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A Kriging-NARX model for uncertainty quantification of nonlinear stochastic dynamical systems in time domain

Biswarup Bhattacharyya¹,

Eric Jacquelin²,

and Denis Brizard³

1 ABSTRACT

A novel approach, referred to as sparse Kriging-NARX (KNARX), is proposed in the 2 present paper for the uncertainty quantification of nonlinear stochastic dynamical systems. 3 It combines the Nonlinear AutoRegressive with eXogenous (NARX) input model with the 4 high fidelity surrogate model Kriging. The sparsity in the proposed approach is introduced in 5 the NARX model by reducing the number of polynomial bases using the least angle regression 6 (LARS) algorithm. Sparse KNARX captures the non-linearity of a problem by the NARX 7 model, whereas the uncertain parameters are propagated using the Kriging surrogate model 8 and, further, LARS makes the model efficient. The accuracy and the efficiency of the sparse 9 KNARX is measured through uncertainty quantification applied to three nonlinear stochastic 10 dynamical systems. The time dependent mean and standard deviation are predicted for all 11 the numerical examples. Instantaneous stochastic response characteristics and maximum 12 absolute response are also predicted. All the results are compared with the full scale MCS 13 results and a mean error is calculated for all the numerical problems to measure the accuracy. 14 All the results show excellent agreement with the MCS results in a very limited computational 15

UMR_T9406, F69622, Lyon, France. E-mail: biswarup.bhattacharyya@ifsttar.fr ²Professor, Univ Lyon, Université Claude Bernard Lyon 1, IFSTTAR, LBMC UMR_T9406, F69622, Lyon,

France. E-mail: eric.jacquelin@univ-lyon1.fr ³Researcher, Univ Lyon, Université Claude Bernard Lyon 1, IFSTTAR, LBMC UMR_T9406, F69622, Lyon, France. E-mail: denis.brizard@ifsttar.fr

¹Corresponding author, Ph.D. student, Univ Lyon, Université Claude Bernard Lyon 1, IFSTTAR, LBMC

cost. Along with this, the efficiency of the sparse KNARX is also measured by the CPU time
and the required number of surrogate model evaluations. In all instances, sparse KNARX
outperforms other state-of-the-art methods which justifies the applicability of this model for
nonlinear stochastic dynamical systems.

Keywords: NARX model, Kriging, Nonlinear stochastic dynamical system, LARS, Uncer tainty quantification

22 INTRODUCTION

Uncertainty is an inherent property for any type of real world engineering problem which 23 may arise due to material heterogeneity, variability in dimensions, external forces. It is 24 evident from various studies (Grigoriu 1996; Lucor et al. 2004; Kundu and Adhikari 2014; 25 Chakraborty and Chowdhury 2015; Mai and Sudret 2017) that these sources of uncertainties 26 are always present in a dynamical system. Now, if the input quantities are uncertain, it is 27 obvious that the response characteristics would also be uncertain. The propagation of those 28 uncertain input parameters through a dynamical system and the prediction of uncertain 29 response characteristics are the main objectives of this paper. 30

The most used method for uncertainty quantification of any engineering problem is Monte 31 Carlo simulation (MCS) (Sheppard 1969; Muscolino et al. 2003). Mostly, MCS is used to pre-32 dict the stochastic response characteristics for any type of problem and often result found by 33 MCS is used as the principal result for any problem. However, the accuracy of MCS greatly 34 depends on the number of simulations because MCS requires a large number of model evalu-35 ations to predict an accurate result for a complex engineering problem. Thus, for a nonlinear 36 dynamical system, this method is highly time consuming and very much computationally 37 expensive. To overcome the issues of MCS, several surrogate models have been developed 38 by the researchers (Lucor and Karniadakis 2004; Lucor et al. 2004; Gerritsma et al. 2010; 39 Kundu and Adhikari 2014; Luchtenburg et al. 2014; Mai and Sudret 2017) in the last few 40 decades for stochastic dynamical systems. These surrogate models are the combination of 41 MCS and some kind of polynomials which maintain a trade-off between efficiency and accu-42

⁴³ racy such that the stochastic response behavior can be predicted with higher accuracy and ⁴⁴ lower computational cost. In this regards, one class of surrogate model widely known as ⁴⁵ polynomial chaos expansion (PCE) (Xiu and Karniadakis 2002) has been used extensively in ⁴⁶ the last few decades for the uncertainty propagation in stochastic dynamical systems (Lucor ⁴⁷ et al. 2004; Wan and Karniadakis 2005; Kundu and Adhikari 2014; Jacquelin et al. 2015; ⁴⁸ Jacquelin et al. 2017; Ozen and Bal 2017).

PCE was proposed only to propagate Gaussian input random variables in (Wiener 1938) 49 which was further improved in (Xiu and Karniadakis 2002) to account the other types of 50 random variables. This method is also known as generalized PCE (gPCE). Most of the 51 methods developed till date have utilized gPCE as the basic tool for propagating uncertainties 52 in the stochastic dynamical systems. Therefore, Wan and Karniadakis (Wan and Karniadakis 53 2005) developed a multi-element gPCE to capture the non-linearity of the problem. This 54 method decomposes the domain into multiple segments (when the variance of the stochastic 55 response becomes too worse) such that the non-linearity and the probability density function 56 (PDF) of the response can be captured efficiently. A similar method has been developed in 57 (Gerritsma et al. 2010) and (Luchtenburg et al. 2014) using some different criteria. However, 58 for a system of ordinary differential equations (ODE) having three random variables, it is 59 shown in (Gerritsma et al. 2010) that PCE needs to be constructed at every time-step. On 60 the other hand, a different type of development has been made in (Maitre et al. 2010) and 61 (Mai and Sudret 2017) by rescaling the time domain which is often called time warping 62 PCE. However, it can be seen clearly in (Mai and Sudret 2017) that the time warping 63 PCE cannot predict the variance of the stochastic response properly in the later time for 64 nonlinear dynamical system with a few random variables. In contrast, a surrogate model has 65 been recently proposed (Spiridonakos and Chatzi 2015; Mai et al. 2016) by combining PCE 66 and Nonlinear Auto-Regressive with eXogenous input (NARX) (Billings et al. 1989; Chen 67 et al. 1990; Wei and Billings 2009; Billings 2013) model to account for the dynamic behavior 68 and the non-linearity of the problem. In this method, the non-linearity of the problem is 69

taken care by the NARX model while the uncertain parameters of the dynamical system are
propagated by PCE. However, the proposed model still uses high degree polynomials even
for nonlinear single degree of freedom (SDOF) dynamical systems (Mai et al. 2016) which
increases the computational cost drastically.

Another class of surrogate model widely known as Gaussian process regression or, Kriging 74 surrogate model (Krige 1951; Santner et al. 2003) has proved the efficiency in predicting 75 the stochastic response characteristics for high-dimensional problems (Mukhopadhyay et al. 76 2017; Bhattacharyya 2018). However, if one wants to predict the time-dependent stochastic 77 response behavior of an uncertain dynamical system, a new Kriging model is required to fit 78 for each time-instances and almost seems the limitation like MCS. It is also mentioned in 79 (Chakraborty and Chowdhury 2015; Chatterjee and Chowdhury 2017) that for a non-linear 80 dynamical systems, Kriging requires a large number of model evaluations. However, the 81 efficiency in predicting the stochastic response behavior for the engineering system having 82 spatial random parameters has been well established through several researches (Simpson 83 et al. 2001; Tong et al. 2015; Sugai et al. 2015; Huang et al. 2016; Lu et al. 2018), but the use 84 of Kriging surrogate model is still questionable for nonlinear stochastic dynamical systems. 85 Therefore, several improvements have been made by the researchers (Kersaudy et al. 2015; 86 Chakraborty and Chowdhury 2017; Bayarri et al. 2007; Chatterjee and Chowdhury 2018) 87 to alleviate the issue of the curse of dimensionality and account for the non-linearity of 88 the response behavior, but still these methods are suffering to describe the time dependent 89 response behavior of random non-linear dynamical systems efficiently. To address this issue, 90 a surrogate model is constructed in the present paper in a similar way to (Mai et al. 2016) 91 by combining the NARX model with the Kriging surrogate model. Therefore, the issue 92 of capturing the high order non-linearity of a stochastic dynamical system can be resolved 93 by utilizing the NARX model and the uncertainties are propagated by the Kriging. Indeed, 94 NARX model has been investigated by very few researchers in context of stochastic dynamical 95 systems (Spiridonakos and Chatzi 2015; Mai et al. 2016; Worden et al. 2018) as compared 96

⁹⁷ to system identification tool for deterministic nonlinear dynamical systems (Billings et al.
⁹⁸ 1989; Wei and Billings 2009; Xie et al. 2009; Zhang and Li 2015).

The rest of the paper is organized as follows. A brief description of Kriging and NARX model are given in section 2 and section 3 respectively. Section 4 introduces the proposed model along with an algorithm to implement it for dynamical systems. Further, the applicability of the proposed approach for dynamical systems is illustrated through three typical nonlinear stochastic dynamical systems in section 5 and section 6 describes the important conclusion drawn from the present study.

105 KRIGING

Kriging is a well established surrogate model technique which combines a regression function with a Gaussian process. Kriging was first introduced in geostatistics (Matheron 1963) and afterwards it was used for the analysis of computer experiments (Sacks et al. 1989). One of the important characteristics of Kriging is that it predicts the quantity of interest in a finite region by an unbiased estimator. A brief description of Kriging is presented in this section.

