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Article Performance analysis of LDS Multi Access Technique and New 5G waveforms for V2X Communication

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- Abstract: Low Density Signature (LDS) is an emerging non-orthogonal multiple access (NOMA)
- ² technique that has never been evaluated under a vehicular channel in order to simulate the
- ³ environment of a V2X communication. Moreover, the LDS structure has been combined with
- only Orthogonal Frequency Division Multiplexing (OFDM) and Filter-Bank Multi-Carrier (FBMC)
- waveforms to improve its performances. In this paper, we propose new schemes where the LDS
- ⁶ structure is combined with Universal Filtered Multi-Carrier (UFMC) and Filtered-OFDM waveforms
- ⁷ and the Bit Error Rate (BER) is analysed over a frequency selective channel as a reference and over a
- ⁸ vehicular channel to analyse the effect of the Doppler shift on the overall performance.

• Keywords: V2X, LDS-F-OFDM, LDS-UFMC, EVA channel model

10 1. Introduction

Vehicular communications have recently caught a lot of attention in the research community 11 thanks to the advantages that can provide the overall vehicular experience. In fact, several technologies 12 have provided the requirements for this type of communication. Connected to the Infrastructure 13 (V2I), to another vehicle (V2V) or to a pedestrian (V2P), the vehicle to everything (V2X), as referred 14 to, is a new solution for road users to enhance safety and improve the traffic efficiency. The Long 15 Term Evolution (LTE) as a widely deployed infrastructure is proposed to be extended in order to 16 support the V2X services, namely the LTE-based V2X [1]. The 3rd Generation Partnership Projet 17 (3GPP) Release 14 is an evolutionary standard that is dedicated to the LTE-based V2X and published 18 on September 2016 defining two new modes, mode 3 and mode 4 [2][3]. In mode 3, the radio resource 19 is managed by the cellular network consequently vehicles can only communicate under a cellular 20 coverage. Meanwhile in mode 4, the radio resource is managed autonomously by the vehicle itself for 21 the direct V2V communication overcoming the coverage limitation of mode 3. However, LTE-based 22 V2X standard suffers from severe performance degradation in a high density environment - it doesn't 23 allow a high number of users to access to the network. In addition, LTE-based V2X is based on Single 24 Carrier Frequency Divison Multiple Access (SC-FDMA) which requires high complexity equalizers. 25 The ITS-G5 is another standard that is introduced by the European Telecommunications Standards 26 Institute (ETSI) and operates in 5 GHz frequency band [4]. The main advantage of ITS-G5 is its low latency, the short transmission delay is due to the fact that data is being transferred directly between 28 neighbors. However, in best case scenarios, ITS-G5 has a short range of 1 km and is extremely sensitive 29 to dense environment which reduces the total throughput and increases the end-to-end latency. Similar 30 to the IEEE 802.11p US standard, both LTE-based V2X and ITS-G5 rely on OFDM on PHY layer, while 31 maintaining the subcarriers orthogonality could be challenging in the vehicular environment leading to a high BER. This is why the 5G cellular network can be a promising technology to support the 33 vehicular communications [5], namely New Radio-V2X (NR-V2X). 34

