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On the Performance of Coefficient of Variation Charts in the Presence of Measurement Errors

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Abstract

In the literature, coefficient of variation control charts have been introduced under the assumption of no measurement errors. However, measurement errors always exist in practice and they do affect the performance of control charts in the detection of an out of control situation. In this paper, we therefore study the performance of a coefficient of variation Shewhart type control chart (Shewhart-CV chart) and also one-sided coefficient of variation EWMA type control charts (EWMA- γ^2 charts) using a model with linear covariates. Moreover, we propose and study the performance of a two-sided EWMA- γ^2 chart using a model with linear covariates. Several figures and tables are provided and analyzed to evaluate the statistical performance of these control charts for different sources of measurement errors. The obtained results show that the precision and accuracy errors significantly affect the performance of both the Shewhart-CV and EWMA- γ^2 control charts. An example illustrating the use of this study is finally presented.

Keywords: Measurement Errors; Coefficient of Variation; Textile manufacturing; Shewhart Control Chart; EWMA Control Charts; Markov chain.

1 Introduction

Statistical Process Control (SPC) is an important methodology in quality control. Control charts, the simplest type of on-line SPC procedure, are very useful tools for the detection and elimination of assignable causes shifting a process that is being monitored. In the SPC literature, Shewhart-type control chart for monitoring the coefficient

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of variation (CV), which is defined as the ratio of the population standard deviation to the population mean, has already been investigated by Kang et al. ¹; subsequently, several control charts have been developed in the literature for monitoring the coefficient of variation. For further details, see, for instance, Castagliola et al. ², Calzada and Scariano ³, Castagliola et al. ⁴, Castagliola et al. ⁵, Zhang et al. ⁶, Castagliola et al. ⁷, Castagliola et al. ⁸, Amdouni et al. ⁹, You et al. ¹⁰ and Tran and Tran ¹¹, among others. For example, in textile manufacturing industry, the variation among tensile strength measurements from thin thread is significantly smaller than measurements taken from heavy thread due to the inherent physical properties of fiber. In this scenario, CV control charts are useful tools to monitor the process.

It is important to note that the control charts cited above for monitoring the CV are designed under the assumption that the measurements on the characteristic are made without error. However, in many industrial scenarios, there often exist significant measurement errors that affect the performance of control charts. Since Bennet ¹² investigated the effect of measurement errors on the Shewhart \bar{X} chart, the consequences of the measurement errors on the performance of various control charts have been studied by a number of authors, including Kanazuka ¹³, Linna and Woodall ¹⁴, Linna et al. ¹⁵, Maravelakis ¹⁶, Costa and Castagliola ¹⁷, Maravelakis ¹⁸, Hu et al. ¹⁹, Noorossana and Zerehsaz ²⁰, Tran et al. ²¹, Tran et al. ²² and Tran ²³.

Quite recently, Yeong et al. 24 investigated the effect of measurement errors on the one-sided CV charts. However, they have assumed that the ratios σ_M/σ and A/μ , which will be detailed in Section 3, are constants. This assumption may not be true in practice because when the process is out-of-control, these values do get changed. This study is designed to address the performance of the Shewhart-CV control chart proposed by Kang et al. 1 and the one-sided EWMA- γ^2 control charts proposed by Castagliola et al. 2 in the presence of measurement errors by assuming the same measurement errors model as the one in Linna and Woodall ¹⁴. In addition, we propose and study the performance of two-sided EWMA- γ^2 chart in the presence of measurement errors. We also take into account the changes of these ratios when investigating the performance of Shewhart-CV and one-sided EWMA- γ^2 control charts. The organization of the rest of this article is as follows: In Section 2, the coefficient of variation distribution is introduced. In Section 3, the linear covariate error model for the coefficient of variation is introduced. Section 4 provides the formulas for the control limits and the performance metrics of the Shewhart-CV control chart. In Section 5, the effect of measurement errors on the performance of Shewhart-CV control chart is investigated. Section 6 provides the formulas of the control limits and the performance metrics of the one-sided and two-sided EWMA- γ^2 control charts. In Section 7, the effect of measurement errors on the performance of the onesided and the two-sided EWMA- γ^2 control charts are investigated. Section 8 presents an example to illustrate the methods developed here, and finally some concluding remarks and recommendations are made in Section 9.

