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## Sliding motion of a bubble against an inclined wall from moderate to high bubble Reynolds number

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The motion of a bubble sliding over an inclined wall from moderate to high bubble Reynolds number is studied experimentally for a wide range of liquid properties and bubbles sizes, considering wall inclination angles from nearly horizontal to nearly vertical. All experiments are restricted to sliding behavior, below the transition to steady bouncing motion. We study both the shape of the bubble and its drag coefficient. For small angles, the bubble shape is dominated by gravitational effects resulting in a flattened shape against the wall; for large angles, the bubble remains in constant contact with the wall but adopts a shape that is aligned perpendicularly to the wall, closer to that observed for an inertia-dominated free rising bubble. We model this transition of shape considering balances among surface tension, gravitational, and inertial forces; we observe good agreement with experiments. We found that the drag coefficient is strongly influenced by the shape that the bubble adopts as it slides over the wall. By considering the flow in the film and around the bubble, we propose a correlation to predict the drag coefficient for each regime of bubble shape. In the regime dominated by viscous effects, the drag of a single bubble is increased due to the mirror effect with the wall and by the friction in the film formed between the wall; conversely, for the case dominated by inertial effects, the drag coefficient is constant. The behavior for a single bubble is changed: no significant increase due to deformation. In both shape regimes the proposed expression agrees well with the experimental measurements.

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### I. INTRODUCTION

Two phase flows are present in many natural phenomena and practical applications. For the case of dispersed gas-liquid flows, or bubbly flows, a good understanding of the overall dynamics has been reached [1]. Such progress is mainly supported by the knowledge of the motion of single bubbles and hydrodynamic interactions in unbounded fluids [2]. One of the remaining challenges in the understanding of these flows is the effect of walls. Although most flows are contained within walls, their effect on the bubble motion is still a subject of active research. For the particular case of bubbles, most studies have addressed the interaction of single bubbles with either vertical [3–6] or horizontal walls [7–9]. The interaction of a bubble with an inclined wall has been shown to be more complex: a bubble of a certain size and moving in a certain liquid may interact with the wall in a significantly different manner depending on the inclination. For small angles, the bubbles slide over the wall at a constant speed; for large inclinations, instead, the bubbles bounce repeatedly at a constant average speed. This phenomenon was first reported by Tsao and Koch [10]. The conditions for transition were recently explained by Barbosa *et al.* [11]: when the inertia

of the motion is sufficiently large, the wake behind the bubble induces a wall-repulsive lift force that pushes the bubble away from the wall. In the present paper we focus only on the sliding regime.

There have been several investigations that address the sliding motion of a bubble over an inclined wall, both experimentally [10,12–17] and by numerical simulations [16,18–20]. In particular, what is most relevant for practical applications is the determination of the drag coefficient of the bubble as it slides over the wall and the extent of contact with the wall. Both of these quantities can be used, for instance, to calculate the amount of heat and mass transfer that a bubble may extract from a heated wall [21].

Maxworthy [12] conducted experiments of sliding bubbles over an inclined plane but focused mostly on large bubbles, which in free rise state would have a spherical-cap shape (large Bond numbers,  $Bo = \rho g D_{eq} / \sigma$ , where  $\rho$  and  $\sigma$  are the density and surface tension, respectively, and  $g$  and  $D_{eq}$  are gravitational acceleration and the diameter of the bubble, respectively). Conversely, Maslyiah *et al.* [13] and Tsao and Koch [10] conducted experiments for nearly spherical bubbles (small Weber numbers,  $We = \rho U d_{eq} / \sigma$ , where  $U$  is the bubble speed) sliding on an inclined plane. They both proposed empirical correlations for the drag coefficient. In the investigation by Aussillous and Quéré [14], experiments were conducted for bubbles in highly viscous fluids and with very small angles of inclination. In this regime, a formal modeling of the flow was possible. They calculated the viscous lubrication force in the film between the bubble and the wall. An implicit formula for the capillary number ( $Ca = \mu U / \sigma$ , where  $\mu$  is the liquid viscosity) is obtained from the force balance between the drag force and the buoyancy. Hodges *et al.* [22] studied the same configuration but for the case of droplets. Podvin *et al.* [16] conducted both numerical simulations and experiments to study the same system. They analyzed, in detail, the initial process of bubble-wall interaction. The existing numerical studies have focused on different aspects of the problem, covering the change of shape with inclination and Bond number [18], the shape and dynamics of large Bond number bubbles [19], and the change of shape with inclination [20]. The recent study by Dubois *et al.* [17] showed that the bubble shape could be aligned with the wall or be perpendicular to it depending on both the angle and the values of the Weber and Bond numbers. This behavior was captured in the numerical results of Senthilkumar *et al.* [20]. Dubois *et al.* [17] proposed a model based on a balance equation among buoyancy drag and the viscous resistance due to the film between the bubble and the wall.

In this article we report the experimental results of bubble sliding over an inclined wall. We cover a wide range of parameters by considering different fluids and bubble sizes. In particular, the bubble wall Reynolds number based on bubble diameter is varying from 10 to 650. The analysis of both the bubble shape and speed allowed us to separate the behavior of the sliding bubble into two distinct regimes: when the bubble shape is aligned with the wall and when the bubble is nearly perpendicular to it. Due to this significant change in the way the bubble moves on the wall, the resulting drag law is different. We propose drag correlations for each regime, based on the relevant forces for each case. The propose drag law depends on the Reynolds number, as expected, but it also includes lubrication effects, accounted for by the Bond and capillary numbers.

## II. EXPERIMENTAL SETUP

### A. Methods and experimental conditions

Figure 1 shows the bubble-wall interaction considered in this study: a bubble rising at terminal conditions interacts with an inclined solid wall. The experimental device is described in detail in [11]. In essence, it is a container in which an inclined wall is inserted. The angle of inclination of the wall can be varied from  $5^\circ$  to  $80^\circ$ . The motion of the bubble during the interaction is captured using a high speed camera (Phantom v1) at a rate of at least 1000 frames/s, with a spatial resolution of  $11.5 \mu\text{m}/\text{pixel}$ .

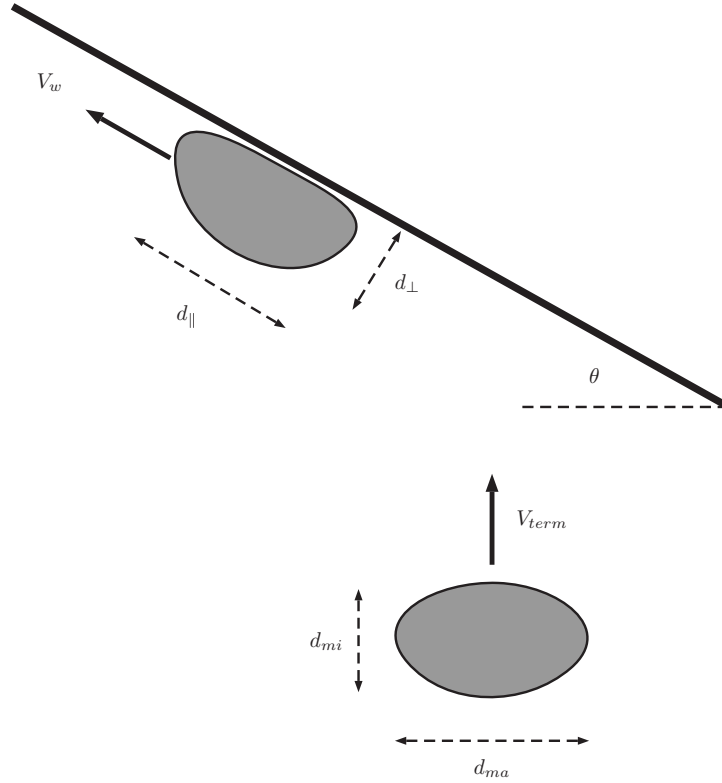


FIG. 1. Sketch of bubble terminal and wall conditions. Away from the wall, the bubble ascends at  $V_{term}$ , with a constant aspect ratio  $d_{ma}/d_{mi}$ , where  $d_{ma}$  and  $d_{mi}$  measure the major and minor axis of the bubble. While sliding on the wall, the bubble moves at a constant speed,  $V_w$ , with an aspect ratio  $d_{\parallel}/d_{\perp}$ , where  $d_{\parallel}$  and  $d_{\perp}$  measure the bubble length and width with respect to the wall.

