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IRON-RICH CLAY MINERAL SYNTHESIS USING DESIGN OF EXPERIMENTS

APPROACH

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Abstract

The precipitation of iron-rich clay minerals has been reported in various geologic environments. However, large quantities of these minerals are not widely accessible to study their thermodynamic properties and thus improve our understanding of these particular geological systems. To obtain sufficient amount of iron-rich minerals, their synthesis can be foreseen. A design of experiments and surface response methodology was used in this study to find optimum synthesis conditions for these clay minerals. Three parameters were considered: quantity of OH⁻, synthesis time and temperature. The quantity of OH⁻ had the largest influence on the synthesis result. The amount of 2:1 type clay mineral with respect to 1:1 type clay mineral increased with OH/Fe molar ratio. Time and temperature had less significant impact on the synthesis outcome, yet the formation of 2:1 type phase was favored at short synthesis time (1 day) and high temperature (160°C). The findings suggested that the kinetic of 2:1 type clay

mineral phase formation with respect to 1:1 type phase was faster, yet the precipitation was strongly dependent on the availability of the reactants.

Key words

iron-rich clay minerals, design of experiments, synthesis, nontronite, berthierine

Introduction

Clay minerals are layered silicate materials, where silica tetrahedra are arranged in continuous sheet combined with hexagonally coordinated metal-containing octahedral sheet. In general, two types of structures can be distinguished, a so-called 2:1 type clay mineral where the metal-containing octahedral sheet is sandwiched between two silicate sheets forming a 2:1 layer, and a 1:1 type clay mineral, where one silicate sheet is combined with one octahedral sheet forming a 1:1 layer (Figure 1). These minerals are widely encountered in natural sedimentary rocks and soils. The most common elements found in natural clay minerals are Si, Al, Mg, Fe, O and H (i.e., montmorillonite, beidellite, vermiculite, kaolinite, saponite). Minerals containing solely Si, Fe, O and H are known, but less common (i.e., greenalite, cronstedtite, hisingerite, nontronite).

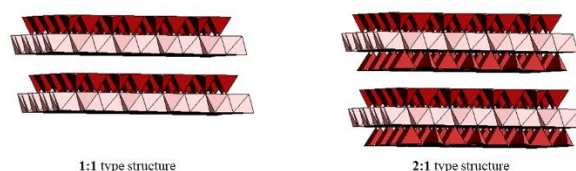


Figure 1. Schematic representation of clay mineral structures.

The environments where the formation of iron-rich clay minerals have been reported include deep-sea sediments (Baldermann et al., 2015; Tosca et al., 2016), subduction zones (Beaufort et al., 2015; Sforza et al., 2018), transform faulting (Kodolányi et al., 2012), the surface of Mars (Chemtob et al., 2015) and meteorites (Zolotov, 2015). Their presence has also been reported at the interface between different materials such as steel and glass (Schlegel et al., 2016) and steel and clay-rich rocks (Lanson et al., 2012) studied for the conception of radioactive waste repository sites.

For the different geological systems, it is of great interest to predict the evolution of these systems whether millions of years in the past, as in the case of Mars and Earth surfaces, or other thousands of years in the future as in the case of long-term radioactive waste repository sites. In order to do this, geochemical modelling is required to predict the evolution with time of the mineralogical composition of these different systems. The prediction of this evolution is crucial as it enables assessing the changes of key properties such as porosity and permeability.

To assess the clay mineral thermodynamic properties for geochemical modelling, different approaches were developed (Tardy and Fritz, 1981; Vieillard, 2000). The thermodynamic properties of clay minerals are particularly challenging to constrain owing to the great chemical and structural variability of these minerals (Gailhanou et al., 2013). A common approach to assess them is the summation of oxide/hydroxide parameters, which on the other hand are well-known. However, the knowledge of experimental thermodynamic and kinetic properties of iron-rich clay minerals would enhance the robustness of the models, as well as allow the comparison of experimental data with modelling (Gailhanou et al., 2013).

As Fe-rich clay mineral phases and especially tri-octahedral ones are seldom encountered in environments and as only very small quantities can be extracted, their synthesis can be foreseen. Two reviews have recently gathered the different methods carried out to prepare iron-rich clay minerals (Dzene et al., 2018; Petit et al., 2017). The hydrothermal synthesis route remains the

preferred one because it is a versatile and easy to use process which allows the attainment of well crystallized compounds (Jaber et al., 2013; Klopogge, 1998; Le Forestier et al., 2010; Reinholdt et al., 2005). The key parameters governing the formation of clay minerals are the sources of reactants, synthesis time, temperature and the pH of the hydrogel. Regarding the preparative methods, the formation of a sol followed by a gel is expected to yield a homogeneous repartition of elements in the final product (Dzene et al., 2018). The use of Fe^{2+} source for the preparation of precursor is expected to increase the kinetics of synthesis and to allow obtaining faster a well-crystallized product compared to the use of Fe^{3+} source (Petit et al., 2017). The three other parameters, pH, time and temperature, have been widely varied in literature and no particular tendency can be extracted. Thus, the variation from neutral to alkaline pH has been previously reported, and syntheses have been performed in various time and temperature ranges. Nevertheless, the three later parameters can significantly influence the type of synthesized clay mineral and its crystallinity (Jaber et al., 2013; Klopogge et al., 1999). For this reason, the three parameters (time, temperature and the initial quantity of OH^-) were chosen as the variables for this study. In general, time will intervene in reaction kinetics and crystal growth processes. The increase of synthesis time will allow attaining the equilibrium or pseudo-equilibrium conditions and will allow growing larger crystals. The temperature will intervene in both, in reaction kinetics and thermodynamics. On the one hand the increase of temperature is expected to accelerate the kinetics of reaction. Thus, higher temperature would lead to shorter synthesis time. On the other hand, the increase of temperature will influence the thermodynamics of the reaction. As the precipitation of clay minerals is in general an endothermic process (Giffaut et al., 2014), the increase of the temperature is expected to favor the formation of products. Finally, the quantity of OH^- will influence the condensation reactions (Cundy and Cox, 2005).

