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Gamma irradiation effects on morphology and properties of PHBV/PLA blends in presence of compatibilizer and Cloisite 30B

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ABSTRACT

The effects of gamma irradiation on the morphology and physical properties of various blends based on poly(3-hydroxybutyrate-*co*-3-hydroxyvalerate) (PHBV) and polylactide (PLA): 50/50 w/w were studied with and without PHBV-*g*-MA and organomodified montmorillonite used as the compatibilizer and reinforcement agent, respectively. The different blend compositions prepared by melt compounding were compression molded to thin films of an average thickness of 150 μ m, and subjected to 25, 50 and 100 kGy at room temperature; the dose rate being 1.0 Gy/h. Infrared spectra analysis indicated the occurrence of some chemical modifications in the irradiated samples, in particular an absorbed dose of 100 kGy resulted in the formation of a large absorption band in the carbonyl region. Size exclusion chromatography (SEC) data showed a decrease in the average molecular weight for all irradiated samples with increasing absorbed dose due to chain scission. Nanoindentation tests showed that γ -irradiation significantly decreased both modulus and hardness of neat PHBV and neat PLA after 100 kGy, whereas no noticeable changes were observed for PHBV/PLA blends. Thermogravimetric analysis (TGA) and pyrolysis combustion flow calorimetry (PCFC) tests revealed that the organomodified clay can act as a compatibilizer and compensate for the effect of irradiation on both thermal stability and fire retardancy of PHBV/PLA blends.

Keywords: PHBV PLA Polymer blends Gamma radiation Morphology Relationship structure/properties

1. Introduction

Plastics packaging is one of the biggest sectors of the polymer processing industry, with the food sector being its principal customer [1]. However, most synthetic polymers used for this application often have short service life, so they end up mostly in landfills. The non-biodegradability of such commercial plastics has caused many environmental problems associated with their disposal [2,3]. Due to their biodegradability and biocompatibility through non toxic intermediates, PHBV and PLA are considered as ideal candidates to replace non biodegradable polymeric materials for packaging applications [4]. Further, they can be processed in equipment commonly used for synthetic polymers. On the other hand, there has been significant interest in the gamma sterilization

* Corresponding author. E-mail address: stephane.bruzaud@univ-ubs.fr (S. Bruzaud). of polymers being used in some technological fields such as biomedical and food packaging to guarantee microbiological safety [5,6]. However, it is known that γ -irradiation may cause some undesirable effects on polymers [7]. Therefore, it becomes necessary to study the chemical and physical effects that are induced by the transfer of energy to the polymer [8]. Often, the occurrence of these effects makes the irradiated materials unsuitable for some applications. Indeed, several papers [9-12] reported that γ -irradiation of polymers generally produces simultaneous scission and crosslinking of the polymeric chains. The latter causes the formation of a macroscopic network, which reduces gas permeability and improves mechanical properties, whereas the former decreases mechanical properties, but increases the biodegradation rate. In this respect, considerable work has been published on oxidative degradation of PHBV or PLA under gamma irradiation at both higher and lower doses [13–18]. One of the significant conclusions that can be drawn from these publications is, in particular, the decrease in molecular weight of the irradiated polymers below

100 kGy due to chain scission, which occurs in the amorphous region and continues further to crystalline regions at higher doses. Melting point (T_m) and glass transition temperature (T_g) are reduced with increasing radiation dose, while the degree of crystallinity increases. The values of the surface potential of the irradiated biopolymers were higher in comparison with the non-irradiated samples. However, to the best of our knowledge, literature data dealing with γ -irradiation effects on polymer blends, in particular those based on PHBV/PLA, are rather scarce.

In this work, which is a continuation of previous ones devoted to the characterization properties of PHBV/PLA blends, and the methods for improving their compatibility and recycling [19–22], the assigned objective was to study the effects of γ -irradiation up to 100 kGy on the chemical structure, morphology and physical properties of blends based on PHBV/PLA: 50/50 w/w. Furthermore, the changes induced by γ -irradiation on the morphology and properties of PHBV/PLA blends were evaluated in the presence of 5 wt.% of PHBV-g-MA and 3 wt.% of Cloisite 30B used as compatibilizer and filler, respectively.

2. Experimental part

2.1. Materials used

PLA was supplied in pellets form by NatureWorks under the trade name 7001D. The polymer is semi crystalline having the following properties: density = 1.25 g/cm^3 , MFI = 6 g/10 min (210 °C, 2.16 kg), $T_g = 60 \text{ °C}$ and $T_m = 160 \text{ °C}$.

PHBV was manufactured by Tianan Biological Materials Co. Ltd. (China) and commercialized in pellets form under the trade name ENMAT Y1000P. According to the manufacturer, PHBV has the following properties: density = 1.25 g/cm^3 , $T_g = 8 \degree \text{C}$ and $T_m = 165 \degree \text{C}$. This grade has been comprehensively characterized in a recent paper [23].