The bubble shape was determined by directly measuring the major and minor bubble axes  $d_{ma}$  and  $d_{mi}$ , respectively, from each image. The equivalent diameter,  $D_{eq}$ , is then calculated as

$$D_{eq} = (d_{ma}^2 d_{mi})^{1/3}. \quad (1)$$

The bubble aspect ratio was calculated from

$$\chi = \frac{d_{ma}}{d_{mi}}. \quad (2)$$

The terminal velocity,  $V_{term}$ , is determined from the displacement of the bubble geometric centroid of consecutive frames, considering a central difference scheme. To calculate mean and standard deviations values of the measurements, each experiment was repeated five times. The uncertainty in the measurement of the bubble size and velocity is about 8%.

To generate a range of experimental conditions, seven different liquids and two capillary sizes were used. The physical parameters of the corresponding liquids as well as the terminal conditions for all cases are summarized in Table I. Note that we use the nomenclature in the first column of the table when referring to a specific case. The same symbols for each experiment are used in all the figures. The viscosity and surface tension of the different liquids were measured with a stress controlled rheometer (MCR101) and a Wilhelmy balance with a DuNouy ring, respectively. The density was measured with a 25  $\mu\text{L}$  pycnometer. We characterize each experiment (a combination of bubble size with the physical properties of the liquid used) through the terminal Reynolds and

TABLE I. Physical properties for all the experiments conducted in this investigation. In all cases, the liquids were mixtures of water (W), glycerol (G), and triethanol amine (T); percentages in the second column are by weight. Three experiments were performed using silicon oil (SO). The type of trajectory for bubbles before reaching the wall is shown in the first column: rectilinear (R) or oscillatory (O).

Experiment	Composition, %	$\rho$ ( $\text{kg}/\text{m}^3$ )	$\mu$ ( $\text{mPa}\cdot\text{s}$ )	$\sigma$ ( $\text{mN}/\text{m}$ )	$D_{\text{eq}}$ ( $\text{mm}$ )	Mo	$\text{Re}_{\text{erm}}$	$\text{We}_{\text{erm}}$	$\chi$	$\theta_{\text{trans}}$
E1, ■ (R)	SO, 100	855	1.280	18.0	1.1	$5.32 \times 10^{-9}$	$138 \pm 3$	$1.8 \pm 0.05$	$1.31 \pm 0.02$	$80^\circ$
E2, ◆ (R)	SO, 100	855	1.280	18.0	1.2	$5.32 \times 10^{-9}$	$172 \pm 8$	$2.6 \pm 0.17$	$1.32 \pm 0.05$	$80^\circ$
E3, ● (O)	SO, 100	855	1.280	18.0	2.2	$5.32 \times 10^{-9}$	$313 \pm 7$	$4.7 \pm 0.23$	$2.06 \pm 0.04$	$45^\circ$
E4, ▲ (R)	W-G, 80-20	1045	1.555	70.2	1.7	$1.59 \times 10^{-10}$	$305 \pm 7$	$1.9 \pm 0.09$	$1.26 \pm 0.04$	$70^\circ$
E5 (6), ◀ (O)	W-T, 99.88-0.12	1001	1.529	61.3	2.8	$1.15 \times 10^{-9}$	$250 \pm 9$	$2.0 \pm 0.11$	$1.16 \pm 0.02$	$70^\circ$
E6, ▲ (O)	W-G, 85-15	1033	1.363	70.0	1.6	$9.56 \times 10^{-11}$	$367 \pm 16$	$2.1 \pm 0.16$	$1.44 \pm 0.05$	$65^\circ$
E7, ▼ (O)	W-G, 90-10	1021	1.165	70.6	1.6	$5.03 \times 10^{-11}$	$469 \pm 14$	$2.5 \pm 0.15$	$1.63 \pm 0.08$	$60^\circ$
E8, ■ (O)	W-G, 95-5	1009	1.038	70.8	1.7	$3.18 \times 10^{-11}$	$536 \pm 21$	$2.6 \pm 0.20$	$1.58 \pm 0.07$	$60^\circ$
E9, ◆ (O)	W-G, 90-10	1021	1.165	70.6	2.9	$5.03 \times 10^{-11}$	$640 \pm 77$	$2.6 \pm 0.5$	$1.69 \pm 0.28$	$50^\circ$
E10, ● (O)	W, 100	998	0.955	72.6	1.6	$2.18 \times 10^{-11}$	$601 \pm 40$	$2.7 \pm 0.3$	$1.78 \pm 0.10$	$50^\circ$
E11, ★ (O)	W, 100	998	0.955	72.6	3.1	$2.18 \times 10^{-11}$	$955 \pm 46$	$3.6 \pm 0.3$	$1.93 \pm 0.13$	$45^\circ$

Weber numbers:

$$\text{Re}_{\text{term}} = \frac{\rho V_{\text{term}} D_{\text{eq}}}{\mu}, \quad \text{We}_{\text{term}} = \frac{\rho V_{\text{term}}^2 D_{\text{eq}}}{\sigma}, \quad (3)$$

where  $V_{\text{term}}$  is the bubble terminal velocity. The Morton number, defined as

$$\text{Mo} = \frac{g\mu^4}{\rho\sigma^3}, \quad (4)$$

is a dimensionless group that only contains fluid properties, so it is often used to characterize the fluid. Its value, for each liquid, is also reported in Table I.

When the bubble collides with the wall (always at its terminal velocity), it experiences few transient bounces and then achieves a new time-average steady state. As reported previously [10,11], the bubble can either slide steadily or bounce periodically with a constant mean tangential velocity. The conditions to observe one behavior or the other are discussed by Barbosa *et al.* [11]. They found that for wall angles below a certain critical value,  $\theta < \theta_{\text{trans}}$ , the buoyancy force dominates the repulsive lift induced by the wake and the bubble slides under the wall; when  $\theta > \theta_{\text{trans}}$  the lift induced by the wake is strong enough to push the bubble away from the wall and to generate a stable periodic bouncing. In this investigation we only consider bubbles that slide steadily on the wall after the initial wall interaction. Hence, for each bubble-fluid combination only the experiments for inclinations below the critical angle,  $\theta < \theta_{\text{trans}}$ , are considered. To characterize the sliding steady state, wall Reynolds and wall Weber numbers are defined using the mean sliding velocity,  $V_w$ :

$$\text{Re}_w = \frac{\rho V_w D_{\text{eq}}}{\mu}, \quad \text{We}_w = \frac{\rho V_w^2 D_{\text{eq}}}{\sigma}. \quad (5)$$

For the range of experimental conditions, the bubbles slide in a rectilinear manner over the wall. Maxworthy [12], for instance, did observe zigzagging for Bond numbers larger than 10.