The 3GPP Release 16 defines the first specifications for NR-V2X sidelink where it supports 35 subcarrier spacings of 15, 30, 60 and 120 kHz. Their associations to Cyclic Prefix (CPs) and frequency 36 ranges are as for NR Uplink/Downlink (UL/DL), but using only the CP-OFDM waveform. The 37 modulation schemes available are Quadrature Phase Shift Keying (QPSK), Quadrature Amplitude 38 Modulation 16-(QAM), 64-QAM, and 256-QAM [6]. Meanwhile, another study has been published for 39 NOMA signature candidates [7] proposing some of the main technologies such as Interleaver Division 40 Multiple Access (IDMA) [8][9][10], Pattern Division Multiple Access (PDMA) [11][12] and Sparse Code 41 Multiple Access (SCMA) [13][14]. However, for V2X communication, no specifications invoke NOMA. As an efficient multiple access technique, we have chosen to modulate LDS and analyse its 43 performances under a vehicular channel for V2X communication. Its sparse structure enables each user 44 to spread its data over a small subset of subcarriers, which means that a single subcarrier will support 45 only a small number of users or symbols, hence reducing the multiuser interference (MUI). Firstly, it is 46 proposed in [15] for a Code Division Multiple Access (CDMA) system and proves that it can afford 47 a high system overload with affordable complexity. To improve its performances, LDS is enhanced 48 by combining it with OFDM [16] to apply the spreading over OFDM subcarriers and evaluate over a 49 frequency selective channel. Furthermore, the LDS has been recently combined with FBMC[17] and a 50 joint sparse graph receiver combing pulse shaping property, NOMA and channel coding is proposed to 51 improve the overall result at the cost of very high complexity. Although LDS-OFDM and Joint Sparse 52 Graph - Isotropic Orthogonal Transfer Algorithm (JSG-IOTA) have shown improved performance 53 evaluation, these schemes have only been analysed over a frequency selective channel. Our objective 54 is to extend the state-of-art work to evaluate the performance of LDS over a high mobility channel 55 to simulate the vehicular environment for V2X applications and combine it with other advanced 5G 56 waveforms, specifically for an application that requires a high data rate, a medium number of users 57 connected to the network in a certain geographical area and a time of latency smaller than 1 ms [5]. Among these promising 5G waveforms, UFMC [18] has drawn attention due to its ability to 59 overcome OFDM shortcomings. By applying properly designed sub-band filtering, UFMC reduces 60 the high out-of-band (OOB) power emission while retaining the simplicity of the conventional OFDM 61 signal. In fact, one the main advantages of UFMC is its compatibility with the OFDM signals which 62 achieves low system complexity in the NOMA schemes. 63 Filtered-OFDM [19][20] is also one of the proposed advanced waveforms for the future cellular network. Both UFMC and f-OFDM signals use filtering per subband in order to achieve a low OOB, 65 the main difference is the filter length and its flexibility. F-OFDM uses a long filter with different 66 lengths for each subband (Windowed Sinc filter) exceeding the CP while UFMC signals use short 67 fixed length filters for each subband (Chebyshev filter). In this paper, our goal is to propose a 68 scheme that benefits from the waveforms robustness and multicarrier transmission combined with 69 the non-orthogonality of a spreading based NOMA to provide a system with less complexity while 70 keeping the transmission model flexible to any future changes and maintaining a certain compatibility 71 with the current techniques. It is why, we have developed a new LDS-UFMC and LDS-F-OFDM 72 schemes in which the LDS spreading is applied to UFMC and f-OFDM signals. Among the different 73 filters that f-OFDM can offer, we adopt computing the Hann, Hamming and Blackman filters thanks 74 to the great performance they shown in terms of BER and OOB reduction [21] and also to provide a 75 better comparison. These schemes will be BER analysed for a V2X communication i.e. a high mobility 76 channel. The multiuser detector will be based on Message Passing Algorithm (MPA) [22]. It will be 77 proved that LDS-F-OFDM outperforms the LDS-OFDM and LDS-UFMC by allowing the filter length 78 to exceed the CP length of OFDM and designing the filter appropriately. 79

The remainder of this paper is organized as follow. Section II introduces the system model of LDS-UFMC. Section III is devoted to the LDS-F-OFDM system model. Section IV presents simulation

results of LDS-UFMC and LDS-F-OFDM compared to LDS-OFDM in different environments. Finally,

⁸³ section V concludes this work.

