heptahydrated ferrous sulfate (FeSO<sub>4</sub>·7H<sub>2</sub>O) and sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) were purchased from Thermo-Fisher Scientific (Karlsruhe, Germany). All the chemicals were of analytical grade and were used as is.

#### 2.2. Effluent characteristics

The fate of inorganic chlorinated species taking into account Cl<sup>-</sup>, ClOH/ClO<sup>-</sup>, ClO<sub>2</sub><sup>-</sup>, ClO<sub>3</sub><sup>-</sup>, ClO<sub>4</sub><sup>-</sup> and chlorinated volatile species (Cl<sub>volatile</sub>) was determined first in synthetic wastewater to better understand each mechanism independently. A concentration of 150 mg L<sup>-1</sup> for Cl<sup>-</sup> was implemented, which is a representative concentration in reclaimed wastewater [27], while a concentration of 20 mg L<sup>-1</sup> was used for ClOH/ClO<sup>-</sup>, ClO<sub>2</sub><sup>-</sup>, ClO<sub>3</sub><sup>-</sup>, ClO<sub>4</sub><sup>-</sup>. The concentration of Cl<sub>volatile</sub> was estimated by mass balance, considering that Cl<sup>-</sup>, ClOH/ClO<sup>-</sup>, ClO<sub>2</sub><sup>-</sup>, ClO<sub>3</sub><sup>-</sup> and ClO<sub>4</sub><sup>-</sup> were the main stable dissolved inorganic chlorinated species present in the treated solution. The influence of phosphate (PO<sub>4</sub><sup>3</sup>-) (20 mg L<sup>-1</sup>) and carbonate (CO<sub>3</sub><sup>2</sup>-) (20 mg L<sup>-1</sup>) has been also assessed in synthetic solution, as they can be found in reclaimed wastewater in a range of concentrations that can vary according to the treatment implemented before the exit of the plant. In all experiments, the synthetic solutions were prepared with ultrapure water from a Purelab<sup>®</sup> water purification system (Veolia Water, Antony, France) with a resistivity higher than 18 MΩ cm at room temperature. The concentration profiles of the inorganic chlorinated species were then monitored in reclaimed wastewater sampled at the outlet of a municipal wastewater treatment plant (Reims, France). The main physico-chemical characteristics of the reclaimed wastewater has been

described in a previous study [27]. In order to avoid the presence of any potential residual particulate pollution, the reclaimed wastewater has been filtered (0.45  $\mu$ m) first before use.

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#### 2.3. Electrolytic treatments

Electrolysis experiments were conducted in a 180 mL-undivided cylindrical glass reactor connected to a HAMEG 7042-5 (Beauvais, France) power supply and operated in batch mode at  $25 \pm 1$  °C [27]. The current density was set at 2.5 mA cm<sup>-2</sup>, since it is the average optimal value depicted in previous works in similar electro-Fenton conditions [27,37,38]. Both cathode and anode used for the experiments were made out of carbon felt pieces (Mersen; Gennevilliers, France) having a geometric surface area of 50 cm<sup>2</sup>. They were pre-conditioned in order to remove any impurity from the surface though a one-hour sonication in a acetone/ultrapure water mixture [39]. Subsequently, they were rinsed with ultrapure water and stored at 60°C for 24 h. The pieces have been renewed for each experiment in order to have a better repeatability and to avoid any contamination by adsorption phenomena that could interfere the subsequent experiment using the same felt. The electrodes were placed in parallel by keeping the interelectrode distance to 1.5 cm [27]. An active anode, i.e. low O<sub>2</sub> evolution overvoltage (1.6 V vs SHE), has been selected in order to avoid the production of 'OH at its surface as previously shown in literature [27,40,41]. It ensured that the only source of 'OH could come from the Fenton reaction while only direct electron transfer could occur at cathode and anode [27]. The pH of solution was adjusted to a value of 3 with H<sub>2</sub>SO<sub>4</sub>, which has been found to be optimal for the Fenton process [42], and ferrous iron (FeSO<sub>4</sub>·7H<sub>2</sub>O) was maintained at the optimal concentration (0.1 mM) referenced in literature [27,42– 44]. A source of O<sub>2</sub> from air for H<sub>2</sub>O<sub>2</sub> electrogeneration was supplied continuously throughout the electrolysis. The solutions were continuously stirred at 500 rpm with a magnetic stirrer (Corning PC-410D) for homogeneous mixing. The addition of supporting electrolyte was not required since the average conductivity of synthetic and reclaimed wastewater was around 1 mS cm<sup>-1</sup> which was high enough. It also minimized the possible interference of the additional electrolyte with the mechanism of oxidation and reduction of the studied species during the electrolytic treatments.