### B. Terminal conditions

The terminal conditions can be used to assess the degree of bubble deformation and surface contamination for each experiment. As shown below, these two effects determine the velocity of the bubble as it slides over the wall. According to the shape map proposed by Clift *et al.* [23], the range of experimental conditions studied here corresponds to ellipsoidal and wobbling bubbles with rectilinear and zigzag paths.

The evolution of the terminal aspect ratio with the terminal Weber number for the entire range of experimental conditions considered in this investigation is presented in Fig. 2. The measurements are compared with the expression proposed by Legendre *et al.* [24]:

$$\chi = \frac{1}{1 - \frac{9}{64} \text{We}_{\text{term}} (1 + K(\text{Mo}) \text{We}_{\text{term}})^{-1}}, \quad (6)$$

where  $\text{We}_{\text{term}}$  and  $\text{Mo}$  are the Weber and Morton numbers. For this expression  $K(\text{Mo}) = 0.2 \text{Mo}^{1/10}$ . The prediction of Eq. (6) is plotted for two cases. First, the prediction without the Morton number correction ( $\chi = 1 + 9\text{We}_{\text{term}}/64$ ) is shown by the continuous line; the dashed line shows the prediction corresponding to  $\text{Mo} = 2 \times 10^{-11}$ .

In general, the experiments agree well with the prediction. For large values of the Weber number, cases E3 and E11, Eq. (6) overestimates the experimental values. In these two data sets wobbling bubbles are observed; such motion affects measurement of the aspect ratio. For case E5, the experimental measurements are below the prediction of Eq. (6). For this particular experiment the liquid is strongly contaminated (this is shown below), as it contains a small amount of triethanol amine which is a long surfactant-like molecule. We can argue that in this case the surface contamination would alter the shape.

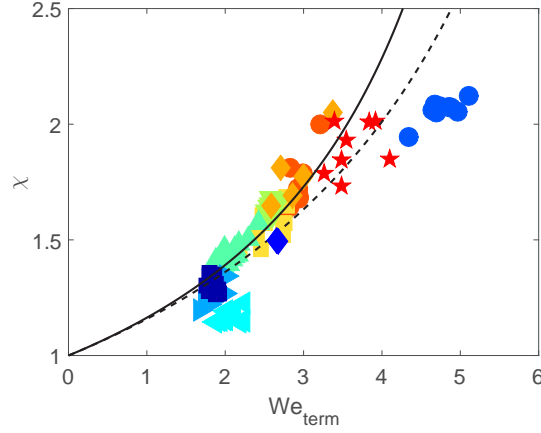


FIG. 2. Aspect ratio,  $\chi$ , as a function of terminal Weber number, for all the experiments. Each bubble-fluid combination is represented by a different symbol, according to Table I. The continuous and dashed lines correspond to Eq. (6) plotted without the Morton term and for  $Mo = 2.1 \times 10^{-11}$ , respectively.

Now, considering the value of the drag coefficient we can further assess the effects of bubble deformation and the possible presence of surface impurities. The experimental steady drag coefficient is inferred indirectly from the balance between the buoyancy force and the drag force acting on the bubble in the vertical direction:

$$C_D = \frac{4 D_{eq} g}{3 V_{term}^2}. \quad (7)$$

The terminal drag is shown as a function of terminal Reynolds number for all the experiments conducted in this investigation in Fig. 3.

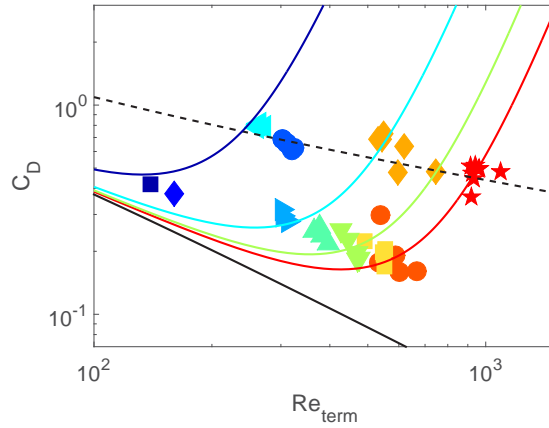


FIG. 3. Drag coefficient,  $C_D$ , as a function of terminal Reynolds number,  $Re_{term}$ , for all the experiments in Table I. The continuous black line shows the prediction of Eq. (9). The other continuous lines show the predictions of Eq. (10) for four cases: blue line, for  $Mo = 5.32 \times 10^{-9}$  (E1, E2, E3); cyan line, for  $Mo = 1.15 \times 10^{-9}$  (E5); green line, for  $Mo = 5.03 \times 10^{-11}$  (E7, E9); and red line, for  $Mo = 2.18 \times 10^{-11}$  (E10, E11). The colors correspond to the nomenclature in Table I. The dashed black line shows the drag calculated according to Eq. (11).



For a spherical bubble at large Reynolds numbers, Levich [25] calculated that the drag coefficient would be

$$C_D^{\text{Levich}} = \frac{48}{\text{Re}} \quad (8)$$

resulting from the total viscous dissipation through the velocity potential of irrotational flow. Considering the effect of the boundary layer, but retaining the spherical shape, Moore [26] found that

$$C_D^{\text{Moore}} = \frac{48}{\text{Re}} \left[ 1 - \frac{2.211}{\text{Re}^{1/2}} \right], \quad (9)$$

which extended its validity to  $\text{Re} \approx 50$ .

By additionally considering that the bubble was an oblate spheroid, Moore [27] calculated the drag coefficient to be

$$C_D^{\text{Moore}^*} = \frac{48}{\text{Re}} G(\chi) \left[ 1 + \frac{H(\chi)}{\text{Re}^{1/2}} + \dots \right], \quad (10)$$

where  $G(\chi)$  and  $H(\chi)$  are functions of  $\chi$ , the bubble aspect ratio. Note that the aspect ratio corresponds to that in the terminal state, as in Eq. (2).

If the experimental results are in agreement with the prediction in Eq. (10), we can argue that the increase in drag is the result of deformation. In Fig. 3 we show the prediction for a few selected cases. For cases E1, E7, and E11 the agreement is reasonable. Hence, in these cases, we can argue that the interfacial contamination is not significant. On the other hand, the comparison between the prediction and the measurements for case E5 are significantly different. The experimental drag is well above the prediction, despite the fact that the bubble is not largely deformed ( $\chi = 1.16$ ). In fact, for this particular experiment the drag coefficient is close to that calculated for a fully contaminated surface (a solid sphere), according to the prediction by Schiller and Naumann [28]:

$$C_D^{\text{SN}} = \frac{24}{\text{Re}} [1 + 0.15\text{Re}^{0.687}]. \quad (11)$$

Therefore, as discussed above, for this particular experiment we consider that the bubble surface is immobile, resulting from surface active contaminants.

### III. RESULTS

We now examine the motion and shape of bubbles as they slide on the wall. We show that the shape that the bubble adopts during its interaction with the wall strongly affects the drag and, therefore, the bubble speed.

