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1 Optimization of Electrochemical Time of Flight Measurements for Precise  
2 Determinations of Diffusion Coefficients over a Wide Range in Various Media

3

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6

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13

14 **Abstract:** Diffusion coefficients are an important physical property to both physical and  
15 analytical electrochemistry and the role they play in sensors, batteries, and catalysis. In  
16 electrochemical time of flight (ETOF), the time needed for an electrochemically generated  
17 species to travel to an adjacent electrode is measured. Previously relegated to verifying  
18 diffusion modeling and theoretical work, ETOF is a powerful and elegant technique whose  
19 broad applicability has been overlooked. In the determination of diffusion coefficients,  
20 ETOF does not require setting delicate hydrodynamic conditions required by rotating ring  
21 disk (RDE) methods. In addition, no foreknowledge about the complete electrochemical  
22 mechanistic system, nor about its electron stoichiometry is required. ETOF is ideal for  
23 determining the diffusion coefficients for non-elucidated systems, such as for short-lived  
24 intermediates assuming they survive ETOF travel time. Here we report the construction  
25 of an empirical calibration curve for the determination of diffusion coefficients using  
26 experimental parameters optimized by computer modeling. Using a platinum micro  
27 electrode array, diffusion coefficients were determined for a variety of species including  
28 ferrocenium, ruthenium(III) bisbipyridine dichloride, and vanadium(III) acetylacetonate,  
29 some of which being previously unreported. The elegance of the method is that the  
30 calibration curve constructed with a few well-established species in a given electrolyte  
31 can be used for any species in any electrolyte.

32

33 **Keywords:** Electrochemical time-of-flight, Diffusion coefficient, Generator-collector  
34 mode, Calibration curve, vanadium(III) acetylacetonate

35

## 36 1. Introduction

37 In addition to being a fundamental property of any solute, diffusion coefficient values are  
38 crucial in several applications of electrochemistry. Diffusion plays a pivotal role in  
39 analytical or mechanistic investigations as well as for amperometric and potentiometric  
40 sensors(1), electrosynthesis(2), redox flow batteries(3), etc. These are all applications  
41 where the electrical response depends on the diffusion of molecules to and from an  
42 electrode. Typically, precise diffusion coefficients values,  $D$ , are determined either by  
43 electrochemical means using for example scanning electrochemical microscopy (SECM)  
44 (4-9) or rotating ring disk (RDE) methods (10-17). RDE methods are based on the Levich  
45 equation, Eq 1. The RDE limiting diffusion current plateau value,  $i_{Lev}$ , is directly  
46 proportional to the two-thirds root of diffusion coefficient of the analyte,  $D$ . However, prior  
47 knowledge of the number of electrons transferred,  $n$ , the active area of the electrode,  $A$ ,  
48 the kinematic viscosity of the supporting electrolyte,  $\nu$ , and the analyte concentration of  
49 the bulk solution,  $C_s$  (12) is also required. To determine the diffusion coefficients  $i_{Lev}$   
50 values are plotted as a function of  $\sqrt{\omega}$ . The slope is determined and  $D$  is calculated.

$$51 \quad i_{Lev} = 0.620nFAD^{\frac{2}{3}}\omega^{\frac{1}{2}}\nu^{\frac{-1}{6}}C_s \quad (1)$$

52 This can lead to experimental challenges, as several of the terms in the slope of Eq. 1  
53 must be known to calculate the diffusion coefficients. Due to specific mechanistic  
54 circumstances,  $n$  may not be an exact integer (18) since it may vary continuously with the  
55 timescale of the experiment(19). Kinematic viscosity of the solution and the concentration  
56 of the analyte can be determined through additional experiments, but this makes for an  
57 additional burden. In addition, every electroactive analyte experiences different diffusion

58 coefficient values in different media. Using RDE to determine diffusion coefficients  
59 requires a new Levich plot to be constructed for each Red/Ox analyte every time any of  
60 the terms  $n$ ,  $A$ ,  $\nu$ , and  $C_s$  change. Finally, it should be noted that Eq. 1 relates to the  
61 diffusion coefficient of the bulk electroactive species in solution and not the product(s)  
62 formed by reduction or oxidation. Diffusion coefficients of reaction products can be  
63 measured by RRDE, but that technique is not used routinely for this purpose.

64 It is also possible to determine values of  $n$  and  $D$  simultaneously by comparing responses  
65 from a transient technique to that of a steady state technique at a microelectrode.  
66 However, in order to avoid biases introduced by the exact electrode surface area and  
67 size, the method requires the use of an internal standard with known  $n$  and  $D$ . The  
68 techniques also requires high experimental precision and accuracy. In addition, when  $n$   
69 values are susceptible to depend on the time scale due to kinetics special care is required  
70 to compare responses corresponding to the same time-scale as detailed in reference(18).

71 In SECM, the probe serves as the detecting electrode for a redox species generated at  
72 the surface under examination. The diffusion coefficient is determined by measuring the  
73 time of maximum collection at different probe distances from the surface. In this respect,  
74 SECM and electrochemical time of flight (ETOF) (20) are formally identical as both involve  
75 generation and collection of the species of interest. SECM and ETOF approaches differ  
76 only in that SECM relies on collector-generator current feedback magnitude (viz., on  
77 collection efficiencies), while ETOF relies on direct measurements of travel times of the  
78 generated species of interest between its source (the generator electrode) and its sink  
79 (the collector electrode(s))(21). Additionally, SECM-based methods may not be applicable

80 in structured electrolyte media such as polymers or sol-gel materials in which diffusion  
81 coefficient values may be required (17).

### 82 1.1 ETOF principle

83 ETOF is a well established method, first developed by Royce Murray(22) to determine  
84 diffusion coefficients. In this work we wish to introduce a new and universal application of  
85 its principle to measure diffusion coefficients in any medium and electrolyte based on  
86 reference measurements made in another one. For this reason let us first recall the  
87 principle and theoretical basis of ETOF to allow the introduction of its present application.

88 ETOF consists in measuring the time that a generated species took to travel from one  
89 electrode to an adjacent detecting electrode; the travel time could then be related to the  
90 diffusion coefficient. Murray was interested in determining the apparent diffusion  
91 coefficients of electron-hopping across conducting polymers sandwiched between two  
92 electrodes. For ETOF travel time of maximum collection,  $t_{mc}$ , relates the diffusion  
93 coefficient,  $D$ , through Einstein's equation, (Eq. 2), to the distance traveled or gap,  $g$ ,  
94 between the two electrodes and a numerical dimensionless constant,  $K$ , that depends  
95 exclusively on the electrode array geometry. The latter does not depend on the  
96 electrochemical medium, nor on the half-life time,  $t_{1/2}$ , of the species of interest provided  
97 that  $t_{1/2}$  is greater than  $t_{mc}$ .

$$98 \quad g = K\sqrt{Dt_{mc}} \quad (2)$$

99  $K$  can be predicted computationally for generator-collector systems having ideal  
100 geometries (23, 24) or evaluated empirically based on calibrations performed for micro-  
101 systems of any geometry (25-27). In the most popular procedure of ETOF, the generator

102 is pulsed to a potential that generates a swarm of diffusible species, while the detector is  
103 held at a constant potential in order to re-reduce or re-oxidize the generated species (Fig.  
104 1A). These experiments have been limited to model compounds such as ruthenium  
105 hexamine(24, 26), ferricyanide(23, 24), hydroxymethylferrocenium(28) or the analyte of  
106 interest in a previous study(25). Most of the literature reports the use of ETOF as a way  
107 to verify computational models of diffusion between electrodes, viz., as a way to assess  
108 experimentally the “ideality” of the microfabricated electrode pattern. The current ETOF  
109 approach has been to measure  $t_{mc}$  at various distances between the generating and  
110 detecting electrodes to determine diffusion coefficients, and then compare to the  
111 theoretical estimate. Here we point out that the practical applications of ETOF have been  
112 largely over looked, and ETOF is a simple technique capable of measuring the diffusion  
113 coefficients of a variety of substances in various media.

