# Personal navigation with handheld devices 

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## IPIN 2015 TUTORIAL

## Personal Navigation with Handheld Devices

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Banff, Canada, 13 October 2015


IFSTTAR

## Instructor Bio: Valérie Renaudin

## Current

- Head of GEOLOC Lab at the French institute of science and technology for transport, development and networks (IFSTTAR)


## Graduation

- MSc in Geomatic Eng. from the ESGT, France
- PhD in Computer, Communication and Information Sciences from the EPFL, Switzerland


## Research Focus is on

- Methods and systems for personal mobility in multimodal transport
- Pedestrian navigation using signals from Global Satellites Navigation



## IFSTTAR



## Overview and motivation

Background on strapdown inertial navigation system (INS)

The challenge of personal navigation with handheld device

Alternative positioning strategies

## A Paradigm Shift!



## Why navigating with handheld devices?

## PAST/PRESENT

- Strapdown navigator in motorized bodies $\rightarrow$ physics of solid
- Principally outdoors
- One device for each application: to guide private car, one to hike, etc.
- General navigation functionalities


## FUTURE

- Connected human $\rightarrow$ not well known human kinematic
- Indoors $\rightarrow 70 \%$ of mobile phone calls and $80 \%$ of data telecom in indoor spaces [Strategy Analytics 2012]
- The smartphone is a toolkit for everything including navigation
- We want the connected object to understand my particularities: Who am I? Physiological parameters?


## Targeted performances

- Continuous, reliable and accurate
- In figures
- 1 m accuracy
- 95\% percentile of the error distribution law
- 99\% coverage
- Applications from recreational use up to safety critical services

Shopping Mall in Nantes : Passage Pommeraye


## Beyond Navigation Expectations

- Adaptive to all dynamics
- Different motion modes
- Comfortable walking
- walking disabilities
- Active transport
- walk, run, bike
- Motorized transport
- private car
- public transit
- Providing personal (positive) feedback
- on physiological performance: a training tool
- on general health: a medical diagnostic tool


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## Many different coordinate frames

- Inertial Navigation involves several coordinate frames
- Inertial Frame (Inertial Signals)
- Earth Centered Earth Fixed Frame (GNSS)
- Local Frame (Map)
- Body Frame (IMU)
- Pedestrian Frame (Handheld Sensor)
- Preliminary comments
- The definition of these frames may differ depending on the application and the context
- These choices impact the mechanization equations of inertial navigation


## Inertial Frame (i-frame)

- The inertial frame is close to a Galilean frame
- non-rotating \& non accelerating frame
- The approximation comes from the fact that the earth is accelerating while it orbits the sun
- Accelerometer and gyroscope measurements are given in this frame

http://hronrad.wordpress.com/

| Parameter | Description |
| :---: | :--- |
| Origin | Earth's Center of Mass |
| Z axis | Parallel to the earth spin axis |
| X axis | Pointing toward mean vernal equinox |
| Y axis | Form a right handed orthogonal frame |

## Earth Centred Earth Fixed Frame (eframe)

- Principally used for satellite signals based navigation (GPS, GLONASS, Beidou, Galileo) because orbital data are computed in this frame
- Also called terrestrial equatorial frame
- Satellite signals and inertial navigation are often combined in this frame


| Parameter | Description |
| :---: | :--- |
| origin | Earth's Centre of Mass |
| Z axis | Parallel to earth spin axis |
| X axis | Pointing towards mean meridian of Greenwich |
| Y axis | Completing right-handed orthogonal frame |

## Local Frame (l-frame)

- Its choice and axis convention depend on the application
- On the illustration: North, East, Down (N,E,D)
- Often linked to the geographic
 information system used to display the navigation solution

| Parameter | Description |
| :---: | :--- |
| origin | Arbitrary: point on the earth surface |
| Z axis | Orthogonal to the reference ellipsoid |
| Y axis | Directed to the geodetic north |
| X axis | Completing right-handed orthogonal frame |

## Transformation between e-frame and i-frame

- The $\mathrm{Xn}, \mathrm{Yn}, \mathrm{Zn}$ axes of the l-frame are expressed in the e-frame with

$$
\begin{aligned}
& -Z_{n}=\left[\begin{array}{c}
-\cos \varphi \cos \lambda \\
-\cos \varphi \sin \lambda \\
\sin \varphi
\end{array}\right] \\
& -X_{n}=\frac{1}{\cos \varphi} \frac{\partial Z_{n}}{\partial \lambda} \\
& -Y_{n}=-\frac{\partial Z_{n}}{\partial \varphi}
\end{aligned}
$$