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#### 2.4. Analytical procedures

134 To measure the total organic carbon (TOC), total inorganic carbon (TIC) and total nitrogenous species (TN) a Shimadzu (Marne-La-Vallée, France) V<sub>CSH</sub> analyzer combined with a TNM-1 analyzer was used. 135 The ion chromatography was conducted on a Dionex/Thermo-Fisher ICS 3000 (Noisy-Le-Grand, 136 137 France) and measured nitrite (NO<sub>2</sub><sup>-</sup>), nitrate (NO<sub>3</sub><sup>-</sup>), chloride (Cl<sup>-</sup>), chloride (ClO<sub>2</sub><sup>-</sup>), chlorate (ClO<sub>3</sub><sup>-</sup>), perchlorate (ClO<sub>4</sub><sup>-</sup>), phosphate (PO<sub>4</sub><sup>3-</sup>) and sulfate (SO<sub>4</sub><sup>2-</sup>) ions using an AS-19 anion-exchange column 138 in the conditions described previously [27]. 139 Hypochlorous acid and ammonium ions have been quantified by colorimetric method using diethyl-p-140 phenylene diamine (DPD) (program 80) and salicylate (program 801) procedures, respectively, from 141 Hach kit tests using DR-2400 Hach equipment (Lognes, France). 142

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#### 2.5. Kinetic modeling

MATLAB® modeling software was used to create a kinetic model of the concentration profiles of inorganic chlorinated species. The model used ordinary differential equations (ODE15s) to solve the system. The FMINSEARCH tool of MATLAB® was used to calibrate the model. To assess the fitting of the model in comparison with experimental data, the root mean square error (RMSE), model efficiency (ME) and the index of agreement (IoA) were calculated according to the following equations (Eqs. 4-6) [27,44]:

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151 RMSE = 
$$\sqrt{\frac{\sum_{i=1}^{K} (y_i - y_i')^2}{K}}$$
 (4)

152 ME = 
$$1 - \frac{\sum_{i=1}^{K} (y_i - y_i')^2}{\sum_{i=1}^{K} (y_i - y_M)^2}$$
 (5)

153 IoA = 
$$1 - \frac{\sum_{i=1}^{K} (y_i - y_i')^2}{\sum_{i=1}^{K} (|y_i' - y_M| + |y_i - y_M|)^2}$$
 (6)

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where K is the number of observed values,  $y_i$  is the single numerically simulated value,  $y'_i$  is the corresponding experimentally observed value,  $y_M$  is the average of the numerically simulated values.

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3. Results and discussion
Before discussing about the fate of the inorganic chlorinated species, it is important to check whether
the sulfate ions added for pH adjustment was involved in the redox reactions or not. A previous study
has shown that in the applied conditions the sulfate ions did not have any impact on the reactions [27].
Therefore, it is assumed that only chlorinated species are involved in the results presented in this section.
3.1. Redox cycle of inorganic chlorinated species in synthetic solution
3.1.1. Profiles of single inorganic chlorinated species
Experiments with single inorganic chlorinated species (Cl <sup>-</sup> , ClOH, ClO <sub>2</sub> <sup>-</sup> , ClO <sub>3</sub> <sup>-</sup> , ClO <sub>4</sub> <sup>-</sup> ) have been
performed in synthetic solutions and in acidic media (pH 3). At this pH, hypochlorous acid is the
dominant species as compared to hypochlorite ion (ClO-), since the acid dissociation constant (pKa) of
ClOH/ClO couple is 7.5 [45]. Therefore, only ClOH was considered in this study. The profiles of Cl-,
ClOH, ClO <sub>2</sub> -, ClO <sub>3</sub> -, ClO <sub>4</sub> - and Cl <sub>volatile</sub> species as function of the specific charge (Q) are displayed in
Fig. 1. Cl <sub>volatile</sub> could be ascribed to Cl <sub>2</sub> , ClO <sub>2</sub> and Cl <sub>2</sub> O that were the main volatile inorganic chlorinated
species identified in electro-oxidation process with BDD according to a previous study [46]. Moreover,
the bubbling applied during the process should facilitate the volatilization of Cl <sub>volatile</sub> .
All the equations, i.e. direct and indirect oxidation/reduction reactions involved in the redox cycle of
inorganic chlorinated species, have been represented in Table 1.

**Table 1.** direct and indirect oxidation/reduction reactions involved in the redox cycle of inorganic chlorinated species.