Cloisite 30B (C30B) is an organically modified montmorillonite, which is commercially available and supplied by Southern Clay Products (Texas). C30B is a montmorillonite modified with bis-(2-hydroxyethyl)methyl tallow alkyl ammonium cations. C30B was dried under vacuum at 60 °C for at least 24 h before any use.

Maleic anhydride (MA) and dicumyl peroxide (DCP) were obtained from Sigma–Aldrich and used as received.

PHBV-g-MA was prepared by reactive extrusion in the laboratory according to the process previously described in the literature [21]. The MA content was 0.29 wt.%.

2.2. Sample preparation

Prior to use, all materials were dried under vacuum at 60 °C for 24 h. Drying was necessary in order to minimize the hydrolytic degradation of the polymers during melt processing. The samples of various blend compositions shown in Table 1 were prepared in an internal mixer according to the procedure previously described [21]. The mixing temperature, screw speed and residence time were set at 180 °C, 50 rpm and 8 min, respectively. The resulting materials were ground into pellets. Prior to compression molding, the pellets were dried under vacuum at 60 °C and compression molded in a Carver[®] hydraulic press at 180 °C under a pressure of 10 metric tons for 3 min to obtain films of about 150 µm of thickness.

2.3. Gamma irradiation test

Gamma irradiation was carried out on circular film samples of almost 20 cm diameter, placed in the 60 Co pilot irradiator at the Nuclear Research Center of Algiers (CRNA), Algeria. The samples were exposed to 25, 50 and 100 kGy at a dose rate of 1 Gy h⁻¹ in the

presence of air at room temperature.

2.4. Technical characterization

2.4.1. Fourier transform infrared spectroscopy (FT-IR)

FT-IR spectra of various film samples were recorded by an FT-IR spectrometer (Shimadzu 8400 M) using 4 cm⁻¹ resolution and 40 scans. All spectra were recorded in the absorbance mode in the 4000–400 cm⁻¹ region.

2.4.2. Molecular weight measurements by SEC

Size exclusion chromatography (SEC) was used to determine the evolution of molecular weight. The apparatus was equipped with a set of three columns: two ResiPore and one PLgel Mixed C (Polymer Labs.). The detection system was composed by a refractometer and a UV detector. Chloroform was used as an eluant with a flow rate of 0.8 mL/min. The elution profiles were analyzed by the Empower SEC module software (Waters). Calculations were based on calibration curves obtained from polystyrene standards ranging from 200 g/mol up to 6×10^6 . The weight-average molecular weight \overline{M}_w and number-average molecular weight \overline{M}_n were obtained from the SEC analysis. The polydispersity index (PDI) was calculated as the ratio of $\overline{M}_w/\overline{M}_n$.

2.4.3. Differential scanning calorimetry (DSC)

DSC analyzes were performed on weighted samples of about 10 mg, using a Mettler-Toledo DSC-882 equipment. The samples were subjected to two heating and cooling ramps starting from $-40 \,^{\circ}$ C up to $+200 \,^{\circ}$ C and down to $-40 \,^{\circ}$ C with a scanning rate of 10 $\,^{\circ}$ C min⁻¹ under nitrogen atmosphere. In the first run, the samples were heated from $-40 \,^{\circ}$ C for 2 at a rate of 10 $\,^{\circ}$ C/min. After keeping the temperature at 200 $\,^{\circ}$ C for 2 min, the samples were rapidly quenched to $-40 \,^{\circ}$ C. In the second run, they were heated at a rate of 10 $\,^{\circ}$ C/min to $+200 \,^{\circ}$ C. From DSC thermograms, thermal characteristics, i.e. crystallization temperature (T_c), cold crystallization enthalpy (Δ H_c), melting temperature (T_m) and melting enthalpy (Δ H_m) were determined.

2.4.4. Thermogravimetric analysis (TGA)

TGA experiments were carried out in a thermal analyzer (Setaram TG/DTA 92-10) using a heating rate of 10 °C min⁻¹ under nitrogen atmosphere, between 20 and 600 °C. The average sample mass was almost 10 mg.

2.4.5. Nanoindentation test

Nanoindentation testing involves the contact of an indenter on a material surface and its penetration into it to a specified load or depth. In this study, a flattened conical indenter was used. This geometry is well suitable to nanocomposites due to the high contact surface, generally inducing results with a low spread. Both the nanoindentation principle and method used to determine hardness and elastic modulus were described in previous work [24].

2.4.6. Scanning electron microscopy (SEM)

Morphological changes were observed using a Jeol JSM-6031 scanning electron microscope (SEM) to examine the fracture surface of the film samples. The neck region for the broken specimens fractured in liquid nitrogen is parallel to the draw direction in order to reveal the internal morphology. Prior to observation, the fracture surface was coated with a thin gold layer by means of a polaron sputtering apparatus.