- $\varphi$ is the latitude
- $\lambda$ is the longitude

Earth Frame Axes

## Body Frame (b-frame)

- The body frame can be defined in many different ways
- Usually right-handed 3D Cartesian frame related to an object
- In strapdown applications, the body frame is considered as rigidly attached to the vehicle
- This hyp. doesn't always hold for pedestrian navigation applications


| Parameter | Description |
| :---: | :--- |
| origin | Specific point within the object |
| X axis | Pointing along the forward direction |
| Y axis | Pointing along the lateral axis of the IMU |
| Z axis | Completing right-handed orthogonal frame |

## Pedestrian Frame

- The pedestrian frame is attached to the "skeleton" of the human body
- Its origin describes the pedestrian position on the map
- Intermediate frame between the body and the local frames
- Usually right-handed 3D Cartesian frame

| Parameter | Description |
| :---: | :--- |
| origin | Human Body Center of Mass |
| X axis | Pointing along the forward direction |
| Y axis | Pointing along the lateral axis of the IMU |
| Z axis | Completing right-handed orthogonal frame |

6


## History of Navigation



## History of Navigation

- Radio Navigation
- Use of radio signals to measure the distance
- Accurate time measurement becomes critical
- At speed of light: $1 \mu \mathrm{sec}$ error gives 300 m error
- Trilateration positioning is introduced.
- Dead Reckoning
- Estimates the current position based on the previous one and distance/speed, angle measurements extracted from embedded seniors
- A recursive process common for aircraft navigation


## History of Navigation

- Inertial Navigation
- Is a dead reckoning navigation
- The measurements are accelerations and angular rates relative to an inertial navigation frame
- Processing
- Estimates the Position, Velocity and Attitude changes of a body
- Its mechanization is based on Newton's 1st and 2nd law of motion
- Definition
- INS $\rightarrow$ Inertial Navigation System
- IMU $\rightarrow$ Inertial Measurement Unit


## Inertial Sensors

Stable platform
$\rightarrow$ A triad of acc. is kept physically aligned with respect to the local vertical and north axes
$\rightarrow$ Mechanically complicated, bulky

Strapdown sensors configuration
$\rightarrow$ Introduced in the early 80s
$\rightarrow$ The stabilization is achieved mathematically
$\rightarrow$ Smaller size, weight and consumption

Solid State Inertial Sensors

## Micro-Electro-

Mechanical
Systems: MEMS
$\rightarrow$ Latest introduced inertial sensors
$\rightarrow$ Small and less
expensive
$\rightarrow$ Mass production
$\rightarrow$ Embedded in daily life equipment (smartphone, remote control, ...)
$\rightarrow$ Consumer Grade sensors
$\rightarrow$ Solid state optics
$\rightarrow$ Nanotechnol ogy
$\rightarrow$ Atomic
Physics

## Gyroscope

- Gyroscopes are angular rate sensors
- Measure the rotation rates of the body frame relative to the inertial frame
- Parameterized in the body frame, it is $\omega_{\mathrm{ib}}^{\mathrm{b}}$

Valérie Renaudin@ - 13/10/2015 - IPIN, 2015 - Banff Canada

## Gyro. Main Operation Principles

- Spinning Mass
- Uses the principle of conservation of angular momentum
- Directions in inertial space are defined by bodies/particles rotating with constant momentum
- One example is the rotor gyro designed for stable platform
- Optical Gyros
- Uses Sagnac effect
- Based on relativistic principle that speed of light is conserved in rotating body
- Widely used in automotive applications
- Vibratory or Resonator Gyro
- Uses Coriolis principle
- An oscillating inertial body will preserve the plane of vibration even under rotation
- Angular rates are derived from rotating accelerometers to which a high frequency vibration is applied
- Primary choice for MEMS


## Accelerometer

- They are specific force sensors
- mesure the acceleration plus the gravity:

$$
f^{\mathrm{i}}=\ddot{x}^{\mathrm{i}}-g^{\mathrm{i}}
$$

- free fall: $\ddot{x}^{i}=-g^{i}$
- the gravitational acceleration needs to be removed from the accelerometer data prior to using it for inertial navigation

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## Acc. Main Operation Principles

- Force-rebalanced accelerometer
- These servo acc. restrain a proof of mass and measure the electrical current needed to supply the restoring force, which is proportional to the acceleration
- "standard" translational or pendulous design still used
- Vibratory accelerometer (MEMS)
- Measure the acc. as a frequency difference in a pendulous system
- Vibrating string acc., quartz resonator or integrated silicon acc.
- Not as accurate as the force-balanced acc.
- Electrostatic levitated accelerometer (MEMS)
- Position change of a suspended small element by electrostatic is sensed by a capacitance in a closed-loop servo system
- High performance acc.