Reactions		Ref.
(7)	$Cl^{-} + 3H_2O \rightarrow ClO_3^{-} + 6H^{+} + 6e^{-}$	[47]
(7')	$ClO_3^- + 6H^+ + 6e^- \rightarrow Cl^- + 3H_2O$	[47]
(8) a	$2\mathbf{Cl}^2 \to \mathbf{Cl_2} + 2\mathbf{e}^2$	[45]
b	$Cl^{-} + 2H_2O \rightarrow ClO_2 + 4H^{+} + 5e^{-}$	[28]
c	$2\mathbf{Cl}^{-} + \mathbf{H}_2\mathbf{O} \rightarrow \mathbf{Cl_2O} + 2\mathbf{H}^{+} + 4\mathbf{e}^{-}$	[46]
(8') a	$Cl_2 + 2e^- \rightarrow 2Cl^-$	[45]
b	$ClO_2 + 4H^+ + 5e^- \rightarrow Cl^- + 2H_2O$	[28]
c	$\mathbf{Cl_2O} + 2\mathbf{H}^+ + 4\mathbf{e}^- \rightarrow 2\mathbf{Cl}^- + \mathbf{H}_2\mathbf{O}$	[46]
(9)	$CI + OH \rightarrow CIOH$	[46]
(9')	$CIOH^- \rightarrow CI^- + OH$	[46]
(10)	$ClO_3^- + 5Cl^- + 6H^+ \rightarrow 3H_2O + 3Cl_2$	[48]
(10')	$3Cl_2 + 3H_2O \rightarrow ClO_3^- + 5Cl^- + 6H^+$	[48]
(11)	$\mathbf{ClO_3}^{-} + 2\mathrm{H}^{+} + 2\mathrm{e}^{-} \rightarrow \mathbf{ClO_2}^{-} + 2\mathrm{H}_2\mathrm{O}$	[26]
(11') a	$ClO_2^- + 2H_2O \rightarrow ClO_3^- + 2H^+ + 2e^-$	[26]
b	$ClO_2^- + {}^{\bullet}OH \rightarrow {}^{\bullet}ClO_2 + HO^-$	[26]
c	${}^{\bullet}\text{ClO}_2 + {}^{\bullet}\text{OH} \rightarrow \text{ClO}_3 + \text{H}^+$	[26]
(12)	$2\text{ClO}_3^- + 4\text{Cl}^- + 3/2\text{O}_2 + 12\text{H}^+ + 6\text{e}^- \rightarrow 6\text{ClOH} + 3\text{H}_2\text{O}$	[26]
(12') a	$6\text{CIOH} + 3\text{H}_2\text{O} \rightarrow 2\text{CIO}_3^- + 4\text{Cl}^- + 3/2\text{O}_2 + 12\text{H}^+ + 6\text{e}^-$	[26]
(12) a	CIOH + $2\text{ClO}_2$ + $4\text{Cl} \rightarrow 2\text{ClO}_3$ + $4\text{Cl} + 3/2\text{O}_2$ + $12\text{H} + 6\text{Cl}$ ClOH + $2\text{ClO}_2$ + $4\text{Cl} \rightarrow 2\text{ClO}_3$ + $4\text{Cl} + 3/2\text{O}_2$ + $12\text{H} + 6\text{Cl}$	[49]
(13)	$ClO_2^- + 3H^+ + 2e^- \rightarrow ClOH + H_2O$	[26]
(13') a	$CIO_2 + 3H + 2C \rightarrow CIO_1 + H_2O$ $CIOH + H_2O \rightarrow CIO_2 + 3H^+ + 2e^-$	[26]
(13) a	$Clon + 112O \rightarrow Clo_2 + 511 + 2C$	[20]
ь	CIOH + 'OH $\rightarrow$ 'CIO + H <sub>2</sub> O	[26]
c	$^{\circ}ClO + ^{\circ}OH \rightarrow ClO_2^{-} + H^{+}$	[26]
(14)	$ClO_2^- \rightarrow ClO_2 + e^-$	[28]
(14')	$ClO_2 + e^- \rightarrow ClO_2^-$	[28]

During the electrolysis of chloride ion, only chlorate (Eq. 7) and Cl<sub>volatile</sub> (Eqs. 8a-8b) accumulated in solution (Fig. 1a).

The oxidation power involved in this process was not high enough to produce perchlorate, which is the inorganic chlorinated compound having the highest oxidation state. This is an interesting feature since this compound is known to be hazardous and has been classified as disinfection by-products [33]. This can be an advantage compared to non-active anode system, such as BDD-based electrolysis, that preferentially produce perchlorate [29,36]. The absence of generation of perchlorate is confirmed through the other experiments performed with ClOH (Fig. 1b), ClO<sub>2</sub>- (Fig. 1c) and ClO<sub>3</sub>- (Fig. 1d). The electrolysis of ClO<sub>4</sub>- itself (Fig. 1d) did not lead to any oxidation or reduction as its concentration remain constant all along the electrolysis, which further emphasized the stability of this compound. Perchlorate

is known to be a stable species that is the inorganic chlorinated end-product in strong oxidation conditions involved in anodic oxidation process [29,50]. During the electrolysis of ClOH, its reduction into chloride (Eq. 9') was rather quick and the decay of ClOH was complete at a specific charge of 0.5 Ah L<sup>-1</sup>. However, ClOH did not convert quantitatively into Cl<sup>-</sup> because the later was oxidized to chlorate at the anode (Eq. 7). ClOH could be also directly oxidized into chlorate (Eq. 12'a) (Fig. 1b). Contrastingly, chlorite was quickly oxidized into chlorate (Eq. 11'a-11'c) along with the chlorinated volatile production (Eq. 14) (Fig. 1c). Cl<sub>volatile</sub> seems to be predominantly produced from chlorate according to their respective opposite concentration evolution. This is in agreement with previous results that highlighted the fast formation of  $ClO_{2(g)}$  from  $ClO_2^-$  (Eq. 14) [28]. The fast decay of chlorite could explain why it was not accumulated in the experiments with Cl<sup>-</sup> and ClOH (Eqs. 13'a-13'c) unlike perchlorate that has been found to accumulate in every experiment, except with perchlorate. It is important to note that in acidic condition (pH 3), HClO<sub>2</sub> is also present in solution (10%) while ClO<sub>2</sub><sup>-</sup> remain predominant (90%), according to their pKa (HClO<sub>2</sub>/ClO<sub>2</sub><sup>-</sup>) of 2.0. It could slightly decrease the ClO<sub>2</sub> reactivity as compared to experiments performed at neutral pH or in alkaline condition such as anodic oxidation process. During the electrolysis of chlorate, Cl<sub>volatile</sub> was the main intermediate, while chloride was produced at lower extent. A reduction reaction (Eq. 7') could occur in acidic media as suggested by previous authors [47].