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Figure 1. LDS-UFMC block diagram

2. LDS-UFMC system model

In this section, we are going to define the major blocks of an LDS-UFMC system. The LDS-UFMC 85 block diagram is shown in Fig. 1. After coding and modulation, the symbols are multiplied with a Low 86 density spreading sequences then modulated and transmitted simultaneously. Afterwards, spreaded 87 data is shaped into a time-frequency grid. In this configuration, we address the pilots aided channel 88 estimation. For simplicity, we propose to insert the pilots using the Comb Type arrangement. Then, 89 this grid is UFMC modulated using a N-point Inverse Fast Fourier Transform (IFFT) and filtered by a 90 L-length Dolph-Chebyshev filter. At the receiver side, the received signal is UFMC demodulated, then 91 the pilots extraction is performed in order to estimate the channel using the Least Square (LS) method 92 and linear interpolation. The equalizer block uses Zero-Forcing to eliminate the channel effect. The 93 output of the equalizer is passed to the LDS detector where an iterative detection process based on 94 MPA is performed to separate the users' symbols. 95 2.1. LDS Spreader 96

Consider an LDS-UFMC system with *K* users and the users are indexed as follow k = 1, ..., K and all users are assumed to transmit the same number of data streams *M* and they are indexed as follow m = 1, ..., M. Assume the number of subcarriers is N, and they are indexed as follow n = 1, ..., N. We define the spreading matrix of the k^{th} user as:

$$\boldsymbol{S}_{\boldsymbol{k}} = [\boldsymbol{s}_{\boldsymbol{k},\boldsymbol{1}}, \dots, \boldsymbol{s}_{\boldsymbol{k},\boldsymbol{M}}] \in \mathbb{C}^{N \times M}$$
(1)

 $s_{k,m} = [s_{k,m}^1, ..., s_{k,m}^N]^T$ is the sparse vector of length N used to spread the m^{th} symbol of the k^{th} user. Thus, the matrix of spreading of all users can be represented as :

$$\mathbf{S} = [\mathbf{S}_1, ..., \mathbf{S}_K] \in \mathbb{C}^{N \times MK}$$
(2)

Thanks to the sparse nature of this matrix, only a small number of users can share the same subcarrier, we define it as d_c the interference degree. Hence, among N subcarriers only d_v will be used to serve one user, d_v is called the effective spreading gain. Unlike the conventional CDMA system, we require $d_v \ll N$ and $d_c \ll K$. Let a_k be user's k symbols :

$$a_k = [a_{k,1}, \dots, a_{k,M}]^T$$
(3)

After the spreading process, the signal of the k^{th} user $x_k = [x_k^1, ..., x_k^N]^T$ is a vector of length N can be written as follow:

$$x_k = S_k . a_k \tag{4}$$

and x_k^n will be the data transmitted over the n^{th} subcarrier by the k^{th} user:

$$x_{k}^{n} = \sum_{m=1}^{M} a_{k,m} s_{k,m}^{n}$$
(5)

Hence, the signal transmitted over the n^{th} subcarrier is given by (6):

$$x^n = \sum_{k \in \xi_n} x_k^n \tag{6}$$

 ξ_n is considered as the group of users interfering in the n^{th} subcarrier.

Fig.2 represents the spreading process of the LDS. In this example, we consider that each user transmits one symbol (i.e M = 1). The system transmits over 4 subcarriers and serves 8 users which means that the overloading is at 200%. Each subcarrier is allocated to 4 users ($d_c = 4$), and each user spreads its data over 2 subcarriers ($d_v = 2$). The symbols are the variable nodes and the subcarriers are the functions nodes respectively. The edges that connect the nodes define if a symbol will be spreaded over the adjacent subcarrier. For instance the first user is connected to subcarriers 1 and 2, consequently, the first symbol will be spreaded over these adjacent subcarriers only. This representation of spreading process is called the Tanner Graph.



