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Jérémy Vessaire, Nicolas Plihon, Romain Volk, Mickaël Bourgoin. Sedimentation of a suspension of paramagnetic particles in an external magnetic field. Physical Review E , 2020, 102 (2), pp.023101. 10.1103/PhysRevE.102.023101 . hal-02929144

HAL Id: hal-02929144

https://hal.science/hal-02929144

Submitted on 12 Oct 2020

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Sedimentation of a suspension of paramagnetic particles in an external magnetic

field

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(Dated: 12 October 2020)

We investigate the sedimentation of initially packed paramagnetic particles in the presence

of a homogeneous external magnetic field, in a Hele-Shaw cell filled with water. Although

the magnetic susceptibility of the particles is small and the particle-particle induced mag-

netic interactions are significantly smaller compared to the gravitational acceleration, we do

observe a measurable reduction of the decompaction rate as the amplitude of the applied

magnetic field is increased. While induced magnetic dipole-dipole interactions between

particles can be either attractive or repulsive depending on the particles relative alignment,

our observations reveal an effective overall enhancement of the cohesion of the initial pack

of particles due to the induced interactions, very likely promoting internal chain forces in

the initial pack of particles. The influence of the magnetic field on the particles once they

disperse after being decompacted is on the other hand found to remain marginal.

Keywords: Particles-interactions, magnetic particles, sedimentation

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#### I. INTRODUCTION

The present study is motivated by the general topic of transport of particles in flows, which is of broad interest for fundamental scientific issues, industrial applications and natural systems. In nature, the formation of rain droplets in clouds, pyroclastic flows, dispersion of pollutants in the atmosphere or planet formation in accretion disks are just a few examples. In industrial applications, one can mention spray combustion in diesel engines, fluidized beds, pneumatic transport of granular media, or mixing processes. Most of these situations are quite complex due to the turbulent nature of the carrier flow, or to the fact that they are densely seeded, which makes the coupling between the particle dynamics and the flow random and multi-scale.

When it comes to the modeling of such particle laden flows, several situations must be distinguished depending on i) the nature of the particles, and ii) their local concentration. In a very dilute situation, with sufficiently small particles, a point-wise approximation is relevant so that the dynamics of the particles is well captured by the celebrated Maxey-Riley-Gatignol equation<sup>1</sup>. In the recent years, experimental and direct numerical simulations studies of turbulent transport proved this approach to be valid, providing that the particle size is of the order of the smallest length-scale in the flow<sup>2-6</sup>. When the particle mass fraction is no longer negligible as compared to the one of the fluid, both the fluid and particles are fully coupled so that one has to resolve the flow around moving objects from first principles<sup>7,8</sup>, or to model the mixture as a continuous medium<sup>9-11</sup>. This situation corresponds for instance to dense suspensions which exhibit non trivial behaviors even in very simple configurations such as sedimentation<sup>12,13</sup> or gravity currents<sup>14</sup>. Indeed, the rheology of such complex systems is strongly influenced by inter-particle interactions<sup>2</sup>, which can lead to strong fluctuations even at moderate Reynolds number<sup>15</sup>.

In this broad context of inertial particle laden flows, the present work is a preliminary study in a long-term perspective aiming at addressing more particularly the role played by particle-particle interactions on the dynamics of particulate systems at high volume fraction. Such interactions are common in fluidized beds, or natural systems such as clouds, where water droplets tend to be charged.

In order to improve our understanding of the role played by the many possibly coupled phenomena above mentioned, it is wise to go step by step and consider first simpler situations in order to disentangle possible individual contributions of the different effects, before considering the fully coupled situation. In the present article, we therefore focus on some basic aspects of the role played

by particle-particle interactions, considering the simplified situation where the flow is initially at rest and the particles are initially packed and also at rest. More precisely, we investigate in a Hele-Shaw cell the sedimentation of paramagnetic particles subjected to gravity and to a tunable external homogeneous magnetic field perpendicular to gravity. The interest of using paramagnetic particles relies on the fact that the –dipole-dipole– interactions between particles can be directly tuned by adjusting the amplitude of the applied magnetic field. The chosen configuration for this pre-liminary study, with initially packed particles in a fluid at rest aims at considering first the most favorable situation regarding the possible impact of magnetic forces. The choice of such a configuration somehow moves the original motivation in the context of particle-laden flows, to the field of granular physics, where we investigate the decompaction of a granular system of sub-millimetric particles with tunable interactions. Interestingly, beyond our longterm goal in the context of particle laden flows, this opens new perspectives for future dedicated studies with the same experimental setup to address interesting questions in the field of granular and deformable porous media.