## IMU Errors

- All sensors are affected by errors:
- deterministic \& stochastic
- Sensor assembly error linked to orthogonal tri-axis arrangement
- Sensor axis misalignment
- Non-orthogonality
- Nominal scale factor
- For the others, their behavior is described with statistical terms (stochastic processes)
- in run bias
- scale factor

- Inertial sensors performances vary a lot depending on the technology and the application
- The quality of inertial sensors depend on
- the accuracy
- the dynamic range
- the sensitivity


## Gyroscope Error Model

- A sample single axis gyroscope signal modeling is

$$
\omega(t)=b_{\omega}+S_{\omega} \omega(t)+C_{\omega}(t)+W_{\omega}(t)
$$

- $b_{\omega}$ is the turn on to turn on bias term
- $S_{\omega}$ is the scale factor error term
- $C_{\omega}(t)$ is the correlated noise term
- $W_{\omega}(t)$ is the white noise
- The correlated noise is for example described by a GaussMarkov process:

$$
\dot{C}_{\omega}(t)=\frac{-1}{\tau_{C_{\omega}}} C_{\omega}(t)+W_{C_{\omega}}(t)
$$

$-\tau_{C_{\omega}}$ is the correlation time

- $W_{C_{\omega}}(t)$ is the white noise


## Accelerometer Error Model

- A simple single axis accelerometer signal modeling is

$$
f(t)=b_{f}+S_{f} f(t)+C_{f}(t)+W_{f}(t)
$$

- $f(t)$ is the specific-force measurement
- $b_{f}$ is the turn on to turn on bias term
- $S_{f}$ is the scale factor error term
- $C_{f}(t)$ is the correlated noise term
- $W_{f}(t)$ is the white noise
- Allan variance analysis is often conducted to estimate the parameters of the noise stochastic processes (described in textbooks)


## Inertial Sensors Performances

| Sensor | Error | Tactical Grade | Consumer Grade |
| :---: | :---: | :---: | :---: |
| Gyro | Bias Stability | $0.01 \% / \mathrm{hr}$ | $15-100 \% \mathrm{hr}$ |
| Acc | Noise | $0.2-0.5^{\circ} / \mathrm{hr} / \mathrm{vHz}$ | $\mathrm{N} / \mathrm{A}$ |
|  | Bias Stability | 0.1 mg | $1-10 \mathrm{mg}$ |
| Noise | $0.2-0.4 \mathrm{mg} / \mathrm{vHz}$ | $\mathrm{N} / \mathrm{A}$ |  |
| Applications |  |  | Tactical Missile, <br> Automotive, $\ldots$ |

## INERTIAL NAVIGATION EQUATIONS



## Inertial Navigation Algorithm



## INS Equations: Position and Velocity

- Evolution of the velocity ( $\dot{\mathbf{x}}$ ) of the mobile in time

$$
\begin{aligned}
& -\forall u \in[t, \Delta t] \\
& -\dot{\mathbf{x}}_{t+\Delta t}^{\mathrm{n}}=\int_{t}^{t+\Delta t} \ddot{\mathbf{x}}^{\mathrm{n}} d u=\dot{\mathbf{x}}_{t}^{\mathrm{n}}+\ddot{\mathbf{x}}^{\mathrm{n}} \Delta t
\end{aligned}
$$

- Evolution of the position ( $\mathbf{x}$ ) of the mobile in time
- $\forall u \in[t, \Delta t]$
$-\mathbf{x}_{t+\Delta t}^{\mathrm{n}}=\int_{t}^{t+\Delta t} \dot{\mathbf{x}}^{\mathrm{n}} d u=\mathbf{x}_{t}^{\mathrm{n}}+\dot{\mathbf{x}}_{t}^{\mathrm{n}} \Delta t+\frac{1}{2} \ddot{\mathbf{x}}^{\mathrm{n}} \Delta t^{2}$
- With only an accelerometer bias error modeling
$-\ddot{\mathbf{x}}=\mathbf{f}-\mathbf{g}-\mathbf{b}_{f}+\mathbf{w}_{f}$
- $\mathbf{g}$ is known in local map frame and $\mathbf{f}$ measured in the body frame $\rightarrow$ orientation?