2 A brief review of distribution of the sample coefficient of variation

The goal of this section is to present a brief review of the distribution of the sample coefficient of variation (CV). The population CV γ is defined as the ratio of the standard deviation $\sigma = \sigma(X)$ to the mean $\mu = E(X)$; i.e.,

$$\gamma = \frac{\sigma}{\mu}$$
.

Suppose we have a random sample of size n of normal i.i.d. (μ, σ) random variables $\{X_1, \ldots, X_n\}$. Let \bar{X} and S be the sample mean and the sample standard deviation of this sample, i.e.,

$$\bar{X} = \frac{1}{n} \sum_{i=1}^{n} X_i$$

and

$$S = \sqrt{\frac{1}{n-1} \sum_{i=1}^{n} (X_i - \bar{X})^2}.$$

Based on \bar{X} and S, the sample coefficient of variation $\hat{\gamma}$ is defined as (Castagliola et al. ²)

$$\hat{\gamma} = \frac{S}{\bar{X}}.$$

It is important to note that the probability distribution of the sample CV $\hat{\gamma}$ has been studied in the literature by many authors; for further details, see McKay ²⁵, Hendricks and Robey ²⁶, Iglewicz et al. ²⁷, Iglewicz and Myers ²⁸, Warren ²⁹, Vangel ³⁰ and Reh and Scheffler ³¹. Among these authors, Castagliola et al. ² showed that the c.d.f. (cumulative distribution function) $F_{\hat{\gamma}}(x|n,\gamma)$ of $\hat{\gamma}$ is

$$F_{\hat{\gamma}}(x|n,\gamma) = 1 - F_t\left(\frac{\sqrt{n}}{x}\middle| n - 1, \frac{\sqrt{n}}{\gamma}\right),\tag{1}$$

where $F_t\left(.\left|n-1,\frac{\sqrt{n}}{\gamma}\right.\right)$ is the c.d.f. of the noncentral t distribution with n-1 degrees of freedom and noncentrality parameter $\frac{\sqrt{n}}{\gamma}$. With some manipulations, inverting $F_{\hat{\gamma}}(x|n,\gamma)$ gives the inverse c.d.f. $F_{\hat{\gamma}}^{-1}(\alpha|n,\gamma)$ of $\hat{\gamma}$ as (Castagliola et al.²)

$$F_{\hat{\gamma}}^{-1}(\alpha|n,\gamma) = \frac{\sqrt{n}}{F_t^{-1}\left(1 - \alpha \left| n - 1, \frac{\sqrt{n}}{\gamma} \right.\right)},\tag{2}$$

where $F_t^{-1}\left(.\left|n-1,\frac{\sqrt{n}}{\gamma}\right.\right)$ is the inverse c.d.f. of the noncentral t distribution.

Moreover, Castagliola et al. ² showed that $\frac{n}{\hat{\gamma}^2}$ follows a noncentral F distribution with (1, n-1) degrees of freedom and noncentrality parameter $\frac{n}{\gamma^2}$. Then, they deduced the c.d.f. $F_{\hat{\gamma}^2}(x|n,\gamma)$ of $\hat{\gamma}^2$ to be

$$F_{\hat{\gamma}^2}(x|n,\gamma) = 1 - F_F\left(\frac{n}{x}\Big|1, n-1, \frac{n}{\gamma^2}\right),\tag{3}$$

where $F_F\left(.\left|1,n-1,\frac{n}{\gamma^2}\right.\right)$ is the c.d.f. of the noncentral F distribution. Castagliola et al.² showed that the inverse c.d.f. $F_{\hat{\gamma}^2}^{-1}(\alpha|n,\gamma)$ of $\hat{\gamma}^2$ can be obtained as

$$F_{\hat{\gamma}^2}^{-1}(\alpha|n,\gamma) = \frac{n}{F_F^{-1}\left(1 - \alpha \left|1, n - 1, \frac{n}{\gamma^2}\right.\right)},\tag{4}$$

where $F_F^{-1}\left(.\left|1,n-1,\frac{n}{\gamma^2}\right.\right)$ is the inverse c.d.f. of the noncentral F distribution.