112 Construction of model

Consider $\Xi = \{\xi_1, \xi_2, \dots, \xi_d\}$ as the *d*-dimensional input random variables in the probability space \mathcal{P} , where $\Xi \in \mathcal{D} \subset \mathbb{R}^d$. For *N* number of sample points, $Y = \{y(\Xi_1), y(\Xi_2), \dots, y(\Xi_N)\}^T$ are the corresponding function evaluations. In Kriging, the performance function for a realization is given by:

$$\mathcal{M}(\Xi) = \beta^T \phi(\Xi) + Z(\Xi) \tag{1}$$

In Equation 1, the first part of the expression $\beta^T \phi(\Xi)$ represents the regression part of the model which can also be written as:

$$\beta^T \phi\left(\Xi\right) = \sum_{i=1}^{P} \beta_i \phi_i\left(\Xi\right) \tag{2}$$

 $\phi_i(\Xi)$ are the polynomial basis functions which are constructed with the normalized input variables and β_i are the corresponding coefficients of the basis functions. *P* represents the total number of terms in the basis function which depends on the degree of the polynomial. According to the form of the polynomial, Kriging model has several variants in the literature (Mukhopadhyay et al. 2017). A universal Kriging model is utilized in the present work (Equation 2). The second part of Equation 1 defines the Gaussian process with mean zero and the process covariance is

$$\operatorname{cov}\left[Z\left(\Xi_{i}\right), Z\left(\Xi_{j}\right)\right] = \sigma_{Z}^{2} \mathcal{R}\left(\Xi_{i}, \Xi_{j}\right); \qquad i, j = 1, 2, \dots, N$$
(3)

where, Ξ_i and Ξ_j are two different sample points and σ_Z^2 is the process variance. $\mathcal{R}(\Xi_i, \Xi_j)$ is the auto-correlation function between two sample points. A variety of auto-correlation functions have been adopted by the researchers (Kaymaz 2005; Bhattacharyya 2018; Sacks et al. 1989) such as linear, exponential or Gaussian. The mostly used Gaussian auto-correlation function is utilized in the present paper which is given by:

$$\mathcal{R}\left(\Xi_{i},\Xi_{j}\right) = \prod_{k=1}^{d} \exp\left[-\theta_{k}(\xi_{i,k} - \xi_{j,k})^{2}\right]$$
(4)

where θ_k is the hyper-parameter of the auto-correlation function. The Kriging model parameters β and σ_Z , and the hyper-parameter θ_k can be determined by the maximum likelihood estimation (MLE) (Sacks et al. 1989). The procedure of computing the parameters is explained in (Sacks et al. 1989; Santner et al. 2003; Kaymaz 2005).

135 Prediction

Consider any untried sample point for prediction $\Xi_0 \in \mathbb{R}^d$. The function value at the new sample Ξ_0 is predicted by the best linear unbiased predictor (BLUP). The BLUP and the predicted variance are given by:

$$\hat{\mathcal{M}}(\Xi_0) = w^T(\Xi_0) Y \tag{5}$$

$$= \hat{\beta}^{T} \phi\left(\Xi_{0}\right) + r^{T}\left(\Xi_{0}\right) \mathscr{R}^{-1}\left(\hat{\beta}^{T} \phi\left(\Xi_{0}\right)\right)$$

$$\tag{6}$$

$$\sigma_{\hat{M}}^{2}(\Xi_{0}) = \hat{\sigma}_{Z}^{2} \left(1 - \left[\phi^{T}(\Xi_{0}) \quad r^{T}(\Xi_{0}) \right] \left[\begin{array}{c} 0 \quad F^{T} \\ F \quad \mathscr{R} \end{array} \right]^{-1} \left[\begin{array}{c} \phi(\Xi_{0}) \\ r(\Xi_{0}) \end{array} \right] \right)$$
(7)

where, $r(\Xi_0) = \{\mathcal{R}(\Xi_0, \Xi_1), \mathcal{R}(\Xi_0, \Xi_2), \dots, \mathcal{R}(\Xi_0, \Xi_N)\}$ is the correlation matrix between the new untried sample point and the initial samples, and F is the matrix of basis function at the initial sample points of dimension $N \times P$. \mathscr{R} is the correlation matrix for the initial samples. Further, the unknown parameters $\hat{\beta}$ and σ_Z^2 are calculated as:

$$\hat{\beta} = \left(F^T \mathscr{R}^{-1} F\right)^{-1} F^T \mathscr{R}^{-1} Y \tag{8}$$

$$\hat{\sigma}_Z^2 = \frac{1}{N} \left(Y - F\hat{\beta} \right)^T \mathscr{R}^{-1} \left(Y - F\hat{\beta} \right)$$
(9)

Once the unknown parameters using the Kriging model are estimated, the prediction of the response at the untried point can be made easily by utilizing Equation 6.

145 NARX MODEL

146 Overview of NARX model

A brief overview of NARX model is presented in this section. The time dependent response characteristics of a dynamical system at current time instance can be predicted by the responses of some previous time instances and the excitation of some previous and current time instances through a suitable NARX model (Chen and Billings 1989; Billings 2013). If we consider a dynamical system having the time dependent excitation, then according to the ¹⁵² NARX model, the dynamical system can be expressed as:

$$y(t) = \mathcal{F}[z(t)] + \varepsilon(t) \tag{10}$$

where, $z(t) = \{x(t), x(t - \Delta t), x(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - \Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), x(t - n_{x_m}\Delta t), y(t - 2\Delta t), ..., x(t - n_{x_m}\Delta t), y(t - 2\Delta t), x(t - 2\Delta t), x(t - n_{x_m}\Delta t), y(t - n_{x_m}$ 153 $y(t - n_{y_m}\Delta t)$ ^T is the vector having all the lagged system excitation and response compo-154 nents which forms the time-dependent auto-regressive response model $\mathcal{F}[\bullet]$. $\varepsilon(t)$ is the 155 residual of the NARX model which is supposed to be a normally independent distributed 156 (NID) process with zero mean and Δt is the time-step chosen for the NARX model. n_{x_m} and 157 n_{y_m} are the maximum time lags for the excitation and the response quantity respectively. It 158 is obvious that the underlying form of the function must be nonlinear to capture the strong 159 non-linearity of a dynamical system. Consequently, different types of functions have been 160 used by the researchers such as polynomial (Cantelmo and Piroddi 2010), wavelet (Billings 161 and Wei 2005), sigmoid function (Sjöberg et al. 1995), RBF (Li et al. 2005) and neural net-162 work (Tsungnan Lin et al. 1996). Out of these, the effectiveness of polynomial function has 163 already been proved in the literature (Leontaritis and Billings 1985; Cantelmo and Piroddi 164 2010; Cheng et al. 2011). Therefore, a linear-in-parameter form of polynomial has been used 165 in the present paper which is represented by 166

$$\mathcal{F}[z(t)] = \sum_{i=1}^{M} \varphi_i \psi_i [z(t)]$$
(11)

In the above equation, M is the total number of terms in the polynomial basis function, $\psi_i[z(t)]$ are the polynomial basis functions and φ_i are the corresponding coefficients of the NARX model. The polynomial basis function for the NARX model is dependent on the time varying excitation and response. Consequently, the polynomial basis matrix and the coefficient matrix for a particular sample point k are represented by:

$$\Psi_{k}(t,\Xi_{k}) = \{\psi_{1}[z_{k}(t,\Xi_{k})], \psi_{2}[z_{k}(t,\Xi_{k})], \dots, \psi_{M}[z_{k}(t,\Xi_{k})]\}^{T}; \quad \Psi_{k} \in \mathbb{R}^{M \times 1}$$
(12)

$$\varphi^k = \{\varphi_1, \varphi_2, \dots, \varphi_M\}; \quad \varphi^k \in \mathbb{R}^{1 \times M}$$
(13)

Now, if we discretize the total time T in N_t number of time instances i.e. $t \in \{t_1, t_2, \ldots, t_{N_t}\}$, then for N_t number of time-steps, the polynomial basis function matrix can be given by $\Psi_k \in \mathbb{R}^{M \times N_t}$.

The procedure of choosing the type of polynomial for $\mathcal{F}[z(t)]$ and estimating the corresponding coefficients are described in the next section.

¹⁷⁷ Model formulation and parameter estimation of the NARX model

The polynomial basis function for the NARX model can be formulated by two variables, 178 i.e. the excitation and the response of the dynamical system, either as an independent 179 variable basis function (Spiridonakos and Chatzi 2015) or as a composition of both variables 180 (Mai et al. 2016) with certain maximum degree of the polynomial basis. For a nonlinear 181 system, it is always important to use the interaction terms (Billings 2013). Hence, a similar 182 kind of polynomial basis function has been adopted in the present paper. Another important 183 issue with the polynomial basis function is the selection of the maximum time lags n_{x_m} and 184 n_{y_m} for the excitation and the response respectively. The maximum time lags are selected 185 according to (Spiridonakos and Chatzi 2015; Mai et al. 2016) in the present paper, which 186 are two-times the number of DOF of the system. 187

On the other hand, the computation of the NARX coefficients is one of the challenging tasks in the construction of the NARX model. The coefficients of the NARX model can be computed easily by ordinary least square method (for the k-th sample point). However, it has been found often in the literature (Blatman and Sudret 2011; Spiridonakos and Chatzi

2015) that all the terms in the polynomial basis do not get involved in predicting the response 192 characteristics of the system, and reducing the degree of the polynomial may reduce the ac-193 curacy of prediction. Thus, it is important to capture the important terms in the polynomial 194 basis function which are solely responsible for the response behavior of a system. Recently, 195 the important NARX basis terms were identified using genetic algorithm in (Spiridonakos 196 and Chatzi 2015). However, due to the form of NARX model, the important terms can also 197 be identified with the popularly used regularized least square method, least angle regression 198 (LARS) (Efron et al. 2004). Consequently, LARS is used in the present paper for selecting 199 the important terms in the polynomial basis. 200

201 Sparse NARX model

The sparse NARX model is selected in a similar way to (Mai et al. 2016) in the present 202 paper. At first, it is required to select the samples exhibiting high non-linearity. The 203 responses having highly non-linear behavior can be selected by the measurement of non-204 linearity of the response (Spiridonakos and Chatzi 2015) or, specifying some threshold value 205 for the response series (Mai et al. 2016). In the present paper, a combination of both 206 the mentioned methods (Spiridonakos and Chatzi 2015; Mai et al. 2016) has been utilized. 207 Firstly, the response versus restoring force is plotted arbitrarily without performing any 208 simulations (keeping other parameters constant at their mean values). The intensity of 209 the response is increased up to a certain limit till the nonlinear behavior is noticed in the 210 force-displacement relationship. From the restoring force curve, the threshold value for a 211 response series can be selected easily by observing the starting point of the non-linearity of 212 the response series. Imposing the threshold value would reduce the number of samples to 213 $N_1 < N$. Now, for each of the N_1 samples (e.g. for the k-th sample), a full NARX model is 214 formulated as follows: 215

$$y(t, \Xi_k) = \varphi^k \Psi_k(\Xi_k) \tag{14}$$

where, Ψ_k is the matrix having all the M terms of the NARX model polynomial basis for all the time-steps with dimension $M \times N_t$ which is formulated by the current and previous excitation, and previous responses. $y(t, \Xi_k)$ is the response series for the k-th sample point. At this step, the coefficient vector φ^k is the unknown.