The complexity of the studied reactions, make the systematic exploration rather challenging. Therefore, the design of experiments (DOE) can be used. This approach largely applied in natural sciences and engineering has been only recently explored in the synthesis of inorganic materials such as zeolite, aluminophosphate and glass (Carvalho et al., 2013; Cichocki and Kościelniak, 1999; Ji et al., 2014; Katovic et al., 2001; Zhang et al., 2009). This approach has allowed to eliminate insignificant parameters and reveal the most significant ones, which influence material properties such as crystallinity, ion exchange capacity and solubility of the product. However, the method has not yet been explored for lamellar silicate synthesis. This might be due to the fact, that the characterization of synthesis products requires a set of several analytical techniques, thus choosing the response variable(s) for the DOE is not trivial. By using oriented preparation for X-ray diffraction, we took advantage of a particular feature of lamellar materials to characterize them. The objective of this study then is to test this characterization technique for the design of experiments and explore in an efficient way, how, the three parameters: quantity of OH^- , synthesis time and temperature, influence the type of synthesized clay mineral and its crystallinity.

Materials and methods

2.1. Design of experiments

Preliminary experiments identified the three parameters that influence the type and amount of obtained clay mineral: synthesis time t , temperature T and $(\text{OH}/\text{Fe})_{\text{ini}}$ molar ratio. They allowed also to set the relevant range of each of these three parameters ($T=80\text{ }^{\circ}\text{C} - 180\text{ }^{\circ}\text{C}$, $t=1 - 7$ days and $(\text{OH}/\text{Fe})_{\text{ini}}=2 - 4$) for the design of experiments. To analyze the results in terms of synthesis parameters, a methodology based on Design Of Experiments (DOE) and Response Surface Methodology (RSM) was used (Myers et al., 2016).

For this, a central composite design for $k = 3$ factors (T , t , $(OH/Fe)_{ini}$) was used (Anderson and Whitcomb, 2016). It consists of three sets of experimental points: 2^k points coming from classical factorial design (two levels), $2k$ axial points (“star points”) and a center point, i.e. $8+6+1$ experimental tests in this case (Figure 2). Thus, the central point in our study is [130 °C; 4 days; $(OH/Fe)_{ini}=3$]. The eight points (factorial points) define the domain of the study, which is also the domain of the validity to consider for the numerical interpretation of results, i.e. ($T=100$ °C -160 °C, $t=2.3$ - 5.7 days) and $(OH/Fe)_{ini}=2.4$ - 3.6). The “star points” are additional points required to increase the efficiency of the quadratic fitting.

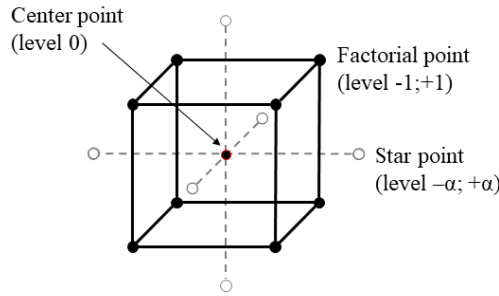


Figure 2. Scheme representing central composite design for $k=3$ factors.

The main objective of DOE is to obtain the maximum of information from a minimum of experiments. RSM enables to explore relationships between the studied functions and the operating factors. To obtain an optimal response a linear quadratic model with 10 parameters is used to numerically approximate the response function. For this, a system of 15 equations with 10 variables is statistically solved by minimizing a quadratic criterion, i.e. $\sum_{i=1}^n (y_{exp}(i) - y_{calc}(i))^2$, where y_{exp} and y_{calc} are the experimental and calculated variable, respectively. The studied parameters (T , t and OH/Fe molar ratio) are standardized in the range $[-1,1]$ to analyze the sensitivity of the calculated response functions. Additional experiments were performed to investigate experimental error. The relevance of the response functions

(presented in paragraph 2.3.) was studied by statistical analysis via the calculation of five criteria, as follows:

- The determination coefficient r^2

$$- \text{The standard error of estimate } S = \sqrt{\frac{\sum_{i=1}^n (y_{exp}(i) - y_{calc}(i))^2}{n-6}}$$

$$- \text{The Marquard's percent standard deviation MPSD} = \sqrt{\frac{1}{n-6} \sum_{i=1}^n \frac{(y_{exp}(i) - y_{calc}(i))^2}{y_{exp}(i)^2}}$$

$$- \text{The mean absolute error EABS} = \frac{1}{n} \sum_{i=1}^n |y_{exp}(i) - y_{calc}(i)|$$

$$- \text{The mean relative error RE} = \frac{1}{n} \sum_{i=1}^n \left| \frac{y_{exp}(i) - y_{calc}(i)}{y_{exp}(i)} \right|$$

The five criteria are used to assess the pertinence of the numerical approximation. The studied functions are studied directly and in power, logarithmic, exponential, hyperbolic, etc. forms. According to the five studied criteria, the best function is chosen and used for the numerical approximation.