3 Linear covariate error model for the coefficient of variation

In this section, the linear covariate error model for the sample CV is introduced. Let us assume that, at times $i=1,2,\ldots$, the quality characteristic X of n>1 consecutive items is equal to $\{X_{i,1},X_{i,2},\ldots,X_{i,n}\}$. We assume that $X_{i,j}$'s are independent normal $(\mu_0 + a\sigma_0,b\sigma_0)$ random variables, where μ_0 and σ_0 are the nominal mean and standard deviation, respectively, both assumed known, while a and b are the standardized mean and standardized deviation shifts. The process has shifted if the process mean μ_0 and/or the process standard deviation σ_0 have changed $(a \neq 0 \text{ and/or } b \neq 1)$. As suggested by Linna and Woodall ¹⁴, let us assume that the true quality characteristic $X_{i,j}$ with mean μ_0 and variance σ_0^2 (when the process is in statistical control) is not directly observable, but can only be assessed from the results $\{X_{i,j,1}^*, X_{i,j,2}^*, \ldots, X_{i,j,m}^*\}$ of a set of $m \geq 1$ measurement operations with each $X_{i,j,k}^*$ being equal to (linear covariate error model)

$$X_{i,j,k}^* = A + BX_{i,j} + \varepsilon_{i,j,k},$$

where A and B are two known constants and $\varepsilon_{i,j,k}$ is a normal $(0,\sigma_M)$ random error term due to the measurement inaccuracy, which is independent of $X_{i,j}$. The smaller σ_M is, the higher the *precision* is. The constants A and B for linear covariate error model can be estimated by using nonparametric estimation; see Li and Vuong ³².

For subgroup $i=1,2,\ldots,$ as $j=1,2,\ldots,n$ and $k=1,2,\ldots,m$, we have $m\times n$ observations $X_{i,j,k}^*$ and the mean $\bar{X}_{i,j}^*$ of the observable quantities $\{X_{i,j,1}^*,X_{i,j,2}^*,\ldots,X_{i,j,m}^*\}$

is equal to

$$\bar{X}_{i,j}^{*} = \frac{1}{m} \sum_{k=1}^{m} X_{i,j,k}^{*} \\
= \frac{1}{m} \sum_{k=1}^{m} (A + BX_{i,j} + \varepsilon_{i,j,k}) \\
= A + BX_{i,j} + \frac{1}{m} \sum_{k=1}^{m} \varepsilon_{i,j,k}.$$
(5)

It can then be easily shown that the mean $\mu^* = E(\bar{X}_{i,j}^*)$ and the standard deviation $\sigma^* = \sigma(\bar{X}_{i,j}^*)$ of $\bar{X}_{i,j}^*$ are equal to

$$\mu^* = A + B(\mu_0 + a\sigma_0), \tag{6}$$

$$\mu^* = A + B(\mu_0 + a\sigma_0),$$

$$\sigma^* = \sqrt{B^2 b^2 \sigma_0^2 + \frac{\sigma_M^2}{m}}.$$
(6)

The coefficient of variation of the measured quantity $\bar{X}_{i,j}^*$ is then

$$\gamma^* = \frac{\sigma^*}{\mu^*} = \frac{\sqrt{B^2 b^2 \sigma_0^2 + \frac{\sigma_M^2}{m}}}{A + B(\mu_0 + a\sigma_0)}.$$
 (8)

Let $\eta = \frac{\sigma_M}{\sigma_0}$ be the square root of the ratio of the measurement system variability. If we set $\gamma_0 = \frac{\sigma_0}{\mu_0}$ and $\theta = \frac{A}{\mu_0}$, the coefficient of variation of the measured quantity $\bar{X}_{i,j}^*$ in (8) can be rewritten as

$$\gamma^* = \frac{\sigma^*}{\mu^*} = \frac{\sqrt{B^2 b^2 + \frac{\eta^2}{m}}}{\theta + B(1 + a\gamma_0)} \times \gamma_0. \tag{9}$$