Remark 1: One should discretize the total time T with a suitable time-step Δt (small enough to capture the dynamics correctly). Besides, the time-step plays a vital role in case of NARX model. In the present paper, we have used the same time-step for the time integration and the construction of the NARX model.

The LARS algorithm is then employed to select the important terms for each of the N_1 full NARX models.

Remark 2: It is evident that N_1 different NARX models are found at this step. The most important terms for all the NARX models are found using LARS algorithm. However, it may happen that more than one NARX model contains similar terms in the polynomial basis matrix. Therefore, only the N_2 different NARX models are selected at this step.

The unique NARX models are selected from the N_1 number of NARX models which may further reduce the number of NARX models to $N_2 \leq N_1$. Hence, for each of the N_2 sparse NARX models, the coefficients of all the N initial samples are computed by ordinary least square. The response series of the initial N samples are then re-constructed using the coefficients and the selected polynomial bases, and the error for each sample point is predicted as follows:

$$\epsilon_{k} = \frac{\sum_{i=1}^{N_{t}} \left[y\left(t_{i}, \Xi_{k}\right) - \hat{y}\left(t_{i}, \Xi_{k}\right) \right]^{2}}{\sum_{i=1}^{N_{t}} \left[y\left(t_{i}, \Xi_{k}\right) - \bar{y}\left(\Xi_{k}\right) \right]^{2}}$$
(15)

where, $\bar{y}(\Xi_k)$ is the time average mean of the k-th response series which is given by:

$$\bar{y}\left(\Xi_k\right) = \frac{1}{N_t} \sum_{i=1}^{N_t} y\left(t_i, \Xi_k\right) \tag{16}$$

The mean predicted error for all the sample points by a particular sparse NARX model out of N_2 sparse NARX models is given by:

$$\bar{\epsilon} = \frac{1}{N} \sum_{k=1}^{N} \epsilon_k \tag{17}$$

The finally selected sparse NARX model is the one having the predicted mean error for N sample points lower than some threshold value. In the present paper, the threshold value of the mean error is imposed as 1×10^{-3} for all the examples.

Remark 3: It is of utter importance to mention that if the predicted mean errors for two different NARX model are found same (or, lower than the threshold value) then the sparse NARX model having less number of terms in the polynomial basis is selected as the final sparse NARX model.

246 KRIGING-NARX MODEL

Consider a dynamical system having some uncertain input parameters $\Xi = \{\xi_1, \xi_2, \dots, \xi_d\}$, then the time dependent response of the system can be represented by a NARX model as:

$$y(t, \Xi_k) = \sum_{i=1}^{M} \varphi_i(\Xi_k) \psi_i[z_k(t)]; \quad k = 1, 2, \dots, N$$
(18)

It is observed from Equation 18 that the coefficients of the NARX model are dependent on the sample points which does not make the model stochastic in nature. To get the independent coefficients of the NARX model, the NARX coefficients are represented by the Kriging surrogate model as given in Equation 1:

$$\varphi_i(\Xi) = \beta_i^T \phi(\Xi) + Z_i(\Xi); \quad i = 1, 2, \dots, M$$
(19)

²⁵³ Further, the model is constructed by the Kriging surrogate model as discussed in section 2.

²⁵⁴ Therefore, the full KNARX model is expressed as:

$$y(t,\Xi) = \sum_{i=1}^{M} \left(\beta_i^T \phi\left(\Xi\right) + Z_i\left(\Xi\right) \right) \psi_i \left[z\left(t\right) \right]$$
(20)

The coefficient of the regression part, β^T and the Gaussian process part $Z(\Xi)$ are dependent on the number of terms in the NARX model, whereas the polynomial basis function of the Kriging model for all the NARX coefficients remain the same as the basis is purely dependent on the uncertain input parameters.

Remark 4: It should be noted that the Kriging model should be calibrated M times (Mis the total number of terms for a full NARX model) because the coefficients of the NARX model for N samples corresponding to a polynomial basis act as the single response quantity for the Kriging model.

The response quantity of a dynamical system at some untried sample points Ξ_0 can be predicted by BLUP as mentioned in Equation 6 in accordance with the full NARX model in an auto-regressive manner.

$$\hat{y}(t,\Xi_0) = \sum_{i=1}^{M} \left[\hat{\beta}_i^T \phi(\Xi_0) + r^T(\Xi_0) R^{-1} \left(\hat{\beta}_i^T \phi(\Xi_0) \right) \right] \psi_i[z(t)]$$
(21)

Equation 21 helps in predicting the time dependent response characteristics of a dynam-266 ical system at large number of sample points having d dimensional random input variables. 267 It is evident from Remark 4 that the computational cost increases with the increase of num-268 ber of terms in the NARX polynomial basis. For that reason, the sparse NARX model as 269 discussed in section 3 is used in accordance with the Kriging surrogate model in the present 270 paper. Consequently, the number of terms for the NARX model is decreased to $M_1 < M$ 271 which ultimately reduces the number of Kriging model calibration (M_1) and computational 272 cost. The algorithm for constructing the sparse KNARX model is provided in Table 1. 273

274 NUMERICAL APPLICATIONS

The sparse KNARX model as described in the previous section has been utilized for

uncertainty quantification of three typical nonlinear stochastic dynamical systems. For each 276 of the examples, the accuracy of the method is measured using the predicted mean error 277 as given in Equation 17 (Mai et al. 2016) (taking MCS as the reference) and the value of 278 the coefficient of correlation R^2 . Uncertainty quantification for all the problems is made 279 by predicting the time dependent mean and standard deviation of the responses. Further, 280 the PDFs of the responses are also predicted at some time instances. The computational 281 efficiency is measured through the computational cost (CPU time), the number of surrogate 282 model calibration and the number of initial sample points N. The first problem is also solved 283 by the Kriging model to measure the efficiency and the accuracy of the sparse KNARX model 284 over the Kriging. For the first two examples, the sparse KNARX predicted results are also 285 compared with the recently proposed sparse PCE-NARX surrogate model (Mai et al. 2016). 286 It is well known that a suitable sample point (often known as experimental design point) 287 generation strategy is required to use for the generation of initial samples in step 2 of Table 1. 288 Consequently, one of the most widely used sampling strategies, Latin hypercube sampling 289 (LHS) (Mai et al. 2016; Chatterjee and Chowdhury 2017) has been utilized for the initial N290 number of sample points generation. 291

²⁹² Duffing oscillator

A non-linear duffing oscillator is considered as the first example for the illustration of the proposed model. The governing differential equations of the duffing oscillator are given by:

$$\ddot{y}(t) + 2\zeta\omega\dot{y}(t) + \omega^{2}\left[y(t) + \varepsilon y^{3}(t)\right] = x(t)$$
(22)

$$x(t) = A\sin\left(\omega_x t\right) \tag{23}$$

In Equation 22, ω represents the natural frequency considering the undamped linear structure ($\varepsilon = 0, \zeta = 0$), ζ is the damping ratio and ε controls the non-linearity of the system. x(t) denotes the excitation part of the dynamical system which is considered sinusoidal in this case (see Equation 23). The initial conditions are y(0) = 0 and $\dot{y}(0) = 0$. The numerical integration has been performed for T = 30 s with a time-step of $\Delta t = 0.01$ s through MATLAB solver *ode45*. All the parameters of the duffing oscillator are considered uncertain (i.e. $\Xi = \{\omega, \zeta, \varepsilon, A, \omega_x\}$) (Mai 2016). The distribution types along with the parameters of the distribution are listed in Table 2.

Time dependent stochastic displacement of the duffing oscillator is predicted by MCS, Kriging, sparse PCE-NARX (Mai et al. 2016) and sparse KNARX model. MCS has been performed with 3×10^4 sample points and N = 50 samples have been generated by LHS for the prediction of the stochastic response behavior using Kriging. The Kriging model has been calibrated for each time-step (i.e. 3001 times). The step by step procedure of constructing the sparse KNARX model (according to Table 1) is described below:

1. For the duffing oscillator,
$$d = 5$$
 (see Table 2)

310 2. The sparse KNARX model is constructed using N = 25 LHS points.

3. For the construction of the sparse KNARX and the sparse PCE-NARX model, it is 311 important to specify the threshold value for capturing the nonlinear response series 312 according to step 3 of Table 1. Full NARX models are to be constructed on those 313 samples which satisfy the criterion of threshold value. For that reason, the displacement 314 y(t) versus restoring force $f_s = \omega^2 [y(t) + \varepsilon y^3(t)]$ has been plotted in Figure 1 (keeping 315 other parameters constant at their mean values). From Figure 1, it is clear that the 316 displacement behaves almost linearly for $y(t) \in [-0.045 \text{ m}, 0.045 \text{ m}]$ and beyond this 317 region, the displacement is highly nonlinear. Consequently, to capture the highly 318 nonlinear response series, the threshold value for the nonlinear displacement is set as 319 $\max(|y(t)|) > 0.045 \,\mathrm{m}$. Thus, only those samples will be picked for the construction 320 of NARX model which falls beyond the region $y(t) \in [-0.045 \text{ m}, 0.045 \text{ m}]$. 321

4. The displacement series are then obtained at the initial N = 25 samples. Out of all the response series, the displacement versus restoring force for two different samples (13-th and 25-th sample point) are plotted in Figure 2. It is clearly seen that the 13-th sample point exhibits higher order non-linearity than the 25-th sample point. It should be noted that the region of displacement value is almost restricted in [-0.02 m, 0.02 m]for the 25-th sample point which is far less than the specified threshold value. On the other hand, the displacement intensities are far beyond the threshold value and behaves nonlinearly for the 13-th sample point.

5. After imposing the above-specified threshold criterion, only $N_1 = 2$ samples are selected as the highly nonlinear response series. Thus, only 2 full NARX models are required for the duffing oscillator using the sparse KNARX model (N = 25). The basis function for the full NARX model is chosen as:

$$\psi_i \left[z\left(t\right) \right] = x^{l_i} \left(t - n_{x_i} \Delta t \right) y^{m_i} \left(t - n_{y_i} \Delta t \right)$$
(24)

where, x and y are the excitation and the response of the duffing oscillator respectively.