## 114 *1.2 Previous Work and Outline of this Work*

115 Previously some of us presented a novel data treatment for ETOF that provided a simple  
116 and elegant method for determining diffusion coefficients(29). In this approach, a  
117 calibration curve is constructed by measuring the time of maximum collection ( $t_{mc}$ )  
118 between two parallel band electrodes in a microelectrode array of having a single and  
119 constant distance,  $g$ , between the generator and collector electrodes. Using species with  
120 known diffusion coefficients as “standards” in the medium of interest,  $t_{mc}$  is recorded for  
121 each electrochemically generated species. Rewriting Eq. 2 as

$$122 \quad \sqrt{t_{mc}} = \frac{g}{K\sqrt{D}} \quad (3)$$

123 and plotting  $\sqrt{t_{mc}}$  variations as a function of  $\frac{1}{\sqrt{D}}$  produces a calibration curve that is used  
124 to determine diffusion coefficients of unknown species regardless of other characteristics  
125 of the medium and of the species.

126 In this paper, we have expanded electrolyte solutions to include non-aqueous solvents.  
127 In addition, computer modeling assisted the optimization of the pulse widths for the  
128 generator so that diffusion coefficients could be determined over a large dynamic range  
129 with an adequate precision and accuracy.

## 130 **2. Theoretical optimization of precision and accuracy in ETOF measurements**

131 As shown in Fig. 1, applying a sufficiently brief potential pulse to the generator electrode  
132 generates a local concentration of B in its immediate vicinity(30). Diffusional broadening  
133 of this concentration pulse over the insulating gap  $g$  allows capture by the collector(s);  
134 because of the short duration of the generator pulse, B is rapidly exhausted. Hence, a  
135 peak-shaped current response is expected at the collector (23, 31) whose maximum time  
136 position,  $t_{mc}$ , in a static solution is directly correlated to the time-of-flight (TOF) of species  
137 B. However, if the pulse width ( $t_{pulse}$ ) is too long, and the electrochemical detection of B  
138 regenerates A at the collector electrode, the regenerated species A may then diffuse back  
139 to the generator electrode where it can again form B. This redox-cycling leads to an  
140 inaccurate value for  $D$ . Specifically, the result of redox-cycling is that the time position of  
141 the maximum collector current  $t_{mc}$  shifts towards greater values since it now represents a  
142 convolution between the shortest TOF and the maximum redox-cycling efficiency. In the  
143 absence of any noise or background interference, a  $t_{pulse}$  value preventing redox-cycling  
144 gives the most accurate values for  $D$  of species B. At the other extreme, too short  $t_{pulse}$



145 values lead to generating small quantities of B which are difficult to detect with proper  
146 precision at the collector, lowering the accuracy of  $t_{mc}$  determination. This experimental  
147 conflict between accuracy and precision indicates that the  $t_{pulse}$  value should be  
148 maximized, yet less than  $t_{pulse}^{max}$ , the value beyond which redox-cycling contributions will  
149 alter the accuracy. Modeling the diffusion demonstrates that the  $t_{pulse}^{max}$  value is not  
150 universal but depends on the rate of diffusion of the species of interest over the insulating  
151 gaps. However, even an unknown diffusion coefficient can be approximated by simple  
152 measurements of  $t_{mc}$ .

153 The present work shows that modeling can guide the selection of experimental  
154 parameters for ETOF resulting in the accurate determination diffusion coefficients, as well  
155 as further validating the experimental principle of determining diffusion coefficients by  
156 ETOF. Because  $K$  and  $g$  are geometric parameters, independent of the properties of the  
157 electrolyte medium and of the substrate whose  $D$  value is sought to be measured, it is  
158 possible to construct an empirical calibration curve relating  $D$  and  $t_{mc}$  values (Eq. 3) using  
159 a series of parallel microelectrode arrays. Once the calibration curve is constructed in one  
160 medium, the same microelectrode array (with the same geometry) may then be used to  
161 determine diffusion coefficients of other species in any media. One can measure the  $t_{mc}$   
162 value of an electrogenerated species in any medium, and take that  $t_{mc}$  to the calibration  
163 curve and estimate the  $D$  for that species in electrolyte medium used. There is one caveat.  
164 Since the diffusion coefficient for a species may vary greatly from one medium to the next,  
165  $t_{pulse}^{max}$  along with  $t_{mc}$  may vary, leading to an inaccuracy in the determination of diffusion  
166 coefficient caused by redox-cycling (*vida supra*). For these reasons, we wish to present

167 the results of a simplified theoretical analysis aimed to evaluate the relationship between  
168  $t_{\text{pulse}}^{\text{max}}$  and  $t_{\text{mc}}$  values.

## 169 2.1 Numerical Simulations using COMSOL

170 Our theoretical analysis was performed using COMSOL simulations of ideal micro-device  
171 systems consisting of three parallel microband electrodes of common width,  $w$ , separated  
172 by insulating gaps of common width  $g$  with the array being imbedded flat in an insulating  
173 plane (Fig. 1A)(20, 29). Owing to its scope, this theoretical analysis was simplified  
174 assuming that the electrodes present no vertical edges and that no metallic conductor  
175 was located within the gap separating the generator and collector electrodes in order to  
176 avoid complications related to any bipolar activity that may be induced over such isolated  
177 conductors(32, 33).

178 We assume that the semi-infinite bulk electrolyte contains only species A. Species A  
179 reduces or oxidizes at the generator electrode whose potential is stepped for a fixed time  
180 duration,  $t_{\text{pulse}}$ , and then returned to an open circuit potential (Fig. 1B). This generates a  
181 peak-shaped current response (Fig. 1C) characterized by its current maximum,  $i_{\text{mc}}$ , and  
182 its time position,  $t_{\text{mc}}$ , after the beginning of the pulse ( $t = 0$ ).