Figure 1 represents a time series of the investigated decompaction and sedimentation process. The situation is relatively canonical in the context of granular media research. Over the last decades, numerous studies have indeed investigated the sedimentation of such a granular pack in newtonian fluids  $^{16-21}$ . The question of the nature and the dynamics of interface instabilities in the early stage of the decompaction has received particular interest. Notably, the emergence of a fingering instability has been demonstrated, recalling the well-known Rayleigh-Taylor instability which classically develops at a horizontal interface between two fluids with different densities (the denser being on top) $^{22,23}$ . Several authors have investigated theoretically and experimentally the fingering instability of the particle pack / fluid interface in a Hele-Shaw cell $^{19-21}$ , proposing fluid interpretation  $\dot{a}$  la Rayleigh-Taylor.

The present study does not address the fingering instability but focuses on characterizing the decompaction and fluidization rate of the particles pack when magnetic interactions are present. These interactions are driven here by the induced magnetization of the particles by the external field and are of the type *induced dipole-induced dipole*. As such, depending on the relative position and alignment of the particles, the interactions can be either attractive or repulsive. It is therefore unclear, *a priori*, whether they will contribute to an increased cohesion of the pack of particles or on the contrary they will accelerate its decompaction. Besides, considering the small value of the magnetic susceptibility of the paramagnetic particles considered, it is also *a priori* unclear whether a measurable influence of the additional particle-particle magnetic interactions could be detected.

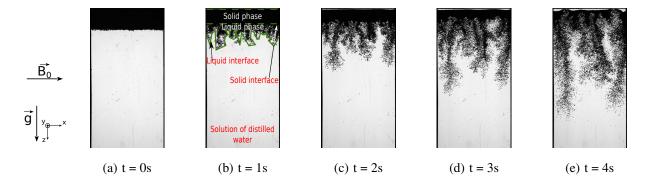


FIG. 1. Temporal series of images showing sedimentation subjected to gravity and a horizontal magnetic field in a steady flow with  $250\mu m$  diameter paramagnetic particles in a closed Hele-Shaw cell. The cell is 200 mm high, 50 mm wide and 1 mm depth. The cell is illuminated with a backlight, such that particles appear as dark spots on the original images.

The article is organized as follows: in section II we present the overall process of sedimentation of paramagnetic particles and the possible relevant dimensionless parameters of the problem; in section III we describe the experimental setup; section IV presents the main results, showing the impact of particle-particle interactions on the decompaction rate. The article ends with a brief discussion of the observed trends and possible perspectives of this work both in the context of particle laden flows and granular media.

# II. SEDIMENTATION OF PARAMAGNETIC PARTICLES WITH AN APPLIED EXTERNAL MAGNETIC FIELD

We briefly describe here the investigated decompaction and sedimentation process of dense particles in water as illustrated in Fig. 1 for one single typical realization. Particles are small (250  $\mu$ m in diameter) monodisperse spherical beads with density  $\rho_p=1.2$  g/cm³. After the particle pack is prepared in order to get a horizontal interface by vibrating the cell with particles initially placed at its bottom (see section III for further details on the preparation step), the Hele-Shaw cell is quickly rotated around the horizontal axis to bring the pack upwards. The time origin (t=0 s) is defined when the cell reaches the vertical position with the particle pack on top. On the first frame (Fig. 1a), we see the initial pack of particles, standing above water (note that the particles are fully permeated with water). The shape of the "particle-bed/water" interface is nearly flat and horizontal. On the next three frames (Fig. 1b-d), showing the subsequent decompaction and sedimentation of the particles, two main regions can be defined for the particle suspension: (i) in the upper part, par-

ticles remain packed and form a homogeneous and compact pack at rest, (ii) below, the interface is disturbed giving rise to fingers of dispersed sedimenting particles. Following classical granular terminology<sup>13</sup>, we shall call solid phase the upper compact region of particles and liquid phase the lower sedimenting region. We therefore distinguish two interfaces: (i) the first between the solid and liquid phases of particles, (ii) the second between the liquid phase of particles and water. As the sedimentation process goes on, the volume of the solid phase reduces (we shall refer to this as the decompaction or the liquefaction of the solid phase) and at the same time the area of the liquid interface increases (the solid-liquid interface slowly moves up while the liquid-water interface develops larger fingers). Note that, as the total number of particles in the system is conserved, and since particles initially in the compact solid phase liquefy into the less compact liquid phase, the total area occupied by the particles grows in time during the decompaction process. In the last frame (Fig. 1e), the solid phase has totally melted and disappeared. As the liquid fingers of particles develop further, the dynamics of the suspension becomes strongly influenced by the induced re-circulation flow of water in the cell and by lateral confinement effects due to the finite size of the cell.