6. The maximum time lags for the excitation and the response are taken as $n_{x_m} = 2$ and 335 $n_{y_m} = 2$ respectively due to 1-DOF system. $n_x \in \{0, 1, 2\}$ and $n_y \in \{1, 2\}$ represent 336 all the time lags for the excitation and the response respectively. $l \in \{0,1\}$ and 337 $m \in \{0, 1, 2, 3\}$ are the degrees for the excitation and the response respectively, with a 338 maximum degree of the polynomial 3 (i.e. $l_i + m_i \leq 3$), due to the cubic non-linearity 339 of the system. A total 22 number of terms have been obtained in the polynomial 340 basis matrix utilizing all the above-mentioned criterion which depicts M = 22 and 341 $i = 1, 2, \ldots, M$ in Equation 24. 342

7. Therefore, 2 full NARX models are constructed using the basis function as given in
 Equation 24, and they have 22 terms in the NARX polynomial basis matrix.



9. The sparse NARX models are then retained which have unique set of polynomial bases
and for the duffing oscillator, both the sparse NARX models are found unique. The
polynomials selected by the LARS algorithm for both the NARX models are listed in
Table 3.

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10. The coefficients for all the 25 samples are obtained with the ordinary least square for both the sparse NARX model. For this step, explicitly $N \times N_2$ number of ordinary least squares is performed.

11. Then, the response series are reconstructed again in a recursive manner using the
 coefficients and the polynomial bases.

12. $\bar{\epsilon}$ is then computed by both the sparse NARX models for the N samples.

- ³⁵⁷ 13. $\bar{\epsilon}$ for both the sparse NARX models is found below the threshold value. Hence, the ³⁵⁸ Model 2 of Table 3 is chosen as the best sparse NARX model (according to Remark 3) ³⁵⁹ and the predicted mean error for the N = 25 samples is found as $\bar{\epsilon} = 1.68 \times 10^{-7}$.
- 14. The coefficient vector $\varphi_i(\Xi) \in \mathbb{R}^{N \times 1}$; i = 1, ..., 8 corresponding to each of the polynomials are uncertain. These 8 coefficient vectors are considered as the uncertain response quantities for the Kriging model. Hence, the unknown parameters of the Kriging model $\hat{\beta}, \hat{\sigma}_Z^2$ and θ_k are computed by the MLE for all the 8 NARX coefficients separately. Consequently, 8 Kriging models are calibrated for converting the model stochastic.
- 15. The same 3×10^4 MCS samples are used here for the prediction by the surrogate model.
- 16. The 8 NARX coefficient vectors for the 3×10^4 samples are then predicted using the 8 calibrated Kriging models by BLUP.
- ³⁶⁸ 17. Further, the predicted coefficients and the selected polynomials are used to predict the ³⁶⁹ response series auto-regressively for the 3×10^4 MCS samples.

The same N = 25 LHS samples are also utilized for uncertainty quantification using 370 the sparse PCE-NARX (Mai et al. 2016) model. Here, the sparse adaptive PCE model 371 is constructed using the UQLab module (Marelli and Sudret 2018). All the parameters 372 of the sparse PCE model are taken similar to (Mai et al. 2016) for the present com-373 putation. Therefore, the maximum interaction is chosen as 2 and the q-norm is taken 374 as 1 with the degree of the polynomials varying between 1 and 20 (Marelli and Sudret 375 2018; Mai et al. 2016). However, the predicted response is not converged using the sparse 376 PCE-NARX model with the same number of samples. For that reason, the number of 377 samples for the sparse PCE-NARX model is increased to N = 35 and the time depen-378 dent responses are predicted with the sparse PCE-NARX model. Here, the final sparse 379 NARX model is found having $M_1 = 9$ terms in the NARX polynomial basis which are 380 $\left\{y\left(t-\Delta t\right), y\left(t-2\Delta t\right), y^{2}\left(t-\Delta t\right), y^{3}\left(t-\Delta t\right), y^{3}\left(t-2\Delta t\right), x\left(t\right), x\left(t-2\Delta t\right), x\left(t\right)y\left(t-\Delta t\right), x\left(t-2\Delta t\right), x\left(t\right)y\left(t-\Delta t\right), x\left(t-2\Delta t\right),$ 381 $x\left(t-2\Delta t\right)y^{2}\left(t-2\Delta t\right)\Big\}.$ 382

To reduce further the computational cost, another study has been performed using less 383 number of initial samples with N = 21 (for sparse KNARX). In this case, 3 samples are 384 retained initially based on the criterion of threshold value of the response series and the 3 385 full NARX models are formulated using the basis function as mentioned in Equation 24. 386 Further, the sparse NARX models are found by applying the LARS algorithm and all the 387 three models are found as the unique sparse NARX models. Therefore, the coefficients for 388 the N = 21 samples are found by the ordinary least square method and then, all the 21 389 response series are reconstructed using the coefficients of the sparse NARX models. The 390 finally selected sparse NARX model is the Model 1 of Table 3 and the predicted mean error 391 of the selected sparse NARX model is found as $\bar{\epsilon} = 1.80 \times 10^{-7}$ for the 21 samples. Further, 392 the coefficients corresponding to the sparse NARX polynomial bases are modelled using the 393 Kriging surrogate model. On the contrary, the sparse PCE-NARX model is not able to 394 predict the response with less samples. 395

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The time varying stochastic response characteristics are predicted by the time dependent

mean and standard deviation which are plotted in Figure 3. The figure clearly depicts the 397 efficiency (initial number of sample points N) and the accuracy of the sparse KNARX model 398 over the Kriging model. The sprase KNARX has predicted better results with fewer number 399 of model evaluations (N = 21) and the sparse PCE-NARX model is incapable to predict a 400 result even using N = 25 samples. To illustrate the accuracy of the sparse KNARX, the 401 instantaneous response characteristics are also plotted. The scatter diagrams and the PDFs 402 of the predicted response are plotted in Figure 4 at three different time instance (10s, 20s 403 and $30 \, \text{s}$). The accuracy metrics of the instantaneous response characteristics are listed in 404 Table 4, they clearly suggest that the sparse KNARX is highly efficient as compared to the 405 Kriging model. The accuracy of the sparse KNARX model is also comparatively higher using 406 less model evaluations than the sparse PCE-NARX model. 407

The stochastic absolute maximum displacement max (|y(t)|), plotted in Figure 5, ultimately measures the safety corridor for the dynamical system. It is seen clearly that the sparse KNARX outperforms the Kriging and the sparse PCE-NARX with very less number of sample points in predicting the PDF of max (|y(t)|), and the accuracy of the sparse KNARX is given by the R^2 value in Table 5 which is very close to 1.0 by N = 25.

Further, the accuracy of the overall model is computed by the mean error (Equation 17) 413 for the predicted responses and the error for the predicted max (|y(t)|). The efficiency of 414 the sparse KNARX has already been shown by the initial number of sample points. An 415 accurate result is predicted by the sparse KNARX even with much less number of model 416 evaluations (N = 21) as compared to the other methods. The efficiency of the sparse 417 KNARX is also measured by the number of surrogate model calibrations (n_K) for a method 418 and by the CPU time. All the accuracy and the efficiency measurement metrics are reported 419 in Table 5. Table 5 is suggesting that the sparse KNARX model outperforms the Kriging 420 and the sparse PCE-NARX in accuracy and efficiency. It is noticeable that the CPU time 421 is lower with higher value of N for the sparse KNARX model due to less number of Kriging 422 model calibration. 423

424 Bouc-Wen oscillator

A non-linear Bouc-Wen oscillator (Bouc 1967; Wen 1976) is investigated in this example.
 The governing differential equation for the Bouc-Wen oscillator is given by:

$$\ddot{y}(t) + 2\zeta \omega \dot{y}(t) + \omega^{2} \left[\rho y(t) + (1 - \rho) w(t) \right] = -A \sin(\omega_{x} t)$$

$$\dot{w}(t) = \gamma \dot{y}(t) - \alpha \left| \dot{y}(t) \right| \left| w(t) \right|^{n-1} w(t) - \beta \dot{y}(t) \left| w(t) \right|^{n}$$
(25)

where, ζ and ω are the damping ratio and the natural frequency of the oscillator respectively. $\rho = 0, \gamma = 1, \beta = 0$ and n = 1 are considered for this problem. The excitation of the oscillator is considered as $x(t) = A \sin(\omega_x t)$ and w(t) is the hysteric displacement as given in (Wen 1976). The initial conditions at rest are $y(0) = 0, \dot{y}(0) = 0$ and w(0) = 0. Similar to (Mai and Sudret 2017), 5 uncertain parameters are considered for the oscillator, which are $\Xi = \{\zeta, \omega, \alpha, A, \omega_x\}$. The type of distributions for all the uncertain parameters are given in Table 6.

The stochastic response is calculated for the oscillator in the time domain $t \in [0, 30, 30]$ 434 with a time-step of $\Delta t = 0.005$ s. As it has already been illustrated through the previous 435 example, Kriging is unable to predict the stochastic response behavior for the non-linear 436 stochastic duffing oscillator even with higher samples than the sparse KNARX. Therefore, 437 Kriging has not been utilized from now onward. Similar to the previous example, the sparse 438 KNARX model has been constructed with two different sizes of sample points N = 40 and 439 N = 10. A different type of basis function has been considered for the Bouc-Wen oscillator 440 according to (Mai et al. 2016), which is given by: 441

$$\psi_i [z(t)] = \left\{ x^{l_i} (t - n_{x_i} \Delta t) \, | \dot{y} (t - \Delta t) |^{m_i}, \, \dot{y}^{l_i} (t - n_{y_i} \Delta t) \, | \dot{y} (t - \Delta t) |^{m_i} \right\}$$
(26)

In Equation 26, the basis function relies on the excitation and the velocity of the oscillator. Thus, the velocity is computed by the sparse KNARX model and further, the displacement of the system is obtained through numerical integration by utilizing the MATLAB solver *ode*45. Due to the hysteric displacement component, the bases are computed by two expressions as given in Equation 26 which has already been considered in (Mai et al. 2016). $l \in \{0, 1\}$ and $m \in \{0, 1\}$ are considered for the oscillator as single degree is noticed for the excitation and the velocity in Equation 25. $n_{x_m} = n_{y_m} = 4$ is considered as the problem can be appraised as 2-DOF system due to an extra hysteric displacement part i.e. $n_x \in \{0, ..., 4\}$ and $n_y \in \{1, ..., 4\}$. A total 21 number of terms are found in the full NARX polynomial basis matrix by utilizing Equation 26 and imposing all the mentioned conditions.

