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► To cite this version:

Linfeng Ding, Karan Doss, Yongjian Yang, Kuo-Hao Lee, Michal Bockowski, et al.. Volume relaxation in a borosilicate glass hot compressed by three different methods. Journal of the American Ceramic Society, 2020, 10.1111/JACE.17482 . hal-02951482

HAL Id: hal-02951482

<https://hal.science/hal-02951482>

Submitted on 29 Sep 2020

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Article type : Article

Volume relaxation in a borosilicate glass hot compressed by three different methods

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Abstract

This article has been accepted for publication and undergone full peer review but has not been through the copyediting, typesetting, pagination and proofreading process, which may lead to differences between this version and the [Version of Record](#). Please cite this article as [doi: 10.1111/JACE.17482](https://doi.org/10.1111/JACE.17482)

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The temperature dependence of glass relaxation has been intensively studied; however, the effect of an imposed pressure history on relaxation behavior is poorly understood. In this study, we subjected SCHOTT N-BK7[®] borosilicate glasses to isostatic compression in a Paterson press (PP) and a gas pressure chamber (GPC). The pressure ranged from 0.1 GPa to 2 GPa for various dwell temperatures and times near the glass transition region. Comparison with our recent results on the same glass using the piston-cylinder apparatus (PC, 0.5-1.5 GPa) reveals that the density of a glass, which has been quenched from the equilibrium state under high pressure at 2 K/min (pressure quench), increases approximately linearly with increasing pressure up to 2 GPa. Considering the volume recovery results at ambient pressure, we assert that the preceding high-pressure treatment in PC (uniaxial loading) generates a similar isostatic pressure effect on N-BK7 glass as those of PP and GPC treatments. Finally, we verify the previously proposed two-internal-parameter relaxation model on the volume recovery data using the three different compression methods. With a new set of parameters in the model, we can account for the pressure and temperature dependence of volume relaxation even for the samples quenched from nonequilibrium states at high pressure.

Keywords: borosilicate glass; densification; volume relaxation; fictive pressure; fictive temperature

1. Introduction

Supercooled liquids and glasses show intriguing universal behavior, such as glass transition and relaxation, whose origins remain poorly understood in many systems.^{1, 2} The temperature and thermal history dependence of glass relaxation³ has been intensively studied; however, the effect of an imposed pressure history on relaxation behavior is not well studied⁴. Moreover, the relaxation of silicate melts/glasses under high pressure is a key parameter to understand the geological formation of the earth (pressure increases approximately 0.3 GPa for every 10 km depth), since magmas and lavas are silicate-rich melts resulting from partial melting of the Earth's mantle.^{5, 6, 7}

Permanent densification of glass has been observed at elevated pressures via hot^{8, 9, 10, 11, 12, 13, 14} and cold¹⁵ compression. The compression treatment can be performed using different high pressure apparatuses, e.g., gas pressure vessels (up to ~2 GPa)^{10, 11, 16}, piston-cylinder apparatus (up to ~4 GPa)¹⁷, multi anvil apparatus (above 5 GPa)¹⁸, etc. During hot compression, glass samples are typically heated to the glass transition range under high pressure and then quenched to ambient pressure. This leads to permanent densification of the glass (i.e., the glass remains densified unless it is heated close to the glass transition region at ambient pressure), which also manifests itself in macroscopic properties changes such as an increase in indentation hardness^{19, 20, 21}. However, the understanding of volume relaxation mechanism of a permanently densified glass is still lacking.

In our previous studies, we evaluated the pressure dependence of volume relaxation²² and viscosity²³ of a commercial borosilicate glass (SCHOTT N-BK7[®]) near the glass transition region via hot compression in a piston-cylinder apparatus and *in situ* deformation in the Paterson press¹⁶. We introduced a two-internal-parameter (fictive temperature T_f and fictive pressure P_f) model²² based on Gupta's approach²⁴ and the Tool-Narayanaswamy model^{25, 26}. Our model can explain the experimental volume relaxation data reasonably well. Results from *ex situ* volume relaxation and *in situ* viscosity measurements show a consistent change from those two different pressure sources.²³ However, a true isostatic high pressure environment around the glass sample is still challenging during a hot compression treatment, especially for the piston-cylinder apparatus which subjects the glass to a uniaxial loading condition.