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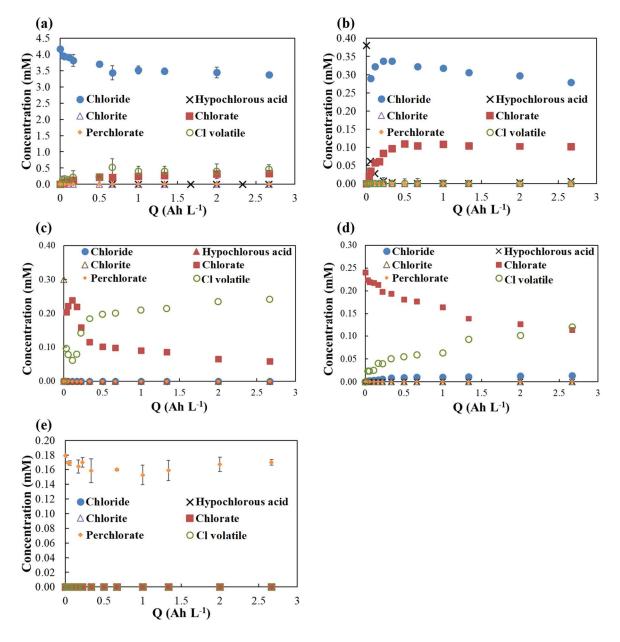
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**Fig. 1.** Profiles of Cl<sup>-</sup>, ClOH, ClO<sub>2</sub><sup>-</sup>, ClO<sub>3</sub><sup>-</sup>, ClO<sub>4</sub><sup>-</sup> and Cl<sub>volatile</sub> in synthetic solutions containing initially (a) Cl<sup>-</sup>, (b) ClOH, (c) ClO<sub>2</sub><sup>-</sup>, (d) ClO<sub>3</sub><sup>-</sup> and (e) ClO<sub>4</sub><sup>-</sup> as a function of the applied charge during electro-Fenton treatment. Initial conditions: pH 3, [Fe<sup>2+</sup>] = 0.1 mM; [Cl<sup>-</sup>] = 4.2 mM (a), [ClOH] = 0.37 mM (b), [ClO<sub>2</sub><sup>-</sup>] = 0.30 mM (c), [ClO<sub>3</sub><sup>-</sup>] = 0.24 mM (d), [ClO<sub>4</sub><sup>-</sup>] = 0.18 mM (e).

3.1.2. Profiles and reaction pathway of inorganic chlorinated species mixture

The kinetics evolution of the chlorinated inorganic species has been then determined in an acidic mixture (Fig. 2). The results were in accordance with the profiles depicted in single compound study (section 3.1.1). The chlorate and Cl<sub>volatile</sub> tended to accumulate while the concentrations of chloride, chlorite and

hypochlorous acid were decreasing and the concentration of perchlorate remained constant. Still, a difference with ClOH profile was noticed, since its decay was not complete after 2.7 Ah L<sup>-1</sup> (Fig. 2b). With the initial presence of ClO<sub>2</sub>, the presence of ClO<sub>2</sub> generated from Eq. 14 could also contribute to the oxidation of ClOH (Eq. 12'b). In the meantime, ClOH could be produced from Cl<sup>-</sup> oxidation (Eq. 9), ClO<sub>2</sub> reduction (Eq. 13) and ClO<sub>3</sub> reduction (Eq. 12), which compensated the rate of ClOH decay.



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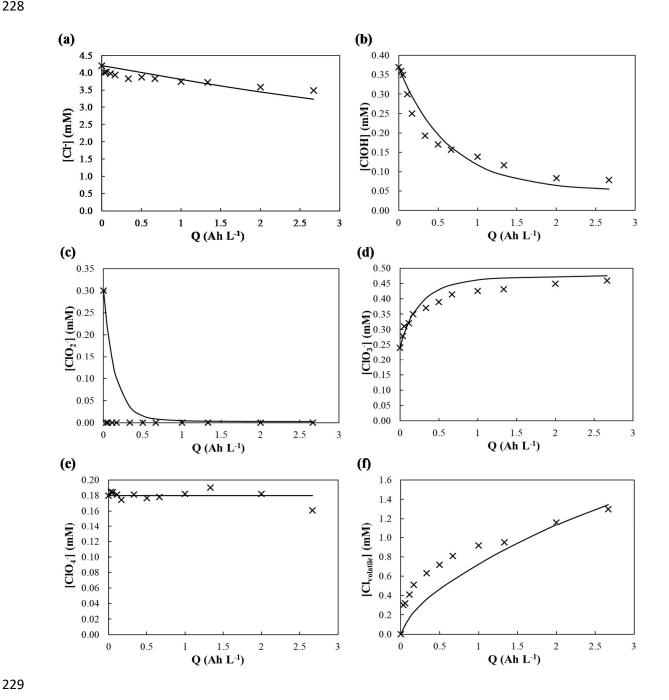
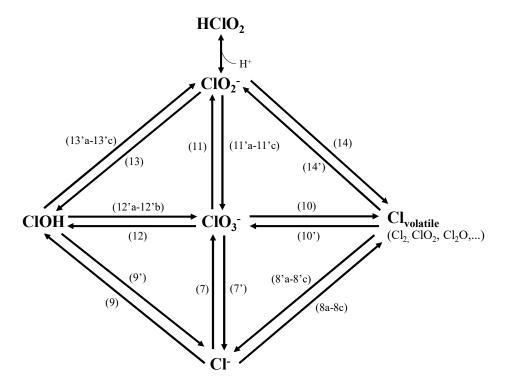