A threshold similar to the previous example was employed to detect the highly non-452 linear samples. The threshold value for the response of the Bouc-Wen oscillator is cho-453 sen as $\max(|\dot{y}(t)|) > 0.3 \,\mathrm{m\,s^{-1}}$. The threshold value reduces the number of samples from 454 N = 40 to $N_1 = 3$ which means only 3 full NARX models are required. Thus, 3 full 455 NARX models are formulated utilizing the basis function of Equation 26 and further the 456 LARS algorithm has been employed to make the full NARX models sparse. All the three 457 sparse NARX models are found unique in this step. Therefore, the coefficients for all the 40 458 initial samples are computed by the ordinary least square method for the 3 sparse NARX 459 models and the mean errors (Equation 17) are predicted by computing the time series in a 460 recursive manner. The finally selected sparse NARX model produces a mean error of $\bar{\epsilon} =$ 461 1.10×10^{-5} for the 40 samples and contains 8 terms in the polynomial basis matrix which are 462 $\left\{\left.\left|\dot{y}\left(t-\Delta t\right)\right|,x\left(t\right),x\left(t-4\Delta t\right),x\left(t-4\Delta t\right)\left|\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right),\dot{y}\left(t-4\Delta t\right),\dot{y}\left(t-\Delta t\right)\left|\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right)\left|\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right)\left|\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left(t-\Delta t\right)\left|\dot{y}\left(t-\Delta t\right)\right|,\dot{y}\left($ 463 $\dot{y}(t-4\Delta t)|\dot{y}(t-\Delta t)|\}.$ 464

A similar procedure is adopted by substantially reducing the initial number of sample points to N = 10. 4 samples are found mostly non-linear based on the previous threshold value. Out of the 4 full NARX models, 2 are found as unique sparse NARX models after applying the LARS for detecting the most important terms. Therefore, one sparse NARX model is selected based on the predicted mean error from both sparse NARX models. The final sparse NARX model is found to have the same terms in the polynomial basis as the previous one with N = 40.

⁴⁷² The stochastic responses are also predicted here by the sparse PCE-NARX model (Mai

et al. 2016) (the sparse PCE model is constructed here with the same conditions as the previous example). However, the sparse PCE-NARX is unable to predict the stochastic response behavior with N = 40 number of model evaluations for the Bouc-Wen oscillator. For that reason, the number of model evaluations is increased to N = 50 and the stochastic responses are predicted with the same $M_1 = 8$ terms in the sparse NARX model as in the sparse KNARX model with N = 40.

This study aims at quantifying the uncertainty associated with the response quantity. 479 The uncertain response characteristics are predicted for the displacement and the velocity 480 of the Bouc-Wen oscillator. The time dependent mean and the standard deviation of y(t)481 and $\dot{y}(t)$ are shown in Figure 6 and Figure 7 respectively. The figures show that both the 482 statistical moments predicted by the sparse KNARX are following the MCS results with 483 utmost accuracy. However, the accuracies of the statistical moments are deteriorating from 484 the initial time-steps using the sparse PCE-NARX model even with more samples. The 485 scatter diagrams and the PDFs at three different time instances (10s, 20s and 30s) are also 486 plotted in Figure 8 and Figure 9 for the displacement and the velocity respectively. It is 487 seen from all the figures that the sparse KNARX performs well in all instances with very few 488 samples. The error metrics for all the instantaneous displacements and velocities are given 489 in Table 7. An excellent accuracy in terms of error (ϵ) and R^2 value is noticed for all the 490 time instances by the sparse KNARX model. 491

For the prediction of the safety corridor under uncertainty, the scatter plots and the PDFs of the maximum absolute displacement and velocity are plotted in Figure 10 and Figure 11 respectively. The worst prediction is noticed for the PDFs by the sparse PCE-NARX model, whereas an excellent accuracy is observed in both the cases for the predicted maximum responses by the sparse KNARX model. These plots, which represent the uncertain maximum response behavior, can be utilized to measure the safety margin of the system.

To observe the accuracy of the surrogate models, the mean of the displacement and the velocity are plotted in state space by the MCS, the sparse PCE-NARX and the sparse

KNARX in Figure 12. It is evident from the figure that the accuracy in predicting the state 500 space behavior of the response is greatly achieved even using much less number of samples 501 (N = 10) by the sparse KNARX model whereas the sparse PCE-NARX predicted result is 502 the worst even with more samples. Similar to the previous example, the accuracy and the effi-503 ciency measurement metrics are given in Table 8. The table is showing clearly that the sparse 504 KNARX has predicted results with higher accuracy by minimum computational cost. The 505 efficiency of the proposed sparse KNARX method is also observed over the recently proposed 506 method time warping PCE (Mai and Sudret 2017) which required N = 100 (>> N = 10)507 samples to predict the stochastic response behavior for the same example. 508

⁵⁰⁹ A 2-DOF dynamical system

Finally, a 2-DOF dynamical system (Mai et al. 2016) has been considered for the applicability of the proposed sparse KNARX model. The dynamical system is shown in Figure 13 and the governing differential equation of the problem is:

$$m_{s}\ddot{y}_{1}(t) = -k_{s}[y_{1}(t) - y_{2}(t)]^{3} - c[\dot{y}_{1}(t) - \dot{y}_{2}(t)]$$

$$m_{u}\ddot{y}_{2}(t) = k_{s}[y_{1}(t) - y_{2}(t)]^{3} + c[\dot{y}_{1}(t) - \dot{y}_{2}(t)] + k_{u}[x(t) - y_{2}(t)]$$
(27)

where m_s is the sprung mass which is connected with the mass m_u by a non-linear spring with stiffness k_s and a damper with damping coefficient c. k_u is a linear spring attached to the ground having a sinusoidal displacement function $x(t) = A \sin(\omega_x t)$.

Similar to (Mai et al. 2016), all the parameters of the system are considered uncertain i.e. $\Xi = \{k_s, k_u, m_s, m_u, c, A, \omega_x\}$. The mean and the standard deviation of all the uncertain parameters are given in Table 9.

The main aim of this example is to predict the uncertain response $y_1(t)$ of mass m_s which is attached with the non-linear spring. This system has been solved by the sparse KNARX model with two different number of sample points (N = 50 and N = 20). As it has already been seen from the previous two examples that the sparse PCE-NARX model is unable to predict the stochastic response behavior of the dynamical systems properly, the sparse PCE- ⁵²⁴ NARX model is not utilized for this problem. It should be noted that the problem has been ⁵²⁵ solved in the time domain $t \in [0 \text{ s}, 30 \text{ s}]$ with a time-step of $\Delta t = 0.01 \text{ s}$ by *ode45*. The initial ⁵²⁶ conditions for the system at rest (t = 0 s) are given by:

$$y_{1}(0) = 0$$

$$\dot{y}_{1}(0) = 0$$

$$y_{2}(0) = 0$$

$$\dot{y}_{2}(0) = 0$$

(28)

For the construction of the NARX model, the NARX basis function is chosen similar to the first example. The NARX basis function for this problem is given by:

$$\psi_i[z(t)] = x^{l_i} \left(t - n_{x_i} \Delta t \right) y_1^{m_i} \left(t - n_{y_i} \Delta t \right)$$
(29)

In Equation 29, $l \in \{0, 1\}$ and $m \in \{0, 1, 2, 3\}$ with $l_i + m_i \leq 3$ are chosen due to cubic non-529 linearity of the system. $n_x \in \{0, 1, ..., 4\}, n_y \in \{1, ..., 4\}$ are chosen because the system 530 is having 2-DOF. The full NARX model is constructed with this NARX basis function 531 which has M = 58 terms. Initially, after investigating the response versus restoring force, 532 a threshold criterion of responses has been decided as $\max(|y_1(t)|) > 1.2 \text{ m}$ which reduces 533 the number of samples to $N_1 = 10$. Consequently, only 10 number of full NARX models 534 are constructed by using the basis function as mentioned in Equation 29. The sparsity is 535 introduced in this step by using the LARS algorithm on the 10 full NARX models to get 536 the unique sparse NARX models which further reduces the number of unique sparse NARX 537 models to $N_2 = 5$. Thus, 5 unique sparse models are used to get the coefficients of the sparse 538 NARX models by ordinary least square for N = 50 samples. Finally, the mean error for each 539 of the sparse NARX models is computed using Equation 17 and the finally selected sparse 540 NARX model has mean error of $\bar{\epsilon} = 2.95 \times 10^{-4}$ with 5 terms in the NARX polynomial out 541 of 58 which are $\{y_1(t - \Delta t), y_1(t - 4\Delta t), y_1^3(t - \Delta t), x(t - 4\Delta t), x(t - 4\Delta t), y_1^2(t - 4\Delta t)\}$. 542 Therefore, only 5 number of Kriging models are required to calibrate for converting the sparse 543

⁵⁴⁴ NARX model stochastic which is highly efficient.

The same example has also been solved by reducing the initial number of sample points 545 with N = 20. For this case, initially, 3 samples are selected as the measure of non-linearity 546 and 3 full NARX models are constructed using the basis function as mentioned in Equa-547 tion 29. Further, all the 3 NARX models are found unique sparse NARX model utilizing 548 the LARS. The predicted mean error for the 20 samples using the finally selected sparse 549 NARX model was $\bar{\epsilon} = 1.85 \times 10^{-6}$ with 5 terms in the polynomial. Here, the 5 terms 550 are $\{y_1(t - \Delta t), y_1(t - 4\Delta t), x(t), x(t - 4\Delta t), x(t - 4\Delta t), y_1^2(t - 4\Delta t)\}$. The same num-551 ber of Kriging models are calibrated as the previous case to make the sparse NARX model 552 stochastic. 553

The time dependent mean and standard deviation of the displacement (y_1) and velocity (\dot{y}_1) are predicted for this problem. The velocities are predicted by numerical differentiation using the Newton's central difference scheme. The time dependent statistical characteristics of displacement and velocity are plotted in Figure 14 and Figure 15 respectively. It is evident from both the figures that the sparse KNARX performs very well even with very few sample points.