2.4.7. Pyrolysis combustion flow calorimeter (PCFC)

Pyrolysis combustion flow calorimeter apparatus from FTT (UK)

Table 1

Molecular weight changes as a function of absorbed doses for neat PHBV, neat PLA and various PHBV/PLA blends determined by SEC analysis.

Samples	Absorbed dose (kGy)	\overline{M}_w (g mol ⁻¹)	\overline{M}_n (g mol ⁻¹)	$\overline{M}_w/\overline{M}_n$
PHBV	0	231,500	153,600	1.60
	50	102,900	65,100	1.57
	100	62,300	40,000	1.55
PLA	0	174,500	105900	1.64
	50	66,500	49,800	1.33
	100	39,300	29,800	1.32
PHBV/PLA (50/50)	0	188,600	128,700	1.46
	50	72,700	50,800	1.43
	100	39,900	26,500	1.50
PHBV/PLA/C30B (50/50/3)	0	176,200	123,500	1.20
	50	68,300	46,700	1.46
	100	42,100	30,000	1.40
PHBV/PLA/C30B/PHBV-g-MA (50/50/3/5)	0	102,300	74,100	1.38
	50	75,200	51,500	1.46
	100	54,700	36,500	1.49

was used to pyrolyze 3 ± 1 mg of sample by heating up to 900 °C at a rate of 1 °C s⁻¹ under a nitrogen flow. The gases released during pyrolysis were sent into a combustor and burnt at a temperature of 900 °C in the presence of oxygen (20%). Peak heat release rate (PHRR) and heat release rate (HRR) of samples were noted and each measurement was performed at least five times (up to ten times). The results were averaged with an error of less than 5%, while the error on temperature of PHRR (T_{PHRR}) measurement is less than 1%. The gases produced at temperature of PHRR observed during the PCFC test were analyzed.

3. Results and discussion

3.1. FT-IR spectra analysis

The material usefulness depends on its durability in the environment in which it is used, and also its interactions with environmental factors. The changes in the chemical structure induced by γ -irradiation exposure of neat polymers and PHBV/PLA blend (50/50 w/w) in the absence and presence of C30B and PHBV-g-MA were analyzed by FT-IR spectroscopy. Representative FT-IR spectra of non-irradiated and irradiated PHBV/PLA/C30B samples with the compatibilizer after absorbed dose of 25 and 100 kGy, and recorded in the hydroperoxide and carbonyl regions are shown in Fig. 1a and b, respectively. From Figs. 1(a), 2(a), 3(a) and 4(a), FT-IR spectrum of the non-irradiated sample exhibits large absorption bands centered at 3503 and 3438 cm⁻¹, which correspond to the hydroperoxide groups probably resulting from the thermal degradation of the polymer blends during melt processing. After γ-irradiation exposure, the bands become stronger in intensity as the absorbed doses increase. In the region 1900–1500 cm^{-1} shown in Fig. 1(b) 2(b), 3(b) and 4(b), which is relative to the carbonyl region, significant changes in the chemical structure have occurred in irradiated samples, especially at 100 kGy. Indeed, at this absorbed dose, the disappearance of the main absorption bands localized at 1779 and 1708 cm⁻¹ characteristic of the neat polymers is observed. The formation of a large absorption band involving various carbonyl products, derived from samples irradiated up to 100 kGy is seen at 1779, 1746 and 1698 cm⁻¹, which correspond to peresters, esters and carboxylic groups, respectively. This indicates that γ -irradiation of the compatibilized PHBV/PLA/C30B leads to oxidation reactions of ester groups resulting in the formation of hydroxyl groups contained in hydroperoxides, carboxylic acids and alcohols [25]. The amount of each species depends on the radiation dose, especially for the concentration of carboxylic groups, which are predominant when the dose is equal to 100 kGy. Similar conclusions can be deduced for with neat polymers, i.e. PHBV and PLA.

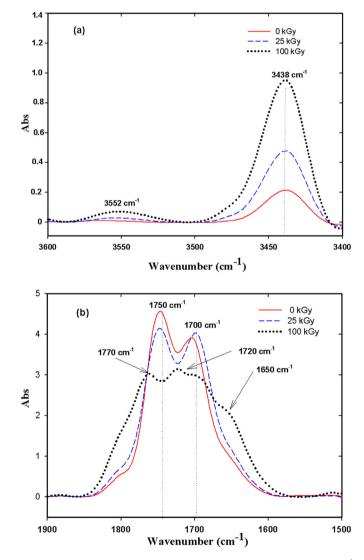


Fig. 1. FT-IR spectra of neat PHBV at various $\gamma\text{-radiation}$ doses: (a) 3600–3400 cm^{-1} and (b) 1900–1500 cm^{-1} .