SCHOTT N-BK7[®] is available in large formats with high homogeneity and has already been used in several studies^{27, 28, 29, 30} as a reference material. Therefore, in this work, we perform isostatic

hot compression experiments on SCHOTT N-BK7[®] glass in the Paterson press (0.1-0.3 GPa) and a gas pressure chamber (1-2 GPa) and then compare the results to our recent data²² from the piston-cylinder apparatus (0.5-1.5 GPa) in a uniaxial loading condition. We aim here to quantify the volume relaxation behavior of this glass.

2. Experimental section

The SCHOTT N-BK7[®] (chemical composition³¹: 74.5 mol% SiO₂, 10.2 mol% B₂O₃, 10.2 mol% Na₂O, 5.1 mol% K₂O and small amounts of CaO and BaO) glass samples were machined to cylinders and mirror-polished prior to the high-pressure treatments. To minimize the density measurement uncertainty, all the samples with the maximum allowable volume were used, which was 10.00±0.05 mm (diameter) × 17.00±0.10 mm (height) and 7.00±0.05 mm × 8.00±0.05 mm for the Paterson press experiments (PP, University of Montpellier) and the gas pressure chamber experiments (GPC, Polish Academy of Sciences, Warsaw), respectively. The samples for the piston cylinder apparatus (PC, University of Mainz) experiments²² were machined to 7.40±0.02 mm × 6.00±0.02 mm. The density of N-BK7 glass at room temperature and ambient pressure is around 2.508 ± 0.001 g/cm³. The glass transition temperature $T_g = 561$ °C is defined as the temperature at which the logarithmic viscosity is 12 log₁₀(Pa·s).²³

The full description of PP is given in Ref. 13. It is mostly used as a *in situ* deformation or static compression gas-medium apparatus with a routine^{25, 26} confining pressure of 0.3 GPa. Nevertheless, we briefly recall the main experimental setup details below. A single glass sample was encapsulated with zirconia and alumina cylinders and alumina spacers inside a thin copper jacket.²³ The hot compression experiments in PP were conducted with argon as the pressure medium. Temperature was fixed at 700 °C using an internal and recalibrated furnace, and the confining isostatic pressure was maintained constant at 0.1, 0.2 or 0.3 GPa for 2 h. The description of GPC can be found in several recent studies^{8, 11, 19}. Two glass samples were placed inside a graphite furnace in a vertical stack, which was separated by a 2 mm alumina disk, and subjected to an isostatic high-pressure treatment using nitrogen as a pressure. The hot compression experiments in GPC were conducted between 560 °C and 700 °C under a pressure of 1 GPa or 2 GPa for 0.5 or 2 h to evaluate the influence from both pressures and temperatures. The PC is self-assembled with an improved design³² based on the

principle of Boyd and England¹⁷ with uniaxial pressure up to 3 GPa. All the PC experiments from our recent study²² were conducted in a customized pressure-cell with NaCl salt as the pressure transmitting medium at 700 °C under 0.5-1.5 GPa for 24 h to ensure an equilibrium state for N-BK7 glass. All the hot compression experiments were followed by a controlled cooling step to room temperature at a constant rate of 2 K/min (pressure quench). Finally, all the systems were decompressed at a rate of 10-30 MPa/min to ambient pressure.

The density of samples was measured by the Archimedes principle after the hot compression treatments. Each density measurement was repeated five times to obtain a standard deviation as the measurement uncertainty. Volume recovery measurements were conducted in the DIL 806 optical dilatometer (TA Instruments) for the samples from PP, which is the same method as the results from PC, and the TMA Q400 (TA Instruments) for the samples from GPC. The temperature of these two dilatometers had been calibrated with an uncertainty of less than 1 °C. The dilatometer was heated from room temperature to 500 °C at a rate of +20 K/min, then at +2 K/min to 525 °C and held for at least 24 h until the sample diameter does not change anymore.