Let \bar{X}_i^* and S_i^* be the sample mean and the sample standard deviation of $\bar{X}_{1,j}^*, \dots, \bar{X}_{n,j}^*$, i.e.,

$$\bar{\bar{X}}_{i}^{*} = \frac{1}{n} \sum_{j=1}^{n} \bar{X}_{i,j}^{*}$$

and

$$S_i^* = \sqrt{\frac{1}{n-1} \sum_{j=1}^n (\bar{X}_{i,j}^* - \bar{\bar{X}}_j^*)^2}.$$

Then, the sample coefficient of variation $\hat{\gamma}_i^*$ is defined as

$$\hat{\gamma}_i^* = \frac{S_i^*}{\bar{\bar{X}}_i^*}.$$

The c.d.f. and i.d.f. of $\hat{\gamma}^*$ can be obtained from (1) and (2) by simply replacing γ by as defined in (9), i.e., the c.d.f. $F_{\gamma^*}(x|n,\gamma^*)$ and i.d.f. $F_{\gamma^*}^{-1}(\alpha|n,\gamma^*)$ of $\hat{\gamma}^*$ are given

$$F_{\gamma^*}(x|n,\gamma^*) = 1 - F_t\left(\frac{\sqrt{n}}{x} \left| n - 1, \frac{\sqrt{n}}{\gamma^*} \right.\right)$$

$$\tag{10}$$

and

$$F_{\gamma^*}^{-1}(\alpha|n,\gamma^*) = \frac{\sqrt{n}}{F_t^{-1}\left(1 - \alpha \left| n - 1, \frac{\sqrt{n}}{\gamma^*} \right.\right)}$$
(11)

Similarly, the c.d.f. and i.d.f. of $\hat{\gamma}^{*2}$ can be obtained from (3) and (4) by simply replacing γ by γ^* as defined in (9), i.e., the c.d.f. $F_{\gamma^{*2}}(x|n,\gamma^*)$ and i.d.f. $F_{\gamma^{*2}}^{-1}(\alpha|n,\gamma^*)$ of $\hat{\gamma}^{*2}$ are given by

$$F_{\gamma^{*2}}(x|n,\gamma^*) = 1 - F_F\left(\frac{n}{x}\left|1, n-1, \frac{n}{\gamma^{*2}}\right.\right)$$
 (12)

and

$$F_{\gamma^{*2}}^{-1}(\alpha|n,\gamma^*) = \frac{n}{F_F^{-1}\left(1-\alpha\left|1,n-1,\frac{n}{\gamma^{*2}}\right.\right)}.$$
 (13)

4 Implementation of the Shewhart-CV control chart with measurement errors

The control limits of Shewhart-CV control chart in the presence of measurement errors are defined as

$$LCL = F_{\gamma^*}^{-1} \left(\frac{\alpha_0}{2} | n, \gamma_0^* \right), \tag{14}$$

$$UCL = F_{\gamma^*}^{-1} \left(1 - \frac{\alpha_0}{2} | n, \gamma_0^* \right), \tag{15}$$

where $F_{\gamma^*}^{-1}(.)$ is the inverse c.d.f. of $\hat{\gamma^*}$ defined in (11) and α is the desired false alarm probability for the control chart. In (14) and (15), the value of γ_0^* is computed as

$$\gamma_0^* = \frac{\sigma^*}{\mu^*} = \frac{\sqrt{B^2 + \frac{\eta^2}{m}}}{B + \theta} \times \gamma_0, \tag{16}$$

where γ_0 is the in-control CV.

The central line CL of the Shewhart-CV chart can be defined as the median value, i.e.,

$$CL = F_{\hat{\gamma}^*}^{-1}(0.5|n, \gamma_0^*).$$
 (17)

Now, let us assume that the occurrence of an out-of-control condition shifts the incontrol CV γ_0 to $\gamma_1 = \tau \times \gamma_0$, where $\tau > 0$ is the size of the shift. Then, it can be easily shown that

$$\gamma_1 = \frac{b}{1 + a\gamma_0} = \tau \times \gamma_0,$$

$$\frac{b}{\tau} = 1 + a\gamma_0. \tag{18}$$

From (18) and (9), the out-of-control coefficient of variation of the measured quantity $\bar{X}_{i,j}^*$ can be rewritten as

$$\gamma_1^* = \frac{\sigma^*}{\mu^*} = \frac{\sqrt{B^2 b^2 + \frac{\eta^2}{m}}}{\theta + \frac{Bb}{\tau}} \times \gamma_0.$$
 (19)