3.2. Molecular weight changes by SEC

The values of $\overline{M}_w, \overline{M}_n$ and PDI determined by SEC analysis at 50 and 100 kGy for neat PHBV, neat PLA and PHBV/PLA blends, with

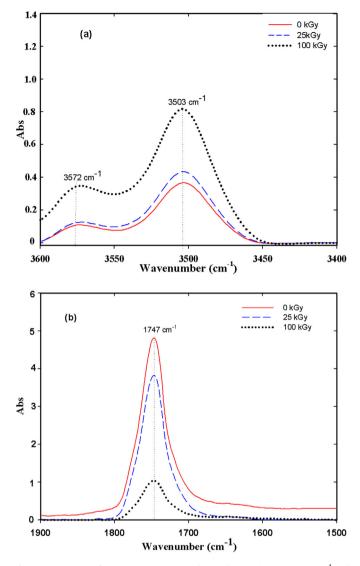


Fig. 2. FT-IR spectra of neat PLA at various γ -radiation doses: (a) 3600–3400 cm $^{-1}$ and (b) 1900–1500 cm $^{-1}$.

and without compatibilizer and C30B, are reported in Table 1. It is observed that the average molecular weight of the whole irradiated samples logically decreases with increase of absorbed dose due to degradation. Indeed, after 50 and 100 kGy, \overline{M}_w of neat PHBV decreases by almost 55 and 73% compared to that of non-irradiated sample, respectively. Further, the significant decrease in both \overline{M}_w and \overline{M}_n of irradiated PHBV samples coupled with a slight increase in the PDI values is an indication of the dominance of chain scission mechanism. A similar trend is also observed for \overline{M}_w and \overline{M}_n of PLA, whose values shift toward smaller ones.

On the contrary, the results reported in Table 1 for PHBV/PLA blend indicate a quasi-stability of the average molecular weight up to the absorbed dose of 50 kGy. This may be explained as a result of some chemical interactions which probably occur between PHBV and PLA to form stronger bonds. In fact, it has been reported in the literature [7,13,14] that, during γ -irradiation exposure of PHBV and PLA, different types of radicals are formed by chain scission, which may lead to some reactions such as transfer or chain recombination occurring separately or simultaneously in the two polymers. However, from 50 to 100 kGy, a significant reduction in both \overline{M}_w and \overline{M}_n is observed. Table 1 also indicates that the incorporation of C30B in PHBV/PLA blend slightly decreases \overline{M}_w and \overline{M}_n compared to

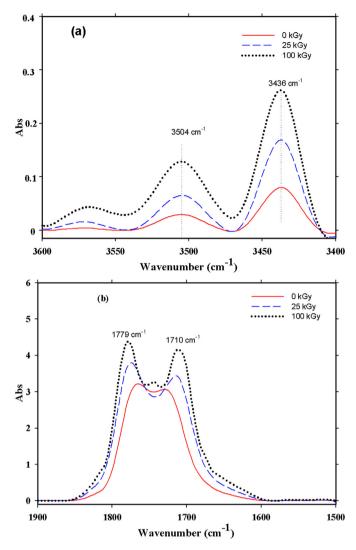


Fig. 3. FT-IR spectra of PHBV/PLA (50/50) blend at various γ -radiation doses: (a) 3600–3400 cm^{-1} and (b) 1900–1500 cm^{-1}.

unfilled material, before γ -irradiation exposure. This is generally attributed to the effects of both shear mixing of PHBV/PLA blend and C30B, resulting in hydrolysis of the two polymers, and also the relatively high processing temperature (180 °C) [7]. At absorbed dose of 50 kGy, PHBV/PLA/C30B samples exhibit more than 60% decrease in both \overline{M}_w and \overline{M}_n compared to non-irradiated ones. This important decrease in molecular weight may be explained as a result of chain scission mechanism, which takes place in the amorphous regions of the two polymers. The addition of 5 wt.% of PHBV-g-MA to PHBV/PLA/C30B induces a large decrease (~40%) in both \overline{M}_w and \overline{M}_n , due probably to the low molecular weight of the compatibilizer. However, at absorbed doses of 50 and 100 kGy, the decrease in both \overline{M}_w and \overline{M}_n of compatibilized PHBV/PLA/C30B is relatively smaller than the uncompatibilized samples. This counterbalancing effect of PHBV-g-MA compatibilizer may be the result of several factors, among them, the reduction of interfacial tension of the system due to increased interfacial interactions between the blend components, and also the localization of the clay in the blend due to the chemical linkage.

3.3. Thermogravimetric analysis (TGA)

The effects of gamma irradiation on the thermal stability of neat

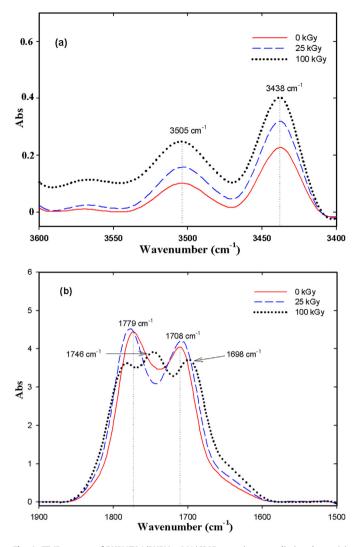


Fig. 4. FT-IR spectra of PHBV/PLA/PHBV-g-MA/C30B at various γ -radiation doses: (a) 3600–3400 cm^{-1} and (b) 1900–1500 cm^{-1}.