183 Fig. 2A illustrates the outcome of the corresponding simulations showing how the  
184 collector peak-shaped response varies when  $t_{\text{pulse}}$  increases. Fig. 2B reports the  
185 variations of  $t_{\text{mc}}$  normalized to its ideal limit when  $t_{\text{pulse}} \rightarrow 0$ , as a function of  $t_{\text{pulse}}$  also  
186 normalized to the same limit. The dimensionless presentation of the theoretical results in  
187 Fig. 2B is independent of the exact nature of the redox system considered and of the  
188 geometry of device used, provided that the width,  $w$ , of the band electrodes remains

189 sufficiently small vs the gap,  $g$ . The results in Fig. 2B evidence that  $t_{\text{pulse}}/t_{\text{mc}}$  must be  
190 smaller than 0.03~0.04 to yield accurate measurements. This constraint is independent  
191 from the exact mechanism involved by the electrochemical processes investigated  
192 provided that the species B generated at the generator by reduction or oxidation of  
193 species A is the only one that is collected at the collector. In the case here, the generator  
194 and collector potentials are experimentally chosen so that the reduction of A (or its  
195 oxidation) and the detection of B are performed at the current limiting plateaus of the  
196 corresponding electrochemical waves. B could be a follow-up product resulting from an  
197 EC mechanism at the generating electrode, e.g.:  $A \pm e^- \rightarrow A^\pm \rightarrow B$ . One constraint is that  
198 the half-life time,  $t_{1/2}$  of  $A^\pm$ , the primary intermediate formed by the reduction of A, must  
199 be negligible compared to  $t_{\text{mc}}$ . If that were not the case, the ETOF method would provide  
200 a “mixed” diffusion coefficient convoluting those of B and  $A^\pm$ . Therefore, the ETOF method  
201 should be reserved for the analysis of redox systems whose CV simultaneously displays  
202 the voltammetric waves of A (forward scan) and B (backward scan) containing no  
203 intermediate wave within a single voltammetric scan. The time scale is such that the scan  
204 rate,  $v_{\text{mc}}$ , should be approximately  $v_{\text{mc}} \sim RT/(Ft_{\text{mc}})$  where  $R$  is the gas constant,  $F$  is the  
205 Faraday value, and  $T$  is the absolute temperature(34). As discussed later we discovered  
206 such a case when determining the diffusion coefficient for the oxidation product of  
207  $\text{VO}(\text{acac})_2$ . (*vida infra*) whose oxidation has been reported to provide a chemical  
208 conversion to  $\text{V}(\text{acac})_3$ .(35).

## 209 2.2 Conclusions from Simulations with COMSOL

210 The first conclusion of this theoretical analysis is that the duration of the generator pulse  
211 duration,  $t_{\text{pulse}}$ , should not exceed a maximum value being ca. 0.03 to 0.04 times that of

212 the minimal value of the experimentally determined  $t_{mc}$ . This is especially important when  
213 dealing with an unknown system.  $t_{mc}$  can be evaluated from several experiments at  
214 different  $t_{pulse}$  to respect the criterion in Fig. 2B. A second conclusion is that the ETOF can  
215 determine the diffusion coefficient of any species that is the product of the reduction or  
216 oxidation of a precursor species, A or a chemical product from an EC mechanism  
217 provided the  $t_{1/2}$  of its formation from the primary generated product is negligible vs  $t_{mc}$ .

### 218 **3. Experimental**

#### 219 *3.1 Materials and electrochemical device*

220 All electrochemical measurements were performed using a CHInstruments 750a  
221 bipotentiostat. The time duration and application of  $t_{pulse}$  for the generator was controlled  
222 by National Instruments LabVIEW software. Microband electrode arrays of 16 platinum  
223 or gold fingers, 2 mm long, 25  $\mu\text{m}$  wide with gaps of 25  $\mu\text{m}$  were fabricated at the  
224 Arkansas High Density Electronics Center (HiDEC). Using either one of these arrays  
225 provided essentially identical results. A saturated KCl Ag/AgCl reference electrode was  
226 used in aqueous solutions. A saturated calomel electrode fitted with an organic solvent  
227 bridge made with TBAPF<sub>6</sub> in the solvent considered was constructed for use in organic  
228 solvents. Measurements were performed in a VAC-atmospheres glovebox with a purified  
229 anhydrous nitrogen atmosphere. The atmosphere was purged extensively between  
230 experiments while the SCE was sealed in a gastight container.

#### 231 *3.2 Chemicals*

232 Diffusional reference “standards”, potassium ferrocyanide (Certified ACS grade, Fischer),  
233 potassium ferricyanide (Certified ACS grade, Fischer), ruthenium (III) hexamine chloride

234 (Alfa Aesar), ferrocene (98% Sigma Aldrich), ferrocene acetic acid (98% Sigma Aldrich),  
235 and ruthenium bisbipyridine dichloride ( $\text{Ru}(\text{bpy})_2\text{Cl}_2$ ) (97% Sigma Aldrich) were used as  
236 received. Two electrolyte solutions were made: one (aqueous) consisting of 0.1 M KCl  
237 (ACS grade, J.T. Baker); the other (organic) consisting of 0.1 M  $\text{TBAPF}_6$  (98%, Sigma  
238 Aldrich) in acetonitrile (HPLC Grade, Fischer). The vanadyl acetylacetonate ( $\text{VO}(\text{acac})_2$ )  
239 was synthesized from Vanadium(V) Oxide (98%, Sigma Aldrich) and acetylacetone  
240 (Reagent Plus grade, Sigma Aldrich) according to the literature method and was  
241 recrystallized from dichloromethane (36).

### 242 3.3 Conditions of electrochemical measurements

243 5 mM solutions were made of each “reference” electroactive compound, i.e. those with  
244 known diffusion coefficients. Three equally spaced (gap distance of  $g=75\mu\text{m}$ ) microband  
245 electrodes ( $w=25\mu\text{m}$ ) were selected by pairing sets of microbands available in the  
246 microfabricated arrays to perform ETOF measurements. The other 13 microbands  
247 present in the array were left open-circuit. The generator electrode potential was imposed  
248 for a time duration,  $t_{\text{pulse}}$ , and then open circuited to minimize current feedback. The  
249 potentials on the two flanking collector electrodes remained continuously poised(29).

250 The applied potentials values were determined using cyclic voltammetry (CV). CV was  
251 also used to ensure that the condition  $t_{1/2} \ll t_{\text{mc}}$  was valid for complex mechanisms.  
252 Measurements were performed in either 0.1 M KCl or in 0.1 M  $\text{TBAPF}_6$  / acetonitrile. For  
253 the latter case, unless otherwise noted, all potentials were referenced to a SCE using a  
254 double salt bridge. The potential window for the CV for ferrocene and ferrocenyl acetic  
255 acid solutions was from -0.6 V to +0.8 V, and the ETOF potentials were selected as

256 follows. For experiments with ferrocene, the generator was pulsed to +0.8 V while the  
257 collectors were held at +0.1 V. For ferrocene acetic acid, the generator was pulsed to  
258 +0.5 V while the collectors were held at +0.1 V. The CV potential window for  
259 Ru(II)(bpy)<sub>2</sub>Cl<sub>2</sub> was +0.5 V to -0.2 V and the ETOF potentials were set at +0.5 V for the  
260 generator pulse and -0.1 V for the collectors. The ferrocene/ferrocenium had a known  
261 diffusion coefficient in the literature(37) and Ru(II)(bpy)<sub>2</sub>Cl<sub>2</sub> was compared to an estimated  
262 diffusion based on its mass(38).