3. Results

3.1 Volume densification

The density of N-BK7 glass compressed from PC at 0.5 GPa to 1.5 GPa and 700 °C ($1.25T_g$) was found to increase approximately linearly with pressure in our preceding study²² as illustrated in Figure 1(a) (squares). The measured densities of N-BK7 glass after hot compression from PP and GPC are compared with the results from PC in Fig. 1(a). The compile densities of N-BK7 glass, which is pressure quenched from equilibrium states (700 °C for a holding time longer than 2 h) in three different machines, show a linear function of the pressure from 0.1 GPa to 2 GPa,

$$\rho = 0.0662P + 2.5026, \quad (1)$$

where ρ is the density of samples after hot compression in g/cm³ and P is the applied pressure in GPa. Despite the difference in pressure medium for the hot compression treatments, viz., argon gas in PP (0.1-0.3 GPa), NaCl salt in PC (0.5-1.5 GPa), and nitrogen in GPC (1-2 GPa), the density of N-BK7 glass increases with increasing pressure at around the same rate of 2.6%/GPa. However, all the samples hot compressed in GPC at various temperatures near the glass transition region for 0.5 h are

slightly off the linear relation, indicating that those samples were pressure quenched from nonequilibrium states. Figure 1(b) shows a non-linear increasing trend of the glass density with the dwell temperature at both 1 GPa and 2 GPa for GPC, which is different from the results at ambient pressure, with the latter showing no increase in density with temperature.

3.2 Volume relaxation

The length change of hot compressed samples was measured by dilatometer at 525 °C ($0.94T_g$) and converted to a volume change following

$$V_{spec} = \frac{(1 + \Delta L/L_0)^3}{\rho_0}, \quad (2)$$

where V_{spec} is the specific volume, $\Delta L/L_0$ is the length change, and ρ_0 is the density of the hot compressed glass. The volume recovery of samples hot compressed up to 2 GPa and pressure quenched from equilibrium states in three different methods are reported in Figure 2(a). Moreover, dwell temperature also influences the volume recovery of glass for results from GPC as shown in Figure 3(a) and Figure 4(a).

In our previous study, a two-internal-parameter relaxation model²² was developed based on Gupta's approach²⁴ and the Tool-Narayanaswamy model^{25, 26}, in which the volume relaxation depends on both fictive temperature (T_f)²⁵ and fictive pressure (P_f)²⁴ to account for both thermal and pressure history. This model assumes a true isostatic pressure during the hot compression in PC²² and the configurational expansion coefficient²⁴ is the key parameter to govern the change in P_f . The specific volume depends on T , T_f , P , and P_f according to

$$V = V_{ref} \exp [J_{froz}(P_{ref} - P) + \Delta J(P_{ref} - P_f) + 3\alpha_{froz}(T - T_{ref}) + 3\Delta\alpha(T_f - T_{ref})], \quad (3)$$

where $T_{ref}=525$ °C, $P_{ref}=0.0001$ GPa, $V_{ref}=0.4065$ cm³/g (fully recovered specific volume), and $\Delta J = J_{liq} - J_{froz}$ is the difference in compressibility between liquid glass and frozen glass with $J=1/K$ (K_{liq} is the bulk modulus of liquid glass which is a free parameter and $K_{froz}=46.5$ GPa). The derivation of T_f and P_f are taken from the rates equation in Gupta's approach²⁴ together with an efficient and stable algorithm from Markovsky and Soules³³. The assumptions $L_{TT} = \frac{T}{\Delta C\tau_c}$, $L_{TP} = L_{PT} = \frac{1}{V\Delta\alpha\tau_\alpha}$, and $L_{PP} = \frac{1}{V\Delta J\tau_J}$ are used for the four kinetic coefficients in Gupta's rates equation²⁴. $\Delta C =$