## INS Equations: Orientation

Body frame


## INS Equations: Quaternion

- Quaternion modeling of the rotation $\theta$ around the vector $\mathbf{u}$

$$
\mathbf{q}_{a}^{b}=\left(\cos \left(\frac{\theta}{2}\right), \sin \left(\frac{\theta}{2}\right) \mathbf{u}\right)
$$

- Multiplication in vector form

$$
\begin{aligned}
\left(0, \mathbf{x}^{b}\right)= & \left(\cos \left(\frac{\theta}{2}\right), \sin \left(\frac{\theta}{2}\right) \mathbf{u}\right) \circ\left(0, \mathbf{x}^{a}\right) \\
& \circ\left(\cos \left(\frac{\theta}{2}\right),-\sin \left(\frac{\theta}{2}\right) \mathbf{u}\right) \\
\left(0, \mathbf{x}^{b}\right)= & \mathbf{q}_{a}^{b} \otimes\left(0, \mathbf{x}^{a}\right) \otimes \overline{\mathbf{q}}_{a}^{b}
\end{aligned}
$$

- $\overline{\mathbf{q}}$ is the conjugate of $\mathbf{q}$


## INS Equations: Orientation

- Acceleration in the local frame

$$
-\left(0, \ddot{\mathbf{x}}^{\mathrm{n}}\right)=\mathbf{q}_{\mathrm{b}}^{\mathrm{n}} \circ\left(0, \ddot{\mathbf{x}}^{\mathrm{b}}\right) \circ \overline{\mathbf{q}}_{\mathrm{b}}^{\mathrm{n}}-\left(0, \mathbf{g}^{\mathrm{n}}\right)
$$

- Evolution of the attitude angles quaternion

$$
-\mathbf{q}_{\mathbf{b}}^{\mathrm{n}}(t+\Delta t)=\mathbf{q}_{\mathbf{b}}^{\mathrm{n}}(t) \circ \mathbf{q}_{\omega}^{\mathrm{b}}(t)
$$

- Relation between quaternion and angular rates

$$
-\mathbf{q}_{\omega}^{\mathrm{b}}(t)=\binom{\cos \left(\frac{\left\|\omega_{\mathrm{n} \|}^{\mathrm{b}}\right\|}{2} \Delta t\right)}{\sin \left(\frac{\left\|\omega_{\mathrm{nb}}^{\mathrm{b}}\right\|}{2} \Delta t\right) \frac{\omega_{\mathrm{nb}}^{\mathrm{b}} \Delta t}{\left\|\omega_{\mathrm{n} \mathrm{~b}}^{\mathrm{b}} \Delta t\right\|}}+\mathbf{w}_{q_{\omega}}^{\mathrm{b}}
$$

- With only a gyroscope bias error modeling

$$
-\boldsymbol{\omega}=\boldsymbol{\omega}+\mathbf{b}_{\omega}+\mathbf{w}_{\omega}
$$

## Impact of IMU errors

- Assuming a non-rotating earth and a single plane body dynamic
- a constant acc. bias error impacts the position (x) at time square rate: $\Delta t^{2}$
- a constant gyro. bias error will impact the position (x) at time cubic rate: $\Delta t^{3}$
- A correlated problem: azimuth errors are propagated in the horizontal velocity via the specific force
- Solutions consists in
- adopting aided navigation solution : GNSS, Map, Telecom signals, Opportunistic signals, ...
- estimating the instrument errors with augmented state equations


## Hybridization with GNSS signals

|  | Pros | Cons |
| :--- | :--- | :--- |
|  | Bounded errors | Lower attitude <br> accuracy |
| GNSS |  | Vulferable to <br> interference, <br> jamming |
|  | Self contained | Lower data rate <br> Unbounded <br> error growth |
| INS | Attitude <br> estimation <br> Higher data rate | Needs Initial <br> state is needed |


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## Zero Velocity Update

- Biomechanics features in walking gait captured by foot mounted IMU (widely adopted)