As with any other Shewhart control chart, the run length of the Shewhart-CV control chart with measurement errors is defined as

$$\beta = F_{\hat{\gamma}^*}(UCL|n, \gamma_1^*) - F_{\hat{\gamma}}(LCL|n, \gamma_1^*). \tag{20}$$

It is straightforward to get an expression for the out-of-control ARL as

$$ARL = \frac{1}{1-\beta}. (21)$$

5 The effect of measurement errors on the Shewhart-CV control chart

In this Section, we investigate the performance of the Shewhart-CV control chart in the presence of measurement errors. When the process is in-control, the ARL is denoted by ARL_0 and here we set $\alpha=0.0027$ corresponding to $ARL_0=370.4$. Without loss of generality, we assume in the remaining part of this section that b=1. From Section 4, for fixed values of m, n, B and η , we can obtain the ARL and SDRL values of the Shewhart-CV chart with linear covariate error model.

Table 1 shows the values of the probability control limits (LCL, UCL) for the values of $n \in \{5, 7, 10, 15\}$, $\eta \in \{0.1, 0.28\}$, $\theta \in \{0.01, 0.05\}$, $\gamma_0 \in \{0.05, 0.1, 0.15, 0.2\}$, B = 1, m = 1 and $ARL_0 = 370.4$. The specific value of $\eta = 0.28$ is motivated by assuming an acceptable value for the signal-to-noise ratio

$$SNR = \sqrt{\frac{\frac{2}{1+\eta^2}}{1-\frac{1}{1+\eta^2}}} = \frac{\sqrt{2}}{\eta},\tag{22}$$

which is a measure of performance of the *precision* adequacy of the measurement system; see Montgomery ³³. As discussed in Tran et al. ²¹, assuming $\eta = 0.28$ corresponds to SNR = 5, which is the lower bound value to get an acceptable *precision* of the measurement system.

INSERT TABLE 1 ABOUT HERE

Some simple conclusions can be drawn from Table 1 as follows:

- In general, given n, B and γ_0 , the values of LCL and UCL depend on (η, θ) . In particular, for smaller values of (η, θ) , the values of LCL and UCL are smaller. For example, when n = 5, B = 1 and $\gamma_0 = 0.05$, we have LCL = 0.0081 and UCL = 0.1053 when $(\eta, \theta) = (0.10, 0.01)$, and LCL = 0.0080 and UCL = 0.1047 when $(\eta, \theta) = (0.28, 0.05)$;
- In general, given n, γ_0 , η and θ , the values of LCL and UCL depend on B. In particular, for smaller B, the values of LCL and UCL are smaller. For example, when n=5, $\gamma_0=0.1$ and $(\eta,\theta)=(0.10,0.01)$, we have LCL=0.0161 and UCL=0.2130 when B=1, and LCL=0.0162 and UCL=0.2137 when B=5.

Table 2 shows the out-of-control ARL_1 values for the Shewhart-CV for different combinations of the *precision* error ratio $\eta \in \{0, 0.1, 0.2, 0.3, 0.5, 1.0\}, \ \gamma_0 \in \{0.05, 0.1, 0.2\}, \ \tau \in \{0.5, 0.65, 0.8, 1.25, 1.5, 2\}$ and $n \in \{5, 7, 10, 15\}$ when $m = 1, \theta = 0.05$ and B = 1.

INSERT TABLE 2 ABOUT HERE

The obtained results show that, for fixed values of n, η , γ_0 , m=1 and B=1, the smaller the precision error ratio η is, the faster the control chart is in detecting the out-of-control condition, demonstrating the negative effect of measurement errors on the performance of Shewhart-CV chart. However, when $\eta \leq 0.3$, the values of ARL in the presence of a precision error are not significantly larger than the value of ARL without the measurement error. For instance, when n=5, B=1, m=1, $\gamma_0=0.05$ and $\tau=0.7$, we have ARL=148.13 for $\eta=0$ and ARL=148.15 for $\eta=0.3$ (see Table 2). So, we can conclude that the precision error does not significantly affect the performance of the Shewhart-CV control chart with a normal measurement system.