Figure 2. Spreading process of LDS-UFMC system

105

106 2.2. Signal Model

After the LDS spreading, the UFMC modulation is applied to each subcarrier. In fact, UFMC divides the entire bandwidth B of N subcarriers into multiple subbands S_u , each subband consists of Q subcarriers. Hence, the n^{th} subcarrier can now be regarded as the q^{th} subcarrier of the s^{th} subband. After that, the IFFT is performed over the signal of each subband and will be filtered using a L-length prototype filter, usually, the filter is a Dolph-Chebyshev window. The subbands are then superimposed and sent over the channel. The baseband discrete UFMC signal is represented in (7):

$$x_{LDS-UFMC}[n] = \sum_{s=0}^{S_u-1} g_s[n] * x_s[n]$$
(7)

 $g_s[n]$ defines the filter used in the s^{th} subband :

$$g_{s}[n] = g[n]e^{j(2\pi nQ/2)/N}e^{j(2\pi n(S_{0}+sQ))/N}$$
(8)

where S_0 denotes the starting frequency of the lowest subband and g[n] is a well-localized Chebyshev pulse filter of length L. The third term of the equation is the one responsible for frequency shifting to the appropriate subband. $x_s[n]$ is signal transmitted over the s^{th} group of subcarriers. It can be expressed as follow:

$$\mathbf{x}_{s}[\mathbf{n}] = \sum_{q=0}^{Q-1} x^{s,q} e^{j(2\pi nq/2)/N} e^{j(2\pi n(S_{0}+sQ))/N}$$
(9)

hence, $x^{s,q}$ can be nothing but the signal transmitted over the q^{th} subcarrier of the s^{th} subband and just like in (6), it is given by:

$$x^{s,q} = \sum_{k \in \xi_{s,q}} x_k^{s,q} \tag{10}$$

where $\xi_{s,q}$ is considered as the group of users interfering in the q^{th} subcarrier of the s^{th} subband.

The received signal is represented as follow:

$$y_{LDS-UFMC}[n] = h[n] * x_{LDS-UFMC}[n] + z[n]$$

$$\tag{11}$$

where z[n] and h[n] are the additive white gaussian noise with variance σ_z^2 and the channel impulse response respectively. The length of the signal $y_{LDS-UFMC}$ is $N_y = N + L - 1$ due to the convolution with the subband filter, consequently, a 2N-point Fast Fourier Transform (FFT) is performed at the UFMC receiver. After the UFMC demodulation process, the input of the LDS Detector corresponding to the n^{th} subcarrier is :

$$Y_n = H_n \sum_{k \in \xi_n} \sum_{m=1}^M a_{k,m} s_{k,m}^n$$
(12)

where Y_n and H_n are the 2N-point FFT of the time domain signal respectively. In our system, we have chosen to use the equalizer embedded with the LDS detector for a better performance. Regarding the LDS decoding, firstly, the LDS turbo receiver uses MPA and Forward Error Correction (FEC) decoder to find the reliability of the symbols. Secondly, the JSG receiver uses pulse shaping, NOMA, and channel coding, however, it is highly complex. For simplicity, we chose to implement the basic LDS detector that uses the Tanner Graph for implementing the MPA receiver in which we consider subcarriers and symbols as function nodes and variable nodes respectively. Adjacent nodes are connected via edges. Based on an extrinsic manner, each node will update its information containing the reliability of the symbol based on the received reliability from other edges and send it back. After an appropriate number of iterations, the reliability which is the log likelihood ratio (LLR) of the symbols will converge and the symbols are transmitted to the FEC decoder. The major goal behind this complex implementation is to find the value of \hat{a} that maximizes the joint a posteriori probability based on the observed signal:

$$\hat{a} = \arg\max_{a \in \mathbb{X}} p(a|y) \tag{13}$$

where X is the modulation constellation. The first LLR update can be written as follow :

$$\ell_{c_n \leftarrow u_k}(a_k) = \log \frac{P_{\text{ext},n}(a_k = +1)}{P_{\text{ext},n}(a_k = -1)}$$
$$= \sum_{m \in \varphi_k \setminus n} \ell_{c_m \to u_k}$$