- Main principle: during the stance phase, the foot velocity equals zero: $\dot{\mathbf{x}}^{\mathrm{n}}=\mathbf{0}$
- Observation Equations
- $\delta$ is the perturbation of the state

$$
-\left[\begin{array}{c}
0 \\
\delta \dot{\mathbf{x}}^{\mathrm{n}}
\end{array}\right]=\mathbf{q}_{\mathrm{b}}^{\mathrm{n}} \circ\left[\begin{array}{ll}
0 & \left(\mathbf{f}^{\mathrm{n}}-\mathbf{b}_{\mathrm{f}}^{\mathrm{n}}\right)^{T}
\end{array}\right]^{T} \circ\left(\mathbf{q}_{\mathrm{b}}^{\mathrm{n}}\right)^{-1} \delta t+\left[\begin{array}{c}
0 \\
\mathbf{g}^{\mathrm{n}}
\end{array}\right] \delta t
$$

$$
-\left[\begin{array}{c}
0 \\
\delta \mathbf{x}^{\mathrm{n}}
\end{array}\right]=\dot{\mathbf{x}}^{\mathrm{n}} \delta t+\frac{\mathbf{q}_{\mathrm{b}}^{\mathrm{n}}}{2} \circ\left[\begin{array}{ll}
0 & \left(\mathbf{f}^{\mathrm{n}}-\mathbf{b}_{\mathrm{f}}^{\mathrm{n}}\right)^{T}
\end{array}\right]^{T} \circ\left(\mathbf{q}_{\mathrm{b}}^{\mathrm{n}}\right)^{-1} \delta t^{2}+\left[\begin{array}{c}
0 \\
\mathbf{g}^{\mathrm{n}}
\end{array}\right] \delta t^{2}
$$

- Following the same strategy, Zero Angular Rate Update has been proposed


## Mature Technologies ?

- With "body fixed" sensors
- on foot (smart insole), waist, trunk
- the closest to foot motion, the better
- Biomechanics for calibration
- Stance phase (Foot)
- Zero Velocity Update (ZUPT)
- Zero Angular Rate Update (ZARU)
- Trunk Roll Constraint
- Aiding
- Principal Building Directions
- Visual Odometry/Gyro
- Magnetometer Gradient



## Overview and motivation

## Background on strapdown inertial navigation system (INS)

The challenge of personal navigation with handheld device

Alternative positioning strategies

## conclusion

## Dead Reckoning with Handheld IMU



- Hand motion can hide global pedestrian locomotion
- "Strapdown" Mechanization cannot be applied
- Algo. (freely carried devices) can take several forms
- Sensors \& context dependent
- Common Assumption
- The user is watching the screen while walking
- 'body fixed' like case


## Strapdown INS with Handheld IMU

- Motion Lab
- Multi-Camera tracking system with optical markers
- Tree marker attached to the handheld IMU
- High-accuracy
- 60 Hz
- IMMU: inertial and magnetic mobile unit
- ADIS 16488



## Strapdown INS with Handheld IMU

- $5 \mathrm{~km} / \mathrm{hr}$ walk on a treadmill with texting and swinging hand


Swinging Mode


## Strapdown INS with "Texting" Hand



## Strapdown INS with "Texting" Hand



## Strapdown INS with "Texting" Hand



## Strapdown INS with "Swinging" Hand

Horizontal position estimation (Gylnt)


## Strapdown INS with "Swinging" Hand



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## Review of Alternative INS Strategies

- Biomechanics of human walking gait
- Repetitive steps
- Assumed symmetry between right and left step
- Upper body part contribute to the equilibrium
- Repetitive arm motion during the displacement
- Alternative processing strategies
- Different forms of algorithms (freely carried devices)
- Sensors \& context dependent
- Existing methods
- Classification of activity and sensor carrying modes
- Step/stride length modeling (no integration)
- Sensor calibration with opportunistic signal (artificial magnetic field) or motion (quasi-static acceleration)
- Hybridization with other sensors: camera, microphone, etc.