In the present work we focus on the dynamics of the initial decompaction process  $(t \lesssim 3 \text{ s})$  and do not address specific long-term effects which are strongly affected by the finite size of the  $\text{cell}^{24}$ . We investigate the liquefaction rate of the solid phase as well as the growth rate of the liquid phase, with the goal to highlight the impact of particle-particle interactions on the global sedimentation behavior, when imposing a tunable homogeneous horizontal magnetic field  $\vec{B}_0 = B_0 \vec{x}$ , with  $\vec{x}$  the horizontal direction along the width of the Hele-Shaw cell and  $\vec{z}$  the vertical direction such that gravity acceleration is  $\vec{g} = g\vec{z}$ .

In the absence of any external magnetic field ( $B_0 = 0$  G), particles are only subjected to gravity  $\vec{g}$  (and eventually hydrodynamic interactions).

In the presence of a homogeneous magnetic field ( $B_0 \neq 0$  G), all particles acquire an identical induced magnetic moment  $\vec{M}$  given by:

$$\vec{M} = \frac{4}{3}\pi r^3 \frac{\chi_m}{\mu_0} \vec{B}_0,\tag{1}$$

where r is the radius of the particles,  $\mu_0$  the vacuum permittivity and  $\chi_m$  the magnetic susceptibility of the particles. In addition to gravity, each particle is then subjected to the magnetic force exerted by the magnetization of the other particles. The magnetic force  $\vec{f}_m^i$  acting on particle i can then be

written as

$$\vec{f}_m^i = \left( \vec{M}_i \cdot \vec{\nabla} \right) \vec{B}_i, \tag{2}$$

where  $\vec{M}_i$  is the induced magnetization of particle i and  $\vec{B}_i = \vec{B}_0 + \sum_{k \neq i}^{N_p} \vec{b}_{ki}$  the total magnetic field at the position of particle i, including both the applied field  $\vec{B}_0$  and the total induced magnetic field  $\vec{b}_i = \sum_{k \neq i}^{N_p} \vec{b}_{ki}$  from all other particles than i. Note that as we consider here the case of a homogeneous applied magnetic field  $\vec{B}_0$ , there is no net force exerted by  $\vec{B}_0$  on the magnetized particles and  $f_m^i$  is simply given by

$$\vec{f}_m^i = \left( \vec{M}_i \cdot \vec{\nabla} \right) \vec{b}_i. \tag{3}$$

We recall that the dipolar magnetic field  $\vec{b}_{ki}$  generated by a particle k with magnetization  $\vec{M}_k$  at the position of particle i is given by

$$\vec{b}_{ki} = \frac{\mu_0}{4\pi} \left( \frac{3\vec{r}_{ki} \left( \vec{M}_k \cdot \vec{r}_{ki} \right)}{|\vec{r}_{ki}|^5} - \frac{\vec{M}_k}{|\vec{r}_{ki}|^3} \right) \tag{4}$$

where  $\vec{r}_{ki}$  is the separation vector between particle k and particle i. Considering the rapid decay of  $\vec{b}_{ki}$  with  $|\vec{r}_{ki}|$ , contributions to  $\vec{b}_i$  mostly come from the nearest neighbors, which in the initially compact pack are at a distance  $\vec{r}_{ki}$  commensurate with the particle diameter d=2r (although the orientation –repulsive or attractive– of the force changes depending on the position of the considered neighbors around particle i). As a consequence, the typical expected order of magnitude for  $\left|\vec{b}_i\right|$  is given by  $\mu_0 M/4\pi r^3$ , and considering Eqs. (1) & (3), the typical order of magnitude of the magnetic force is

$$\mathcal{O}\left(\left|\vec{f_m^i}\right|\right) \propto \frac{r^2 \chi_m^2 B_0^2}{\mu_0} \tag{5}$$

Based on these estimates, we can then define a dimensionless number  $\Psi$  comparing the amplitude of particle-particle magnetic force and gravity (including effect of buoyancy) acting on each particle:

$$\Psi = \frac{\chi_m^2 B_0^2}{\mu_0 r |\rho_p - \rho_w| g} \tag{6}$$

with  $\rho_p$  and  $\rho_w$  the density of the particles and of water respectively. We shall refer to  $\Psi$  as the magneto-gravitational number.

#### III. EXPERIMENTAL SETUP

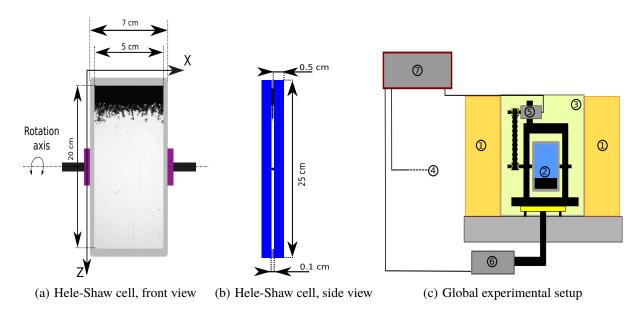


FIG. 2. (a) Front and (b) side views of the Hele-Shaw cell and (c) automated experimental setup with magnetic coils (1), Hele-Shaw cell (2), backlight LED panel (3), high speed camera (4), stepper motor (5), shaker (6), Raspberry-Pi controller (7).