263 The mechanism occurring during the V<sup>IV</sup>O(acac)<sub>2</sub> oxidation wave is complex (34,35),  
264 possibly leading to formation of V(acac)<sub>3</sub> (see Appendix A). The potential window for the  
265 CV of VO(acac)<sub>2</sub> was thus extended from +2.0 V to -2.0 V to identify the ETOF potentials.  
266 These were set at +1.0 V for the generator pulse and -1.5 V for the collectors in order to  
267 determine the diffusion coefficient of V(acac)<sub>3</sub>, the suspected product. Under these  
268 conditions, only two waves were observed, the oxidation one of V<sup>IV</sup>O(acac)<sub>2</sub> and the  
269 reduction one of its oxidation product observed during the backward scan (35)

## 270 **4. Results and Discussion**

### 271 *4.1 ETOF calibration curve*

272 An experimental ETOF calibration curve (Fig. 3) was constructed with a constant value  
273 of  $t_{\text{pulse}} = 61$  ms using the same electrode array as before(29). A calibration curve was  
274 constructed based on the experimental  $\sqrt{t_{mc}}$  values determined in 0.1 M KCl, using three  
275 “reference” species, formed at the generator. The respective  $D$  values taken from  
276 literature reports, vis. ferrocyanide ( $D = 6.5 \times 10^{-6}$  cm<sup>2</sup>/s)(24), ferricyanide ( $D = 7.2 \times 10^{-6}$   
277 cm<sup>2</sup>/s)(39), and ruthenium(II) hexamine ( $D = 7.8 \times 10^{-6}$  cm<sup>2</sup>/s)(24). The  $K$  constant in Eq.

278 3, was determined from the slope  $(3.23(\pm 0.03) \times 10^{-3})$  of the regression line after forcing  
279 the line through the origin in order to comply with the theory. A band separation of  $g =$   
280  $75\mu\text{m}$  provided a value for  $K = 2.32(\pm 0.02)$ . The  $t_{\text{mc}}$  measured for these three “reference”  
281 species using a  $t_{\text{pulse}} = 61$  ms, satisfied the criterion  $(t_{\text{pulse}}/t_{\text{mc}} = 0.037)$ , developed by the  
282 modeling ensuring no recycling and sufficient collection current to determine  $t_{\text{mc}}$  with  
283 precision.

284 Using this calibration curve, the diffusion coefficients values for the other species  
285 ferrocenium and ferrocenium acetic acid could be determined based on their  $t_{\text{mc}}$  values.  
286 However, the case of ferrocene/ferrocenium serves to illustrate the danger of using too  
287 large a value for  $t_{\text{pulse}}$ . The ferrocenium generated has a three times larger diffusion  
288 coefficient,  $D = 2.24(\pm 0.07) \times 10^{-5} \text{ cm}^2/\text{s}$  (37), than those used to construct the calibration  
289 line in Fig. 3. Use of the same pulse width  $t_{\text{pulse}} = 61$  ms, resulted in a  $t_{\text{mc}}$  value of 0.93 s,  
290 which the calibration curve translated as a diffusion coefficient for ferrocenium of  
291  $1.22(\pm 0.03) \times 10^{-5} \text{ cm}^2/\text{s}$ , i.e., half the value of  $2.24(\pm 0.07) \times 10^{-5} \text{ cm}^2/\text{s}$  reported in the  
292 literature (37). Ferrocenium diffuses rapidly making  $t_{\text{pulse}}/t_{\text{mc}} = 0.065$ , resulting in recycling,  
293 and yielding an incorrect value. We described this result to illustrate the necessity of  
294 respecting the criterion in Fig. 2B, i.e.,  $t_{\text{pulse}}/t_{\text{mc}} < 0.037$ .  $t_{\text{pulse}}$  was then decreased from 61  
295 ms to 24 ms, and the resulting diffusion coefficient value of  $2.4(\pm 0.1) \times 10^{-5} \text{ cm}^2/\text{s}$  for  
296 ferrocenium, falling within 7% of the reported literature value in acetonitrile. Fig. 3 shows  
297 the relative positions of the two corresponding data points for ferrocenium using both  
298 values for  $t_{\text{pulse}}$ . A similar yet inaccurate value was obtained for the diffusion coefficient of  
299 ferrocenium acetic acid (not shown). Using  $t_{\text{pulse}} = 61$  ms afforded  $D = 1.10(\pm 0.05) \times 10^{-5}$   
300  $\text{cm}^2/\text{s}$  for ferrocenium acetic acid using the calibration line in Fig. 3, or half the value of

301 the predicted based on its molecular weight(38). In the case of determining the diffusion  
302 coefficient for an unknown species, this illustrates the importance of verifying that the  
303  $t_{\text{pulse}}/t_{\text{mc}}$  criterion be satisfied; easily determined as  $t_{\text{pulse}}$  is selected and  $t_{\text{mc}}$  is measured.

#### 304 *4.2 Aqueous Diffusion Coefficient Calibration Curves Can Extend to Organic Solvents*

305 The previous calibration curve in Fig. 3 was constructed using literature values for  
306 diffusion coefficients ( $D_s$ ) and measuring  $t_{\text{mc}}$  in 0.1 M KCl for each “reference” species.  
307 However, the value of the constant  $K$  is an intrinsic characteristic of the microelectrode  
308 array and not of the redox system investigated nor the electrolyte medium used. Hence,  
309 the calibration curve in Fig. 3 should be valid in all electrolytes even if the curve was  
310 constructed using different redox couples in 0.1M KCl. To test the validity of this  
311 prediction,  $t_{\text{mc}}$  was determined in 0.1 M TBAPF<sub>6</sub> / acetonitrile for the oxidation product of  
312 ferrocene and Ru(bpy)<sub>2</sub>Cl<sub>2</sub>. The corresponding results are shown in Fig. 4, the dotted  
313 regression line being taken from Fig. 3, using 0.1 M KCl electrolyte. Using the  $t_{\text{mc}}$  values  
314 taken in acetonitrile, and the calibration curve constructed using 0.1 M KCl electrolyte,  
315 the resulting diffusion coefficients for ferrocenium (37) and Ru(bpy)<sub>2</sub>Cl<sub>2</sub><sup>+</sup> (38) matched  
316 perfectly the literature data for their diffusion coefficients in acetonitrile. This validates our  
317 claim that diffusion coefficient calibration curves constructed using a few “reference”  
318 species in a given electrolyte can then be used to determine diffusion coefficients in other  
319 electrolytes including organic media. As we will note in the next section the ETOF method  
320 is not at all restricted to A/B redox systems involving a single reversible electron transfer  
321 step but is also applicable to more complex kinetic sequences, as in the case reported  
322 for VO(acac)<sub>2</sub> (35).