Where *u* nodes are the variable nodes and *c* nodes are the function nodes, hence $\ell_{c_n \leftarrow u_k}$ is the message sent from u_k node to the c_n node and $\ell_{c_n \rightarrow u_k}$ message sent from c_n node to the u_k node respectively. It is clear from the above equation that the update of $\ell_{c_n \leftarrow u_k}(a_k)$ is dependent to all nodes besides the node n i.e $m \in \varphi_k \setminus n$, hence, the notation of extrinsic update. Second Update can be calculated as follow:

$$\ell_{c_n \to u_k}(a_k) = \log(\sum_{a_n \in X} P(y_n | a_n) \prod_{l \in \xi_n \setminus k} P_n(a_l))$$

Where φ_k is the group of subcarriers allocated to the k^{th} user and $P(y_n|a_n)$ is the channel observation

function at subcarrier y_n . Further explanations are provided in [22].



Figure 3. LDS-F-OFDM block diagram

110 3. LDS-F-OFDM system model

Based on the same LDS spreader used in LDS-UFMC, LDS-F-OFDM applies Filtered-OFDM 111 waveform on the users' spreaded signals and transmits them over the channel. The LDS based on 112 f-OFDM block diagram is presented in Fig.3. As depicted, the signal is mapped into a time-frequency 113 grid and then the pilots are inserted for channel estimation. Afterwards, a N-point IFFT is performed 114 to transfer the grid from the frequency domain to the time domain, data is then serialized and CP is 115 added to combat Inter Symbol Interference (ISI) effect. Like UFMC, the main advantage of f-OFDM 116 is its compatibility with OFDM, with a difference of passing the signal through a long length filter 117 before the transmission. Extended over the CP, the filter helps to lower the high OOB radiation while 118 maintaining the OFDM orthogonality between the subcarriers. Usually, a truncated sinc window is 119 used as a shaping filter, however in our system we have chosen to implement other types of filters for 120 a better comparison. For LDS-F-OFDM, we consider all the subcarriers as one subband to lower the 121 overall complexity. Therefore, our transmitted signal is an OFDM modulated signal passed through an 122 appropriate shaped filter. Without loss of generality, the signal expression can be written as follow: 123

$$x_{LDS-F-OFDM}[n] = x_{LDS-OFDM}[n] * f_{TX}[n]$$
(14)

where $f_{TX}(n)$ represents the well-designed filter and $x_{LDS-OFDM}[n]$ is the discrete LDS-OFDM signal after the spreading and modulation, it is represented as follow:

$$x_{LDS-OFDM}[n] = \sum_{q=0}^{N-1} x^q e^{j2\pi nq/N}$$
(15)

the transmitted signal is given by (16):

$$x_{LDS-F-OFDM}[n] = \sum_{q=0}^{N-1} x^q e^{j2\pi nq/N} * f_{TX}[n]$$
(16)

124 3.1. Filter design

The main reason behind the filtering is to eliminate the side lobes for an efficient transmission, it is why filters based on cardinal sin are taken into consideration thanks to their sharp filter response. However, the filter characteristic should be truncated due to its infinite impulse response. As a result, we obtain a finite sinc filter and a window pulse w[n] is applied to smooth its transitions. Once the filter is computed, it should be shifted around the central frequency of the subband.

$$p[n] = sinc(\frac{W + 2\delta_W}{N}n) \tag{17}$$

$$p_B[n] = \frac{p[n]w[n]}{\sum_n |p[n]w[n]|}$$
(18)

$$f_{TX}[n] = p_B[n]e\frac{j2\pi n f_c}{N\Delta_f}$$
(19)

where W is the number of active subcarriers, δ_W is the tone offset, N is the FFT size, f_c is the frequency

of the centre subcarrier in the baseband and Δ_f is the subcarrier spacing. The window function of the chosen windows are defined in Table I.