Fig. 2. Comparison of simulated (continuous line) and experimental data (x) about the profiles of (a) Cl<sup>-</sup>, (b) ClOH, (c) ClO<sub>2</sub><sup>-</sup>, (d) ClO<sub>3</sub><sup>-</sup>, (e) ClO<sub>4</sub><sup>-</sup> and (f) Cl<sub>volatile</sub> in synthetic solutions containing initially a mixture of Cl<sup>-</sup>, ClOH, ClO<sub>2</sub><sup>-</sup>, ClO<sub>3</sub><sup>-</sup>, ClO<sub>4</sub><sup>-</sup> as a function of the applied specific charge during electro-

Fenton treatment. Initial conditions: pH 3,  $[Fe^{2+}] = 0.1 \text{ mM}$ ,  $[Cl^-] = 4.2 \text{ mM}$ , [ClOH] = 0.37 mM,  $[ClO_2^-] = 0.30 \text{ mM}$ ,  $[ClO_3^-] = 0.24 \text{ mM}$ ,  $[ClO_4^-] = 0.18 \text{ mM}$ .

The experiments made with single chlorinated compounds and with a mixture of them allowed establishing a pathway of the redox cycle of inorganic chlorinated species subjected to electro-oxidation/reduction combined to homogeneous Fenton oxidation with carbon felts electrodes in synthetic acidic solution (Fig. 3).

On the contrary to the pathway given with anodic oxidation using BDD anode [26,51], perchlorate is not appearing in this scheme since the oxidation power was not high enough in the present process. Moreover, the reduction reactions have been considered as well, since electron transfer could occur at both cathode and anode in the electrochemical cell. This reaction pathway highlights the central role of chlorate that directly interact with all the inorganic chlorinated species.



**Fig. 3**. Scheme of redox cycle of inorganic chlorinated species under electro-oxidation/reduction combined to homogeneous Fenton oxidation with carbon felts electrodes in synthetic acidic solution (pH 3). The equations involved are written in brackets.

- 3.1.3. Kinetics analysis of inorganic chlorinated species in a synthetic mixture
- A kinetic model was proposed based on the results presented in sub-section 3.1.2 that allowed
- identifying the main chlorinated species involved during the electro-Fenton process.
- 254 The order of direct oxidation/reduction reactions was determined according to the initial limiting current
- density  $(j^{\circ}_{lim})$  (Eq. 15) values compared to the applied current density [52,53].

$$j_{lim}^{\circ} = nFk_mC_0 \tag{15}$$

- where *n* is the number of electron exchanged, *F* is the Faraday constant (96485 C mol<sup>-1</sup>),  $k_{\rm m}$  is the mass
- 258 transport coefficient (m s<sup>-1</sup>),  $C_0$  is the initial concentration of the electroactive inorganic chlorinated
- species (mM).

- An average  $k_{\rm m}$  value of  $6 \times 10^{-6}$  m s<sup>-1</sup> has been taken into account, since it is the common value of the
- 261 mass transport of species towards electrodes in such electrochemical reactor [39,54]. All the  $j^{\circ}_{lim}$  values
- were below 1.5 mA cm<sup>-2</sup>, considering the oxidation of Cl<sup>-</sup> into ClO<sub>3</sub><sup>-</sup> (Eq. 7). This reaction involves the
- highest number of electrons exchanged and the highest initial concentration of compounds ([Cl] = 2.4
- 264 mM), indicating that all other direct oxidation/reduction reactions led to lower joint. Thus, the applied
- current density (2.5 mA cm<sup>-2</sup>) was always higher than j°<sub>lim</sub>. Consequently, the mass transport was the
- rate-limiting step compared to charge transfer mechanism [52,53]. The rate (r) of direct
- oxidation/reduction reactions under mass transport control can be expressed as follow (Eq. 16) [52,53]:

$$268 r = Ak_mC (16)$$

- where A is the surface area of the electrode, C is the concentration during the electrolysis of the species
- 270 that react by direct oxidation/reduction reaction.
- 272 Considering Eq. 16, the kinetic of reaction is a first order towards C, the other parameters being
- 273 constants. It corroborated the kinetic analysis suggested in previous studies that involved first order
- kinetics for direct oxidation/reduction reactions [24,27]. In addition, based on the quasi-steady state
- approximation towards 'OH concentration, a pseudo-first order kinetic model has been also considered
- 276 for the reactions between inorganic chlorinated species and 'OH [27,42].
- 277 Therefore, the following system of differential equations considering first order kinetics was proposed
- to model the reaction kinetics of the species during electrolysis (Eqs. 17-22):

279 
$$\frac{d[Cl^{-}]}{dt} = k'_{1}[ClO_{3}^{-}] + k'_{2}[Cl_{gas}] + k'_{3}[ClOH] - (k_{1} + k_{2} + k_{3})[Cl^{-}]$$
 (17)

280 
$$\frac{d[ClOH]}{dt} = k_3[Cl^-] + k_7[ClO_2^-] + k_6[ClO_3^-] - (k'_3 + k'_6 + k'_7)[ClOH]$$
 (18)