Similar to the previous examples, the instantaneous predicted displacements by the sparse 560 KNARX are compared with the MCS results at three different time instances. The instan-561 taneous scatter plots and the PDFs are plotted in Figure 16. The error of the predicted 562 responses at instantaneous time instances along with the R^2 values are given in Table 10. 563 The error for a particular time instance $(\epsilon_{y(t)})$ is computed using Equation 15. The results 564 show a high accuracy of the sparse KNARX in predicting the instantaneous response char-565 acteristics. The accuracy and the efficiency are also noticed for the sparse KNARX at 30 s 566 $(N = 50, \epsilon_{y_1(t)} = 2.3 \times 10^{-3})$ as compared to the recently proposed sparse PCE-NARX 567 model $(N = 100, \epsilon_{y_1(t)} = 4.21 \times 10^{-3})$ (Mai et al. 2016). The accuracy of the stochastic 568 response behavior has also been checked by plotting the absolute maximum displacement 569 and the velocity in Figure 17 and Figure 18 respectively. A very accurate result is noticed 570

using sample points N = 50.

The mean state space behavior of the predicted responses are also plotted in Figure 19. 572 It is noticeable that the mean state space behavior is predicted well even with low number of 573 sample points (N = 20) by the sparse KNARX. The global mean error of the predicted time 574 series is measured by using Equation 17. Along with this, the accuracy in predicting the 575 maximum absolute displacement using different sample points are calculated using Equa-576 tion 15 and R^2 value. All these results along with the efficiency measurement metrics of the 577 proposed sparse KNARX are listed in Table 11. Here, the efficiency of the sparse KNARX 578 model has not been emphasized by the number of surrogate model calibration (n_K) , instead 570 it is greatly affected by the initial number of model evaluations (N). All the results show 580 sparse KNARX perform very well in all instances. 581

582 CONCLUSION

A novel method has been proposed in the present paper for uncertainty propagation and quantification of nonlinear stochastic dynamical systems in the time domain. The well known NARX model (a nonlinear system identification technique) has been coupled with Kriging (a high fidelity surrogate model) to propose the method referred as KNARX. Further, the sparsity in the NARX model has been introduced by utilizing the LARS algorithm to formulate the sparse KNARX model.

The proposed sparse KNARX model has been used for uncertainty quantification on three 589 typical nonlinear stochastic dynamical systems: a 1-DOF duffing oscillator, a Bouc-Wen 590 oscillator and a 2-DOF dynamical system. Time dependent mean and standard deviation 591 are predicted for all the examples. Along with this, PDFs are plotted for instantaneous 592 response characteristics at some time instances and for maximum absolute response. All 593 the results have been compared with full scale MCS. The first example is also solved with 594 Kriging, whereas the first two examples are computed by the sparse PCE-NARX model (Mai 595 et al. 2016). The accuracy has been measured by a global mean error of the predicted model 596 whereas the efficiency has been measured by number of initial sample points, number of 597

surrogate model evaluations and CPU time. The results for the first example have shown 598 that sparse KNARX outperforms Kriging in all cases even with a very limited number of 599 initial samples. Consequently, Kriging has not been utilized for the last two examples. On 600 the other hand, the sparse PCE-NARX model predicted acceptable results by using a higher 601 number of sample points than the sparse KNARX for the first two examples. Along with 602 this, the efficiency of the sparse KNARX model is higher as compared to the sparse PCE-603 NARX model considering the CPU time. All the results predicted by the sparse KNARX are 604 in excellent agreement with the full scale MCS results in all instances. The introduction of 605 sparsity has reduced substantially the number of Kriging model evaluations which ultimately 606 enhanced the efficiency of the sparse KNARX model. All the examples have also been solved 607 by reducing number of model evaluations to check the accuracy of the fitted model with less 608 sample points. All the results have been predicted very close to the MCS results even with 609 very few model evaluations for all the examples. This study suggests that reducing the 610 number of model evaluation does not affect the accuracy too much due to the fact that the 611 major non-linearity of the system has been captured by the sparse NARX model. 612

In conclusion, the proposed sparse KNARX outperforms the state-of-the-art methods (Mai and Sudret 2017; Mai et al. 2016) in predicting the time dependent stochastic response characteristics for nonlinear dynamical systems. The accuracy and the efficiency of the proposed method has also been illustrated through several examples. The proposed sparse KNARX model is limited to use for the nonlinear dynamical systems having parametric uncertainties only. Therefore, this model is not useful for the dynamical systems with white noise excitation for the prediction of time dependent statistical responses.

620 DATA AVAILABILITY

⁶²¹ Some or all data, models, or code generated or used during the study are available from ⁶²² the corresponding author by request.

• NARX model

625 **REFERENCES**

- Bayarri, M. J., Berger, J. O., Cafeo, J., Garcia-Donato, G., Liu, F., Palomo, J.,
 Parthasarathy, R. J., Paulo, R., Sacks, J., and Walsh, D. (2007). "Computer model validation with functional output." *The Annals of Statistics*, 35(5), 1874–1906.
- Bhattacharyya, B. (2018). "A Critical Appraisal of Design of Experiments for Uncertainty
 Quantification." Archives of Computational Methods in Engineering, 25(3), 727–751.
- Billings, S. and Wei, H.-L. (2005). "A New Class of Wavelet Networks for Nonlinear System
 Identification." *IEEE Transactions on Neural Networks*, 16(4), 862–874.
- Billings, S. A. (2013). Nonlinear System Identification: NARMAX Methods in the Time,
 Frequency, and Spatio-Temporal Domains. Wiley, first edition.
- Billings, S. A., Chen, S., and Korenberg, M. J. (1989). "Identification of MIMO non-linear
 systems using a forward-regression orthogonal estimator." *International Journal of Con- trol*, 49(6), 2157–2189.
- Blatman, G. and Sudret, B. (2011). "Adaptive sparse polynomial chaos expansion based on
 least angle regression." *Journal of Computational Physics*, 230(6), 2345–2367.
- Bouc, R. (1967). "Forced vibration of mechanical systems with hysteresis." Proceedings of
 the Fourth Conference on Nonlinear Oscillation, Prague, Czechoslovakia, 315.
- ⁶⁴² Cantelmo, C. and Piroddi, L. (2010). "Adaptive model selection for polynomial NARX
 ⁶⁴³ models." *IET Control Theory & Applications*, 4(12), 2693–2706.
- ⁶⁴⁴ Chakraborty, S. and Chowdhury, R. (2015). "Polynomial Correlated Function Expansion for
- Nonlinear Stochastic Dynamic Analysis." Journal of Engineering Mechanics, 141(3), 1–11.
- ⁶⁴⁶ Chakraborty, S. and Chowdhury, R. (2017). "An efficient algorithm for building locally
- refined hpadaptive H-PCFE: Application to uncertainty quantification." *Journal of Computational Physics*, 351, 59–79.
- ⁶⁴⁹ Chatterjee, T. and Chowdhury, R. (2017). "An efficient sparse Bayesian learning framework
- ⁶⁵⁰ for stochastic response analysis." *Structural Safety*, 68, 1–14.

- ⁶⁵¹ Chatterjee, T. and Chowdhury, R. (2018). "Refined sparse Bayesian learning configuration
 ⁶⁵² for stochastic response analysis." *Probabilistic Engineering Mechanics*, 52, 15–27.
- ⁶⁵³ Chen, S. and Billings, S. A. (1989). "Modelling and analysis of non-linear time series."
 ⁶⁵⁴ International Journal of Control, 50(6), 2151–2171.
- ⁶⁵⁵ Chen, S., Billings, S. A., and Grant, P. M. (1990). "Non-linear system identification using
 ⁶⁵⁶ neural networks." *International Journal of Control*, 51(6), 1191–1214.
- ⁶⁵⁷ Cheng, Y., Wang, L., Yu, M., and Hu, J. (2011). "An efficient identification scheme for a
 ⁶⁵⁸ nonlinear polynomial NARX model." Artificial Life and Robotics, 16(1), 70–73.
- Efron, B., Hastie, T., Johnstone, I., and Tibshirani, R. (2004). "Least angle regression." The
 Annals of Statistics, 32(2), 407–499.
- Gerritsma, M., Steen, J.-B. V. D., Vos, P., and Karniadakis, G. (2010). "Time-dependent
- generalized polynomial chaos." Journal of Computational Physics, 229(22), 8333–8363.
- Grigoriu, M. (1996). "Response of dynamic systems to poisson white noise." Journal of
 Sound and Vibration, 195(3), 375–389.
- Huang, X., Chen, J., and Zhu, H. (2016). "Assessing small failure probabilities by AKSS:
 An active learning method combining Kriging and Subset Simulation." *Structural Safety*,
 59, 86–95.
- Jacquelin, E., Adhikari, S., Sinou, J.-J., and Friswell, M. (2015). "Polynomial chaos expansion in structural dynamics: Accelerating the convergence of the first two statistical
 moment sequences." *Journal of Sound and Vibration*, 356, 144–154.
- ⁶⁷¹ Jacquelin, E., Dessombz, O., Sinou, J. J., Adhikari, S., and Friswell, M. I. (2017). "Polyno-
- ⁶⁷² mial chaos-based extended Padé expansion in structural dynamics." International Journal
- for Numerical Methods in Engineering, 111(12), 1170–1191.
- Kaymaz, I. (2005). "Application of kriging method to structural reliability problems." Struc-*tural Safety*, 27(2), 133–151.
- ⁶⁷⁶ Kersaudy, P., Sudret, B., Varsier, N., Picon, O., and Wiart, J. (2015). "A new surrogate
 ⁶⁷⁷ modeling technique combining Kriging and polynomial chaos expansions Application to