$C_{liq} - C_{froz}$ is the specific heat capacity of the liquid (equilibrium) state C_{liq} and the frozen (glassy) state C_{froz} , and similarly, $\Delta \alpha = \alpha_{liq} - \alpha_{froz}$ is the difference in thermal expansion coefficient between liquid and frozen glass. This assumption introduces another three free parameters, f_c , f_α , and f_J , which account for the different factors for the characteristic relaxation time (τ_G) change in the shear modulus by specific heat ($\tau_c = f_c \tau_G$), thermal expansion coefficient ($\tau_\alpha = f_\alpha \tau_G$), and compressibility ($\tau_J = f_J \tau_G$), respectively. The characteristic relaxation time can be calculated as

$$\tau_G = \tau_{ref} \exp \left\{ \frac{x}{T} \left[\frac{\Delta H}{R} + \frac{\Delta V_a}{R} (P - P_{ref}) \right] + \frac{1-x}{T_f} \left[\frac{\Delta H}{R} + \frac{\Delta V_a}{R} (P_f - P_{ref}) \right] - \frac{\Delta H}{RT_{ref}} \right\}, \quad (4)$$

where ΔH is the activation enthalpy, R is the gas constant ($\Delta H/R = 74000 \text{ K}$), x is a fixed factor in Tool-Narayanaswamy model^{25, 26} ($x=0.7$ for N-BK7 glass), ΔV_a is the activation volume³⁴ and $\tau_{ref}=0.45 \text{ h}$. Thus, the model has five free parameters: K_{liq} , f_c , f_α , f_J and ΔV_a . In the case that no pressure is applied in the experiments, this model reduces to the original Tool-Narayanaswamy model^{25, 26}.

As shown in Figures 2(a), 3(a), and 4(a), the two-internal-parameter relaxation model²² captures both the influence of the pressure history and thermal history on the volume recovery of N-BK7 glass at 525 °C with a single set of parameters (see figure caption in Figure 2(a)). The best-fit parameters were detected by fitting all the data in the three figures simultaneously using a multidimensional unconstrained nonlinear minimization optimization algorithm (i.e., the Nelder-Mead Simplex search algorithm as incorporated in the MATLAB function *fminsearch*³⁵). The initial cooling, the high pressure treatment (if any), the heating-up stage, and finally, the isothermal volume recovery measurement are all considered with the two-internal-parameter relaxation model. To check the evolution of the internal parameters, the corresponding changes of T_f and P_f of samples versus time are given in Figure 2(b). The results indicate that T_f increases with the increasing applied pressure. The crossover phenomenon³⁶ is also detected in the evolution of T_f . The value of P_f is initially equal to the applied pressure during hot compression but gradually decreases to ambient pressure when the volume is fully recovered. Moreover, both T_f and τ_G at the beginning of the relaxation process (values are reported in Table 1) increase approximately linearly with fictive pressure, consistent with our previous investigations.²² The increase of τ_G at higher pressures indicates that samples compressed at higher pressure require longer times to relax towards a new equilibrium in the glass transition region.

Figure 3(a) shows the volume recovery of samples at 525 °C and 1 atm fitted by the two-internal-parameter relaxation model with the same set of fitting parameters as in Figure 2(a). Prior to relaxation, the glass samples were hot compressed in GPC at 1 GPa and various dwell temperatures (560 °C, 580 °C and 600 °C) for 0.5 h. The model captures the volume relaxation of samples quenched from 580 °C and 600 °C for 0.5 h under 1 GPa, while it does not reproduce well the sample quenched from 560 °C for 0.5 h. The corresponding changes in T_f and P_f with time are shown in Figure 3(b) as well as in Table 1 where the strong coupling of temperature and pressure histories in the two-internal-parameter relaxation model can be observed. The T_f of the sample pressure quenched from 600 °C for 0.5 h at the beginning of relaxation at 525 °C and 1 atm is slightly (3.4 °C) lower than the T_f of the sample pressure quenched from equilibrium state under 1 GPa equals to 571.5 °C, which in turn is slightly higher (2.1 °C) than the one pressure quenched from 580 °C. On the other hand, the T_f of the sample pressure quenched from 560 °C for 0.5 h under 1 GPa is 18.1 °C lower than that of the 600 °C sample. More interestingly, the P_f of the sample pressure quenched from 560 °C for 0.5 h under 1 GPa is only 0.4 GPa, which is much lower than the samples quenched from 580 °C and 600 °C around 0.9 GPa. To conclude, samples quenched from 1 GPa in nonequilibrium states have lower T_f and P_f compared with the one quenched from 1 GPa after equilibrium was reached.