2.2. Synthesis protocol and chemicals used

The following chemicals were used: iron (II) sulfate heptahydrate ($\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$, Merck, 99.9 %) as Fe(II) source, fumed silica (SiO_2 , Aerosil® 380, Evonik) as silicon source, sodium hydroxide (NaOH, Sigma Aldrich, 97 wt.%) to provide an alkaline medium and sodium dithionite ($\text{Na}_2\text{S}_2\text{O}_4$, Sigma Aldrich, ca. 85 wt.%,) to maintain reducing conditions. Double distilled water (DDW, $18.2 \text{ M}\Omega \cdot \text{cm}$) was used for all the experiments.

The procedure is based on a hydrothermal synthesis starting from a suspension having an Fe to Si molar ratio equal to 1.5. The procedure consisted of dissolving successively in 70 mL of distilled water 0.041 g of $\text{Na}_2\text{S}_2\text{O}_4$, 4.510 g of $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$, 0.647 g of SiO_2 and a given quantity

of NaOH at the desired OH/Fe molar ratio corresponding to each run of experiment (Table 1). Thus, the initial theoretical concentrations were $c(\text{Fe}^{2+}) = 0.23 \text{ mol}\cdot\text{L}^{-1}$, $c(\text{Si})=0.15 \text{ mol}\cdot\text{L}^{-1}$ and $c(\text{OH}^-)=0.45 - 1.00 \text{ mol}\cdot\text{L}^{-1}$. The mixture was stirred during 2 hours at room temperature before being sealed in a Teflon-lined stainless-steel autoclaves (Top Industrie ®, 150 mL) and put at the desired temperature (T) ranging from 80 °C to 180 °C and time (t) ranging from 1 to 7 days. After the synthesis, the autoclaves were cooled down at room temperature. The run products were then recovered and washed by centrifugation (8000 rpm for 10 min), and dried at 60 °C.

2.3. Choice of response for the design of experiments

Clay minerals are highly anisotropic, therefore, it is challenging to obtain truly un-oriented sample for powder XRD. To overcome this drawback, oriented preparations can be made, recording solely (00 ℓ) reflections, which are characteristic for different clay mineral types. An example of X-ray diffractogram of oriented preparation is shown in Figure 3. Thus, 1:1 type structure would have $d_{(001)}$ value of ca. 7 Å and 2:1 type structure would have $d_{(001)}$ value in the range of 10 Å to 15 Å.

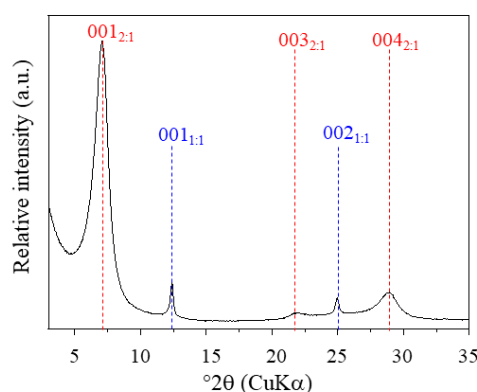


Figure 3. Example of XRD pattern of oriented preparation (Run N°01). Red dashed lines indicate (00 ℓ) plane reflections of 2:1 type clay mineral and blue dashed lines indicate (00 ℓ) plane reflections of 1:1 type clay mineral.

The absence of other (hkl) plane reflections was systematically checked in the analyzed samples. The measured peak areas of different phases then represent the relative abundance of each phase in the sample. Moreover, it is also possible to assess the information regarding the coherent scattering domain size (CSDS) in the direction perpendicular to the corresponding (00ℓ) plane. In conventional powder X-ray diffraction, this information can be obtained from the Full Width at Half Maximum (FWHM) of a reflection. However, in this particular case of oriented preparations, the simplifications can be done so that the peak intensity can provide this information on the CSDS in the direction perpendicular to the corresponding (00ℓ) plane. The chosen synthesis protocol revealed the formation of both types of clay minerals (1:1 and 2:1). The assumption was made that the chemical composition of 2:1 type phase is very similar in all samples and the chemical composition of 1:1 type phase is very similar in all samples. The objective of the study was to find optimum synthesis conditions for each type of phase. For this reason, the area and intensity ratios of (001) reflection, (respectively $R(A)$ and $R(I)$), between 1:1 and 2:1 type structures were chosen as the studied responses in the design of experiments (Figure 4).