#### A. Bubble shape on the wall

The shape of the bubble as it slides on the wall can be significantly different from that at its terminal condition. Furthermore, it can change importantly depending on the angle of inclination of the wall. Figure 4 shows sliding bubbles for different inclination angles for experiment E3. For small angles, Figs. 4(a) and 4(b), the bubble moves slowly and its shape is the result of the action of buoyancy pushing it against the wall. In other words, the bubble is elongated along the wall. For large wall inclinations, Figs. 4(d) and 4(e), the component of buoyant force that pushes the bubble against the wall is smaller. At the same time, the component of buoyancy in the direction parallel to the wall is larger resulting in a higher bubble velocity. In turn, the larger bubble velocity induces a deformation due to inertial effects similar to that observed under terminal conditions. Therefore, for these large angles, the bubble appears to be “standing” over the wall: its elongation is in the direction perpendicular to the wall. Clearly, for an intermediate inclination the bubble slides with a nearly spherical shape. Observations of the transition in bubble shape as the wall inclination increases

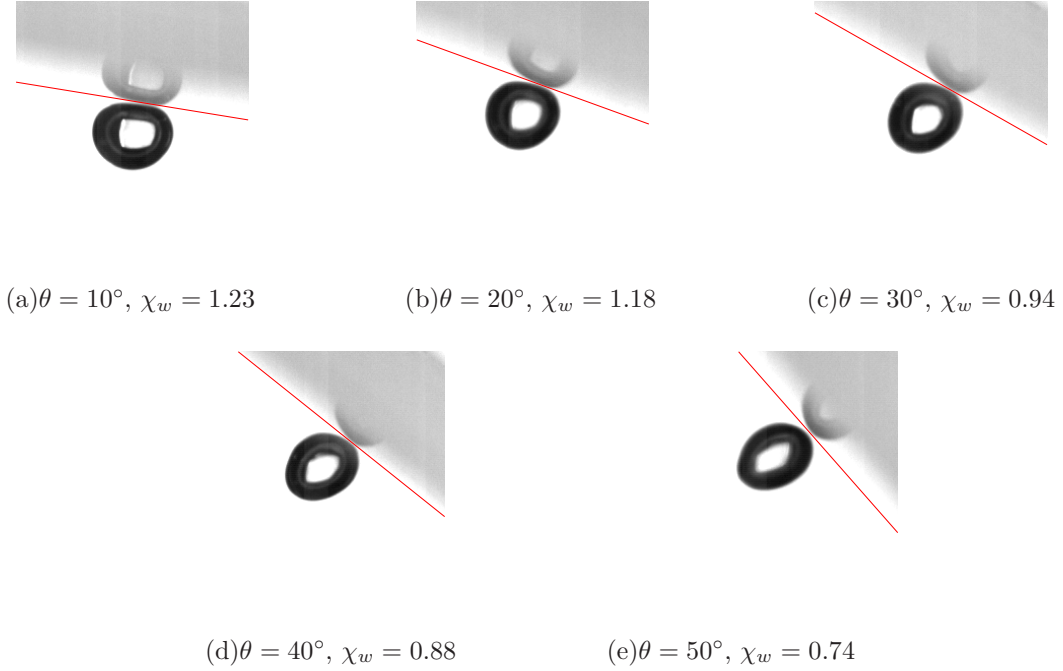


FIG. 4. Images for the sliding bubble shape evolution at different inclination angles in experimental conditions E3 (see Table I): (a)  $V_w = 40.1$  mm/s,  $Re_w = 59$ ,  $We_w = 0.04$ ; (b)  $V_w = 80.9$  mm/s,  $Re_w = 119$ ,  $We_w = 0.16$ ; (c)  $V_w = 115.0$  mm/s,  $Re_w = 169$ ,  $We_w = 0.33$ ; (d)  $V_w = 138.8$  mm/s,  $Re_w = 204$ ,  $We_w = 0.48$ ; (e)  $V_w = 155.2$  mm/s,  $Re_w = 228$ ,  $We_w = 0.60$ . Images are shown with the same scale.

were recently reported by Dubois *et al.* [17]. They showed that the shape transition depends on both Weber and Bond numbers.

Therefore, we propose to use a different measure of bubble deformation when it interacts with the wall. The wall aspect ratio is defined as

$$\chi_w = \frac{d_{\parallel}}{d_{\perp}}, \quad (12)$$

where  $d_{\parallel}$  and  $d_{\perp}$  are the bubble length parallel and normal to the wall, respectively. Therefore, for deformation controlled by gravity  $\chi_w > 1$ , whereas  $\chi_w < 1$  is observed when deformation is controlled by inertia. Below, we propose a model that considers the combination of these two effects to predict the bubble shape at the wall.

As observed, for a nearly horizontal wall, the bubble is pushed over the wall by the buoyant force and deformation is expected to be mainly controlled by gravity and the shape can be determined following Mahadevan and Pomeau [29], who considered the motion of a droplet rolling over a slightly inclined wall. In an analogous manner, we can consider that the bubble is nearly spherical everywhere except at the contact region, a flat horizontal disk of radius  $\ell$ . By geometrical considerations, the vertical displacement of the bubble center  $\delta$  due to the buoyancy and the radius of the contact disk  $\ell$  are related to each other by  $\ell^2 \sim R\delta$ , where  $R$  is the equivalent radius. The bubble deformation induces an increase of the bubble surface area by an amount  $\Delta a \sim \ell^4/R^2$  and an increase of its radius  $\Delta R \sim \ell^4/R^3$ . For the interaction with an inclined wall, the component of gravity acting towards the wall is  $g \cos \theta$ . Thus, balancing the decrease in potential energy  $\rho g \cos \theta R^3 \delta$  with the gain in interfacial energy  $\sigma \Delta a$ , the following scalings can be deduced:  $\delta \sim Bo \cos \theta R$ ,  $\ell \sim Bo^{1/2} \cos^{1/2} \theta R$ , and  $\Delta R \sim Bo^2 \cos^2 \theta R$ . Therefore, the wall aspect ratio can

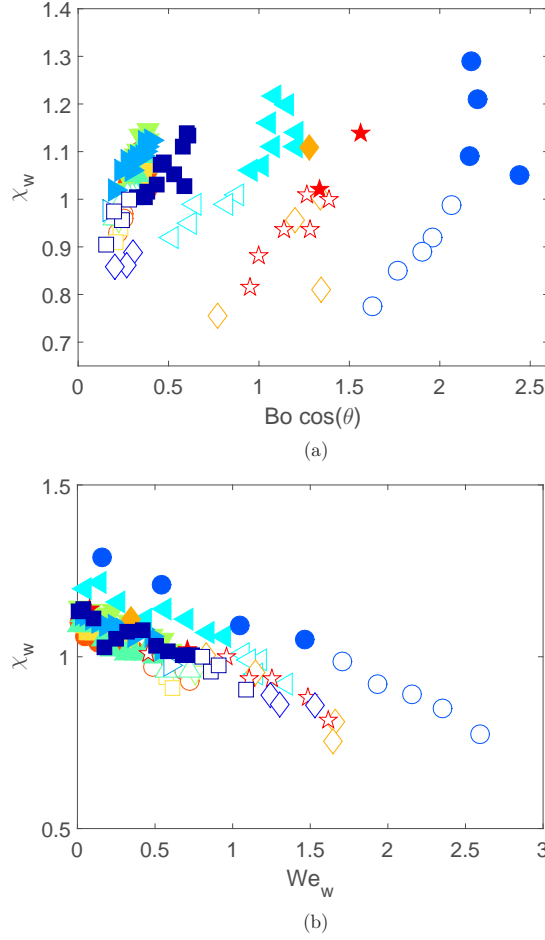


FIG. 5. Dependence of wall aspect ratio for gravitational and inertial effects for all the experiments. (a) Wall aspect ratio,  $\chi_w$ , as a function of  $Bo \cos \theta$ . (b) The wall aspect ratio,  $\chi_w$ , as a function of the wall Weber number,  $We_w$ . The symbols correspond to Table I: open and solid symbols represent experiments for  $\chi_w > 1$  and  $\chi_w < 1$ , respectively.