Figure 4(a) shows the volume recovery of samples at 525 °C and 1 atm fitted by the two-internal-parameter relaxation model with the same set of fitting parameters as in Figure 2(a). Prior to relaxation, the glass samples were hot compressed in GPC at 2 GPa and various dwell temperatures (580 °C, 600 °C and 700 °C) for 0.5 h. Overall, the model predicts the influence of dwell temperature on volume relaxation of N-BK7 glass, although the fit is not perfect. The corresponding changes of T_f and P_f with time are presented in Figure 4(b) and Table1, where again the coupling of temperature and pressure histories is significant. The cross-over of T_f is significant in Figure 4(b), which is strongly correlated with P_f . The sample quenched from 700 °C for 0.5 h under 2 GPa has slightly lower T_f and P_f at the beginning of relaxation compared to samples quenched from 700 °C for 2 h under 2 GPa. This indicates that the sample has not reached equilibrium during the hot compressing in GPC for 0.5 h. Moreover, the T_f and P_f of samples quenched from 600 °C for 0.5 h under 2 GPa at the beginning of relaxation are 20.0 °C and 0.72 GPa lower, respectively, than those of the sample quenched at 700 °C (0.5 h/2GPa), which in turn are significantly higher than the samples quenched at

580 °C (0.5 h/2GPa). T_f of the sample pressure quenched from 580 °C for 0.5 h under 2 GPa at the beginning of relaxation is approximately 549.4 °C, which is between the values for samples quenched from equilibrium under 0.3 GPa and 0.5 GPa (see Table 1). The P_f of this sample is only 0.32 GPa. The difference in T_f and P_f is even larger for samples quenched from nonequilibrium and equilibrium states at 2 GPa.

4. Discussion

In the previous study²², we restricted the ΔV_a to be equal to the molar volume ($\sim 8.13 \text{ cm}^3/\text{mol}$) of glass during relaxation at 525 °C in the two-internal-parameter relaxation model. However, recent rheological research on N-BK7 glass reported a ΔV_a of $\sim 1.4 \text{ cm}^3/\text{mol}$ for plastic yielding and $\sim 2.0 \text{ cm}^3/\text{mol}$ for viscous flow, which are lower than the molar volume during relaxation in this study. Moreover, results from tribology^{37, 38, 39} (Arrhenius-type activation) indicates that the ΔV_a can be either lower or higher than the molar volume. Indeed, studies on metallic and polymer glasses indicate that ΔV_a can go up to $100 \text{ cm}^3/\text{mol}$ ³⁴. Therefore, in this work, the ΔV_a is set to be a free parameter, which allows the ΔV_a to be either lower or higher than the molar volume depending on the experimental data. The ΔV_a is found to be the dominant factor in the fitting of dwell temperature dependence in Figures 3 and 4. The best-fit ΔV_a value is around $28.6 \text{ cm}^3/\text{mol}$ during the pressure-dependent relaxation process, which is ~ 3.5 times of the molar volume. This relatively large ΔV_a reveals the strong coupling of temperature and pressure histories for samples quenched from the nonequilibrium state under high pressure.

Figure 2(b) displays a significant minimum in T_f followed by a crossover back to higher T_f (nonmonotonic decay) while the corresponding P_f decays monotonically with time. A similar crossover phenomenon has been reported in the relaxation of selenium glass from various temperature histories^{40, 41} where the nonmonotonic decay is observed both experimentally and computationally (Mauro-Loucks enthalpy landscape model⁴²) in density and enthalpy fluctuations while the relaxation of enthalpy and density is monotonic. The crossover of T_f in this work could be related with the initial fast relaxation of the number of remaining internal degrees of freedom (floppy modes) in the system that results in a rapid decrease of P_f until most of the faster-relaxing floppy modes have relaxed

resulting in a minimum for T_f . This is followed by a slower long-range relaxation of the remaining floppy modes.^{42, 43, 44} Moreover, the nonmonotonic decay of T_f is reduced and even disappears upon pressure quenching from nonequilibrium states at 1 and 2 GPa (Figures 3(b) and 4(b)) due to the relative lower P_f than the those of the samples pressure quenched from equilibrium states.