#### 323 *4.3 ETOF Applied to VO(acac)<sub>2</sub> in acetonitrile / 0.1 M TBAPF<sub>6</sub>*



324 As mentioned in the Experimental section, the electrochemical oxidation of vanadyl  
325 acetylacetonate,  $\text{VO}(\text{acac})_2$  is reported to lead to  $\text{V}(\text{acac})_3$  (35). The generation of  
326  $\text{V}(\text{acac})_3$  from  $\text{VO}(\text{acac})_2$  has been previously studied(35), (40), (41), (42) but a definitive  
327 mechanism of reaction following  $\text{VO}(\text{acac})_2$  oxidation could not be presented. However,  
328 the following critical observations were made. 1) The CV reduction wave of the oxidation  
329 product of  $\text{VO}(\text{acac})_2$  and that of  $\text{V}(\text{acac})_3$  appear to be the same CV. 2) CV reduction of  
330  $\text{V}(\text{acac})_3$  affords the oxidation wave of  $\text{VO}(\text{acac})_2$  and 3) the oxidation products of  
331  $\text{V}(\text{acac})_3$  formed by controlled potential coulometry can re-form  $\text{VO}(\text{acac})_2$ . With these  
332 critical observations in hand it is reasonable to conclude that oxidation of  $\text{VO}(\text{acac})_2$  forms  
333 an intermediate that upon some combination of chemical steps and electron transfer from  
334 a variety of homogeneous vanadium species likely leads to the formation of  $\text{V}(\text{acac})_3$   
335 through a complex but pseudo-reversible redox system.

336 The ETOF method amounts to determining the diffusion coefficient of the species  
337 generated at the generator and not of that present in the solution bulk. The  
338  $\text{VO}(\text{acac})_2/\text{V}(\text{acac})_3$  system offered a good opportunity to test the applicability of ETOF  
339 when the electron stoichiometry of the electrochemical reaction(s) producing the species  
340 of interest (here  $\text{V}(\text{acac})_3$ ) is complex and a priori unknown under analytical conditions.  
341 Ultimately ETOF determined the diffusion coefficient for the products of reaction to be  
342 consistent with previously measured diffusion coefficients for  $\text{V}(\text{acac})_3$  (3) offering support  
343 to the mechanistic proposals of previous studies suggesting the generation of  $\text{V}(\text{acac})_3$   
344 from  $\text{VO}(\text{acac})_2$  and vice versa. However, depending on the side products co-generated  
345 with  $\text{V}(\text{acac})_3$ , the electron stoichiometry is impossible to ascertain due to the expected  
346 involvement of father-son reactions (see Appendix)

347 The diffusion coefficient of  $V(acac)_3$  in acetonitrile with 0.1 M  $TBAPF_6$  as the supporting  
348 electrolyte was thus deduced experimentally based on the corresponding  $t_{mc}$  value using  
349 the calibration curve without any hypothesis about its exact nature. This afforded a value  
350 of  $1.71(\pm 0.08) \times 10^{-6} \text{ cm}^2/\text{s}$  (Fig. 4). Such value is in total disagreement with the estimated  
351 diffusion coefficient based on the molecular weight of its primary oxidation intermediate  
352  $V^VO(acac)_2^+$ . Conversely, a diffusion coefficient has been reported for  $V^{III}(acac)_3$  (3), viz.,  
353  $1.8 \times 10^{-6} \text{ cm}^2/\text{s}$ , being only 5% greater than the value measured by ETOF. This finding  
354 demonstrates the utility and elegance of the ETOF method allowing for the determination  
355 of a diffusion coefficient without a complete mechanistic understanding of the reaction  
356 occurring and allowing for identification of the products offering further support for a  
357 mechanistic proposal.

## 358 **5. Conclusions**

359 This work shows that ETOF is an elegant, effective, and simple method that easily  
360 determines the diffusion coefficient of the product of a redox reaction in any medium and  
361 even when the product is formed through a complex and possibly unknown mechanistic  
362 sequence. The ETOF approach relies only on the duration of the diffusional transport  
363 between a generator electrode where the species of interest is formed and a collector(s)  
364 electrode(s) at which it can be detected electrochemically. In contrast to other methods,  
365 ETOF does not rely on the electrochemical current intensities measured. This unique  
366 advantage of the ETOF approach has been successfully illustrated in the context of  
367 vanadyl acetylacetonate,  $VO(acac)_2$ , oxidation that underwent a complex mechanism with  
368 unknown fractional electron stoichiometry.

369 A second unique advantage of the ETOF method is that the relationship between the

370 measured time of flights,  $t_{mc}$ , and the sought diffusion coefficients,  $D$ , are independent of  
371 the electrolyte / solvent media in which the ETOF measurements are performed. Instead,  
372 ETOF measurements depend exclusively on the geometrical characteristics of the  
373 microband electrode array used. The lack of dependence on solvent / electrolyte media  
374 has been illustrated by establishing a calibration curve,  $\sqrt{t_{mc}} \propto 1/\sqrt{D}$  (Fig. 3), based on  
375 the measurements of  $t_{mc}$  values in 0.1 M KCl for a series of species whose diffusion  
376 coefficients were reported in the literature and validating its use in 0.1 M TBAPF<sub>6</sub> /  
377 acetonitrile (Fig. 4).

378 Albeit these are important and unique advantages, it is emphasized that a proper use of  
379 the ETOF method requires that the duration,  $t_{pulse}$ , of the potential pulse applied to the  
380 generator electrode is sufficiently small compared to the experimental time of flight,  $t_{mc}$ .  
381 This can be ensured experimentally as shown in Fig. 2B, since for a given species using  
382 too large  $t_{pulse} / t_{mc}$  values produces an increasing drift of  $t_{mc}$  values. Numerical modeling  
383 with COMSOL, was especially useful in establishing quantitatively the criterion fixing the  
384 upper limit of  $t_{pulse}$  values for a given experimental value of the time-of-flight  $t_{mc}$

385

## 386 **Acknowledgements**

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390 by in parts by Ecole Normale Supérieure, PSL Research University, CNRS (UMR8640),  
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393 arrays. C.A. thanks the University of Xiamen, China, for his Distinguished Scientist  
394 position.