then be estimated to be

$$\chi_w = \frac{d_{\parallel}}{d_{\perp}} \sim \frac{2R + 2\Delta R}{2R + \Delta R - \delta} \sim \frac{1}{1 - \alpha Bo \cos \theta}, \quad (13)$$

where  $\alpha$  is a fitting constant. As shown by this relation, gravity flattens the bubble towards the wall. Note that this prediction is expected to only agree with measurements with small values of  $Bo \cos \theta$ . In Fig. 5(a) the wall aspect ratio is shown as a function of  $Bo \cos \theta$ . Note that the data are shown according to their  $\chi_w$  value: for  $\chi_w > 1$  solid symbols are used, while open symbols are used when  $\chi_w < 1$ . Clearly, for all liquids the value of  $\chi_w$  does increase with  $Bo \cos \theta$ . However, the data do not collapse into a single band of values including for  $\chi_w > 1$  corresponding to deformation mainly induced by gravity; hence,  $Bo \cos \theta$  is not the only parameter that determines the change of shape.

When the wall inclination is large, closer to vertical, the bubble shape seems to be close to that observed for a free rising case as shown in Fig. 4. For such a case, the bubble deformation is the result of the balance between inertial and surface tension forces. For freely ascending bubbles Moore [30] proposed a method to calculate the bubble deformation. Assuming that the bubble shape

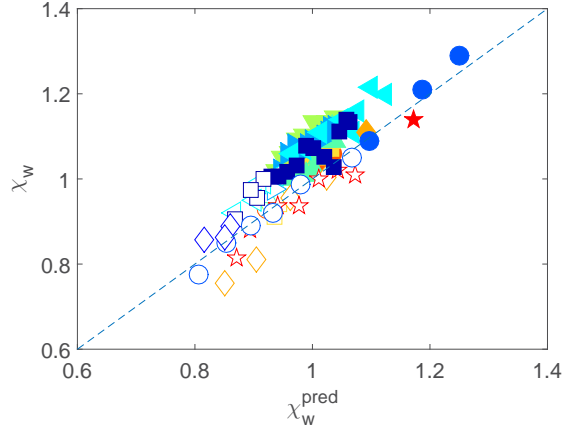


FIG. 6. Comparison between the experimental value of  $\chi_w$  and the prediction of Eq. (15), considering  $\alpha = 0.1$  and  $\beta = 3/32$ , for all experiments in Table 1: open and solid symbols represent experiments for  $\chi_w > 1$  and  $\chi_w < 1$ , respectively. The dashed line shows the perfect correlation.

is an ellipsoid of revolution one can write  $d_{\perp} = 2R(1 - \eta/2)$  and  $d_{\parallel} = 2R(1 + \eta)$ , with  $\eta \ll 1$ . By balancing the pressure distribution (from the irrotational flow around the bubble) with the surface tension force, it can be shown that  $\eta = -3/32We$ . For a bubble moving over a nearly vertical wall, considering  $We_w$  instead of  $We$ , the wall aspect ratio can be expected to vary as

$$\chi_w = \frac{d_{\parallel}}{d_{\perp}} \sim \frac{1 - \beta We_w}{1 + \frac{\beta}{2} We_w} \quad (14)$$

with  $\beta = 3/64$  for a freely ascending bubble. This expression would only be able to predict the bubble shape for inclinations near the vertical value, corresponding to large values of  $We_w$ . The effect of the interaction with the wall could be calculated by considering a mirror bubble. The potential solution of the velocity disturbance due to the mirror bubble is  $V_w(1 + \frac{2}{16}s)$ , where  $s = D_{eq}/L$ , taking  $L$  as the distance between the bubble center and the wall [31]. Considering that the bubble is in contact with the wall at  $s = 0.5$ , the velocity involved in the pressure at the bubble surface needs to be corrected by the prefactor  $1 + 1/16 = 17/16$ . Therefore, the corrected value of the  $\beta$  coefficient would be  $\beta_c = \beta(\frac{17}{16})^2$ . This correction would result in a slight increase in the bubble deformation, of about 10%. For simplicity, we do not account for this effect. Therefore, in Fig. 5(b), we plot  $\chi_w$  as a function of the corresponding  $We_w$  for all the experiments. As expected, the deformation (in the direction perpendicular to the wall) increases with  $We_w$ . However, considered alone the Weber number is not able to make possible a simple description of the bubble deformation when  $\chi_w < 1$ .

Both the gravitational and inertial effects on the bubble deformation need to be considered together to predict the wall aspect ratio. We now consider that a bubble deformed by gravity under the wall is also deformed by inertia due to its sliding motion. Combining both effects, the aspect ratio appears now under the form

$$\chi_w = \frac{(1 - \beta We_w)}{(1 - \alpha Bo \cos \theta)(1 + \frac{\beta}{2} We_w)}, \quad (15)$$

where  $\beta = 3/32$  and  $\alpha$  can be determined experimentally. Figure 6 shows the measured  $\chi_w$  as a function of the prediction from Eq. (15) considering a value of  $\alpha = 0.1$ , obtained from a minimum square fit scheme of the data and the prediction. The prediction that takes into account both gravitational and inertial effects provides a much better correlation than those tested above. Note

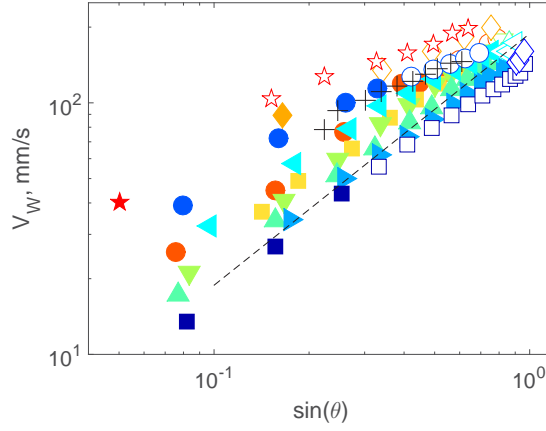


FIG. 7. Sliding bubble velocities,  $V_w$ , as a function of  $\sin \theta$ , where  $\theta$  is the inclination of the wall, for all the experimental conditions of Table I. The black + symbols show the results of Dubois *et al.* [17] for water ( $D_{\text{eq}} = 2.0$  mm). The dashed line shows the trend of the experiments by Tsao and Koch [10] ( $D_{\text{eq}} = 1.6$  mm), also for water.

that from Eq. (15) it is possible to determine the values of  $We_w$  and  $Bo$  for the transition, considering that  $\chi_w \approx 1$ .

### B. Sliding velocity and wall drag coefficient

The evolution of the steady sliding velocity with the inclination angle is shown in Fig. 7 for all the experimental conditions of Table I. For all experimental conditions, the bubble-wall velocity increases monotonically with the inclination angle. For all cases, the bubble velocity increases with wall inclination angle. When  $\chi_w > 1$ , the wall velocity appears to increase linearly with  $\sin \theta$ ; when the shape is such that  $\chi_w < 1$ , the increase of velocity with wall inclination is less pronounced. Clearly, the value of the velocity depends on both the size of the bubble and the properties of the liquid. As shown, the trend for the velocity is found to be in good agreement with previous experimental results [10,17].