Experiments were performed in a sealed Hele-Shaw cell (200 mm in height, 50 mm in width, with a gap of 1 mm), filled with distilled water and paramagnetic particles. A small amount of surfactant (Sodium dodecyl sulfate) is also added to stabilize the solution and to prevent aggregation of the particles. Fig. 2(a)-(b) shows a schematic of the cell and a typical recorded image of settling particles. The gap of the Hele-Shaw cell is fixed by a thin (1 mm in thickness) internal plastic frame clamped between two plexiglass plates. Two pivots screwed on the sides of the cell at mid-height allow to rotate the cell around the horizontal axis  $\vec{x}$ .

As particles, we used 250  $\mu m$  (in diameter) polythene (PE) micro-spheres, with density  $\rho_p=1.2~{\rm g.cm^{-3}}$  doped with iron oxyde (FeO) in order to be paramagnetic (BKPMS particles from Cospheric LLC, Santa Barbara, CA USA). We have determined their magnetic susceptibility  $\chi_m$  from a SQUID magnetometer measurement on individual particles, carried at the CML (Center of Magnetometry of Lyon), leading to a value  $\chi_m \simeq 4.2 \cdot 10^{-3}$ .

Two coils in Helmholtz configuration surround the cell in order to apply a homogeneous horizontal magnetic field  $\vec{B}_0$ , parallel to the x axis, aligned with the width of the cell (Fig. 2). The water-cooled coils are driven with a 10 kW power supply (*Danfysik System 9100*). The maximum amplitude of the applied magnetic field is  $B_0^{max} \approx 0.12$  T. It is turned on during all runs and is

therefore applied during the iniatilisation protocol of the particle pack described in next paragraph.

In order to carry out a systematic investigation with good statistical convergence, for a given value of the applied magnetic field, of the order of 50 sedimentation experiments are repeated with the same initialization protocol. For a good reproducibility of experimental conditions, the setup is fully automatized, the rotation been ensured by a stepper motor controlled from a Raspberry Pi nano-computer with a pre-programmed cycle. Special care has been taken to properly condition the initial pack of particles in between rotations in order to have a particle-bed/water interface as flat and horizontal as possible before each rotation. This is achieved by applying to the cell several rapid oscillations and simultaneously vibrating the cell with an electrodynamic shaker. This optimal pack conditioning protocol is also automatized (and is part of the global rotation cycle controlled by the nano-computer) and warrants that the exact same protocol is applied for every experiment. Note that in spite of this care, the initial compaction of the particle bed may still present some variations from one realization to another. To limit any bias due to such variations of initial conditions, we remove from the ensemble of realizations those for which the initial height of the particle bed deviates from the average height by more than 10%. This ensures considering realizations with almost identical initial compaction. As a consequence of this selection, of the order of 15% of the realizations are dropped.

Measurements are based on high-speed backlight imaging of the cell, which is illuminated from behind by a LED panel. Recordings are performed using a high speed camera (*Flare 2M360-CL from IO Industries*) operated with a resolution of 2048×1088 pixels at a frame rate of 300 fps. The starting of the recordings is triggered by the controller nano-computer and is synchronized with the rotation cycle.

#### IV. EXPERIMENTAL RESULTS

We present in this section results on the *liquefaction* rate of the *solid* phase and the simultaneous growth of the *liquid* phase of the suspension in the early stage of the sedimentation, right after the cell reaches its vertical position.

We recall here the phenomenology introduced in section II: the particles, initially packed and forming a compact *solid* phase, gradually feed a lower, dilute, *liquid* phase. It is important to note here that the phase classification follows the granular *terminology*<sup>13</sup> and that the *liquid* phase

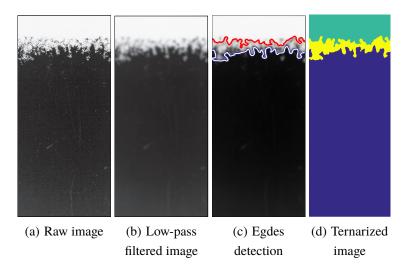


FIG. 3. Successive steps of image processing to determine the *solid* phase (upper green area in (d)) and *liquid* phase (middle yellow area in (d)) of particles starting from the raw image (a).

may indeed be compressible. The goal of the present study is to address the dynamics of the granular phases and, in particular, the influence of the magneto-gravitational number  $\Psi$  on the time evolution of the areas of the *liquid* phase  $A_l$  and of the *solid* phase  $A_s$  as the decompaction process goes on. The most important results being that i) inter-particle interactions foster the liquefaction rate during the initial phase, while ii) they mitigate the terminal liquefaction rate, and iii) after a initial strongly compressible transient of the *liquid* phase, the *liquid* phase is about four times more dilute than the *solid* phase, regardless of the intensity of the inter-particles interactions. These experimental results, reported in the remaining of this section, have been obtained following a careful and systematic image processing to detect the solid and liquid phases, detailed in next subsection.