395

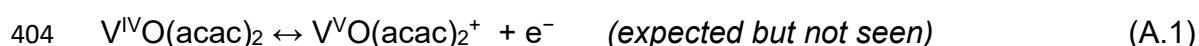
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397

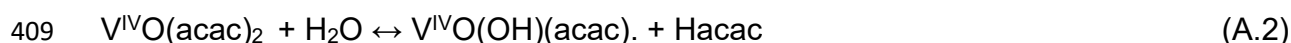
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## 399 **Appendix A**

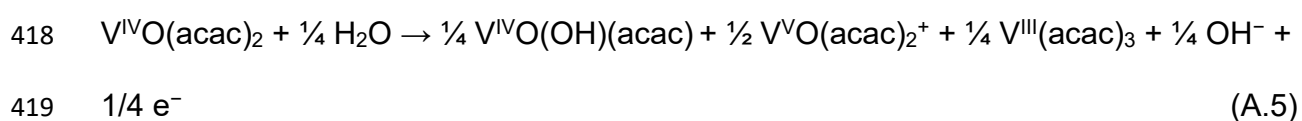
400 The electron stoichiometry of  $V^{IV}O(acac)_2$  oxidation at the generator electrode is expected  
401 to generate the cation  $V^{VO}(acac)_2^+$  as the primary intermediate. The oxidation numbers  
402 of the vanadium center are noted in the following to help in recognizing father-son  
403 sequences:



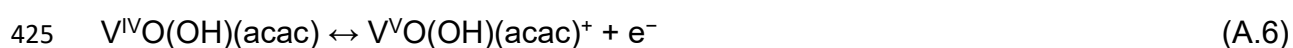
405 The chemical instability of this primary intermediate was confirmed by the absence of a  
406 reduction wave for  $V^{VO}(acac)_2^+$  in the CV (Eq. A1). Owing to the reported instability of  
407  $V^{IV}O(acac)_2$  (35),  $V^{VO}(acac)_2^+$  is expected to undergo a rapid father-son follow-up  
408 mechanism (19) in the presence of adventitious water:



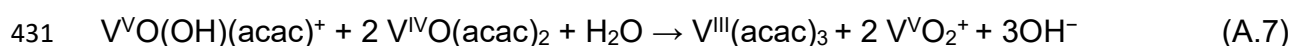
412 Eqs. A1-A4 provide one possible mechanism for the extremely fast formation the neutral  
 413  $V^{III}(acac)_3$  species whose diffusion over the generator-collector(s) gap would then be  
 414 measured instead of that of the primary oxidation intermediate  $V^VO(acac)_2^+$ . Note that the  
 415 overall electron stoichiometry of the mechanism in Eqs. A1-A4 is equal to  $\frac{1}{4}$  electrons  
 416 since one unreacted  $V^VO(acac)_2$  is consumed by the ligand exchange in Eq. A2 and an  
 417 additional two equivalents of  $V^VO(acac)_2$  are consumed in Eq. A4 (see Eq. A5).



420 It is also noteworthy that the proposed mechanism is expected to generate an additional  
 421 two equivalents of  $V^VO(acac)_2^+$  that can further react extremely fast with free ligand and  
 422 generate additional  $V^{III}(acac)_3$  near the generator electrode. This global stoichiometry  
 423 would even be more complex if  $V^VO(OH)(acac)$  is oxidizable at the oxidation wave of  
 424  $V^VO(acac)_2$ :



426 as suggested by the absence of a reduction wave that could be ascribed to this species  
 427 in the CV of the  $V^VO(acac)_2 / V^{III}(acac)_3$  redox system. This may look unlikely at first  
 428 glance, however, one expects the resulting  $V^VO(OH)(acac)^+$  species to react much faster  
 429 in the presence of adventitious water with the parent  $V^VO(acac)_2$  species than  
 430  $V^VO(acac)_2^+$ :



432 Eq. A6 may thus displace the oxidation wave of  $V^VO(acac)_2$  much before its standard  
 433 potential (43) so that it may occur before that of  $V^VO(acac)_2$ . The result is that a

434 complicated sequence of electrochemical and chemical events take place at the potential  
435 of the  $V^{IV}O(acac)_2$  oxidation wave leading to a variety of unstable species and further  
436 convoluting the number of electrons passed per vanadyl unit. In other words, depending  
437 on the extent of the conversion in Eqs. A6 and A7, the electron stoichiometry of  
438  $V^{IV}O(acac)_2$  is expected to be at least  $\frac{1}{4} e^-$  and possibly ranging to larger values. If one  
439 were relying on RDE measurements of  $V^{IV}O(acac)_2$  oxidation, using the limiting plateau  
440 current in RDE would require a foreknowledge of the value,  $n$ , the apparent number of  
441 electrons exchanged per  $V^{IV}O(acac)_2$  that would prevail for the RDE rotation rate in order  
442 to determine the diffusion coefficient of the products. Similarly, current feedback  
443 measurements in SECM are highly dependent on the ability of  $V^{IV}O(acac)_2$  to be  
444 quantitatively regenerated by oxidation of  $V^{III}(acac)_3$  at the collector which cannot be  
445 guaranteed within the short time scales of SECM experiments. Conversely, ETOF  
446 measurements rely exclusively on diffusional time durations of the  $V^{III}(acac)_3$  species and  
447 not at all on current intensities.

448

449

450 **Captions of Figures**

451 **Fig. 1:** (A) Schematic cross section of the device considered in the ETOF experiments.  $g$   
452 is the gap distance between the electrodes selected to operate as generator and collector  
453 electrodes. These electrodes are indicated by black rectangles embedded in the  
454 insulating plane. (B) Schematic time dependence of the potential pulse applied at the  
455 generator and of the resulting generator current. (C) Corresponding collector response  
456 characterized by a peak-shaped current with its maximum characterized by its current,  
457 time coordinates ( $i_{mc}$ ,  $t_{mc}$ ). Note that the time scales in (B) and (C) are not identical, that  
458 in (C) being compressed vs that in (B).

459

460 **Fig. 2:** Illustration of the influence of  $t_{pulse}$  on the relative intensity and time position,  $t_{mc}$ ,  
461 of the collector peak response. (A) Collector current responses for increasing  $t_{pulse}$  values  
462 as determined numerically for the system in Fig. 1A.  $t_{mc}$  tends towards a constant value,  
463 independent of  $t_{pulse}$  when  $t_{pulse} \rightarrow 0$ . (B) Variation of the ratio  $t_{mc} / (t_{mc} \text{ at } t_{pulse} \rightarrow 0)$  as a  
464 function of  $t_{pulse} / (t_{mc} \text{ at } t_{pulse} \rightarrow 0)$ ; note that the abscissa in B is in log scale.

465

466 **Fig. 3:** Calibration curve constructed using ferrocyanide, ferricyanide, and ruthenium (II)  
467 hexamine in 0.1 M KCl aqueous solution based on  $t_{mc}$  values determined from ETOF  
468 experiments using  $t_{pulse} = 61\text{ms}$  and known diffusion coefficients of the generated species  
469 (indicated on the graph). The dotted line represents the equation  $\sqrt{t_{mc}} = 3.23(\pm 0.03) \times 10^{-3} \sqrt{D_B}$ .  
470 The incorrect  $t_{mc}$  values determined for ferrocenium and ferrocenium acetic acid

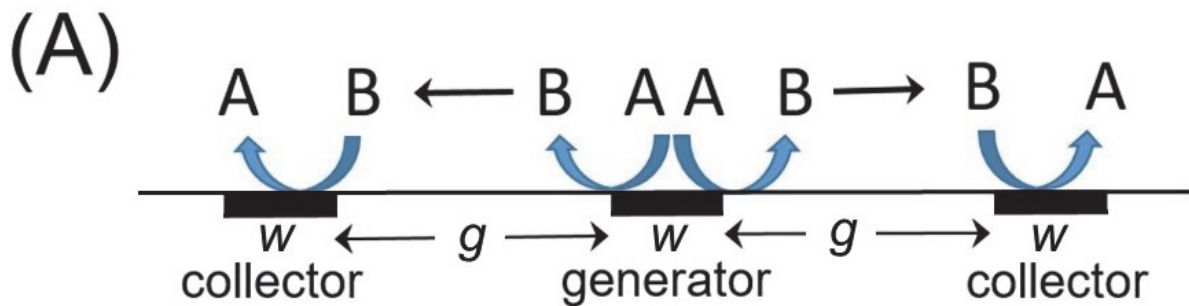
471 in acetonitrile using  $t_{\text{pulse}} = 61\text{ms}$  are shown by orange circles while the correct one  
472 measured for ferrocenium using  $t_{\text{pulse}} = 24\text{ms}$  is shown by a green point.