The model indicates that hot compression experiments on N-BK7 glass at T_g to $1.07T_g$ for 0.5 h under 1 GPa and at $1.03T_g$ to $1.25T_g$ for 0.5 h under 2 GPa do not reach the equilibrium states. This can be verified by our recent study⁴⁵ on the atomic structure of hot compressed borosilicate glass. The recent results from ^{11}B solid-state nuclear magnetic resonance (NMR) spectroscopy shows that the fraction of four coordinated boron increases with increasing of isothermal holding (annealing) temperature for the N-BK7 samples hot compressed from the same conditions (except for the 1 GPa samples which is nearly reach the equilibrium state).

We note that the set of best-fit parameters for the two-internal-parameter relaxation model is not unique and some of the best fittings are not perfect (especially in Figure 4(a)). This is due to limitations of the applied multidimensional unconstrained nonlinear minimization optimization algorithm and the measurement uncertainty of the experimental results. We further tested the two-internal-parameter relaxation model by introducing a weighting factor to discriminate silicate from the other compositions following Narayanaswamy's approach²⁶. However, the fitting is not significantly improved due to the limitation of the experimental measurement uncertainty. Nevertheless, the new best-fit K_{liq} value is equal to 18 GPa, which is closer to the rule of thumb estimation of 15.5 GPa (e.g., one-third of the bulk modulus of the solid glass) than the previous²² fitting result. In summary, the two-internal-parameter relaxation model can generally reproduce the pressure dependence of volume relaxation of N-BK7 glass pressure quenched from nonequilibrium state. This model also provides reference experimental parameters for the isostatic hot compression on N-BK7 glass and could be applied to other glass compositions by adjusting the corresponding composition-temperature-pressure parameters.

5. Conclusion

In this study, we found that the density of N-BK7 glass, pressure quenched from the equilibrium state in three different machines, increases approximately linear with increasing pressure up to 2 GPa.

Together with the volume recovery results, we assert that the preceding high pressure treatment in PC (uniaxial loading) generated a similar isostatic pressure effect on N-BK7 glass as in PP and in GPC. Moreover, the previously proposed two-internal-parameter relaxation model incorporates a new set of free parameters can reasonably address the pressure and temperature dependence of relaxation of glass even for the samples pressure quenched from nonequilibrium states. Also, the model indicates that hot compression experiments on N-BK7 glass at 600 °C ($\sim 1.07T_g$) for 0.5 h under 1 GPa and at 700 °C ($\sim 1.25T_g$) for 0.5 h under 2 GPa does not reach the equilibrium states. The model can be used for predicting the volume relaxation of N-BK7 glass under various pressure and temperature histories and also has the potential to apply to other glass compositions.

Acknowledgments

Linfeng Ding is funded by the Deutsche Forschungsgemeinschaft (DFG) through a DFG Fellowship (GZ: DI 2545). Kuo-Hao Lee is funded by SCHOTT AG, Mainz, Germany. Linfeng Ding appreciates the valuable comments and great support from Dr. Clemens Kunisch, Dr. Seong H. Kim and Dr. Boris Kaus. The authors thank the technicians and engineers at the SCHOTT machine shop for the sample preparation. This study was partially funded by the European Union's Horizon 2020 research and innovation program under the Marie Skłodowska-Curie Grant Agreement No. 642029.

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Table captions

Table 1 Changes in T_f , P_f and τ_G at the beginning of volume recovery at 525 °C and 1 atm in the model.

Figure captions

Figure 1 (a) Pressure dependence of density of hot compressed glass samples from three different experimental methods (PP, PC, GPC) (b) Temperature dependence of density of hot compressed samples at 1 atm, 1 GPa and 2 GPa from GPC. The dashed lines represent the exponential decay function fits.