# A. Edge detection & area calculation

The successive image processing steps are illustrated in Fig. 3 for one specific frame of one realization, at time  $t \sim 1$  s (note that, compared to previous figures, negative images are shown, particles appear now as bright). Fig. 3(a) shows a raw image, where the *solid* phase appears as a continuous bright region on the top whereas the *liquid* phase is characterized by some fragmentation of the intensity pattern below. Our simple image processing algorithm aims at providing a robust segmentation algorithm to detect three fully connected regions: the (granular) *solid* phase, the (granular) *liquid* phase and the clear water. We first apply a Gaussian low-pass filter in order

to blur the image in the liquid phase: as a result (i) nearby particles in the fragmented region become connected and (ii) the locally smoothed intensity in the liquid region decreases as shown in Fig. 3(b). We use a Gaussian convolution kernel with a width of 1.5 particle diameter in order to reconnect the fragmented areas up to this scale<sup>25</sup>. Few blobs of particles separated by more than 1.5 d can still be present; those will be considered as having already left the *liquid* phase and are excluded from the detection. Note that the Gaussian filtering has no major effect on the solid phase region of the image which has constant and homogeneous intensity. Then, two successive thresholdings of the image are operated. The first uses a relatively low threshold chosen in order to keep all the particles (non-dark pixels) in both solid and liquid phases and segment them from the pure water phase. An edge detection algorithm is then run on the binarized image to determine the liquid-water interface (blue line in Fig. 3(c)). The second thresholding uses a higher value of the threshold, chosen to keep only the bright pixels in the continuous region corresponding to the solid phase and segment it from the liquid phase. Another edge detection then retrieves the solid-liquid interface (solid red line in Fig. 3(c)). The two different binarized images can also be combined to create a ternarized image showing the solid phase (upper green region in Fig. 3(d)), the liquid phase (middle yellow region in Fig. 3(d)) and water (lower blue region Fig. 3(d)).

This image processing sequence is performed for all frames at time t of each recording during run k, in order to monitor the time evolution of the areas  $A_s^k(t)$  and  $A_l^k(t)$  of the *solid* and *liquid* phases respectively. In the sequel, for a given experiment (i.e. a given value of the applied magnetic field amplitude  $B_0$ ) we investigate the time evolution of the *solid* and *liquid* phase areas ensemble-averaged over the full set of realizations:

$$\langle A_{s,l} \rangle (t) = \frac{1}{N_{movie}} \sum_{k=1}^{N_{movie}} A_{s,l}^k (t - t_{0,k}), \tag{7}$$

with  $N_{movie}$  the total number of movies (realizations) recorded for each experiment ( $N_{movie}$  being of the order of 50 for each value of applied magnetic field amplitude  $B_0$ ), and  $t_{0,k}$  the instant when the cell reaches its vertical orientation after rotation during run number k. For the sake of clarity, we shall omit from now the average brackets when presenting the results and simply refer to  $A_{s,l}(t)$  for the ensemble-averaged areas of the *solid* and *liquid* phases.

# B. Liquefaction dynamics and particle concentration

#### 1. Evolution of solid and liquid phases

Fig. 4(a) shows the time evolution of the *solid* phase area  $A_s(t)$  for the case without any applied magnetic field ( $B_0=0$  G) and for the case with  $B_0=800$  G ( $\Psi\simeq0.26$ ). A common pattern can be seen, after a short period (of the order of 300 ms) with almost no apparent evolution, where a rapid decrease of  $A_s(t)$  occurs followed by a slower linear decrease. A first visible impact of the magnetic field appears in the long term behavior, where we see that the *solid* phase *liquefies* slower in the presence of an applied magnetic field. At t=3 s we observe indeed that the remaining area of *solid* phase is the largest for  $B_0=800$  G and the smallest when no magnetic field is applied.