To analyze the dynamic behavior of the motion, we need to determine the hydrodynamic force on the bubble as it slides over the wall. The driving force is simply the buoyancy, corrected for the wall inclination. The drag force parallel to the wall balances the buoyancy, and the corresponding balance equation can be written in terms of a wall drag coefficient such that

$$C_{Dw} = \frac{4 D_{\text{eq}} g \sin \theta}{3 V_w^2}. \quad (16)$$

Considering the classical representation, Fig. 8 shows the drag coefficient,  $C_{Dw}$ , as a function of the wall Reynolds number,  $Re_w$ , defined above, for all experimental conditions. As in the previous figure, the experimental values of  $C_{Dw}$  are shown as solid or open symbols for  $\chi_w > 1$  or  $\chi_w < 1$ , respectively. For the case of  $\chi_w > 1$  (bubbles elongated along the wall) a general trend of the form  $C_{Dw} \sim Re_w^{-1}$  is observed in accordance to what is observed for freely rising bubbles. Note that the drag coefficient does not fall into a single band of data, indicating that significant additional effects have to be accounted for. For bubbles with  $\chi_w < 1$  (bubbles elongated in the direction perpendicular to the wall), the drag coefficient appears to reach a constant value with respect to  $Re_w$ .

#### 1. Wall drag coefficient for $\chi_w > 1$

For freely rising spherical bubbles, the drag coefficient can be described by Moore's expression, Eq. (9), for  $Re > 50$ . However, for  $Re < 50$ , this expression is no longer applicable and it displays

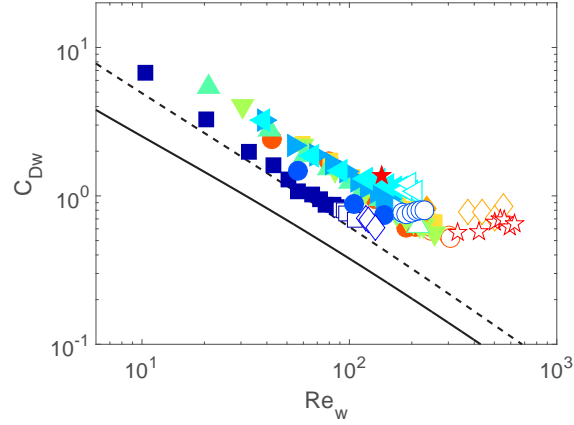


FIG. 8. Wall drag coefficient  $C_{Dw}$ , as a function of wall Reynolds number,  $Re_w$ , for all the experimental conditions of Table I. The solid and open symbols show the experiments for  $\chi_w > 1$  and  $\chi_w < 1$ , respectively. The black continuous and dashed lines show the prediction of Eqs. (17) and (20), respectively.

a nonphysical behavior. Instead we can use the expression proposed by Mei *et al.* [32] (obtained by fitting direct numerical simulations in order to recover Eq. (9) when  $Re \rightarrow \infty$ ):

$$C_D^{Mei} = \frac{48}{Re} [1 + F(Re)] \quad (17)$$

where

$$F(Re) = -\frac{2.211Re^{1/2} + 32/3}{Re + 3.315Re^{1/2} + 16}. \quad (18)$$

The function  $F(Re)$  could be interpreted as the drag correction that accounts for a spherical bubble boundary layer and wake whatever the value of  $Re$ . This relation is shown by the black continuous line in Fig. 8, considering  $V_w$  instead of  $V_{term}$ , to calculate  $C_{Dw}$  and  $Re_w$ . It serves as a reference to be contrasted with the wall measurements. As expected, the prediction is below that found for all experiments because the effect of the additional drag induced by the presence of the wall is not accounted for. Nevertheless, for the case of bubbles with  $\chi_w > 1$ , the decreasing trend of the drag coefficient also follows a  $Re^{-1}$  dominating trend.

When a bubble moves near a wall we can consider two additional contributions to the drag. First, the mirror image of the bubble induces a drag increase [33] which is at first order,

$$C_{Dw} = \frac{48}{Re_w} (1 + s^3), \quad (19)$$

where  $s = D_{eq}/L$ ,  $L$  being the distance between the bubble center and the wall. For a spherical bubble in contact with the wall  $s = 0.5$ . The second mechanism for drag increase is due to the production of additional vorticity on the bubble surface induced by the proximity of the wall. Figueroa *et al.* [6] showed that the additional drag due to vorticity production was  $6s^3 C_D^{Moore}$  for a bubble moving in between two walls. Therefore, considering the effect of only one wall and superposing the mirror effect, we can expect an evolution of the form

$$C_{Dw} = \frac{48}{Re_w} (1 + 4s^3 + F(Re_w)), \quad (20)$$

where  $F(Re_w)$  is defined by Eq. (18) and the term in  $s^3$  accounts for the mirror effect and the additional vorticity production. This prediction, considering a value of  $s = 0.5$ , shown in Fig. 8 by the black dashed line, is now closer to the experimental results for the E1 case. For this case,

the bubbles are nearly spherical (with a maximum  $We_w = 1.26$ ). The rest of the experiments have larger values of the drag coefficient than the prediction. Equation (20) was derived to consider two effects in interaction with a vertical wall: the mirror image of the bubble and the vorticity production at the wall. Although the prediction gives a better estimate of the wall drag, it is still below the experimentally obtained value for most cases. The fact that the predicted drag can be brought closer to the experimental measurements is noteworthy, but it is clear that the formulation is not sufficient to quantitatively calculate the wall drag. It is important to note that the flow analyzed by Figueroa *et al.* [6], from which Eq. (20) was derived, is not exactly the same as that studied here, since a film between the bubble and the wall is formed by the action of gravity. As shown before, this contribution needs to be accounted for in the description of the deformation; it is thus expected to have an effect on the drag force. Below, we directly consider the effect of the film between the bubble and the wall on the total wall drag.

When the bubble slides over the wall a flattened region appears and a thin lubrication film causes an increase of the drag force. The deformed region can be determined by a balance between gravitational and surface tension forces, as discussed by Mahadevan and Pomeau [29] for a horizontal wall and by Hodges *et al.* [22] for small inclination. Extending these results to an inclined wall (Bo being replaced by  $Bo \cos \theta$ ) the size of the contact region can be shown to be

$$\ell \sim (Bo \cos \theta)^{1/2} D_{eq} \quad \text{for } Bo \cos \theta < 1, \quad (21)$$

$$\ell \sim (Bo \cos \theta)^{1/4} D_{eq} \quad \text{for } Bo \cos \theta > 1. \quad (22)$$

The film thickness is obtained by considering the deformation induced by the viscous motion and the viscous effect in it [14]. The resulting film frictional viscous force is

$$F_{film} \sim \sigma \ell Ca_w^{2/3}, \quad (23)$$

where  $Ca_w = V_w \mu / \sigma$  is the wall capillary number. Writing the film force in dimensionless terms, we have

$$C_{Dfilm} \sim \frac{1}{Re_w} \frac{(Bo \cos \theta)^n}{Ca_w^{1/3}}, \quad (24)$$

where  $n = 1/2$  for  $Bo < 1$  and  $n = 1/4$  for  $Bo > 1$ .

Now, assuming that the effects can be superposed, we can write an expression for the drag on the bubble that accounts for the potential interaction and the viscous film drag. The mirror-additional vorticity contribution ( $6s^3 C_D^{Moore}$ ) is now replaced by the film drag [Eq. (24)] and we have

$$C_{Dw} = \frac{48}{Re_w} \left( 1 + s^3 + F(Re_w) + K_o \frac{(Bo \cos(\theta))^n}{Ca_w^{1/3}} \right), \quad (25)$$

where  $K_o$  is a constant that needs to be determined from the experiments.