Window	Window function
Hann	$w[n] = 0.5 \times (1 + cos(\frac{2\pi n}{L-1}))$
Hamming	$w[n] = \frac{25}{46} + \frac{21}{45} \times \cos(\frac{2\pi n}{L-1})$
Blackman	$w[n] = \frac{7938}{18608} + \frac{9240}{18608} \times \cos(\frac{2\pi n}{L-1}) + \frac{1430}{18608} \times \cos(\frac{4\pi n}{L-1})$

Table 1. Window function of the filters

At the receiver side, a matching filter $f_{RX}[n]$ to the transmission filter $f_{TX}[n]$ is performed at the received signal, after that the CP is removed and the signal is transmitted to an OFDM receiver. After the grid demapping and pilot extraction, channel estimation is performed based on the pilots. The output data is then considered as the input of LDS detector explained in Section II.

4. Performance Evaluation

In this section, we propose to compare the performances of the proposed LDS-F-OFDM and LDS-UFMC schemes with the LDS-OFDM over a vehicular channel with different speed limits and over a multipath fading channel. The main simulation parameters are used to match the 3GPP Release 16 standard. Based on 3GPP Release 16, we have fixed the total bandwidth to B = 10MHz and a carrier frequency of $f_c = 5.9GHz$ to match the NR-V2X operating bands in FR1 [23]. Table II summarizes the simulation parameters.

No error correction is employed, so the evaluation is carried out for uncoded bits. The LDS
spreading matrix is generated randomly for all the simulated schemes. However, we do believe
that a well designed matrix with small number of cycle-of-four and a high girth can achieve better
performance.

In order to respect the 3GPP recommendations, no overloading scenario is deployed due to the use of pilots and the waveforms offset. We have overcome this circumstance by respecting the rule of interfering several users in the same resource and allocating a few subcarriers to the same user i.e. respecting the LDS structure to justify these new schemes performances. The maximum number of iterations of the LDS detector is ten.

The first channel we have chosen to evaluate the performance of these schemes is the Tapped Delay Line model, specifically the TDL-A channel. The TDL-A channel model has a Doppler spectrum which is characterized by a Jake's spectrum shape. The Power Delay Profile (PDP) of the model is presented in [24] and the delay spread used to scale the normalized taps delays is $D_s = 93\eta s$. This delay spread is chosen to correspond to a short delay profile in an Urban Macro environment for a 5.9*GHz* carrier frequency.

Fig.4 depicts the simulation results of LDS-F-OFDM and LDS-UFMC over TDL-A channel. We first fix the bandwidth at B = 10MHz, then we investigate the schemes under two systems, the first with 1024 subcarriers and $\Delta_f = 15KHz$ subcarrier spacing and the second with 512 subcarriers and $\Delta_f = 30KHz$. According to the simulation results, the LDS-F-OFDM shows better performance over both LDS-UFMC and LDS-OFDM. The fact that the f-OFDM subband regroups all the available subcarriers concentrates the energy in one main lobe results in less ISI, and thanks to the LDS structure,

Parameters	Symbol	Value		
Release 16	Parameters	3		
Bandwidth	В	10 MHz		
Carrier frequency	f_c	5.9 GHz		
Number of symbols	N _{sym}	14		
Subcarriers spacing	Δ_f	15 KHz		
		30 KHz		
Number of Resource Blocks	N _{RB}	52		
		24		
FFT Size	N _{FFT}	1024		
		512		
Cyclic Prefix Length	I	72		
	LCP	36		
Pilots Parameters				
Pilots Arrangement	-	Comb type		
Pilots Spacing	N_{ps}	4		
Number of Pilots per symbol	Np	156		
	1 v p	72		
UFMC				
Filter Length	I.,	65		
		33		
Filter Type	-	Dolph-Chebyshev		
Side Lobe Attenuation	-	50dB		
Number of Subbands	S	52		
		24		
Subband size	Q	12		
F-OFDM				
Filter Length	LE	513		
	r	257		
Window function		Hann		
	-	Hamming		
		Blackman		
LDS Scheme Parameters				
Effective Processing gain	d_v	3		
Interference Pattern	d_c	3		
Number of Users	Nu	468		
		216		
Modulation		BPSK		