281 
$$\frac{d[ClO_2^-]}{dt} = k'_7[ClOH] + k'_8[Cl_{gas}] + k_5[ClO_3^-] - (k'_5 + k_7 + k_8)[ClO_2^-]$$
 (19)

$$282 \qquad \frac{d[\mathcal{C}lO_3^-]}{dt} = k_1[\mathcal{C}l^-] + k'_4[\mathcal{C}l_{gas}] + k'_6[\mathcal{C}lOH] + k'_5[\mathcal{C}lO_2^-] - (k'_1 + k_4 + k_5 + k_6)[\mathcal{C}lO_3^-]$$

$$\frac{d[ClO_4^-]}{dt} = 0 (21)$$

The main reactions implemented in the system are presented in Table 1. The mathematical model has been compared with the experimental data for chloride, hypochlorous acid, chlorite, chlorate, perchlorate and volatile chlorinated species and the results are displayed in Fig. 2. After calibration of the model, the rate constant values (expressed in s<sup>-1</sup>) could be estimated (Table 2).

Table 2. Estimated kinetic constants values from the model.

Constant	Chlorinated species involved and direction of reaction	<b>Equations</b> involved	Rate constant value (s <sup>-1</sup> )
$k_1$	$Cl^- \rightarrow ClO_3^-$	(7)	$1.54 \times 10^{-5}$
$k'_1$	$ClO_3^- \rightarrow Cl^-$	(7')	$3.86 \times 10^{-7}$
$k_2$	$Cl^{-} \rightarrow Cl_{volatile}$	(8a-8b)	$1.06 \times 10^{-5}$
k' <sub>2</sub>	$Cl_{volatile} \rightarrow Cl^{-}$	(8'a-8'b)	$1.74 \times 10^{-5}$
$k_3$	$Cl^{-} \rightarrow ClOH$	(9)	$1.93 \times 10^{-7}$
<i>k</i> ' <sub>3</sub>	$ClOH \rightarrow Cl^{-}$	(9')	$9.64 \times 10^{-5}$
$k_4$	$\text{ClO}_3^- \to \text{Cl}_{\text{volatile}}$	(10)	$1.74 \times 10^{-4}$
<i>k</i> ' <sub>4</sub>	$\text{Cl}_{\text{volatile}} \rightarrow \text{ClO}_3^-$	(10')	$2.89 \times 10^{-5}$
$k_5$	$\text{ClO}_3^- \to \text{ClO}_2^-$	(11)	$9.64 \times 10^{-7}$
k'5	$\text{ClO}_2^- \to \text{ClO}_3^-$	(11'a-11'c)	$3.86 \times 10^{-4}$
$k_6$	$ClO_3^- \rightarrow ClOH$	(12)	$2.89 \times 10^{-5}$
<i>k</i> ' <sub>6</sub>	$ClOH \rightarrow ClO_3^-$	(12'a-12'b)	$1.54 \times 10^{-4}$
$k_7$	$ClO_2^- \rightarrow ClOH$	(13)	$3.86 \times 10^{-7}$
<i>k</i> ' <sub>7</sub>	$ClOH \rightarrow ClO_2^-$	(13'a-13'c)	$3.86 \times 10^{-5}$
$k_8$	$ClO_2^- \rightarrow Cl_{volatile}$	(14)	$9.64 \times 10^{-4}$
<i>k</i> ' <sub>8</sub>	$\text{Cl}_{\text{volatile}} \rightarrow \text{ClO}_2^-$	(14')	$9.64 \times 10^{-7}$

The validity of the model was tested to see how well the theoretical curve fit the experimental data by calculating the RMSE, ME and IoA. A model that perfectly fits the data would have a RMSE value of zero and ME and IoA values of one. The RMSE, ME and IoA values for the model are shown in Table

3. RMSE, ME and IoA were below 0.084 and higher than 0.919 and 0.991, respectively, descripting a good correlation considering the sixteen rate constants that have been taken into account.

The estimated values of parameters were ranging from  $1.93 \times 10^{-7} \text{ s}^{-1}$  to  $9.64 \times 10^{-4} \text{ s}^{-1}$ . The highest rate was attributed to the conversion of  $\text{ClO}_2^-$  into  $\text{Cl}_{\text{Volatile}}$  (i.e.  $\text{ClO}_{2(g)}$ ), which corroborates the fast conversion observed with single species in section 3.1.1. The oxidation of  $\text{ClO}_2^-$  into  $\text{ClO}_3^-$  was also very quick according to the rate constant  $(3.86 \times 10^{-4} \text{ s}^{-1})$ , which confirmed the fast decay of  $\text{ClO}_2^-$  compared to the other species during the electrolysis.

**Table 3.** Efficiency of the kinetic model in comparison with experimental data obtained in synthetic solution.

	RMSE	ME	IoA
Cl <sup>-</sup> curve	0.042	0.959	0.990
ClOH curve	0.053	0.940	0.990
ClO <sub>2</sub> - curve	0.084	0.919	0.941
ClO <sub>3</sub> curve	0.025	0.970	0.994
ClO <sub>4</sub> - curve	0.021	0.992	0.999
Cl <sub>volatile</sub> curve	0.070	0.976	0.989

The model proposed in this study allowed confirming the pathway proposed in Fig. 3. This scheme and the model is valid in synthetic solution with inorganic chlorinated species only, considering no interference with other species that could be present in the effluent. The possible matrix effect has been studied in the following sections to evaluate these aspects.