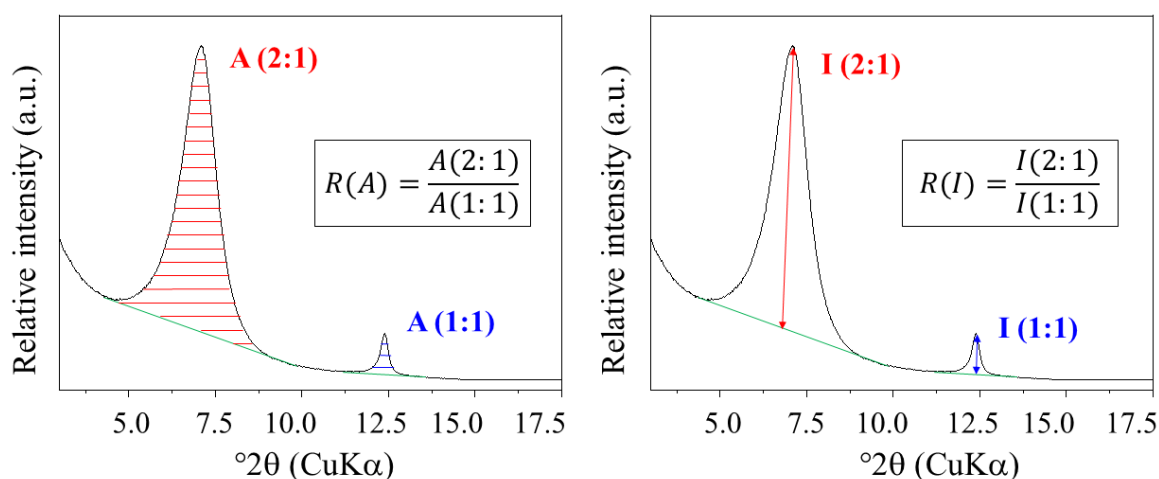


Figure 4. Illustration of $R(A)$ and $R(I)$ between 1:1 and 2:1 type clay minerals.

2.4. X-ray diffraction

The mineralogical composition of the samples and, more specifically, the type of clay mineral was determined using X-ray diffraction of powder and oriented preparations. The powders were previously ground and then introduced into PMMA sample holder with a cavity 25 mm in diameter and 1.2 mm deep, whereas the thin films of oriented samples were prepared from diluted suspensions by deposition onto a glass slide. All the samples, powder and oriented, were characterized on a Bruker D8 Advance X-ray diffractometer with a LYNXEYE XE-T high resolution energy dispersive 1-D detector ($\text{CuK}\alpha_{1,2}$) fully opened (2.938°). This kind of detector allows to avoid Fe fluorescence effects with Cu X-ray tube.

For the powder samples, the X-ray diffractograms were recorded from 3° to 70° 2θ at a step scan of 0.017° 2θ , a step time of 1.80 s with variable divergence slits that ensure that the irradiated sample length (*i.e.*, 15 mm) is kept equal over a measured range of 2θ . For the oriented samples, the XRD patterns were recorded in the range from 3 to 40° 2θ at a step scan of 0.017° 2θ , a step time of 3.3 s with a fixed divergence slits width of 0.08° . For both kind of samples (powder and oriented), automatic motorized anti-scatter screen is used for effective suppression of air-scatter at low angles 2θ .

Results

3.1. Experiments used for modelling

Examples of powder XRD patterns for selected experiments are given in Figure 5. The experimental synthesis conditions corresponding to each run N° are reported in Table 1. The formed reaction products were not pure phases, but containing also iron oxides: hematite and magnetite/maghemite. Two sets of experiments were performed in order to extract the optimal conditions to obtain a single type of clay mineral. The first set of experiments was designed

considering the central composite model. It contained a minimal number of experiments equal to 15 performed for OH/Fe molar ratio [2.0 – 4.0].

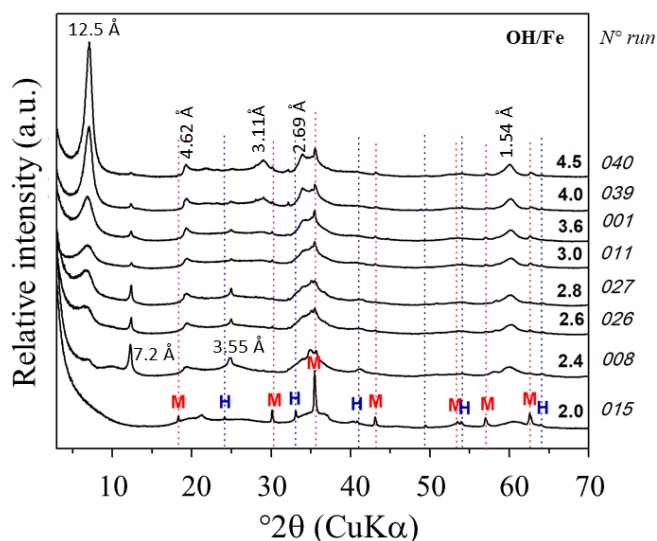


Figure 5. Powder XRD patterns of selected experiments. For the experimental conditions corresponding to each run N° see Table 1.

The first set of experiments produced satisfactory results in the validity range (2.4 – 3.6, i.e. standardized parameters = +1 / -1), but the errors increased significantly at the boundaries of the studied range ($r^2 = 0.94$ for OH/Fe = [2.4 – 3.6] and 0.89 for OH/Fe = [2 – 4]). The addition of a second set was consequently necessary in order to extract the optimal conditions from the quadratic equation. In fact, when calculating the extracted responses R(A) and R(I), different tendencies were noticed between the experiments performed for high OH/Fe molar ratios [2.4 – 4.0] in comparison with the lower values [2.0 – 2.4]. The studied response could therefore not be estimated based on the same model. The second set of experiment was then focused on high OH/Fe ratios, up to 4.5, and the linear quadratic model was studied accordingly in the range [2.4 – 4.5]. In order to improve the relevance of the model, 4 tests were added (N°26, N°27, N°39 and N°40) for the calculation of R(A) and R(I).