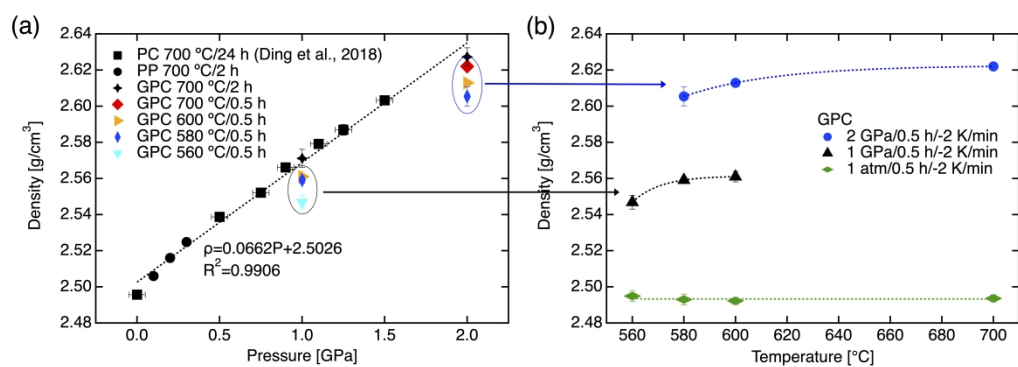
Figure 2 (a) Isothermal volume recovery of glasses at 525 °C and 1 atm fitted by the two-internal-parameter relaxation model with $K_{liq}=18$ GPa, $f_c=3$, $f_j=4$, $f_a=39$, $\Delta V_a=28.6$ cm³/mol. Prior to relaxation, the glass samples have been hot compressed up to 2 GPa and pressure quenched from equilibrium states (at 700 °C for a holding time of longer than 2 h) in three different methods and compared with an uncompressed sample. Error bars represent the uncertainty of the final fully recovered specific volume at 525 °C. (b) Corresponding change of T_f and P_f versus time as predicted by the two-internal-parameter relaxation model.

Figure 3 (a) Isothermal volume recovery of glass at 525 °C and 1 atm fitted by the two-internal-parameter relaxation model with the same set of fitting parameters as in Figure 2(a). Prior to relaxation, the glass samples were hot compressed in GPC at 1 GPa and various dwell temperatures for 0.5 h. Error bars represent the uncertainty of final fully recovered specific volume at 525 °C. (b) Corresponding change of T_f and P_f of samples versus time as predicted by the two-internal-parameter relaxation model.

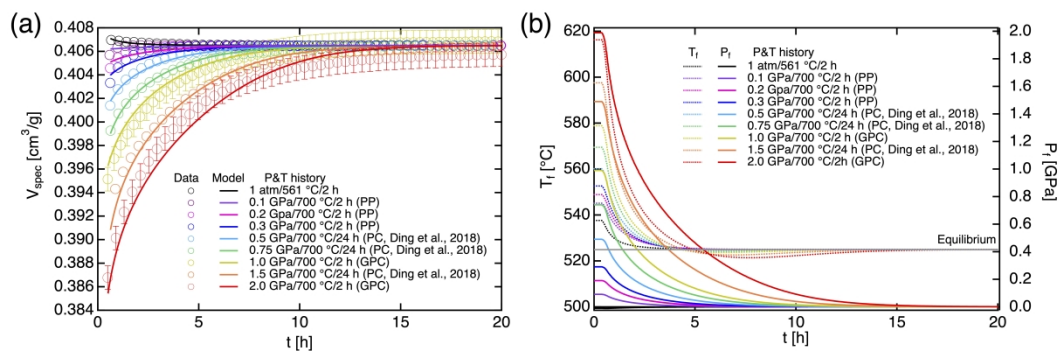
Figure 4 (a) Isothermal volume recovery of glass at 525 °C and 1 atm fitted by the two-internal-parameter relaxation model with the same set of fitting parameters as in Figure 2. Prior to relaxation, the glass samples were hot compressed in GPC at 2 GPa and various dwell temperatures for 0.5 h. Error bars represent the uncertainty of final fully recovered specific volume at 525 °C. (b) Corresponding change of T_f and P_f of samples versus time as predicted by the two-internal-parameter relaxation model.