3.2. Influence of additional inorganic species on concentration profile of chlorinated species

The possible impact of phosphate ion and inorganic carbon has not been studied previously, though
these species are commonly present in municipal wastewater effluents along with chloride ions [27,39].

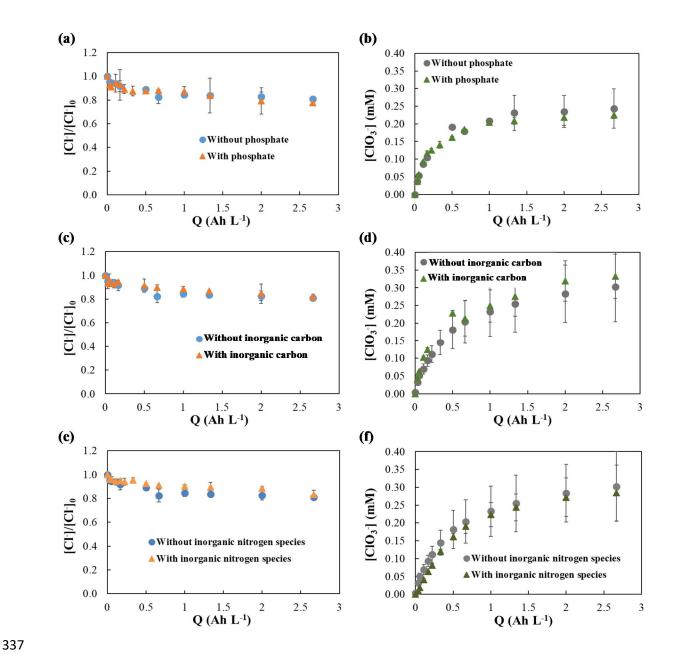
The influence of phosphate on the oxidation of chloride was determined by comparing the results from
an experiment with initial additions of chloride and phosphate to an experiment with only chloride added
initially (Figs. 4a and 4b). When comparing the normalized chloride concentrations of the experiment
with phosphate to the experiment without phosphate, the values fell within the standard deviation of
each other (Fig. 4a). Both experiments followed a similar trend with a decreasing amount of chloride as
applied specific charge increased until 20% of Cl<sup>-</sup> removal after 2.7 Ah L<sup>-1</sup>. The kinetics of the evolution

of inorganic chlorinated species for both experiments are illustrated in Fig. 4b. ClO<sub>3</sub><sup>-</sup> was the only species quantified in the samples in both experiments, which is in agreement with single chloride experiments (Fig. 1a). Both experiments followed the same trend and the same kinetics considering the standard deviation, i.e. absence of chlorate initially and increasing over applied specific charge until a plateau around 0.24 mM. Therefore, phosphate did not have any impact on the redox evolution of inorganic chlorinated species in such electro-Fenton conditions. It seems that perphosphate (P<sub>2</sub>O<sub>8</sub><sup>4</sup>) was not produced during the electrolysis unlike in advanced electro-oxidation process (Eqs. 23-24) as the phosphate concentration remained constant all along the treatment and P<sub>2</sub>O<sub>8</sub><sup>4+</sup> could have oxidized chlorinated species.

330 
$$PO_4^{3-} \to PO_4^{2-\bullet} + e^-$$
 (23)

331 
$$2 \text{ PO}_4^{2-\bullet} \rightarrow \text{P}_2\text{O}_8^{4-}$$
 (24)

The operating conditions may not be strong enough to allow PO<sub>4</sub><sup>3-</sup> oxidation. It is also important to note that the predominant species at pH 3 are phosphoric acid (H<sub>3</sub>PO<sub>4</sub>) and H<sub>2</sub>PO<sub>4</sub><sup>-</sup> whose pKa is 2.15. In this context, the oxidation of H<sub>3</sub>PO<sub>4</sub> or H<sub>2</sub>PO<sub>4</sub><sup>-</sup> species could be more difficult.



**Fig. 4.** Effect of phosphate ((a) and (b)), inorganic carbon ((c) and (d)) and inorganic nitrogen species ((e) and (f)) contents on the decay of Cl<sup>-</sup> normalized to the initial Cl<sup>-</sup> concentration ([Cl<sup>-</sup>]<sub>0</sub>) ((a), (c) and (e)) and on the generation of ClO<sub>3</sub><sup>-</sup> ((b), (d) and (f)) in synthetic solutions as a function of the applied specific charge during electro-Fenton treatment. Initial conditions: pH 3, [Fe<sup>2+</sup>] = 0.1 mM, [Cl<sup>-</sup>] = 4.2 mM; [PO<sub>4</sub><sup>3-</sup>] = 0.21 mM ((a) and (b)), [CO<sub>3</sub><sup>2-</sup>] = 0.33 mM ((c) and (d)), [NH<sub>4</sub><sup>+</sup>] = 0.8 mM ((e) and (f)), [NO<sub>2</sub><sup>-</sup>] = 0.19 mM ((e) and (f)).

Similarly, the effect of inorganic carbon on the concentration profiles of inorganic chlorinated species was also negligible (Figs. 4c and 4d). In acidic condition the predominant inorganic carbon species present in solution is carbonic acid (H<sub>2</sub>CO<sub>3</sub>), according to the pKa of H<sub>2</sub>CO<sub>3</sub>/HCO<sub>3</sub><sup>-</sup> couple that equal

6.3. Both acidic and milder oxidative stress conditions compared to the anodic oxidation technology might limit the formation of percarbonate (Eqs. 25-26) that could have played a role in the oxidation of chlorinated species otherwise.

