

Actuator grid method for turbulence generation applied to yawed wind turbines

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Actuator grid method for turbulence generation applied to yawed wind turbines. F. Houtin–Mongrolle¹, P. Benard¹, V. Moureau¹, G. Lartigue¹ L. Bricteux², J. Reveillon¹

wind turbine yaw angle seem relevant to reduce wake interactions. [1]

- Need for **predictive tools**[2] to model yawed wind turbine wakes
- **Replicate** and **investigate** wind tunnel results [3,4] of turbine under yaw condition

Problematics

Replicate a wind tunnel configuration involves :

- **Turbulence grid** upstream the turbine (If turbulent inflow)
- Tower and nacelle \rightarrow complex geometry effects
- Confinement of the **wind tunnel**, turbulence decay
- Yawed wind turbine encounters particular aerodynamical effects :
- Dynamic stall, sweep along the blade span

Objectives

 \rightarrow Validation of high fidelity tools, in a complex configuration, for yawed wind turbine wake investigation

• Investigate **9 experimental cases** [4]



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Numerical setup		
w solver: イムレ	ES2 ^[5,6,7] Azi	imu
Low Mach number Navier Stokes equations solver 4^{th} order central finite volume method and 4^{th} order times Turbulence model: SIGMA [8] Unstructured meshes are around 167 Million cells each Wind tunnel walls are body fitted to the mesh Duprat et al. [9] wall model : $\langle y^+ \rangle_{walls} < 200$	me integration h (9 cases)	Nea (-5 Neg
nd turbine: Actuator Line Method [10], 27 actuator elements per b $\left(\frac{\epsilon}{c}\right)_{tip} = 0.57$	olade,	
No additional 3D unsteady effect correction [11,12,13] Tower and nacelle are body fitted to the mesh Duprat et al. [9] wall model : $\langle y^+ \rangle_{tower} < 100$		
bulence grid: Emulated using Dynamic Actuator Lines Method [14] turbulence grid geometry	Tu fro and the actual	rbin om t C _P
mputation cost: Each computation on 1092 cores for 10s (15 flow throu	ıgh) ~ 40khCPU	Hig
Inflow and yaw impact on wa	<u>ke</u>	tun
ocity and Turbulent Kinetic Energy profiles:	D = 2 $m/D = 6$	Flov
$\langle u \rangle / u_{ref} [-]$ 1.2 0.5 $x/D = 3$		
$\langle k \rangle / u_{ref}^2 [-]$ 0.02 0.00		
Velocity deficit slightly underestim experimental data [3] TKE profiles show slightly overestim	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{1}{\langle u \rangle / u_1}$
wake Similar results to experiment for the		
ke deflection quantification using a		, , , , , , , , , , , , , , , , , , ,
inflow	(iii), $\gamma = -30^{\circ}$	0.01
	$\langle k \rangle / u_{\rm ref}^2$	$\langle k \rangle / u_1^2$
ke deflection overlaying the mean velocity field		
This study Experimental results (at 3D and 6D) Bastankhah and Porté-Agel wake deflection model [16]		s w orm 0721 ppli
Slightly higher estimation of the deflection (at 3D and 6 Good agreement with Bastankhah and Porté-Agel [16] → confinement redirect the wake towards it's center a	D) model up to 6D fter 6D	



Performances and azimuthal loads

uthal angle of attack (AoA)

- ar hub variation of AoA due to azimuth for yawed cases ° up to 30°) potential **dynamic stall**
- **gative AoA** \rightarrow local negative contribution to turbine Torque



- ne performances (power and thrust coefficient) differs significantly the experimental results:
- up to +20% and C_T up to 9% \rightarrow due to the absence of corrections

Conclusion

sh fidelity simulations show the ability to represent mplex operating conditions (turbulence injection, wind nel confinement, complex geometries)



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