- uncertainty analysis in computational dosimetry." Journal of Computational Physics, 286,
 103–117.
- Krige, D. (1951). "A Statistical Approach to Some Basic Mine Valuation Problems on
 the Witwatersrand." Journal of the Chemical, Metallurgical and Mining Society of South
 Africa, 52(6), 119 139.
- ⁶⁸³ Kundu, A. and Adhikari, S. (2014). "Transient Response of Structural Dynamic Systems
 ⁶⁸⁴ with Parametric Uncertainty." *Journal of Engineering Mechanics*, 140(2), 315–331.
- Leontaritis, I. J. and Billings, S. A. (1985). "Input-output parametric models for non-linear
 systems Part II: stochastic non-linear systems." *International Journal of Control*, 41(2),
 329–344.
- Li, K., Peng, J.-X., and Irwin, G. (2005). "A fast nonlinear model identification method."
 IEEE Transactions on Automatic Control, 50(8), 1211–1216.
- Lu, C., Feng, Y.-W., Liem, R. P., and Fei, C.-W. (2018). "Improved Kriging with extremum response surface method for structural dynamic reliability and sensitivity analyses." Aerospace Science and Technology, 76, 164–175.
- Luchtenburg, D. M., Brunton, S. L., and Rowley, C. W. (2014). "Long-time uncertainty propagation using generalized polynomial chaos and flow map composition." *Journal of Computational Physics*, 274, 783–802.
- Lucor, D. and Karniadakis, G. E. (2004). "Adaptive Generalized Polynomial Chaos for
 Nonlinear Random Oscillators." SIAM Journal on Scientific Computing, 26(2), 720–735.
- Lucor, D., Su, C. H., and Karniadakis, G. E. (2004). "Generalized polynomial chaos and
 random oscillators." *International Journal for Numerical Methods in Engineering*, 60(3),
 571–596.
- Mai, C. V. (2016). "Polynomial chaos expansions for uncertain dynamical systems Applications in earthquake engineering." Ph.D. thesis, Chair of Risk, Safety & Uncertainty
 Quantification, ETH Zurich, Switzerland.
- ⁷⁰⁴ Mai, C. V., Spiridonakos, M. D., Chatzi, E. N., and Sudret, B. (2016). "Surrogate modeling

- for stochastic dynamical systems by combining nonlinear autoregressive with exogenous 705 input models and polynomial chaos expansions." International Journal for Uncertainty 706 Quantification, 6(4), 313-339. 707
- Mai, C. V. and Sudret, B. (2017). "Surrogate models for oscillatory systems using sparse 708 polynomial chaos expansions and stochastic time warping." SIAM/ASA Journal on Un-709 certainty Quantification, 5(1), 540-571. 710
- Maitre, O. P. L., Mathelin, L., Knio, O., and Hussaini, M. (2010). "Asynchronous Time 711 Integration for Polynomial Chaos Expansion of Uncertain Periodic Dynamics." Discrete 712 Continuum Dynamic Systems - Series A, 28(1), 199–226. 713
- Marelli, S. and Sudret, B. (2018). "UQLab user manual Polynomial chaos expansions." 714
- Report no., Chair of Risk, Safety & Uncertainty Quantification, ETH Zurich. Report 715 UQLab-V1.1-104. 716
- Matheron, G. (1963). "Principles of geostatistics." *Economic Geology*, 58(8), 1246–1266. 717
- Mukhopadhyay, T., Chakraborty, S., Dey, S., Adhikari, S., and Chowdhury, R. (2017). "A 718
- Critical Assessment of Kriging Model Variants for High-Fidelity Uncertainty Quantifica-719
- tion in Dynamics of composite Shells." Archives of Computational Methods in Engineering, 720 24(3), 495-518.721
- Muscolino, G., Ricciardi, G., and Cacciola, P. (2003). "Monte Carlo simulation in the stochas-722 tic analysis of non-linear systems under external stationary Poisson white noise input." 723 International Journal of Non-Linear Mechanics, 38(8), 1269–1283.

724

- Ozen, H. C. and Bal, G. (2017). "A dynamical polynomial chaos approach for long-time 725 evolution of SPDEs." Journal of Computational Physics, 343, 300–323. 726
- Sacks, J., Welch, W. J., Mitchell, T. J., and Wynn, H. P. (1989). "Design and Analysis of 727 Computer Experiments." Statistical Science, 4(4), 409–423. 728
- Santner, T., Williams, B., and Notz, W. (2003). The design and analysis of computer exper-729 *iments*. Springer, 1 edition. 730
- Sheppard, C. (1969). "Computer simulation of stochastic processes through model-sampling 731

- ⁷³² (Monte Carlo) techniques." *FEBS Letters*, 2, S14–S21.
- Simpson, T. W., Mauery, T. M., Korte, J. J., and Mistree, F. (2001). "Kriging Models
 for Global Approximation in Simulation-Based Multidisciplinary Design Optimization."
 AIAA Journal, 39(12), 2233–2241.
- ⁷³⁶ Sjöberg, J., Zhang, Q., Ljung, L., Benveniste, A., Delyon, B., Glorennec, P.-Y., Hjalmarsson,
- H., and Juditsky, A. (1995). "Nonlinear black-box modeling in system identification: a
 unified overview." *Automatica*, 31(12), 1691–1724.
- ⁷³⁹ Spiridonakos, M. and Chatzi, E. (2015). "Metamodeling of dynamic nonlinear structural
 ⁷⁴⁰ systems through polynomial chaos NARX models." *Computers & Structures*, 157, 99–113.
- ⁷⁴¹ Sugai, M., Mori, Y., and Ogawa, K. (2015). "Application of Kriging method into practical
- estimations of earthquake ground motion hazards." Journal of Structural and Construction
 Engineering, 80(707), 39–46.
- Tong, C., Sun, Z., Zhao, Q., Wang, Q., and Wang, S. (2015). "A hybrid algorithm for reliability analysis combining Kriging and subset simulation importance sampling." *Journal*of Mechanical Science and Technology, 29(8), 3183–3193.
- Tsungnan Lin, Horne, B., Tino, P., and Giles, C. (1996). "Learning long-term dependencies
 in NARX recurrent neural networks." *IEEE Transactions on Neural Networks*, 7(6), 1329–
 1338.
- ⁷⁵⁰ Wan, X. and Karniadakis, G. E. (2005). "An adaptive multi-element generalized polynomial
 ⁷⁵¹ chaos method for stochastic differential equations." *Journal of Computational Physics*,
 ⁷⁵² 209(2), 617–642.
- ⁷⁵³ Wei, H. and Billings, S. (2009). "Improved parameter estimates for non-linear dynamical
 ⁷⁵⁴ models using a bootstrap method." *International Journal of Control*, 82(11), 1991–2001.
- Wen, Y.-K. (1976). "Method for Random Vibration of Hysteretic Systems." Journal of the
 Engineering Mechanics Division, 102(2), 249–263.
- ⁷⁵⁷ Wiener, N. (1938). "The homogeneous chaos." American Journal of Mathematics, 60(4),
 ⁷⁵⁸ 897–936.

- Worden, K., Becker, W. E., Rogers, T. J., and Cross, E. J. (2018). "On the confidence bounds
 of Gaussian process NARX models and their higher-order frequency response functions." *Mechanical Systems and Signal Processing*, 104, 188–223.
- ⁷⁶² Xie, H., Tang, H., and Liao, Y.-H. (2009). "Time series prediction based on NARX neural
- networks: An advanced approach." *Eighth International Conference on Machine Learning*
- and Cybernetics, Baoding, IEEE, 1275–1279 (jul).
- ⁷⁶⁵ Xiu, D. and Karniadakis, G. E. (2002). "The Wiener-Askey polynomial chaos for stochastic
- differential equation." SIAM Journal on Scientific Computing Scientific Computing, 24(2),
 619–644.
- ⁷⁶⁸ Zhang, L. and Li, K. (2015). "Forward and backward least angle regression for nonlinear
- ⁷⁶⁹ system identification." *Automatica*, 53, 94–102.

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TABLE 1: Algorithm for the sparse KNARX model

1. Declare the d number of uncertain variables with the type of distribution.

2. Generate N number of sample points for the uncertain variables.

3. Draw the restoring force versus response curve to decide the threshold value for capturing nonlinear response series.

4. Get the response of the dynamical system up to time T for each of the N samples.

5. Select the samples and the response series having high order non-linearity using some $(N \in N)$

threshold (according to step 3) on the response series. This step selects N_1 samples $(N_1 < N)$. 6. Decide the maximum time lags n_{x_m} and n_{y_m} for the excitation and response quantity, respectively. Decide the type of NARX polynomial basis function along with the maximum degrees also.

7. For each of the N_1 samples, build the NARX model (see Equation 10 and 11) which has M number of terms.

8. Select the most important terms for each of the N_1 NARX models using LARS (Efron et al. 2004).

9. Select the N_2 different sparse NARX models (see Remark 2) having similar terms in the NARX polynomial basis ($N_2 \leq N_1$).

10. Perform ordinary least square on N samples for the N_2 sparse NARX models to get the NARX coefficients of all the response series.

11. Reconstruct the N response series using the coefficients computed in step 10 by all the N_2 sparse NARX models.

12. Predict the mean error $\bar{\epsilon}$ for all the N_2 number of sparse NARX models using Equation 17. 13. Select the most appropriate sparse NARX model having $\bar{\epsilon}$ lower than some threshold value $(1 \times 10^{-3} \text{ in the present paper})$ and less number of terms (M_1) in the polynomial.

14. Calibrate $M_1 < M$ number of Kriging models using the NARX coefficients as the response parameter and the sample points generated in step 2 as the uncertain input quantities. 15. Generate a large number of new untried samples for the prediction.

16. Predict the NARX coefficients for the untried samples using Kriging models generated in step 14.

17. Predict the response series, in a auto-regressive way (see Equation 21), at the untried samples generated in step 15 using the coefficients of step 16 and the M_1 number of NARX polynomial bases selected in step 13.