In order to further characterize the influence of the magnetic field on the acceleration/deceleration of *liquefaction* we introduce the *liquefaction rate*:

$$V_s(t) = -\frac{dA_s(t)}{dt}. (8)$$

Note that  $V_s$  has units of  $\mathrm{m}^2\mathrm{s}^{-1}$ . Fig. 4(b) shows the time evolution of the *liquefaction* rate. Two regimes are clearly visible: after a short transient with a rapid increase of the *liquefaction* rate followed by a local maximum, a constant asymptotic terminal value  $V_s^\infty$  is reached. It can be noted that in spite of the large number of recorded movies for each experiment, while the raw curves for  $A_s(t)$  appear relatively smooth and well converged, their derivative still exhibit some visible noise. We therefore estimate  $V_s^\infty$  by averaging  $V_s(t)$  typically on the time interval  $t \in [2 \mathrm{ s} - 3 \mathrm{ s}]$ .

During the initial transient of the liquefaction, a systematic trend can be observed where the larger the magnetic field, the larger the *liquefaction* rate. Moreover we find that the initial liquefaction rate without magnetic field is negative as opposed to the case with an applied magnetic field. This is related to the fact that in absence of magnetic field ( $B_0=0~\rm G$ ), magnetic interactions between particles are absent so that the initial pack obtained by vibrating the cell is the most compact, leading to a slightly smaller initial value of  $A_s$ . As a consequence, when no magnetic field is applied, the solid phase slightly expands at short time due to small relative motions of the beads. The mild overshoot preceding the terminal regime occurs at a similar time  $t\approx 0.7~\rm s$  regardless of the amplitude of the magnetic field, although it seems slightly more peaked as the amplitude of the magnetic field increases.

Concerning the terminal liquefaction regime, Fig. 5(a) shows the liquefaction average terminal

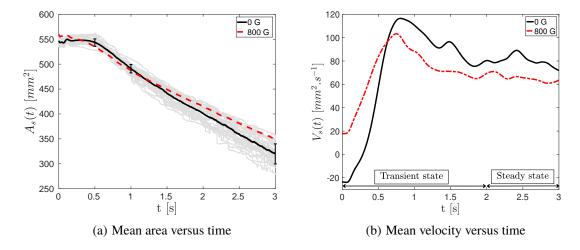


FIG. 4. (a) Averaged time evolution of the solid area without any applied magnetic field (solid black line) and with an applied field with amplitude  $B_0 = 800$  G (dashed red line, corresponding to a magneto-gravitational number  $\Psi \simeq 0.26$ ). To illustrate the averaging procedure, the light gray lines represent the individual time evolution of the solid area for 50 independent realizations for the case without any applied magnetic filed. The solid black line correspond to the average of the light gray lines. The bars at 0.5 s, 1 s and 3 s indicate the standard deviation among the 50 realizations at each of these instants. (b) Time evolution of the *liquefaction* velocity for  $B_0 = 0$  G (solid black line);  $B_0 = 800$  G (dashed red line).

rate  $V_s^{\infty}$  as a function of the magneto-gravitational number. In agreement with the qualitative observed trend of  $A_s(t)$ , we see that, in spite of some scatter, the terminal *liquefaction* rate of the *solid* phase globally decreases when the magnetic field increases.

A similar analysis has been performed for the growth of the *liquid* phase, defining the *liquid* growth rate as:

$$V_l(t) = \frac{dA_l(t)}{dt}. (9)$$

Fig. 5(b) shows the *liquid* average terminal growth rate as a function of the magneto-gravitational number. Trends similar to those of the *liquefaction* of the *solid* phase are observed, with a global decrease of the *liquid* growth rate as the magnetic field increases.

The observed trends for the *solid* and the *liquid* phases show consistently that as the magnetic field amplitude increases, the *solid* phase is stabilized (in the sense that it *liquefies* slower) while the *liquid* phase is less supplied with particles and hence it also grows slower. To further characterize the trends of the terminal liquefaction rate of the *solid* phase and the terminal growth rate of the *liquid* phase, we introduce the relative terminal rates defined respectively as  $s1 - V_s^{\infty}/V_{s,0}^{\infty}$  and  $1 - V_l^{\infty}/V_{l,0}^{\infty}$  where the subscript 0 indicates the values when no magnetic field is applied ( $B_0 = 0$ ). Fig. 5(c)-(d) show a log-log representation of the relative terminal rates as a function of the