351 
$$CO_3^{2-} \to CO_3^{--} + e^-$$
 (25)

352 
$$2 \text{ CO}_3$$
  $\rightarrow$   $C_2 \text{O}_6^{2-}$  (26)

It further highlights that in this acidic condition, the formation of calcium carbonate (CaCO<sub>3</sub>) at the cathode due to local pH increase [26] can be avoided. In the presence of Ca<sup>2+</sup> and CO<sub>3</sub><sup>2-</sup>, which is the case of reclaimed wastewater [27,39], this local precipitation is frequent and cause scaling effect that can impede the electrolysis.

The influence of inorganic nitrogen species has been also tested using concentration of 0.8 mM, 0.37 mM and 0.19 mM for NH<sub>4</sub><sup>+</sup>, NO<sub>3</sub><sup>-</sup> and NO<sub>2</sub><sup>-</sup> respectively, which corresponds to the concentration employed in a previous study [27]. The results are shown in Figs. 4e and 4f and the same trends and kinetics of chloride and chlorate concentrations where observed regardless of the presence or absence of nitrogen species. However, the kinetics evolution of nitrogen species is impacted by the presence of chlorinated species as previously shown in electro-Fenton condition [27]. The ammonia tends to decrease due to the formation of monochloramine (NH<sub>2</sub>Cl), dichloramine (NHCl<sub>2</sub>) and trichloramine (NCl<sub>3</sub>) with ClOH, while nitrate tends to accumulate in solution [27].

Thus, the presence in the initial effluent of phosphate, inorganic carbon and inorganic nitrogen species should not affect the concentration profiles and the proposed pathway of the inorganic chlorinated species in electro-Fenton condition. This is verified in reclaimed wastewater in the following section 3.3.

3.3. Validation of the suggested model on the concentration profiles of inorganic chlorinated species in reclaimed wastewater

Experiments have been performed with reclaimed wastewater from the outlet of a municipal wastewater treatment plant in Reims, France. The characteristics of the initial effluent are given in a previous paper [27]. The inorganic chlorinated species have been monitored and only chloride and chlorate were

detected in the samples from the wastewater electrolysis and their concentrations are graphed in Fig. 5a and Fig. 5b, while Cl<sub>volatile</sub> is plotted in Fig. 5c. The model that has been proposed in section 3.1.2 has been applied for the experiments with real effluent and the results are depicted in Figs. 5a-c. The same kinetic rate constant values and ordinary differential equations were used. The model fitted quite well the experimental concentrations of the chlorinated species. RMSE, ME and IoA were lower than 0.071 and higher than 0.910 and 0.937, respectively (Table 4). It further confirmed that phosphate, inorganic carbon contents and nitrogenous species were not impacting the fate of chloride and chlorate species. The pathway proposed in Fig. 3 could be then validated with real wastewater.

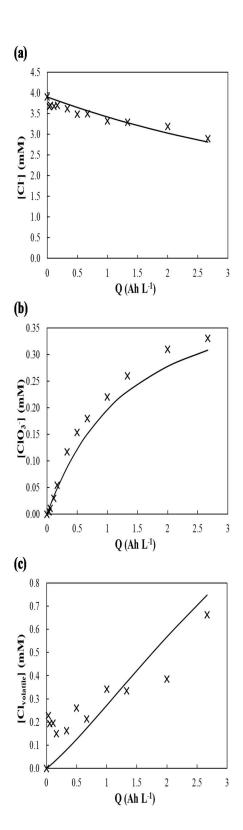


Fig. 5. Comparison of simulated (continuous line) and experimental data (×) about the profiles of (a) Cl<sup>-</sup>, (b) ClO<sub>3</sub><sup>-</sup> and (c) Cl<sub>volatile</sub> in reclaimed wastewater as a function of the applied specific charge during electro-Fenton treatment. Initial conditions: pH 3, [Fe<sup>2+</sup>] = 0.1 mM.

	RMSE	ME	IoA
Cl <sup>-</sup> curve	0.059	0.990	0.991
ClO <sub>3</sub> - curve	0.034	0.990	0.997
Cl <sub>volatile</sub> curve	0.071	0.910	0.937

#### 4. Conclusions

For the first time, the concentration profiles of inorganic chlorinated species in synthetic and reclaimed municipal wastewater in electro-Fenton process have been investigated in detail. The redox cycles of chloride, hypochlorous acid, chlorite, chlorate, perchlorate and volatile chlorinated species have been established. A kinetic model considering first order kinetics and sixteen rate constants has been proposed. After calibration and validation of the model with experimental data obtained in synthetic solution, the model has been further validated with a real solution. A reaction pathway has been suggested for both synthetic and reclaimed wastewater.

The acidic and mild oxidation conditions compared to anodic oxidation with non-active anode permit

The acidic and mild oxidation conditions compared to anodic oxidation with non-active anode permit to avoid the interference of phosphate, carbonate and inorganic nitrogen species with the redox cycles of inorganic chlorinated species. Furthermore, perchlorate could not accumulate unlike in advanced electro-oxidation. However, chlorate and volatile chlorinated species were still accumulating with the applied specific charge for all tested solutions. In this context, these intermediates need to be carefully assessed during the electro-Fenton treatment of real chlorinated effluents.

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