Variable	Distribution type	Mean	Standard deviation	Unit
ω	Uniform	2π	$\frac{\pi}{\sqrt{3}}$	$ m rads^{-1}$
ζ	Uniform	0.03	$\frac{0.015}{\sqrt{3}}$	—
ε	Uniform	100	$\frac{10}{\sqrt{3}}$	—
A	Normal	0.6	0.06	Ν
ω_x	Normal	1	0.1	$\rm rads^{-1}$

TABLE 2: Uncertain parameters for the duffing oscillator

Model 1 ($M_1 = 9$)	Model 2 ($M_1 = 8$)
$x\left(t ight)$	$x\left(t ight)$
$x\left(t-2\Delta t ight)$	$x\left(t-2\Delta t\right)$
$y\left(t-\Delta t ight)$	$y\left(t-\Delta t ight)$
$y\left(t-2\Delta t ight)$	$y\left(t-2\Delta t ight)$
$y^2 \left(t - \Delta t\right)$	$y^2 \left(t - \Delta t\right)$
$y^{3}\left(t-\Delta t ight)$	$y^3 \left(t - \Delta t ight)$
$y^3 \left(t - 2\Delta t\right)$	$y^3 \left(t - 2\Delta t\right)$
$x\left(t-2\Delta t\right)y^{2}\left(t-2\Delta t\right)$	$x\left(t-2\Delta t\right)y^{2}\left(t-2\Delta t\right)$
$x\left(t-2\Delta t\right)y\left(t-2\Delta t\right)$	

TABLE 3: The polynomials selected by the LARS algorithm for the duffing oscillator

TABLE 4: Accuracy of the surrogate models in predicting instantaneous response characteristics for the duffing oscillator

Method	N	Time instance	$\epsilon_{y(t)}$	R^2
Kriging	50		337.8×10^{-3}	0.6622
Sparse PCE-NARX	35	<i>t</i> — 10 c	9.6×10^{-3}	0.9904
Sparse KNARX	21	l = 108	$8.8 imes 10^{-3}$	0.9912
Sparse KNARX	25		4.6×10^{-3}	0.9954
Kriging	50		926.9×10^{-3}	0.0731
Sparse PCE-NARX	35	$t = 20 \mathrm{g}$	4.4×10^{-3}	0.9956
Sparse KNARX	21	$\iota = 20.8$	5.4×10^{-3}	0.9946
Sparse KNARX	25		3.1×10^{-3}	0.9969
Kriging	50		1701.1×10^{-3}	_
Sparse PCE-NARX	35	$t = 30 \mathrm{c}$	2.3×10^{-3}	0.9977
Sparse KNARX	21	$\iota = 50.8$	3.0×10^{-3}	0.9970
Sparse KNARX	25		2.0×10^{-3}	0.9980

TABLE 5: Comparison of accuracy and efficiency of the surrogate models for the duffing oscillator

		Accuracy			fficiency
Method	$\overline{\epsilon}$	$\epsilon_{\max(y(t))}$	$R^2_{\max(y(t))}$	n_K	CPU time
$\overline{\text{Kriging } (N = 50)}$	1.4971	2100.7×10^{-3}	_	3001	$530.95\mathrm{s}$
Sparse PCE-NARX $(N = 35)$	1.1×10^{-3}	2.9×10^{-3}	0.9971	9	$30.55\mathrm{s}$
Sparse KNARX $(N = 21)$	1.2×10^{-3}	1.4×10^{-3}	0.9986	9	$26.13\mathrm{s}$
Sparse KNARX $(N = 25)$	$5.89 imes 10^{-4}$	1.0×10^{-3}	0.9990	8	$24.63\mathrm{s}$
MCS	_	_	_	-	$705.43\mathrm{s}$

Variable	Distribution type	Mean	Standard deviation	Unit
ζ	Uniform	0.02	0.002	_
ω	Uniform	2π	0.2π	$\rm rads^{-1}$
α	Uniform	50	5	—
A	Uniform	1	0.1	Ν
ω_x	Uniform	π	0.1π	$\rm rads^{-1}$

TABLE 6: Uncertain parameters for the Bouc-Wen oscillator

TABLE 7: Accuracy of the surrogate models in predicting the instantaneous response characteristics for the Bouc-Wen oscillator

			Displacement		Velocit	Jy
Method	N	Time instance	ϵ	R^2	ϵ	R^2
Sparse PCE-NARX	50		660.0×10^{-3}	0.3370	44.0×10^{-3}	0.9557
Sparse KNARX	10	$t = 10 \mathrm{s}$	$6.8 imes 10^{-3}$	0.9932	$0.9 imes 10^{-3}$	0.9991
Sparse KNARX	40		3.8×10^{-3}	0.9962	0.5×10^{-3}	0.9995
Sparse PCE-NARX	50		880.0×10^{-3}	0.1224	48.0×10^{-3}	0.9519
Sparse KNARX	10	$t = 20 \mathrm{s}$	8.6×10^{-3}	0.9914	1.0×10^{-3}	0.9990
Sparse KNARX	40		5.6×10^{-3}	0.9944	0.5×10^{-3}	0.9995
Sparse PCE-NARX	50		1140.0×10^{-3}	_	50.0×10^{-3}	0.9503
Sparse KNARX	10	$t = 30 \mathrm{s}$	10.8×10^{-3}	0.9892	1.1×10^{-3}	0.9989
Sparse KNARX	40		7.8×10^{-3}	0.9922	0.5×10^{-3}	0.9995

TABLE 8: Accuracy and efficiency of the surrogate models in computing $\dot{y}(t)$ for the Bouc-Wen oscillator

		Accuracy		F	Efficiency
Method	$\overline{\epsilon}$	$\epsilon_{\max(y(t))}$	$R^2_{\max(y(t))}$	n_K	CPU time
Sparse PCE-NARX $(N = 50)$	9.3×10^{-2}	2.6×10^{-1}	0.7414	8	$27.40\mathrm{s}$
Sparse KNARX $(N = 10)$	1.9×10^{-3}	4.6×10^{-3}	0.9954	8	$19.12\mathrm{s}$
Sparse KNARX $(N = 40)$	$8.0 imes 10^{-4}$	$1.9 imes 10^{-3}$	0.9981	8	$21.72\mathrm{s}$
MCS	_	_	_	_	$1223.17\mathrm{s}$

TABLE 9: Uncertain parameters for the 2-DOF dynamical system

Variable	Distribution type	Mean	Standard deviation	Unit
k_s	Normal	2000	200	N/m^3
k_u	Normal	2000	200	${ m N}{ m m}^{-1}$
m_s	Normal	20	2	kg
m_u	Normal	40	4	kg
c	Normal	600	60	${ m Nsm^{-1}}$
A	Uniform	0.1	$\frac{0.01}{\sqrt{3}}$	m
ω_x	Uniform	2π	$\frac{0.2\pi}{\sqrt{3}}$	$\rm rads^{-1}$

TABLE 10: Accuracy of sparse KNARX in predicting instantaneous response characteristics for the 2-DOF dynamical system

N	Time instance	$\epsilon_{y_1(t)}$	R^2
20	t _ 10 a	11.6×10^{-3}	0.9884
50	$t = 10 \mathrm{s}$	1.1×10^{-3}	0.9989
20	t — 20 g	16.2×10^{-3}	0.9838
50	$\iota = 20.8$	1.9×10^{-3}	0.9981
20	t — 20 g	16.2×10^{-3}	0.9838
50	$\iota = 30 \mathrm{s}$	2.3×10^{-3}	0.9977

TABLE 11: Accuracy and efficiency of sparse KNARX in computing $y_1(t)$ for the 2-DOF dynamical system

		Accuracy		F	Officiency
Method	$\bar{\epsilon}$	$\epsilon_{\max(y_1(t))}$	$R^2_{\max(y_1(t))}$	n_K	CPU time
Sparse KNARX $(N = 20)$	8.9×10^{-3}	15.4×10^{-3}	0.9846	5	$7.76\mathrm{s}$
Sparse KNARX $(N = 50)$	1.2×10^{-3}	$1.7 imes 10^{-3}$	0.9983	5	$22.62\mathrm{s}$
MCS	_	_	_	—	$466.34\mathrm{s}$

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FIG. 1: Displacement versus restoring force plot for the duffing oscillator



FIG. 2: Displacement versus restoring force plots of two different realizations for the duffing oscillator; (a) 13-th sample, (b) 25-th sample



FIG. 3: Statistical response characteristics of the duffing oscillator; (a) Mean, (b) Standard deviation



FIG. 4: Comparison of instantaneous response characteristics for the duffing oscillator at different time instances; (a) Scatter plot at t = 10 s, (b) PDF at t = 10 s, (c) Scatter plot at t = 20 s, (d) PDF at t = 20 s, (e) Scatter plot at t = 30 s, (f) PDF at t = 30 s



FIG. 5: Comparison of predicted max (|y(t)|) for the duffing oscillator; (a) Scatter plot, (b) PDF



FIG. 6: Statistical response characteristics for the displacement of the Bouc-Wen oscillator; (a) Mean, (b) Standard deviation



FIG. 7: Statistical response characteristics for the velocity of the Bouc-Wen oscillator; (a) Mean, (b) Standard deviation



FIG. 8: Prediction of instantaneous displacement characteristics for the Bouc-Wen oscillator at different time instances; (a) Scatter plot at t = 10 s, (b) PDF at t = 10 s, (c) Scatter plot at t = 20 s, (d) PDF at t = 20 s, (e) Scatter plot at t = 30 s, (f) PDF at t = 30 s



FIG. 9: Prediction of instantaneous velocity characteristics for the Bouc-Wen oscillator at different time instances; (a) Scatter plot at t = 10 s, (b) PDF at t = 10 s, (c) Scatter plot at t = 20 s, (d) PDF at t = 20 s, (e) Scatter plot at t = 30 s, (f) PDF at t = 30 s



FIG. 10: Comparison of predicted max (|y(t)|) for the Bouc-Wen oscillator; (a) Scatter plot, (b) PDF



FIG. 11: Comparison of predicted max $(|\dot{y}\left(t)|)$ for Bouc-Wen oscillator; (a) Scatter plot, (b) PDF



FIG. 12: Mean trajectory of y(t) and $\dot{y}(t)$ for the Bouc-Wen oscillator; (a) MCS, (b) Sparse PCE-NARX (N = 50), (c) Sparse KNARX (N = 10), (d) Sparse KNARX (N = 40)



FIG. 13: A 2-DOF dynamical system



FIG. 14: Statistical response characteristics for displacement $(y_1(t))$ of the 2-DOF dynamical system; (a) Mean, (b) Standard deviation



FIG. 15: Statistical response characteristics for velocity $(\dot{y}_1(t))$ of the 2-DOF dynamical system; (a) Mean, (b) Standard deviation



FIG. 16: Prediction of instantaneous displacement characteristics for 2-DOF dynamical system at different time instances; (a) Scatter plot at t = 10 s, (b) PDF at t = 10 s, (c) Scatter plot at t = 20 s, (d) PDF at t = 20 s, (e) Scatter plot at t = 30 s, (f) PDF at t = 30 s



FIG. 17: Comparison of predicted max $(|y_1(t)|)$ for the 2-DOF dynamical system; (a) Scatter plot, (b) PDF



FIG. 18: Comparison of predicted max $(|\dot{y}_1(t)|)$ for the 2-DOF dynamical system; (a) Scatter plot, (b) PDF



FIG. 19: Mean trajectory of $y_1(t)$ and $\dot{y}_1(t)$ for the 2-DOF dynamical system; (a) MCS, (b) Sparse KNARX (N = 20), (c) Sparse KNARX (N = 50)