To compare the experimental measurements with the prediction of Eq. (25) we separate the experimental results depending on whether  $Bo \cos \theta < 1$  or  $Bo \cos \theta > 1$ . Figure 9(a) shows experimental results for the case when  $Bo \cos(\theta) < 1$ . For this group of experiments the Bond number is approximately the same with a maximum value of  $Bo \cos(\theta) = 0.38$ . The continuous and dashed lines in the plot show the prediction of Eq. (25) considering  $n = 1/2$  and two values of the wall capillary number, corresponding to the minimum (continuous line) and maximum (dashed line) values of  $Ca_w$ : the black lines show the predictions for a small angle ( $\theta = 5^\circ$ ), while the red lines show the predictions for a large angle ( $\theta = 74^\circ$ ). The prediction, considering  $K_o = 0.3$  as the only fitting coefficient, agrees well with the experimental measurements. To show the relative importance of the viscous film term, the blue dash-dotted line in the figure shows the drag coefficient with  $K_o = 0.0$  (i.e., neglecting the film drag). For this case, the film friction accounts for up to 75% of the total drag; the mirror-image drag is approximately 5% of the total drag. Note also that the influence of the inclination angle is small.

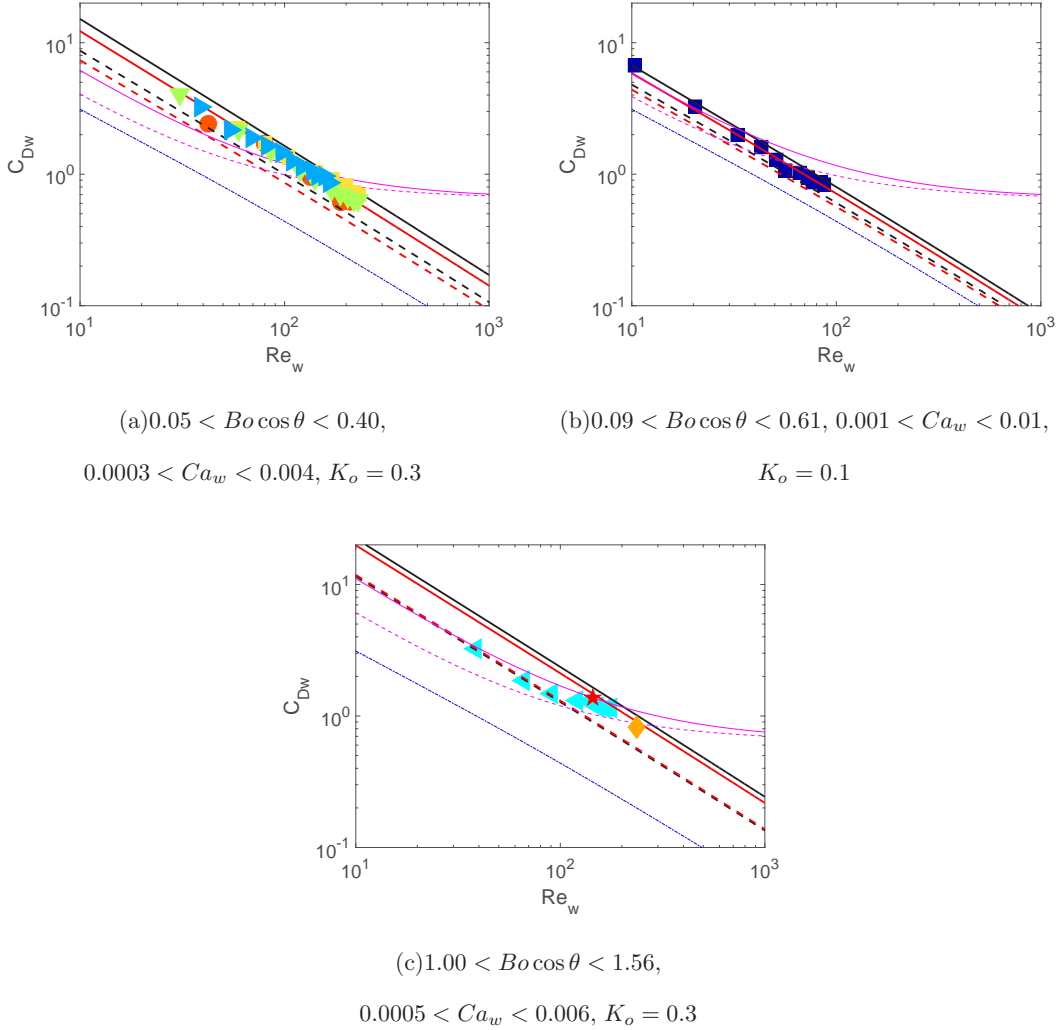


FIG. 9. Comparison between the measured wall coefficient and the prediction of Eq. (25). The continuous and dashed lines are the predictions for minimum and maximum values of  $Ca_w$ , respectively; the black lines show the prediction for  $\theta = 5^\circ$ ; the red lines show the prediction for  $\theta = 74^\circ$ , corresponding to the minimum and maximum angles of the entire set. (a)  $Bo < 1$ ,  $n = 1/2$ , experiments E4, E6, E7, E8, and E10; (b)  $Bo = 0.58$ ,  $n = 1/2$ , experiment E1; and (c)  $Bo > 1$ ,  $n = 1/4$ , experiments E5, E9, and E11. In all cases the blue dash-dotted line shows the prediction of Eq. (25) without the film drag ( $K_o = 0.0$ ). The magenta lines show the prediction from the model of Dubois *et al.* [17] for the corresponding values of the capillary numbers.

Of all the experiments with  $Bo \cos \theta < 1$ , only one case did not appear to be well predicted by Eq. (25) considering  $K_o = 0.3$ . This case is shown in Fig. 9(b), which corresponds to experiment E1. For this case, the bubbles are nearly spherical and the fluid is silicon oil which can be considered free of surface active agents. Considering that in this case we can expect a complete slip of the fluid velocity on the bubble surface, the drag on the film would be smaller than in the case of a partially contaminated bubble. Therefore, we can argue that for this particular experiment the value of the fitting coefficient  $K_o$  would be smaller. The lines on the plot were obtained considering  $K_o = 0.1$ . The Bond number is 0.57 and  $Ca = 0.01$  or  $Ca = 0.001$ . The agreement is also very good. In this case, the film drag accounts for only roughly 40% of the total drag.



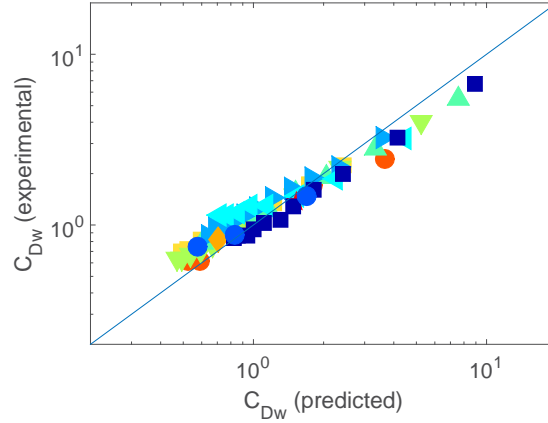


FIG. 10. Comparison between the experimental drag coefficient and the predictions from Eq. (25). The line shows a perfect correlation.