473

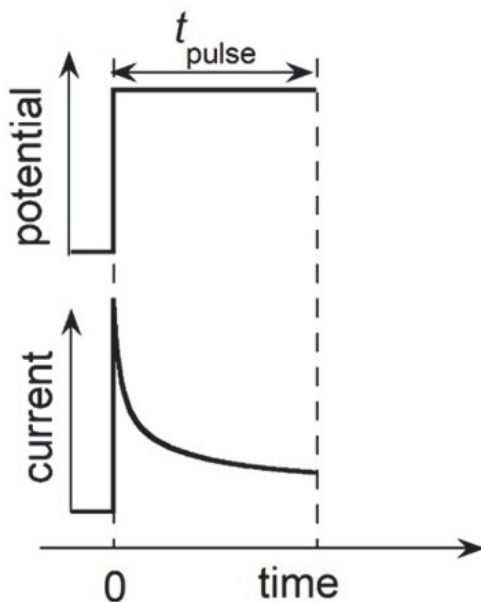
474 **Fig. 4:** Use of the calibration curve,  $\sqrt{t_{mc}} = 3.23(\pm 0.03) \times 10^{-3} / \sqrt{D_B}$ , reported in Fig. 3 in 0.1  
475 M KCl to determine diffusion coefficients from  $t_{mc}$  values determined in acetonitrile with  
476 0.1 M TBAPF<sub>6</sub> as the supporting electrolyte for generated species: Ferrocenium,  
477 Ru(bpy<sub>2</sub>)Cl<sub>2</sub><sup>+</sup>, and V(acac)<sub>3</sub>. In order to fulfill the criterion  $t_{\text{pulse}} / t_{mc} < 0.037$ ,  $t_{\text{pulse}} = 24$  ms  
478 was used for Ferrocenium while  $t_{\text{pulse}} = 61$  ms was used for the three other species. Blue  
479 circles represent the set of data determined for generated species Ru(NH<sub>3</sub>)<sub>6</sub><sup>2+</sup>, Fe(CN)<sub>6</sub><sup>3-</sup>  
480 and Fe(CN)<sub>6</sub><sup>4-</sup> in 0.1 M KCl aqueous solution, while orange circles represent the set of  
481 data determined in acetonitrile / 0.1 M TBAPF<sub>6</sub>.

482

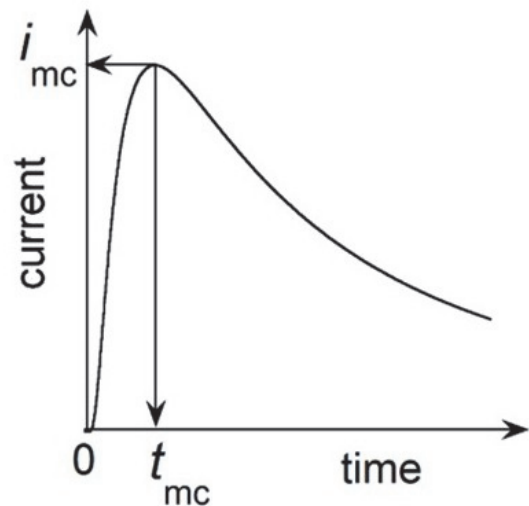




(B)



(C)

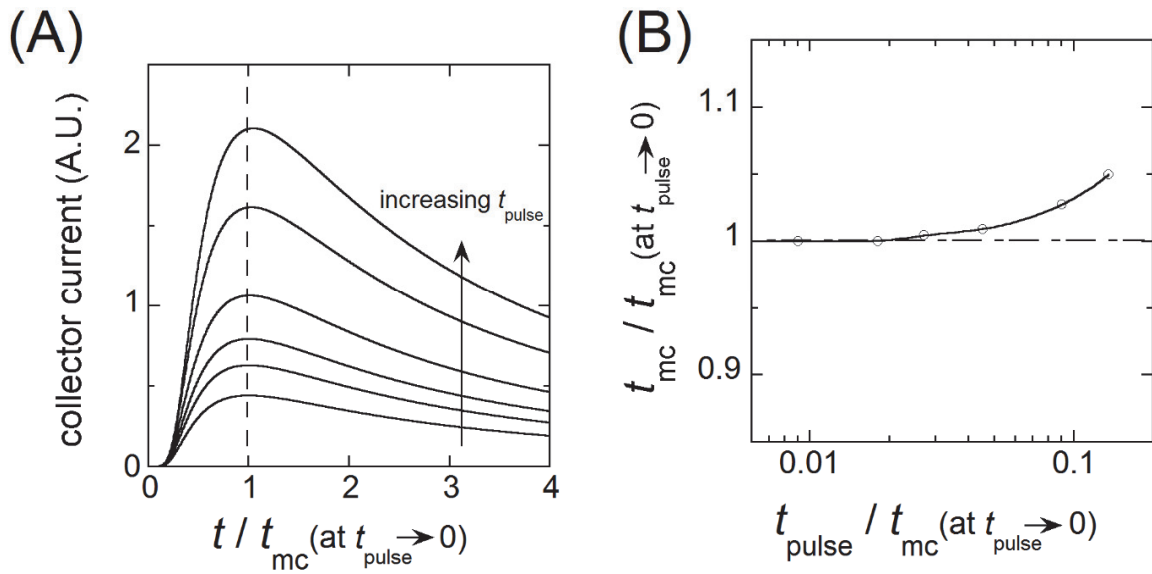


483

484

485 **Fig. 1:** (A) Schematic cross section of the device considered in the ETOF experiments.  $g$   
 486 is the gap distance between the electrodes selected to operate as generator and collector  
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 489 generator and of the resulting generator current. (C) Corresponding collector response  
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 491 time coordinates ( $i_{mc}$ ,  $t_{mc}$ ). Note that the time scales in (B) and (C) are not identical, that  
 492 in (C) being compressed vs that in (B).