Table 1. Experimental conditions and obtained R(I) and R(A) corresponding to each run.

Set	Run N°	T (°C)	(OH/Fe) _{ini}	t (days)	R(I)	R(A)
1	01	160	3.6	2.3	6.9	29.2
	01-R				13.1	44.3
	02	160	2.4	2.3	0.1	1.2
	03	100	3.6	2.3	5.3	15.9
	04	100	2.4	2.3	0.2	2.0
	05	130	3.0	1.0	2.1	8.3
	06	130	3.0	7.0	1.4	5.9
	07	160	3.6	5.7	3.0	11.2
	08	160	2.4	5.7	0.2	0.4
	09	100	3.6	5.7	2.5	10.1
	10	100	2.4	5.7	0.9	5.1
	11	130	3.0	4.0	2.5	10.7
	11-R1				3.9	18.1
	11-R2				2.8	13.0
	12	180	3.0	4.0	1.1	6.0
	13	80	3.0	4.0	7.4	17.0
2	14	130	4.0	4.0	13.1	31.8
	15	130	2.0	4.0	-	-
	16	150	3.0	7.0	0.6	11.4
	26	130	2.6	5.0	0.8	3.5
	26-R				0.9	4.1
	27	130	2.8	5.0	0.6	3.5
	39	180	4.0	1.0	24.6	64.8
	40	180	4.5	1.0	32.1	68.2

4 runs (N°01-R, N°11-R1, R2 and N°26-R) were repeated to investigate the experimental error. These tests were chosen to have an experiment corresponding to predominant 2:1 type clay mineral (test N°01), an experiment resulting in a majority of 1:1 type clay mineral (test N°26) and an experiment with intermediate proportions of 2:1 and 1:1 type clay minerals (test N°11). The obtained experimental error was important but all the repeated tests show a parallel trend. The relevance of RSM is studied on the basis of all the experimental tests. In the run N°15, which was repeated several times, the only crystalline phases identified were iron oxides. No crystalline clay minerals were identified in powder XRD pattern (Figure 5) of this run, thus no values of R(A) and R(I) could be obtained for oriented preparations.

3.2. Study of response function R(A): ratio between relative quantities of 2:1 and 1:1 clay minerals

This function is proportional to the relative quantity of each phase in the sample. The obtained quadratic model for the studied function R(A) is given below (eq. 1). The analysis of sensitivity of the quadratic model for R(A) shows that the response function is highly dependent on OH/Fe molar ratio (coefficients before linear $\frac{\overline{OH}}{Fe}$, square $\frac{\overline{OH}^2}{Fe}$ and coupled $\bar{T} \times \frac{\overline{OH}}{Fe}$ variables). In the same way, linear, quadratic and coupled coefficients relative to time are relatively small, unlike the coupled coefficient $\bar{T} \times \bar{t}$.

$$\ln(R(A)) = 2.292 - 0.268\bar{T} - 0.059\bar{T}^2 + 1.275\frac{\overline{OH}}{Fe} - 0.46\frac{\overline{OH}^2}{Fe} - 0.062\bar{t} - 0.064\bar{t}^2 + 0.409\bar{T} \times \frac{\overline{OH}}{Fe} - 0.143\bar{T} \times \bar{t} - 0.059\frac{\overline{OH}}{Fe} \times \bar{t} \quad (\text{eq.1})$$

The pertinence of the model is investigated from all trials (20) except run N°15. Averages of tests N°01, N°11 and N°26 are used for the calculation of all the tests for the experimental error.

$$r^2 = 0.961, S = 4.706, \text{MPSD} = 0.512, \text{EABS} = 2.754, \text{RE} = 0.308$$

Figure 6 shows the area ratio versus temperature for different times for a low OH/Fe molar ratio (Figure 6A), an average OH/Fe molar ratio (Figure 6B) and a high OH/Fe molar ratio (Figure 6C). The function increases significantly with OH/Fe molar ratio while it increases with time at low temperature and decreases at high temperature. The same applies for temperature, since an increase of temperature decreases the area ratio except for high OH/Fe molar ratio values. The model represents well experimentally observed tendencies. Considering the significant experimental error, the tendencies given by the model are the same as for the experimental points thus validating the obtained model.

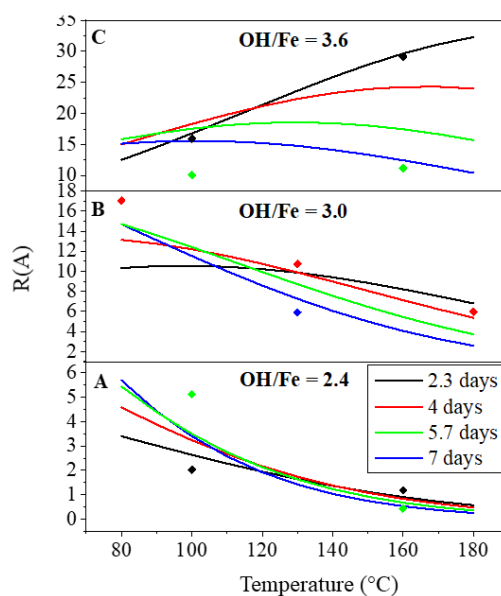


Figure 6. Time and temperature influence on the obtained R(A) for (OH/Fe)_{ini} molar ratios equal to 2.4 (A), 3.0 (B) and 3.6 (C). Diamonds represent experimental points from Table 1, Set I.