PHBV, neat PLA and various PHBV/PLA blends in the presence of both C30B and PHBV-g-MA compatibilizer are shown in Table 2, where the degradation temperature values determined at $T_{5\%}$, $T_{10\%}$, $T_{50\%}$ and the % residue are given at 100 kGy.

From Table 2, it clearly appears that, up to 100 kGy, the effect of gamma irradiation is almost negligible for neat PHBV and PHBV/PLA blends. Only, PLA was significantly affected since $T_{5\%}$ and $T_{10\%}$ were decreased by almost -21 and -12 °C, respectively, after 100 kGy.

On the other hand, the incorporation of C30B in PHBV/PLA blend

leads to an increase inT_{5%}, T_{10%} and T_{50%} of the blend material by almost 10, 9 and 8 °C, respectively. As expected, this result is due to the presence of inorganic layered silicates in PHBV/PLA blends, which restrict the diffusion of volatile degradation products throughout the nanocomposite materials, thus counterbalancing the degradation effect. The data given in Table 2 show clearly that the values of T_{5%}, T_{10%} and T_{50%} of PHBV/PLA/C30B corresponding to 286, 291 and 320 °C, respectively remain almost unchanged after absorbed dose of 100 kGy. This indicates the good thermal stability of PHBV/PLA/C30B compared to unfilled material. Moreover, the addition of PHBV-g-MA to PHBV/PLA/C30B has no noticeable effect on the thermal stability.

3.4. Thermal analysis by DSC

Further information about changes in the crystallinity as well as the thermal characteristics induced by γ -irradiation exposure of the samples was obtained by DSC. In this respect, Fig. 5 displays the DSC thermograms of neat polymers, i.e. PHBV and PLA, and also those of PHBV/PLA blends (50/50 w/w) before exposure and after 100 kGy. The values of thermal characteristics at absorbed dose of 25 and 100 kGy are also shown in Table 3. Before γ -irradiation, DSC thermograms of neat PHBV and neat PLA display one single melting peak at approximately 171 and 150 °C, respectively. As expected, DSC thermogram of PHBV/PLA blend shows the presence of two melting peaks at about 150 and 169 °C, which correspond to those of neat polymers, i.e. PLA and PHBV, respectively. In addition, it can be also observed that all thermal characteristics, i.e. T_c , T_{cc} , ΔH_c , ΔH_{cc} , T_m and ΔH_m of PHBV/PLA/C30B nanocomposites slightly shift to lower values by γ -irradiation exposure. This is attributed to a decrease in the arrangement of PHBV and PLA polymer chains due to the presence of C30B in the blend material [7].

After 100 kGy, the DSC thermograms of all irradiated samples exhibit double peak endotherms when compared to the non irradiated ones having a single peak. According to the literature [18], the formation of a secondary melting peak could be the result of the polymer chains re-organization during γ -irradiation and also the occurrence of different crystal populations with different lamellar thickness. Furthermore, for all irradiated samples the melting peaks shift to lower temperatures and become broader with increased absorbed dose. The decrease in T_m with absorbed dose is attributed to the formation of polymer chains with lower molecular weight. Besides this, T_c shifts to lower temperatures, while ΔH_c slightly decreases with increasing the radiation dose. T_{cc} becomes much sharper and shifts to a lower temperature, indicating a higher crystallization rate in the irradiated samples resulting from chain segments formation. The lower molecular weight resulting from the chain scission is a precondition for the increase of the mobility of macromolecules which reinforces their potential for reorganization and crystallization at a lower temperature [26–28].

Table 2

Values of degradation temperature at T_{5%}, T_{10%}, T_{50%} and char yield at 600 °C of neat PHBV, neat PLA and various PHBV/PLA blend samples before and after 100 kGy of irradiation determined by TGA.

Samples	Absorbed dose (kGy)	T _{5%} (°C)	T _{10%} (°C)	T _{50%} (°C)	Char yield (%)
PHBV	0	267	273	286	1.3
	100	262	271	283	1.2
PLA	0	332	341	362	0.2
	100	311	329	361	0.3
PHBV/PLA	0	276	2	312	0.5
	100	271	272	301	0.5
PHBV/PLA/C30B	0	286	291	320	2.7
	100	284	289	317	2.6
PHBV/PLA/C30B/PHBV-g-MA	0	286	290	315	2.7
	100	282	287	310	2.6