Table 3 shows the out-of-control ARL_1 values for the Shewhart-CV for different combinations of the *precision* error ratio $\theta \in \{0, 0.01, 0.02, 0.03, 0.04, 0.05\}, \gamma_0 \in \{0.05, 0.1, 0.2\}, \tau \in \{0.5, 0.65, 0.8, 1.25, 1.5, 2\}$ and $n \in \{5, 7, 10, 15\}$ when $m = 1, \eta = 0.28$ and B = 1.

INSERT TABLE 3 ABOUT HERE

The obtained results show that, for fixed values of n, τ , γ_0 , m=1 and B=1, the performance of the Shewhart-CV control chart is influenced by the accuracy error, measured by θ . In most cases, the larger the values of θ , the faster the control charts are in detecting the out-of-control condition. For instance, when n=7, $\gamma_0=0.1$, B=1, m=1 and $\tau=0.7$, we have ARL=69.93 for $\theta=0$, and ARL=76.32 for $\theta=0.05$ (see Table 3). We can thus conclude that the accuracy error significantly affects the performance of the Shewhart-CV control chart for the usual levels of accuracy errors provided by calibrated gauges.

INSERT TABLE 4 ABOUT HERE

Table 4 shows the performances of Shewhart-CV chart under linear covariate error model for different combinations of $B \in \{1, 2, 3, 4, 5\}$, $\tau \in \{0.5, 0.65, 0.8, 1.25, 1.5, 2\}$, $\gamma_0 \in \{0.05, 0.1, 0.2\}$ and $n \in \{5, 7, 10, 15\}$ when m = 1 and $\eta = 0.28$, $\theta = 0.05$. It can be noted from Table 4 that, for fixed values of n, τ , η , θ and m, the value of B significantly affects the performance of the Shewhart-CV control chart. For instance, when n = 5, $\eta = 0.28$, $\theta = 0.05$, $\gamma_0 = 0.1$, m = 1 and $\tau = 0.7$, we have ARL = 148.9 for B = 1, and ARL = 141.5 for B = 5 (see Table 4).

As discussed in Linna and Woodall ¹⁴, it is better to take multiple measurements per item in each sample to compensate for the effect of measurement errors. The performance of the Shewhart-CV chart under linear covariate error model is shown in Table 5 for different combinations of $m \in \{1, 3, 5, 7, 10\}$, $\tau \in \{0.5, 0.65, 0.8, 1.25, 1.5, 2\}$, $\gamma_0 \in \{0.05, 0.1, 0.2\}$ and $n \in \{3, 5, 7, 9\}$ when B = 1 and $\eta = 0.28$. For fixed values of n, τ, B and η , as the number m of measurements per item increases, the value of ARL decreases, demonstrating the positive effect of the number of repeated measurements m per item on the performance of the Shewhart-CV chart. For instance, when n = 10, $\eta = 0.28$ and $\tau = 0.7$, $\gamma_0 = 0.1$, we have ARL = 34.14 for m = 1, and ARL = 31.21 for m = 5 (see Table 5).

INSERT TABLE 5 ABOUT HERE

6 Implementation of the EWMA- γ^2 control charts with measurement errors

In this Section, we propose a two-sided EWMA control chart for monitoring $\hat{\gamma}^2$ (denoted as two-sided EWMA- γ^2) with measurement errors. We also study the performance of one-sided EWMA- γ^2 control charts proposed by Castagliola et al. ² in the presence of measurement errors. The two-sided EWMA- γ^2 control chart is useful when the direction of the shift is not known in advance or when the detection of upward and downward shifts is of equal importance. It is important to note that there are no closed-form expressions for $\mu_0(\hat{\gamma}^{*2})$ and $\sigma_0(\hat{\gamma}^{*2})$; see Castagliola et al. ² for more details. In this case, Breunig ³⁴ provided accurate approximations as

$$\mu_0(\hat{\gamma}^{*2}) = \gamma_0^{*2} \left(1 - \frac{3\gamma_0^{*2}}{n} \right), \tag{23}$$

$$\sigma_0(\hat{\gamma}^{*2}) = \sqrt{\gamma_0^{*4} \left(\frac{2}{n-1} + \gamma_0^{*2} \left(\frac{4}{n} + \frac{20}{n(n-1)} + \frac{75\gamma_0^{*2}}{n^2}\right)\right) - (\mu_0(\hat{\gamma}^{*2}) - \gamma_0^{*2})^2}, \quad (24)$$

where γ_0^* is as defined in (9).