For illustration, selected XRD patterns of oriented preparations are given in Figure 7. In agreement with results obtained from R(A) investigation, it can be seen that the initial (OH/Fe) molar ratio significantly influences the type of clay mineral obtained. For low (OH/Fe)_{ini} molar ratios the formation of 1:1 type clay mineral is favored, whereas for high (OH/Fe)_{ini} molar ratios the 2:1 type clay mineral phase is dominant. The relative quantity of 2:1 clay mineral (with respect to 1:1 type clay mineral) increases significantly with (OH/Fe)_{ini}.

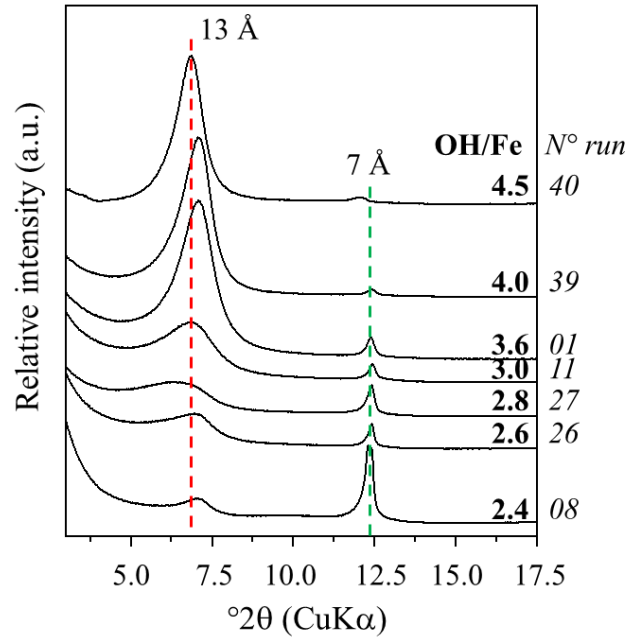


Figure 7. XRD patterns of oriented preparations for selected experiments (red dashed line 2:1 clay mineral type, green dashed line 1:1 type). For the experimental conditions corresponding to each run N° see Table 1.

3.3. Study of phase abundance and crystallinity: response function R(I)

This response function gives additional quantitative information and results about crystallinity. For R(I) (eq.2), it is noted that the conclusions about the sensitivity analysis are almost the same, except for time contribution, which is, in this present case, more significant, especially, the coupled terms with temperature and initial OH/Fe molar ratio. Indeed, the diffracted intensity in the particular case of oriented preparations among other factors also includes the contribution of the size of coherent scattering domain. It is expected that the synthesis time influences the size of formed particles, and thus the coherent scattering domain (Carrado et al., 2006). Thus, the contribution of time in the function of R(I) being more important than in R(A) function is in agreement with expected results.

$$\begin{aligned}
R(I) = & 2.146 - 0.283\bar{T} + 0.531\bar{T}^2 + 3.127\frac{\overline{OH}}{Fe} + 1.100\frac{\overline{OH}^2}{Fe} - 0.734\bar{t} - 0.141\bar{t}^2 + \\
& 0.928\bar{T} \times \frac{\overline{OH}}{Fe} - 0.819\bar{T} \times \bar{t} - 1.834\frac{\overline{OH}}{Fe} \times \bar{t} \quad (\text{eq.2})
\end{aligned}$$

The pertinence of the model is investigated from all trials (20):

$$r^2 = 0.962, S = 2.014, \text{MPSD} = 3.232, \text{EABS} = 1.403, \text{RE} = 1.422$$

For high OH/Fe molar ratio, i.e. $(\text{OH/Fe})_{\text{ini}} = 3.6$, it has to be underlined that whatever the temperature T, R(I) decreases with time (Figure 8). Likewise, the temperature increases the contribution of time on R(I) (Figure 8B). That is to say, the ratio of diffracted peak intensity increases with respect to the background (with no curvature, see Figure 4) without the increase of peak full-width at half-maximum when time decreases and temperature increases. It leads then to a conclusion that 2 :1 type clay mineral phase formation is favored in short times, and this becomes even more important with the increase of temperature.

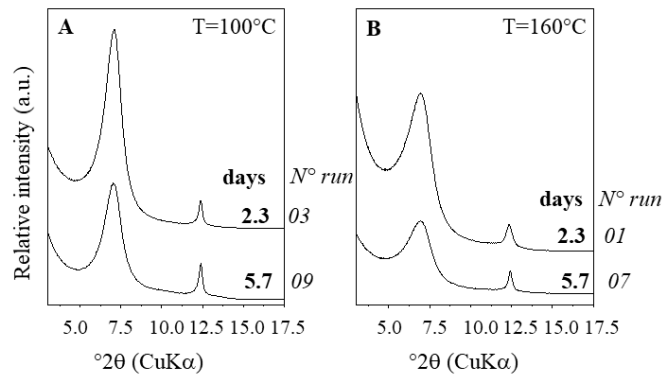


Figure 8. XRD patterns of oriented preparations obtained for $(\text{OH/Fe})_{\text{ini}}$ molar ratio = 3.6 at two different temperatures T=100°C (A) and T=160°C (B) for two different times of 2.3 and 5.7 days (Runs N° 01, N°03, N°07 and N° 09 *cf.* Table 1).