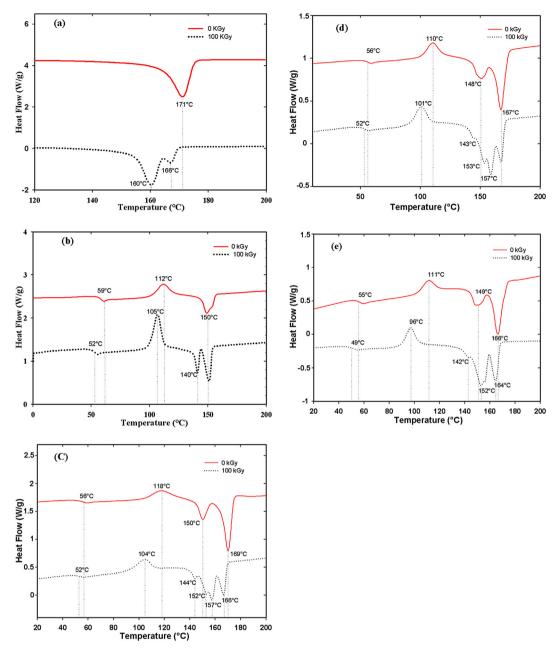


Fig. 5. DSC thermograms of neat PHBV (a), neat PLA (b), PHBV/PLA blend (c), PHBV/PLA/C30B (d) and PHBV/PLA/PHBV-g-MA/C30B (e), before and after 100 kGy of irradiation.

Table 3
Thermal characteristics for neat PHBV, neat PLA and various PHBV/PLA blends before and after absorbed doses of 25 and 100 kGy determined by DSC.

Samples	Doses (kGy)	$T_{c,PHBV}$ (°C)	$\Delta H_{c, PHBV} (J/g)$	$T_{cc,PLA}$ (°C)	$\Delta H_{cc, PLA} (J/g)$	T _m (°C)	$\Delta H_m \left(J/g \right)$
PHBV	0	118	92	_	_	171	103
	25	114	103	-	-	166	108
	100	114	104	-	-	160-166	115
PLA	0	-	-	112	24	150	24
	25	-	-	111	34	145-150	34
	100	-	_	107	41	140-150	46
PHBV/PLA	0	118	47	118	16	150-169	64
	25	116	44	110	17	147-155-165	67
	100	111	40	104	20	144-152-157-166	73
PHBV/PLA/C30B	0	116	36	110	12	148-167	61
	25	114	43	109	16	147-155-165	67
	100	112	44	101	18	143-153-157-167	70
PHBV/PLA/OMMT/PHBV-g-MA	0	115	38	112	15	149-166	56
	25	115	43	108	17	147-155-165	68
	100	112	48	97	19	142-152-155-164	71

3.5. Morphological analysis by SEM

13kU

Fig. 6(a) and (b) show SEM micrographs of the fracture surface of neat PHBV before and after absorbed dose of 50 kGy, respectively, at a magnification of 2000. In Fig. 6(a), before gamma irradiation exposure, the morphology of neat PHBV shows an irregular fracture surface due to its crystalline structure. However, at absorbed dose of 50 kGy, the fracture surface of neat PHBV in Fig. 6(b), exhibits some irregularities and defects as a result of degradation. In Fig. 6(c), corresponding to non-irradiated PLA, it is observed that the sample displays no significant defects on the fracture surface. After 50 kGy (Fig. 6(d)), the fracture surface of irradiated PLA sample exhibits a few irregularities exhibiting less damage compared to that of neat PHBV. For PHBV/PLA blends shown in Fig. 6(e), the SEM micrograph exhibits separated phase morphology between PHBV and PLA with poor adhesion at interfaces [19]. The separated phase morphology indicates immiscibility between the two biopolymers. Indeed, PLA domains appear as beads in PHBV matrix, whose size and distribution are very irregular. At absorbed dose of 50 kGy, the fracture surface of PHBV/PLA blend illustrated in Fig. 6(f) shows an homogeneous distribution of PLA in PHBV matrix with a reduction in domain size of PLA. This result is interesting since it clearly indicates that γ -irradiation may promote and enhance the compatibility between PHBV and PLA. This enhancement in the compatibility between the two components of the blend without any compatibilizer may be induced by the chemical modifications due to the degradation and previously highlighted using FT-IR.

Fig. 6(g) shows the fracture surface of PHBV/PLA blend reinforced with 3 wt.% of C30B in the presence of PHBV-g-MA compatibilizer before γ -irradiation. The SEM micrograph shows that the addition of PHBV-g-MA and C30B improves the interfacial