Table 2. Simulation parameters

the MUI are eliminated, thus, reducing the overall interference. Hence, it is expected that the f-OFDM
with the LDS structure achieve a better BER performance. Meanwhile, LDS-UFMC shows a slight
performance degradation compared to LDS-OFDM. However, UFMC offers lower OOB and the main
advantage of UFMC is the increased spectral efficiency. Consequently, a trade-off must be taken in
consideration depending on the requirements of the application.

The second and main channel used to simulate these schemes is the Extended Vehicular A (EVA) model channel, its power delay profile is provided in [25]. Similarly to the TDL-A model, the EVA model is characterized by a Jake's Doppler spectrum and the maximum speed simulated is 300Km/h, hence the maximum Doppler shift $f_d = 556Hz$ and specifically modeled to simulate a vehicular channel.

Fig.5 (a) shows the BER performance of the LDS-F-OFDM and LDS-UFMC compared to LDS-OFDM over an EVA channel with a computed speed of 100Km/h which means that the maximum Doppler shift is $f_d = 185Hz$ with a subcarrier spacing of $\Delta_f = 15KHz$ and an FFT size of 1024, hence only 468 subcarriers left for data transmissions. For simplicity, we consider 468 users each sending one BPSK modulated symbol with a power of 1 Watt. In fact, this is the worst loading scenario where we have the number of users equal to the number of subcarriers allocated to data transmission which



(b) $\Delta_f = 30 K H z$ **Figure 4.** Performance of the proposed schemes over an TDL-A Channel

means that each user will be able to send only one symbol. It can be noticed that the LDS-F-OFDM 176 slightly outperforms once more both LDS-OFDM and LDS-UFMC with its all different types of filters 177 deployed. While Hann, Hamming and Blackman windows achieve almost the same BER performance, 178 Hann window function is the filter susceptible to give better OOB performance. In terms of spectral 179 efficiency, LDS-UFMC compared to LDS-F-OFDM and LDS-OFDM comes first due to the removal 180 of the CP. However, observing the used subcarriers for data transmission due to the use of the pilot 181 with only 4 subcarrier spacing, we notice the overall degraded spectral efficiency. This is completely 182 justified by the need of an efficient channel estimation because of the high changing nature of the 183 channel. 184

The BER performance of the proposed schemes with a computed speed of 100Km/h and a 185 subcarrier spacing of $\Delta_f = 30 KHz$ and 512 subcarriers is presented in Fig.5 (b). It is worth noting that 186 LDS-F-OFDM shows again better performance at low SNR, while at higher SNR, all the proposed 187 schemes face slight performance degradation. In fact, while employing higher subcarrier spacing 188 to combat the Doppler shift, the spectral efficiency is reduced and also the number of subcarriers 189 allocated to pilots is reduced (156 subcarriers in the first system vs 72 in the second). Consequently, the 190 channel estimation will not be as efficient as in the first system. Furthermore, in order to investigate 191 how the LDS-F-OFDM and LDS-UFMC can be affected by the mobility, the schemes are also simulated 192 over an EVA channel with a speed of 300 Km/h. 193

ER.