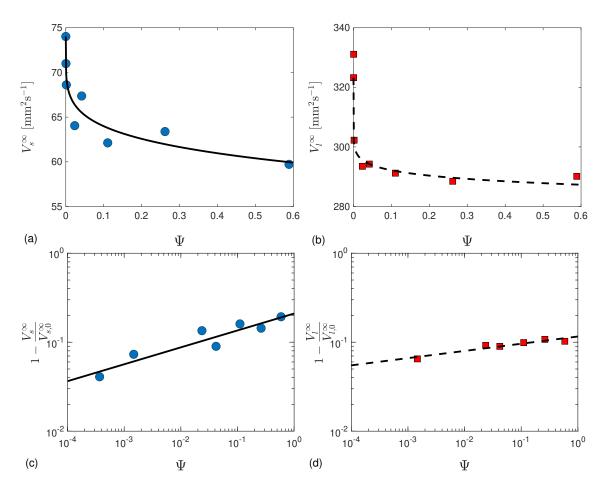


FIG. 5. (a) Terminal *liquefaction* rate of the *solid* phase and (b) terminal growth rate of the *liquid* phase as a function of the magneto-gravitational number  $\Psi$ . (c) Relative liquefaction for the *solid* phase and (d) growth rate for the *liquid* phase, as a function  $\Psi$ . Solid and dashed lines correspond to the power-law fit Eq. (10).

magneto-gravitational number  $\Psi$ . For both the *solid* and the *liquid* phase, the trends are reasonably fitted by a power law such that

$$1 - \frac{V_{s/l}^{\infty}}{V_{s/l,0}^{\infty}} = a_{s/l} \Psi^{b_{s/l}}, \tag{10}$$

with  $a_s=0.21\pm0.08$  and  $b_s=0.19\pm0.08$  for the *solid* phase and with  $a_l=0.12\pm0.01$  and  $b_l=8.1\cdot10^{-2}\pm0.04$  for the *liquid* phase.

These trends reveal that the influence of the magnetic field is significantly stronger in hindering the liquefaction of the *solid* phase, than in hindering the growth rate of the *liquid* phase. This could be expected considering that in the more dilute *liquid* phase the inter-particle distance is larger than in the compact *solid* phase where particles are in contact with each other. The induced magnetic particle-particle interactions are then reduced in the *liquid* phase which is indeed found to be marginally affected by the applied magnetic field. An interesting question then concerns the

evolution of the particle concentration (and hence of the inter-particle distance) in the liquid phase. This particle concentration results from the balance between the particles being supplied from the liquie faction of the solid phase and of the growth with time of the liquid area  $A_l(t)$  as the liquid phase develops. We investigate this balance in the next sub-section.

# 2. Particle concentrations in the solid and liquid phases

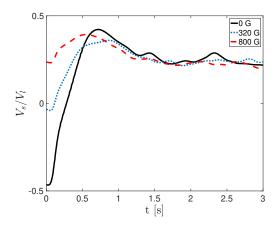


FIG. 6. Evolution with time of the *solid* to *liquid* rate ratio. In the terminal steady state, the *solid* to *liquid* rate ratio reaches an asymptotic value of the order of 0.25, independent of the magnetic field amplitude, indicating that the *liquid* phase is about four times more dilute than the *solid* phase.

Let  $\rho_l$  and  $\rho_s$  be the particle concentration (number density) in the *liquid* and the *solid* phase respectively. The particle concentration  $\rho_s$  is assumed to be constant and fixed by the compacity of the initial pack. Initially, the *liquid* phase is empty and emerges when the *solid* phase starts *liquefying*. The particle concentration in the *liquid* phase is therefore expected to have a non-trivial time evolution.

Keeping in mind that the cell is sealed, and hence the total number  $N_p$  of particles remains constant, the concentration in both phases can be directly related to the rates of *liquefaction* of the solid phase  $V_s$  and the rate  $V_l$  at which the *liquid* phase grows. Assuming that all particles remain either in the *liquid* or the solid phase (this approximation neglects the few particle blobs eventually detaching from the *liquid* phase) and that the concentration within each phase is relatively homogeneous, we can indeed write

$$N_p = \rho_l(t)A_l(t) + \rho_s(t)A_s(t). \tag{11}$$

The conservation of the total number of particles then imposes  $dN_p/dt = 0$  which, considering Eq. 11 and assuming that  $\rho_s$  remains constant, leads to

$$\frac{V_s(t)}{V_l(t)} = \Gamma_{ls}(t) + \frac{d\Gamma_{ls}(t)}{dt} \frac{A_l(t)}{V_l(t)}, \quad \text{with} \quad \Gamma_{ls}(t) = \frac{\rho_l(t)}{\rho_s(t)}.$$
 (12)

This relation directly links the liquid to solid concentration ratio  $\Gamma_{ls}$  to the corresponding areas and growth rates and in particular to the solid to liquid rate ratio  $V_s(t)/V_l(t)$ , which is represented in Fig. 6. In principle, Eq. 12 is a simple differential equation for  $\Gamma_{ls}$  with empirically known time dependent coefficients  $(V_s(t)/V_l(t))$  and  $A_l(t)/V_l(t)$ , which are directly accessible from the measurements), from which we could derive the time evolution of  $\Gamma_{ls}$ . We focus here though on the long term asymptotic behavior, where the ratio  $V_s(t)/V_l(t)$  is constant, and found to be of the order of  $V_s^\infty/V_f^\infty \approx 0.25$  independently of the amplitude of the applied magnetic field (see Fig. 6). In this stationary regime, the solution of Eq. 12 is  $\Gamma_{ls}^\infty = V_s^\infty/V_f^\infty$ , hence  $\Gamma_{ls}^\infty \approx 0.25$  independently of the amplitude of the applied magnetic field. This means that the liquid phase is about four times more dilute than the solid phase, and that the particle average concentration in the liquid phase is not affected by the presence of the magnetic field.