With this function (R(I)), the interpretation is limited for results obtained with low initial OH/Fe molar ratio because R(I) is close to zero (Table 1). To overcome this drawback, the last response

function (1 /R(I)) was defined and studied to investigate the favoring of 1:1 type clay formation.

All the studied parameters influence this function and no contribution can be neglected (eq.3).

$$\ln\left(1 + \frac{1}{R(I)}\right) = 0.453 + 0.188\bar{T} - 0.019\bar{T}^2 - 0.726\frac{\overline{OH}}{Fe} + 0.386\frac{\overline{OH}^2}{Fe} - 0.060\bar{t} + 0.058\bar{t}^2 - 0.217\bar{T} \times \frac{\overline{OH}}{Fe} + 0.139\bar{T} \times \bar{t} + 0.267\frac{\overline{OH}}{Fe} \times \bar{t} \quad (\text{eq.3})$$

The pertinence of the model is investigated from 18 trials (set 1 + tests N°26 and N°27):

$$r^2 = 0.981, S = 0.472, \text{MPSD} = 1.192, \text{EABS} = 0.310, \text{RE} = 0.621$$

Starting from these 3 mathematical models, optimal solutions are searched by minimizing an objective function.

3.4 Optimum parameters favoring the 2:1 type clay mineral formation

The study of the favored formation of 2:1 type clay mineral requires to investigate the parameters (T, time and initial OH/Fe molar ratio) resulting in high values of R(A) and R(I). It was considered that R(A) > 30 and R(I) > 12 (objective functions) are representative values of investigated conditions. Figure 9 shows in a temperature / time diagram the optimal solutions for having a vast majority of 2:1 type clay for R(A) > 30 (Figure 9A) and for R(I) > 12 (Figure 9B) for (OH/Fe)_{ini} = [3.6 – 4.0]. The objective function is reached in the hatched area. This objective (R(A) > 30) is reached for high OH/Fe molar ratio and especially for short synthesis time and high temperature. The same trend is observed for R(I) with temperature but the influence of time is more moderate at low temperatures below 120 °C.

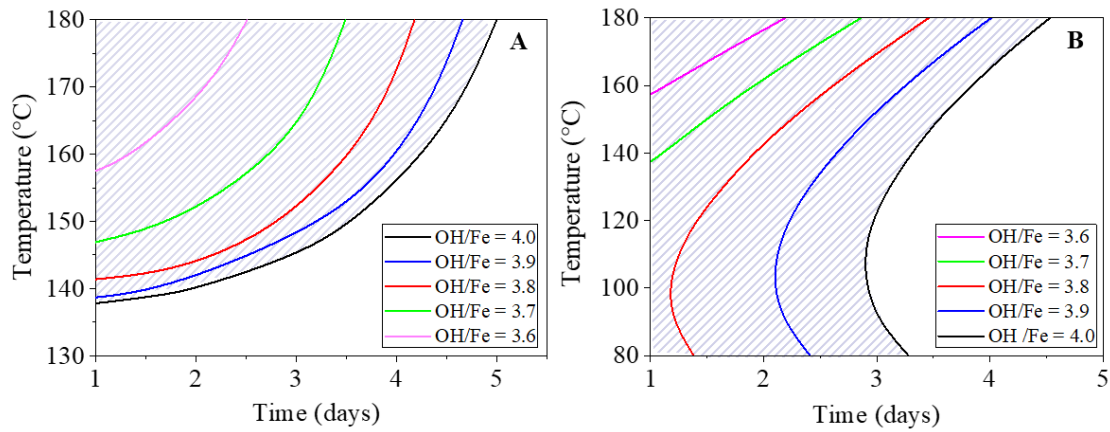


Figure 9. Conditions of temperature and time favoring the formation of the 2:1 type clay mineral with $R(A) > 30$ (A) and for $R(I) > 12$ (B) for $(OH/Fe)_{ini} = [3.6 - 4.0]$.

3.5 Optimum parameters favoring the 1:1 type clay mineral formation

The favored formation of 1:1 type clay mineral, corresponding to the very low values of $R(A)$ and $R(I)$ is studied with response function $(1/R(I))$. It was considered that $1/R(I) > 2$ are representative values of investigated conditions. It was not possible to fix a higher value for $1/R(I) > 2$ due to the experimental error. This objective is reached, when OH/Fe molar ratio is as low as possible, i.e., OH/Fe=2.4 (Figure 10). It is important to mention, that at OH/Fe < 2.2, the formation of crystalline 1:1 type clay mineral phase was not observed (Table 1).

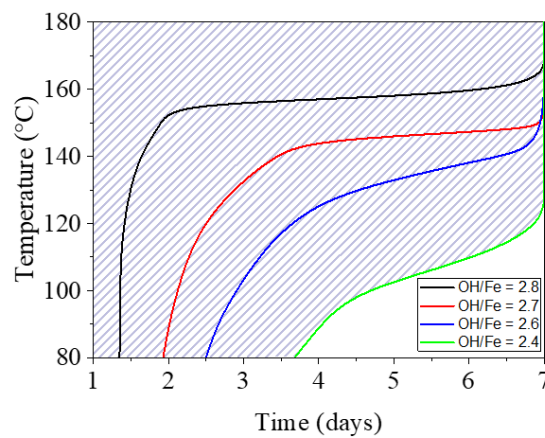


Figure 10. Conditions of temperature and time favoring the formation of the 1:1 type clay mineral with $1/R(I) > 2$ for $(OH/Fe)_{ini} = [2.4 - 2.8]$.