Figure 5. Performance of the proposed schemes over an EVA Channel with speed of 100Km/h

Fig.6 (a) and (b) represents the simulation results for $\Delta_f = 15 KHz$ and $\Delta_f = 30 KHz$ respectively. 194 It can be seen that LDS-F-OFDM shows better performances than LDS-OFDM and LDS-UFMC in 195 low SNR. Moreover, all the techniques demonstrate huge improvements in the second system with 196 $\Delta_f = 30 KHz$ subcarrier spacing than the first. Thanks to the large subcarrier spacing, the Doppler 197 shift does not impact severely the subcarriers orthogonality. In addition, comparing Fig.5 (a) with 198 Fig.6 (a), all the techniques face severe performance degradation due to the high mobility of the UEs. 199 Meanwhile, Fig.5 (b) with Fig.6 (b) presents almost the same BER performances thanks to the large 200 subcarrier spacing. 201

Fig.7. Depicts the comparison of the proposed schemes over the EVA channel with different 202 speed limits with both systems. We have chosen to evaluate the schemes also over the EVA channel 203 with a 500Km/h velocity and analyse the degradation of the performance in such an environment. 204 Obviously, the performance decreases due to the high speed, however as shown in Fig.7(b) i.e. with a 205 large subcarrier spacing, both LDS-F-OFDM and LDS-UFMC seem to suffers less. Meanwhile with 206 $\Delta_f = 15 KHz$, all the techniques seem unable to converge at high speed. To improve this, other receivers 207 can be considered such as the JSG and Expectation Propagation Algorithm EPA receivers. 208



(b) $\Delta_f = 30 KHz$

Figure 6. Performance of the proposed schemes over an EVA Channel with speed of 300Km/h

209 5. Conclusion

In this paper, we have proposed two efficient multiple access techniques namely LDS-F-OFDM 210 and LDS-UFMC in which the LDS structure is combined with the new 5G waveforms. First of all, 211 we have presented the state-of-art of the previous work done on LDS and we have detailed the 212 transmitters and receivers of these new schemes. Then, we have highlighted our contribution that 213 consists in evaluating these new schemes over different types of channels, specifically, a vehicular 214 channel with a high mobility. Simulation results show that LDS-F-OFDM significantly achieves 215 higher performance improvements compared to LDS-OFDM and LDS-UFMC in all scenarios, while 216 maintaining an affordable complexity at the transmitter and the receiver side. The improvements are 217 directly related to the advantages that f-OFDM waveform offers by addressing the adequate filter. 218 In future work, we propose to analyse these schemes with different types of receivers in manner to 219 reduce the complexity and to improve the performances. Some of the receivers that can be found 220 in the literature are the SIC-MPA where we combine SIC and MPA to reduce the overall complexity 221 and the JSG receiver which is a very high complex receiver but provides a lot of improvements to the 222 system. Furthermore, we consider evaluating theses schemes over different vehicular channels such as 223



Figure 7. Schemes comparison over the EVA channel with different speed limits

a confined channel and with different channel specifications considering the other operating band of
 FR1 i.e. 25*GHz*.

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236 Abbreviations

²³⁷ The following abbreviations are used in this manuscript:

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OFDM	Orthogonal Frequency Division Multiplexing
FBMC	Filter-Bank Multi-Carrier
UFMC	Universal Filtered Multi-Carrier
BER	Bit Error Rate
LTE	Long Term Evolution
3GPP	3rd Generation Partnership Project
SC-FDMA	Single Carrier Frequency Division Multiple Access
ETSI	European Telecommunications Standards Institute
NR-V2X	New-Radio V2X
СР	Cyclic Prefix
UL	Uplink
DL	Downlink
QPSK	Quadrature Phase Shift Keying
QAM	Quadrature Amplitude Modulation
IDMA	Interleaver Division Multiple Access
PDMA	Pattern Division Multiple Access
SCMA	Sparse Code Multiple Access
CDMA	Code Division Multiple Access
JSG-IOTA	Joint Sparse Graph-Isotropic Orthogonal Transfer Algorithm
MPA	Message Passing Algorithm
FEC	Forward Error Correction
EPA	Expectation Propagation Algorithm
IFFT	Inverse Fast Fourier Transform
LS	Least Square
FFT	Fast Fourier Transform
ISI	Inter Symbol Interference
OOB	Out Of Band
PDP	Power Delay Profile
EVA	Extended Vehicular A

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