## Pedestrian Dead Reckoning



## Walking Direction



## Accurate Attitude Angles

- Accurate attitude estimation is limited primarily by gyroscopes errors which can be controlled by
- GNSS updates
- New sensor configuration
- Magnetometer
- Reducing the filter error propagation (quaternion space)
- New sensors
- Opportunistic IMU motion
- Unknown sensor orientation relative to body/user


## Error Modeling in Quaternion Set

- Differential equation?

$$
\mathbf{q}_{\mathrm{b}}^{\mathrm{n}}(t+\Delta t)=\mathbf{q}_{\mathrm{b}}^{\mathrm{n}}(t) \circ \cdot \mathbf{q}_{\omega}^{\mathrm{b}}(t)
$$

$$
\mathbf{q}_{\omega}^{\mathrm{b}}=\left[\begin{array}{c}
\cos \left(\frac{\left\|\omega_{\mathrm{nb}}^{\mathrm{b}}\right\|}{2} \Delta t\right) \\
\sin \left(\frac{\left\|\omega_{\mathrm{nb}}^{\mathrm{b}}\right\|}{2} \Delta t\right) \frac{\omega_{\mathrm{nb}}^{\mathrm{b}} \Delta t}{\left\|\omega_{\mathrm{nb}}^{\mathrm{b}} \Delta t\right\|}
\end{array}\right]
$$

- Angular rate error model

$$
\boldsymbol{\omega}_{\mathrm{nb}}^{\mathrm{b}}=\boldsymbol{\omega}+\mathbf{b}_{\omega}+\mathbf{w}_{\omega}
$$

- Error model in the quaternion set


## Magnetic Field Update

- When local magnetic field is constant over $\Delta t$ :
2 updates
- QSF: all $\mathbf{m}^{\mathrm{n}}$ are equal

- MARU: quaternions derived from the magnetic and gyroscope angular rates over $\Delta t$ are the same



## Acceleration Field Update

- When the acceleration is

Constant, over $\Delta t$ : 2 updates

- QSF: all an acc. are equal
- AGU (Acceleration Gradient Update): the quaternions derived from the gyroscope and the QSF acceleration should be the same

Renaudin et al., MAGYQ Based Attitude Estimation with Smartphone
Sensors for Indoor Pedestrian Navigation, Sensors, 2014.

## MAGYQ with "Texting" Hand


$\longrightarrow$ Inertial estimation MotionLab * Stride epochs • Stride epochs

## MAGYQ INS with "Texting" Hand



## MAGYQ INS with "Texting" Hand



## MAGYQ INS with "Swinging" Hand

Horizontal position estimation


## MAGYQ INS with "Swinging" Hand



## Human Gait Analysis



## Motion and Carrying Mode Recognition

## Input Space

 $X=\left[x_{1}, x_{2}, \ldots, x_{n}\right]$
## IMU Signal Features

## Decision Rule:

$X \rightarrow f(X) \rightarrow y_{k} \in Y$
mapping function

## Classifier

## Output Space

$$
y_{k \in\{1, m\}} \in Y=\left[y_{1}, y_{2}, \ldots, y_{m}\right]
$$

- Adapt the algorithms to the context to bound positioning error
- A classification problem
- Pre-processing $\rightarrow$ Feature extraction $\rightarrow$ Decision Making
- Motion states
- User: Standing, Running, Walking, Up/Down Stairs
- IMU/Hand: Phoning, Texting, Bag Carrying, Swinging, Irregular Motion


## Selecting Features

- Manifold features
- Energy
- Variance
- Standard deviation
- Frequencies in subbands
- STFT coefficients

- Pattern Extraction
- Faster Motion modes migrate the signal energy toward highest frequencies (acc. signal)
- Periodic arm rotation induce frequency peaks (gyro signals)

Susi et al., Motion Mode Recognition and Step Detection
Algorithms for Mobile Phone Users, Sensors, 2013.


## Step Frequency Extraction

- Estimated independently from step detection: remove correlation in the filter, more robust
- Extraction of dominant frequencies with Short Time Fourier Transform (STFT) over 2 sec. sliding window
- Three peaks
- Coupling problem of the strongest hand frequency with step or stride
- Binary Detector based on biomechanics feature of walking gait



## Defining a Model

- Experimental approach with controlled walking pace

$$
s=h\left(a f_{\text {step }}+b\right)+c
$$

- $s$ : step length
$-\{a, b, c\} \in \mathbb{R}$ : individual parameters set
$-h$ : the pedestrian's height



Renaudin et al., Step Length Estimation Using Handheld Inertial Sensors, Sensors, 2012.

## Evolutionary Gait



- Walking Gait influenced by varying physiological conditions tiredness, injuries, carrying a bag, ...
- Frequent calibration is needed
- Several approaches are possible depending on the application
- Walking along a known footpath
- Use departure / destination info
- Hybridization with opportune signal (GNSS, WiFi, etc.)