493

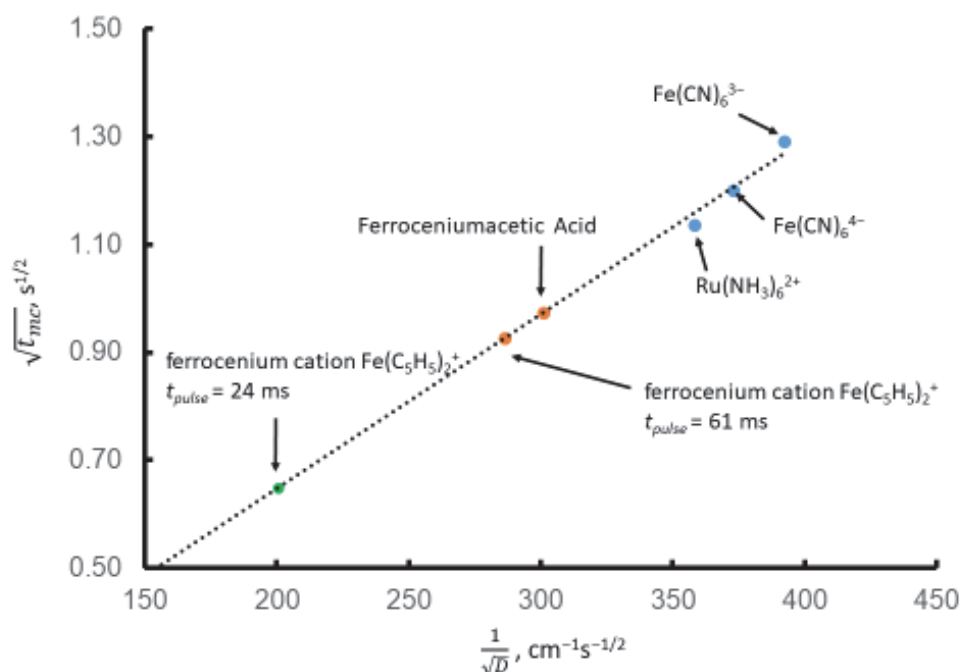


495

496

497 **Fig. 2:** Illustration of the influence of  $t_{pulse}$  on the relative intensity and time position,  $t_{mc}$ ,  
 498 of the collector peak response. (A) Collector current responses for increasing  $t_{pulse}$  values  
 499 as determined numerically for the system in Fig. 1A.  $t_{mc}$  tends towards a constant value,  
 500 independent of  $t_{pulse}$  when  $t_{pulse} \rightarrow 0$ . (B) Variation of the ratio  $t_{mc} / (t_{mc} \text{ at } t_{pulse} \rightarrow 0)$  as a  
 501 function of  $t_{pulse} / (t_{mc} \text{ at } t_{pulse} \rightarrow 0)$ ; note that the abscissa in B is in log scale.

502



503

504 **Fig. 3:** Calibration curve constructed using ferrocyanide, ferricyanide, and ruthenium (II)

505 hexamine in 0.1 M KCl aqueous solution based on  $t_{mc}$  values determined from ETOF

506 experiments using  $t_{pulse} = 61\text{ms}$  and known diffusion coefficients of the generated species

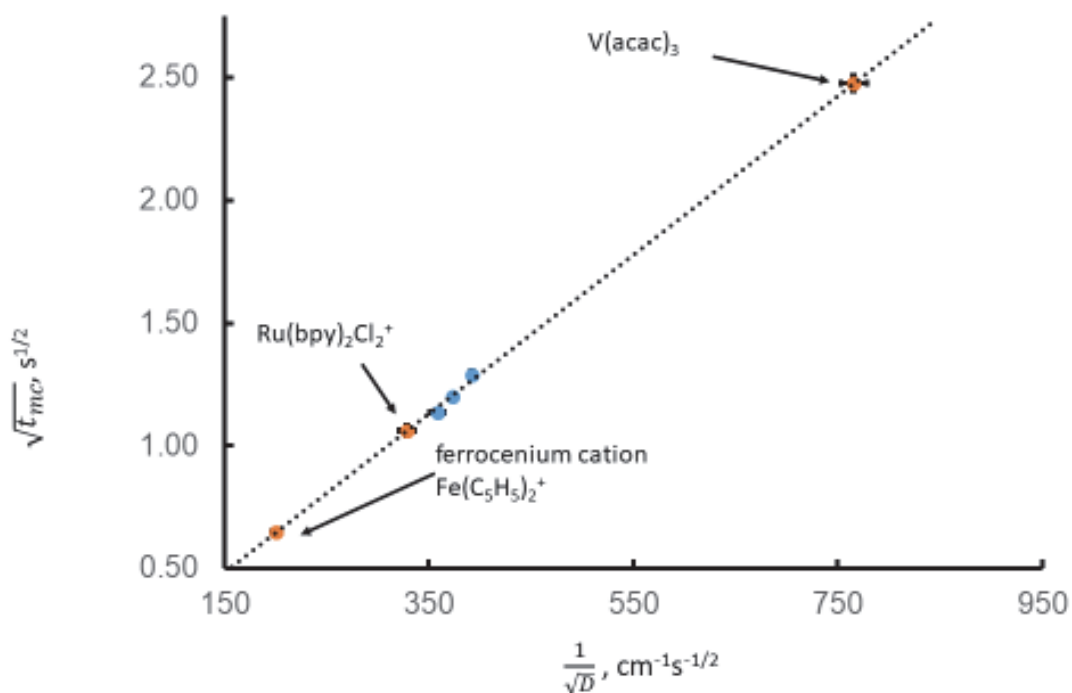
507 (indicated on the graph). The dotted line represents the equation  $\sqrt{t_{mc}} = 3.23(\pm 0.03) \times 10^{-3}$

508  $^3/\sqrt{D_B}$ . The incorrect  $t_{mc}$  values determined for ferrocenium and ferrocenium acetic acid

509 in acetonitrile using  $t_{pulse} = 61\text{ms}$  are shown by orange circles while the correct one

510 measured for ferrocenium using  $t_{pulse} = 24\text{ms}$  is shown by a green point.

511



512

513 **Fig. 4:** Use of the calibration curve,  $\sqrt{t_{mc}} = 3.23(\pm 0.03) \times 10^{-3} / \sqrt{D_B}$ , reported in Fig. 3 in 0.1  
 514 M KCl to determine diffusion coefficients from  $t_{mc}$  values determined in acetonitrile with  
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 516 Ru(bpy)<sub>2</sub>Cl<sub>2</sub><sup>+</sup>, and V(acac)<sub>3</sub>. In order to fulfill the criterion  $t_{pulse} / t_{mc} < 0.037$ ,  $t_{pulse} = 24$  ms  
 517 was used for Ferrocenium while  $t_{pulse} = 61$  ms was used for the three other species. Blue  
 518 circles represent the set of data determined for generated species Ru(NH<sub>3</sub>)<sub>6</sub><sup>2+</sup>, Fe(CN)<sub>6</sub><sup>3-</sup>  
 519 and Fe(CN)<sub>6</sub><sup>4-</sup> in 0.1 M KCl aqueous solution, while orange circles represent the set of  
 520 data determined in acetonitrile / 0.1 M TBAPF<sub>6</sub>.

521

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