Table 1 Changes in T_f , P_f and τ_G at the beginning of volume recovery at 525 °C and 1 atm in the model.

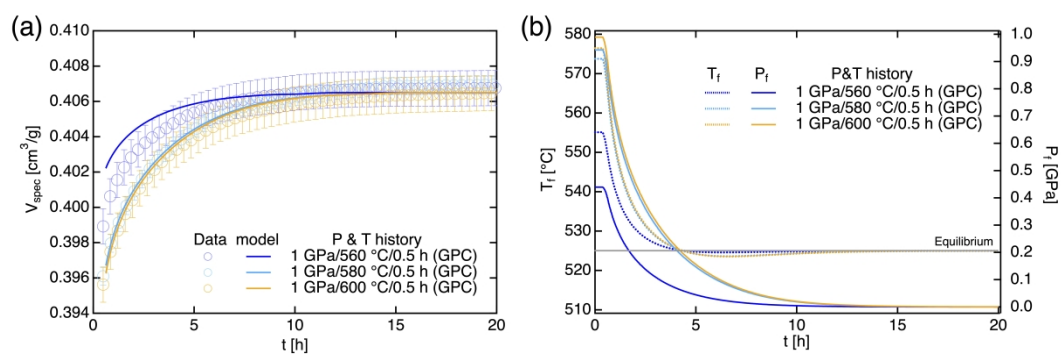
Sample	P & T histories	T_f [°C]	P_f [GPa]	τ_G [h]
1atm	1 atm/560 °C/2 h	534.3	-0.01	0.16
PP-1	0.1 GPa/700 °C/2 h	542.2	0.08	0.28
PP-2	0.2 GPa/700 °C/2 h	545.5	0.18	0.28
PP-3	0.3 GPa/700 °C/2 h	548.7	0.27	0.28
PC-1	0.5 GPa/700 °C/24 h	555.2	0.45	0.29
PC-2	0.75 GPa/700 °C/24 h	563.3	0.69	0.29
GPC-1	1 GPa/700 °C/2 h	571.5	0.92	0.30
PC-3	1.5 GPa/700 °C/24 h	587.8	1.39	0.31
GPC-2	2 GPa/700 °C/2 h	604.1	1.86	0.32
GPC-3	1 GPa/560 °C/0.5 h	550.0	0.40	0.28
GPC-4	1 GPa/580 °C/0.5 h	566.0	0.87	0.30
GPC-5	1 GPa/600 °C/0.5 h	568.1	0.91	0.29
GPC-6	2 GPa/580 °C/0.5 h	549.4	0.32	0.25
GPC-7	2 GPa/600 °C/0.5 h	580.2	1.12	0.25
GPC-8	2 GPa/700 °C/0.5 h	600.2	1.84	0.33



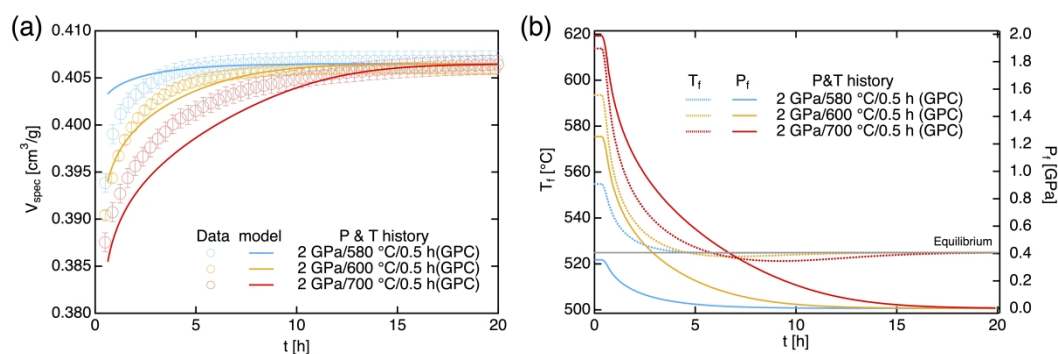
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