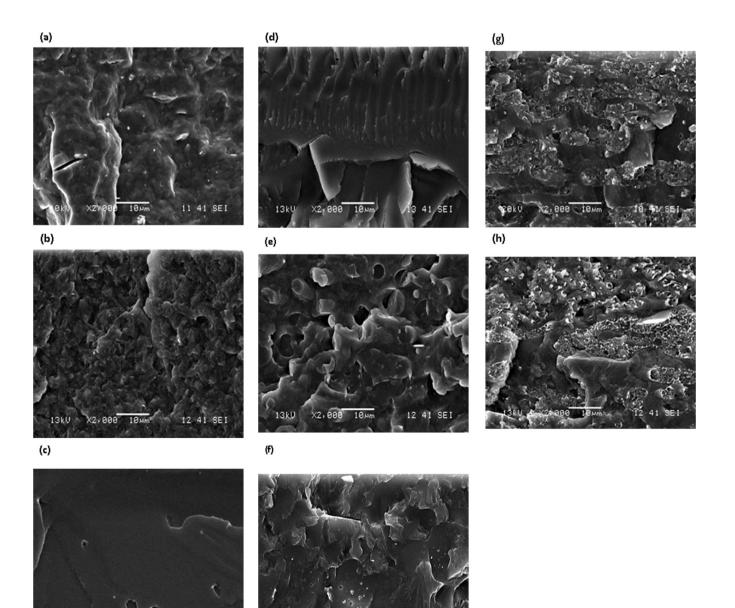


Fig. 6. SEM micrographs of fractured surface of: PHBV (a): 0 kGy and (b): 50 kGy; PLA (c): 0 kGy and (d): 50 kGy; PHBV/PLA blend (e): 0 kGy and (f): 50 kGy; PHBV/PLA/PHBV-g-MA/C30B (g): 0 kGy and (h): 50 kGy.

20kU

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adhesion and the miscibility between PHBV and PLA. After absorbed dose of 50 kGy, the fracture surface of the irradiated sample shown in Fig. 6(h), remains almost the same as the non-irradiated one, despite the presence of a few surface irregularities, which may be probably attributed to an increase in the crystallinity of the irradiated sample.

3.6. Nanoindentation measurements

Table 4 reports the values of nanoindentation modulus and hardness measured for neat PHBV, neat PLA and PHBV/PLA blends in the presence of both C30B and PHBV-g-MA compatibilizer before and after the absorbed dose of 100 kGy. The values are averaged for indentation depths of 1200–1500 nm from a minimum of 64 indents. A Poisson's ratio of 0.35 was used in all modulus calculations [29].

The data provided in Table 4 indicate a very large decrease in both nanoindentation modulus and hardness for neat PHBV and neat PLA after 100 kGy. Indeed, the value of nanoindentation modulus of PHBV and PLA decreases by almost 67 and 45%, respectively, after 100 kGy. This may be explained as being a result of the significant reduction in both \overline{M}_w and \overline{M}_n due to chain scission mechanism. This is in agreement with the literature data [30].

For unexposed PHBV/PLA blends, the expected nanoindentation modulus and hardness, being intermediate between PHBV and PLA could be noted; moreover, a slight increase of the mechanical properties is logically highlighted for the C30B loaded blends. Interestingly, for PHBV/PLA blends, no significant change in the values of modulus and hardness was observed after the absorbed dose of 100 kGy compared with the non-irradiated samples. Indeed, only 8% decrease is obtained in the modulus of PHBV/PLA blend after 100 kGy, while the hardness decreases by almost 11% compared to the non-irradiated sample. Furthermore, one can observe that the values of modulus and hardness remain almost unchanged for all PHBV/PLA blends and seem to be not affected by the presence of either C30B or PHBV-g-MA compatibilizer. This indicates that local mechanical properties of PHBV/PLA blends are stable to γ -irradiation exposure up to 100 kGy, evidencing a morphological effect. In this case, the decrease into the molecular weight, being penalizing for the nanoindentation properties, is positively counter-balanced by both the PHBV/PLA compatibility and crystallinity increase after the irradiation exposure.

3.7. Flammability properties by PCFC

The pyrolysis combustion flow calorimeter (PCFC) is a relevant tool for assessing the flammability of fire retardant polymers at a microscopic scale [31]. PCFC experiments were performed in order to evaluate the fire retardant mechanism of filled blends versus unfilled ones and irradiated films versus non-irradiated ones. As observed for TGA data in Table 2, the temperature of the peak of Heat Release Rate (TpHRR) is lower for PHBV in comparison with that of PLA. PHBV releases a higher amount of heat (THR) in comparison with PLA. For the blends, an intermediate value of THR is obtained. Moreover, it can be noted that PCFC plots of all PHBV/PLA blends exhibit two HRR peaks corresponding, respectively, to the degradation of each polymer. For the unfilled blend, TpHRR of PHBV is increased while TpHRR of PLA is decreased, which tends to suggest the formation of copolymers during the mixing stage or during the pyrolysis.

The incorporation of C30B tends to improve mainly the fire behavior of PHBV since only TpHRR of PHBV is increased. Nevertheless, a decrease of the two pHRR peaks and THR is seen which shows the effect of the organomodified clay. These effects are more pronounced in the presence of PHBV-g-MA which allows better dispersion of C30B to delay the emission of volatile combustibles.

The influence of irradiation on the parameters of pure polymers seems only significant for the pHRR of PLA, which is lowered.