## Distance Estimation Performance

## Step Length Model



- Calibration using GNSS Doppler - 10 sec. PDR/GPS Doppler hybridization
- $2 \%$ mean error over 700 m with 4 test subjects with freely carried device (texting, swinging)



Renaudin et al., MAGYQ Based Attitude Estimation with Smartphone
Sensors for Indoor Pedestrian Navigation, Sensors, 2014.

## MAGYQ + PDR



## Estimating the Walking Direction



## Deformable Model

- Features extraction from the accelerations dataset, in navigation frame, over a step
- Fundamental assumptions
- $\not t \mathrm{t}$ : Pedestrian Gravity Center dynamic is observable
- $\not t 2$ : Acceleration in the navigation frame are unbiased



## Three Strategies

- Principal component analysis of the accelerations
- Algo: find the direction of the horizontal oscillations in the estimated acceleration
- $\mathcal{H}$ : constant misalignment over a step (even several)
- «Pattern Matching » on a reference acceleration signal signature in the forward and lateral directions
- $\mathcal{O l}$ lgo: minimize of the distance between the pre-determined shape and the estimated acceleration
$-\mathcal{A t}: \quad$ availability and validity of a universal model walking model
- Frequency analysis of inertial signals inspired by biomechanics
- Algo: find the direction of oscillations by using the periodicity of the human walking
- $d t$ : robust gait analysis is possible


## Common Elements

- Pre-processing
- Estimation of the IMU's attitude angles
- Estimation of the IMU's acceleration: removing the gravity component
- Biomechanics Outcomes
- The motion of the pedestrian's center of mass is cyclic
- Analysis can be conducted over several steps or stride



## Principal Component Analysis (PCA)

- Observations
- Variance of horizontal acc. is maximum along the forward direction
- Variance of horizontal acc. is minimum along the lateral direction
- Problem statement
- find the horizontal unit vector u that maximizes

$$
\max _{\|\mathbf{u}\|=1}\left(\sum_{i=1}^{n}\left\langle\mathbf{u}, \ddot{\mathbf{x}}_{H}(i)\right\rangle^{2}\right)
$$


over a $n$ samples step/stride

## Forward and Lateral Acc. Modeling (FLAM)

- Assumption
- Forward and Lateral acc. models over a stride/step exist

$$
\ddot{\mathbf{x}}_{m}(t)=\sum_{i=1}^{n} \ddot{\mathbf{x}}_{H} \sin \left(t b_{i}+c_{i}\right)
$$

- Problem statement
- Find $\theta$ that maximizes the correlation
$\max _{\theta} \sum_{i} \ddot{\mathbf{x}}_{m}(i)\left(\ddot{\mathbf{x}}_{H}^{T}(i)\left[\begin{array}{c}\cos \theta \\ \sin \theta\end{array}\right]\right)$
- Waking direction $\theta$ is the
 weighted sum of the 2 angles found for the 2 models


## Frequency analysis of Inertial Signals (FIS)

- Observation
- The energy of the signal is maximum along the forward direction at step/stride frequency
- Problem statement
- Find $\theta$ that maximizes the spectral density of the acc. and gyro. signals energy at step/stride frequency
- Acc. and gyro freq. and phase components $\ddot{\mathrm{X}}(\omega)$ and $\mathrm{W}(\omega)$ estimated by STFT
- Compute forward and lateral power spectral densities ( $P_{\ddot{\mathrm{X}}}, P_{\ddot{\mathrm{X}}}$ ) and ( $P_{\mathrm{Wf}}, P_{\mathrm{Wl}}$ )
$-\max _{\theta}\left(w_{1} P_{\ddot{\mathrm{x}}}(\theta)+w_{2} P_{\ddot{\mathrm{x}}}(\theta)+w_{3} P_{\mathrm{Wf}}(\theta)+w_{4} P_{\mathrm{Wl}}(\theta)\right)$




## Comparative Analysis

## IMU misalignment

- Overall experimental results in Motion Lab (see previous videos)
- Swinging mode : error < $10^{\circ}$
- Texting mode: mean error $<30^{\circ}$


PCA

- sensitive to oscillations FLAM
- need a large database
- IMU carrying mode dependent
- Person dependent (gender, weight, etc.)
FIS
- globally more robust
- Gat Analysis dependent
- Accuracy is not sufficient


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