#### V. DISCUSSION AND CONCLUSION

Our experiments reveal that, even if the magneto-gravitational numbers investigated in the present study remains relatively low ( $\Psi < 0.6$ ), measurable effects are still observed regarding the impact of an applied magnetic field on the terminal decompaction rate under gravity of a pack of paramagnetic particles. Overall, the influence of an increasing magnetic field on the terminal dynamics of the decompaction of the *solid* pack exhibit several interesting features:

- The terminal *liquefaction* rate is reduced by the magnetic field and so is the growth rate of the *liquid* phase, although the impact of the magnetic field on the *liquid* phase remains marginal;
- The terminal concentration of the *liquid* phase is about a quarter that of the *solid* phase and does not depend on the applied magnetic field.

These trends can be qualitatively interpreted in terms of magnetic induced interactions between the particles in the *solid* phase. The reduction of the terminal *liquefaction* rate with magnetic field suggests a stabilizing effect of the magnetic field on the *solid* pack. A plausible origin could be

the formation of chain-forces of particles sustained by attractive magnetic interactions reinforcing the global cohesion of the pack of particles. Finally, the independence of particles concentration in the *liquid* phase very likely reveals that when the particles are sufficiently dilute the typical interparticle distance is so that the magnetic interaction between induced dipoles becomes negligible compared to gravity and hydrodynamic interactions. In such situation, the magnetic field then is not expected to have any significant impact on the inner structure of the dilute *liquid* phase.

While the previous conclusions on the terminal dynamics of the decompaction of the *solid* pack are firmly established from our experimental results, an interesting point during the initial phase should deserve further investigation. Indeed, our analysis shows that, in the initial phase, the *liquefaction* is accelerated in presence of the magnetic field. The origin of the initial acceleration of the decompaction is still speculative but may result from the vertical repulsion between parallel induced dipoles from successive layers in the initially compact *solid* phase which could promote the initial destabilization of the *solid*-water interface. Thus loosen, particles in the interface could then self-organize to form the stabilizing chain-forces aforementioned.

The study of paramagnetic particles still deserves further developments. The proposed qualitative scenario for the decompaction process investigated in the present work suggests indeed that most of the action of the magnetic field affects primarily the solid phase and the solid-liquid interface, while the *liquid* phase itself remains mostly insensitive to the applied field. One could then expect a clear signature of the magnetic field on the fingering (Rayleigh-Taylor like) instability occurring in the early stage of the decompaction at the interface between the solid phase and the water<sup>20?</sup>,<sup>21</sup>. The scenario where the magnetic field would tend to increase the cohesion of the pack by magnetically induced chain-forces can be expected to act as an enhanced effective surface tension of the interface, with a possible stabilizing effect regarding the fingering instability. In the continuity of the present study, we would like to study the fingering instability, by a systematic investigation of the structure and the dynamics of the solid-liquid interface (in order to extract information on the wavelength and growth rate of the instability) as a function of the amplitude of the applied magnetic field. Finally a natural extension of this work would be to using ferromagnetic particles (rather than paramagnetic) to reach magneto-gravitational numbers of the order of unity at reasonable seeding densities. Ferromagnetic particles would indeed allow to reach regimes with particle-particle interactions of similar amplitude to the one of the hydrodynamic forces, thus strongly affecting the dynamics of the *liquid* phase.

#### VI. ACKNOWLEDGMENTS

This work benefited from the financial support of the Project IDEXLYON of the University of Lyon in the framework of the French program "Programme Investissements d'Avenir" (ANR-16-IDEX-0005). We would also like to thank Damien Leroy for helping us with the SQUID measurements to determine the magnetic susceptibility of our particles.

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- <sup>25</sup>The concentration of the liquid phase is four times lower than the closed packed concentration of the solid phase, as shown in Section IV B; the inter-particles distance in the liquid phase is thus of the order of 1 particle diameter. This guides a posteriori the size of the Gaussian convolution kernel width of 1.5 particle diameter; and we checked that the robustness of our results when the convolution width was varied between 1 and 2 particle diameters.