In the unfilled blend, TpHRR does not vary clearly as a function of the absorbed dose. Conversely, pHRR values for each polymer present contrasted evolutions when the dose increases. pHRR for PHBV tends to increase, suggesting the formation of new macromolecular structures from both polymers due to irradiation. Also, at the maximum dose of 100 kGy, the THR value seems close to that of pure PHBV. All these results tend to indicate that the new macromolecular structures formed behave like PHBV and lower the fire reaction of the blend.

Fortunately, the incorporation of C30B alone or in combination with the compatibilizer seems to create a barrier effect to the volatile combustible release through better dispersion of silicate sheets and strong interfacial adhesion. From Table 1, it appears that the influence of radiations on chain scission is reduced due to the silicate dispersion, so the nanostructure can be maintained at higher temperature. Whatever the level of irradiation, the two pHRR are reduced in comparison with these of unfilled and nonirradiated blend. Moreover, the THR values at 100 kGy for the filled blends (with and without PHBV-g-MA) are similar as those of the unfilled and non-irradiated blend. Consequently, good compatibilization owing to the presence of the organomodified clay can compensate the effect of irradiation on fire retardancy of PHBV/PLA blends (Table 5) (Fig. 3).

4. Conclusions

From this study, it can be concluded that the effects of γ -irradiation on PHBV/PLA: 50/50 w/w blends resulted in strong modifications in the chemical structure, especially after 100 kGy of absorbed dose. Indeed, carbonyl products were formed during degradation, which was responsible for the decrease in the average molecular weight of all irradiated samples due to the chain scission mechanism, being much more pronounced for the neat polymers, i.e. PHBV and PLA. However, thermal stability as well as modulus

Table 4

Values of modulus and hardness of PHBV, PLA and various PHBV/PLA blends before and after 100 kGy of irradiation measured by nanoindentation.

Samples	Absorbed dose (kGy)	Modulus (GPa)	Hardness (GPa)
PHBV	0	6.3 ± 0.5	0.22 ± 0.02
	100	2.1 ± 0.8	0.05 ± 0.01
PLA	0	4.3 ± 1.1	0.11 ± 0.03
	100	2.4 ± 0.9	0.08 ± 0.05
PHBV/PLA	0	5.3 ± 0.4	0.23 ± 0.03
	100	5.1 ± 0.5	0.21 ± 0.02
PHBV/PLA/C30B	0	5.5 ± 0.7	0.21 ± 0.04
	100	5.9 ± 0.8	0.24 ± 0.04
PHBV/PLA/C30B/PHBV-g-MA	0	5.5 ± 0.9	0.20 ± 0.04
0	100	5.6 ± 0.5	0.19 ± 0.03

Table 5

TpHRR, pHRR and THR from PCFC tests of neat PLA, PHBV/PLA blend and PHBV/PLA/C30B/PHBV-g-MA before and after γ-irradiation.

Samples	Absorbed dose (kGy)	TpHRR (°C)	pHRR (W/g)	THR (KJ/g)
PHBV	0	293.3 ± 6.4	963 ± 077	20.0 ± 0.2
	25	291.5 ± 0.7	996 ± 022	19.2 ± 0.1
	50	295.0 ± 5.6	896 ± 102	19.9 ± 0.6
	100	293.7 ± 6.7	949 ± 138	20.2 ± 0.9
PLA	0	370.5 ± 2.1	494.5 ± 62	15.0 ± 0.2
	25	373.5 ± 6.4	431.5 ± 13	14.6 ± 0.1
	50	374.5 ± 3.5	428.5 ± 10	14.8 ± 0.1
	100	372.0 ± 4.2	433.5 ± 05	16.4 ± 0.3
PHBV/PLA	0	299/375	208/436	17.5 ± 0.4
	25	298/372	202/431	17.2 ± 0.6
	50	297/370	187/430	16.8 ± 0.6
	100	295/367	130/320	19.0 ± 0.6
PHBV/PLA/C30B	0	307/374	195/372	16.5 ± 0.4
	25	306/369	183/367	16.4 ± 0.4
	50	309/376	171/350	18.3 ± 0.9
	100	310/375	169/346	17.8 ± 0.1
PHBV/PLA/C30B/PHBV-g-MA	0	306/367	201/344	16.1 ± 0.9
	25	309/376	188/345	16.5 ± 0.5
	50	309/374	170/371	16.0 ± 0.3
	100	305/371	177/355	17.0 ± 0.1

and hardness of PHBV/PLA blends remained almost unchanged during γ -irradiation test, and enhancement of these properties was observed in the presence of C30B and PHBV-g-MA. Indeed, SEM data confirm the morphological stability of PHBV/PLA/C30B/PHBV-g-MA after 50 kGy compared to non-irradiated material. These results clearly demonstrate that, up to 100 kGy, such blend materials are stable and may have some potential applications considering that the regular doses for food irradiation are lower than 10 kGy, and for packaging sterilization the doses are lower than 25 kGy.

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