The optimal conditions for the formation of 1:1 type clay mineral phase (with respect to 2:1 phase) are reached for short time and high temperature. Interestingly, the formation of 1:1 type clay mineral phase can also be achieved at low temperature (below 140 °C) and short times (less than 3 days) with low OH/Fe molar ratio. In comparison, the synthesis of 2:1 phase is favored only at high temperatures and high OH/Fe molar ratio. This aspect can be relevant to environmentally friendly synthesis procedure, as less resources (chemicals and energy) are consumed.

Discussion

The observed tendencies in this study are in agreement with previously reported studies. Indeed, Fe-serpentines (1:1 type clay mineral) were observed for the experiments at low temperatures below 150°C (Bertoldi et al., 2005; Lantenois et al., 2005; Pignatelli et al., 2014; Rivard et al., 2013; Tosca et al., 2016), whereas Fe-rich chlorites (2:1 type clay mineral) were identified at higher temperature of 300 °C (Mosser-Ruck et al., 2016). However, it has to be noted that in other studies the duration of experiments was different. The experiments reported in Pignatelli et al. (2014) lasted 6 months and the experiment of Mosser-Ruck et al. (2016) went for 25 months. Also, in these experiments additional phenomena were in operation such as the dissolution of iron from metallic plates, which could have been the limiting step regarding the precipitation of clay mineral phase.

It can be expected that the formation of phyllosilicate phases is strongly governed by sol-gel process as in the case of other silicates such as zeolites. An important step is the precipitation of dissolved silicon. This condensation reaction is strongly governed by the amount of hydroxyl ions (Cundy and Cox, 2005). Then, it is not surprising that the quantity of OH^- has the most

significant impact on both studied functions. It has been noted previously that Si speciation in solution, influence the structure of synthesized nontronite (2:1 type clay mineral) (Baron et al., 2016). In a similar way here, the quantity of OH^- acts on the species and their amount in solution during the synthesis. Also, the study of Tosca et al. (2016) notes the influence of pH. They performed the study at three different pH (7.0, 7.5 and 8.0), and they noted that the concentration of Fe^{2+} and SiO_2 in solution decreased faster when pH increased. Thus, the precipitation of greenalite-like phase occurred faster when pH increased. Although the pH in our study was very different (13 to 14) compared to the study of Tosca et al. (2016), both studies note the important influence of this parameter towards the precipitation of clay minerals.

For synthesis at high OH/Fe ratio, a high temperature favors the formation of 2:1 type clay mineral. Indeed, the thermodynamic constant of the precipitation reaction increases with temperature and favors the formation of clays (enthalpy of precipitation reactions being positive) (Giffaut et al., 2014). In the same way, the reaction kinetics increase with the increase of temperature and the preferential precipitation of 2:1 type clay mineral can be attributed to a faster kinetic. It is in agreement with observations reported in the study of Grubb (1971), which used 1N NaOH solution in his experiments and observed that minnesotaite (2:1 type clay mineral) become the dominant constituent in the three year experiments. Nevertheless, in our study, when synthesis time increases this tendency is reversed (R(A) decreases) possibly due to a limited species (intermediate reaction leading to the precipitation of 2:1 phase clay mineral). This indicates a decrease of the ratio R(A) but the amounts can probably increase.

For synthesis performed at low OH/Fe ratios, the quantity of OH^- is limited. There is no thermodynamic limitation but the kinetics are decreased by the limiting reactant. The reaction leading to the precipitation of 2:1 type clay mineral is favored at high pH and disfavored in these operating conditions. So, the reaction of precipitation of 1:1 phase clay mineral becomes dominating.

To summarize, the ratio of reaction kinetics ($k_{2:1} / k_{1:1}$) increases with temperature and decreases when the available amount of hydroxyl ion in solution decreases. This amount of hydroxyl ion decreases as the precipitation reactions advances (time dependent).

Conclusion

The feasibility of synthesis of 2:1 and 1:1 type clay minerals was demonstrated at given physicochemical conditions. Depending on these conditions, the synthesis can be tailored towards favoured formation of one or another type of phases. To optimize the number of experiments and the amount of information, which can be extracted from them, a design of experiments was used. From few synthesis experiments, the predominant operating parameters and the conditions leading to the formation of 2:1 and 1:1 type clay minerals were identified. From RSM (Response Surface Methodology) investigations the optimal conditions of synthesis were estimated for each type of phase.

Among the studied parameters (synthesis temperature, time and ratio OH/Fe), the ratio OH/Fe (proportional to the available amount of hydroxyl ions in solution) is preponderant. At high OH/Fe ratio, the precipitation of 2:1 type clay mineral is favoured with respect to 1:1 type clay mineral. The decrease of available hydroxyl ions with time slowed down the kinetic. For the same reason, the formation of 1:1 type clay mineral was favoured when the availability of hydroxyl ions decreased (low OH/Fe ratio).

From these results, synthesis of several grams of desired products will be carried out to perform detailed characterizations (full set of thermodynamic properties, different spectroscopic measurements, structural model ...). These investigations will allow to improve the understanding of many aspects related to the presence of either or both 2:1 and 1:1 type iron bearing clays in natural or anthropized environments: identification of each type of phases in experimental products or natural samples, understanding of their neoformation mechanisms,

sensitivity to relevant or discriminant physico-chemical parameters, thermos-kinetic modelling of geochemical systems.

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