Figure 9(c) shows the experimental results for  $Bo \cos \theta > 1$ , for which  $n = 1/4$ . For these experiments, the functional dependence of  $C_{Dw}$  changes, according to Eq. (25). Considering a range of values of  $Bo \cos \theta$  from 1 to 1.56, the minimum and maximum values of  $Ca_w$  and  $K_o = 0.3$ , the prediction of the drag agrees well with the experimental measurements. The film drag for this case is about 70% of the total amount. Note also that the value of  $K_o$  is the same as for the data shown in Fig. 9(a), despite the fact that the Bond number is different.

For clarity we now show the predictions of Eq. (25) as a function of the experimentally determined drag coefficient, for all the experiments conducted in this investigation. The comparison is shown in Fig. 10. Clearly, the predictions are in good agreement with the experimental measurements. The maximum difference between the prediction and the experiments is about 30%.

We can now draw some comparisons with previous models. From Dubois *et al.* [17], we can obtain an expression for the total wall drag coefficient, given by

$$C_{Dw} = \frac{\alpha}{Re} + \beta + a \frac{2}{\pi} \sqrt{\frac{2}{3}} \frac{1}{Re} \frac{Bo^n}{Ca^{1/3}} \quad (26)$$

with  $n = 1/2$  or  $n = 1/4$  for  $Bo < 1$  and  $Bo > 1$ , respectively. The parameters  $\alpha = 16$ ,  $\beta = 0.65$ , and  $a = 9$  are fitting coefficients of their experiments conducted for  $0.026 \leq Re_w \leq 840$ . The first two terms correspond to the drag resulting from the flow around the bubble and the third term corresponds to the film drag. The coefficient  $\alpha$  is much smaller than its equivalent term in Eq. (25) and corresponds to the small Reynolds limit of  $F(Re)$ . The value of the coefficient  $\beta$  is discussed in the next section. For the film drag, the value  $a = 9$  corresponds to  $K_o = 0.0975$ . This value is significantly smaller than ours ( $K_o = 0.3$ ). The predictions from Eq. (26) are shown in Fig. 9, by the magenta lines. Overall, the wall drag coefficient is underpredicted by this correlation for small  $Re_w$ ; the agreement is better for  $Bo > 1$ . There is a significant deviation of behavior for large values of  $Re_w$ .

It is also possible to draw comparisons with the model proposed by Aussillous and Quéré [14]. They addressed only the small  $Re_w$  regime ( $Re_w \leq 0.2$  for their experiments) so their prediction is not reported in our figures for clarity. Writing their force expression in the same format as Eq. (25), we have

$$C_{Dw} = a \frac{16}{3} \frac{1}{Re} + b \frac{8}{3} \frac{1}{Re} \frac{Bo^{1/2}}{Ca^{1/3}}, \quad (27)$$

where  $a = 5$  and  $b = 2.3$  are fitting parameters. The value of  $a$  is larger than that for the viscous drag force of a single bubble ( $a = 3$ ), in agreement with our Eq. (25). The fitting coefficient  $b$  can

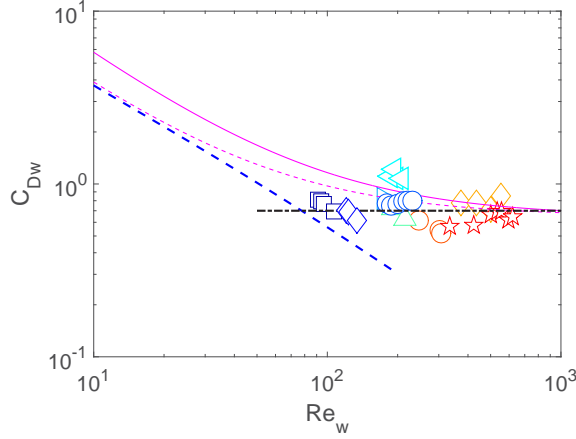


FIG. 11. Wall drag coefficient,  $C_{Dw}$ , as a function of wall Reynolds number,  $Re_w$ , for all the experiments from Table I for which  $\chi_w < 1$ . The dash-dotted line shows  $C_{Dw} = 0.7$ . For comparison, the dashed line shows the prediction from Eq. (20). The solid and dashed magenta lines show the predictions from Eq. (26) from Dubois *et al.* [17], for two different values of the capillary number.

compared to our  $K_o$  in our Eq. (25), leading to  $K_o = b/18 = 0.128$  which is in reasonable agreement considering the differences in the range of  $Re$ .

## 2. Wall drag coefficient for $\chi_w < 1$

As discussed above, when the bubble is deformed due to the inertia of the flow, the wall aspect ratio is smaller than one ( $\chi_w < 1$ ). In this case, the bubble shape is closer to that observed in a freely rising bubble. Barbosa *et al.* [11] argued that the drag force on such bubbles results from the pressure difference between the front and the rear of the bubble where the flow is detached so that the pressure difference scales as  $\rho V_w^2$  and we can expect that  $F_D \sim \rho V_w^2 D_{eq}^2$ . For such a shape, the formation of “proper film” is not clear [see Figs. 4(c), 4(d), and 4(e)]. The contact area between the bubble and the wall is very small; therefore, the induced dissipation in this region is not expected to result in a dominant contribution. In other words, the film drag gives negligible contribution. Considering that the drag force is balanced with the buoyancy, we have

$$\rho V_w^2 D_{eq}^2 \sim \rho g D_{eq}^3 \sin(\theta). \quad (28)$$

Considering the definition of the drag coefficient, from Eq. (16), we can write

$$C_{Dw} \sim \frac{g D_{eq} \sin(\theta)}{V_w^2} = \text{const.} \quad (29)$$

Therefore, if  $\chi_w < 1$  the wall drag coefficient can be expected to be independent of the wall Reynolds number. Note that the Froude number can be defined as  $Fr_w = V_w / \sqrt{g D_{eq}}$  from which we can write  $Fr_w^2 \sim \sin(\theta)$ .

Figure 11 shows the drag coefficient as a function of the Reynolds number, for the data with  $\chi_w < 1$ , which clearly shows that  $C_{Dw} \approx 0.7$  and nearly constant for most experiments. This value is close to the fitting parameter  $\beta = 0.65$  in Dubois *et al.* [17]. The data cover a significant range of wall Reynolds numbers from 150 to 650, approximately. The only case for which the experimental drag is not within the rest corresponds to experiment E5, which has been argued to have significant levels of surface contaminants; therefore, it could be expected to show larger values of the drag. Note that this change of trend was already reported by Tsao and Koch [10] but was not discussed

or identified. In the figure, the prediction from Eq. (26) is shown for two values of the capillary number. Clearly, for large  $Re_w$  the prediction asymptotes to a similar value.

#### IV. CONCLUSION

In this paper we studied the motion of bubbles sliding steadily over a flat inclined wall. Surprisingly, previous studies had not proposed a generalized correlation for the drag coefficient of the bubble in this configuration. More importantly, the alignment of the bubble with respect to the wall had not been identified as a relevant feature to determine such a coefficient. Thanks to the wide range of experimental parameters that were covered in the study, we were able to, first, identify the conditions for the transition between bubble alignment with the wall or perpendicular to it. Consequently, the experimental data were divided into two groups. In this manner, drag correlations were proposed for each case, taking into account only the relevant physical mechanisms involved in each condition. What our results show is that the transition from spherical to oblate shape that leads for a single bubble to a significant increase of the drag coefficient due to deformation (see Fig. 5 in Maxworthy *et al.* [34] and our Fig. 3) is not observed for a bubble moving in a close interaction with a wall. Indeed, the drag coefficient changes directly to a constant value corresponding an inertia dominating drag.

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