The two-sided EWMA- γ^2 is defined as

$$S_i^* = (1 - \lambda)S_{i-1}^* + \lambda \hat{\gamma}_i^{*2},$$

with $S_0^* = \mu_0(\hat{\gamma}^{*2})$ as an initial value. The control limits of a two-sided EWMA control chart in the presence of measurement errors are defined as

$$LCL_{\text{EWMA}-\gamma^2} = \mu_0(\hat{\gamma}^{*2}) - K\sqrt{\frac{\lambda}{2-\lambda}}\sigma_0(\hat{\gamma}^{*2}), \qquad (25)$$

$$UCL_{\text{EWMA}-\gamma^2} = \mu_0(\hat{\gamma}^{*2}) + K\sqrt{\frac{\lambda}{2-\lambda}}\sigma_0(\hat{\gamma}^{*2}),$$

where K > 0 comes from solving $ARL(\gamma_0^*, \lambda, n, m, B, \eta, K) = ARL_0$ and λ is the smoothing constant of the two-sided EWMA- γ^2 chart.

In order to detect shifts on a specific direction, one-sided schemes are more effective than two-sided ones (see also Castagliola et al. ²). According to Castagliola et al. ², the following two separate one-sided EWMA charts in the presence of measurement errors may be used:

• an upward EWMA chart (denoted as "upward EWMA- γ^2 ") is given by

$$Z_i^{*+} = \max(\mu_0(\hat{\gamma}^{*2}), (1 - \lambda^+) Z_{i-1}^{*+} + \lambda^+ \hat{\gamma}_i^{*2}),$$

with $Z_0^{*+} = \mu_0(\hat{\gamma}^{*2})$ as an initial value and with the corresponding upper control limit

$$UCL_{\text{EWMA}-\gamma^2} = \mu_0(\hat{\gamma}^{*2}) + K^+ \sqrt{\frac{\lambda^+}{2-\lambda^+}} \sigma_0(\hat{\gamma}^{*2});$$
 (26)

• a downward EWMA chart (denoted as "downward EWMA- γ^2 ") is given by

$$Z_i^{*-} = \min(\mu_0(\hat{\gamma}^{*2}), (1 - \lambda^-) Z_{i-1}^{*-} + \lambda^- \hat{\gamma}_i^{*2}),$$

with $Z_0^{*-} = \mu_0(\hat{\gamma}^{*2})$ as an initial value and with the corresponding lower control limit

$$LCL_{\text{EWMA}-\gamma^2} = \mu_0(\hat{\gamma}^{*2}) - K^- \sqrt{\frac{\lambda^-}{2-\lambda^-}} \sigma_0(\hat{\gamma}^{*2}),$$
 (27)

where $\mu_0(\hat{\gamma}^{*2})$ and $\sigma_0(\hat{\gamma}^{*2})$ are the mean and standard deviation of $\hat{\gamma}^2$ when the process is in-control, and λ^+ (λ^-) and K^+ (K^-) are the smoothing constant and chart coefficient of the upward (downward) EWMA- γ^2 chart.

Once the control chart parameters (in our case, λ^- or λ^+ and K^- or K^+ for the one-sided EWMA- γ^2 control charts; and λ and K for the two-sided EWMA- γ^2 control chart), are defined, the ARL can be numerically evaluated for particular shifts a and b,

from an in-control value γ_0^* to an out-of-control value γ_1^* . Here, to calculate the ARL of one-sided and two-sided EWMA- γ^2 control charts, we use a Markov-chain approximation based on a flexible and relatively easy to use procedure given in Castagliola et al. ², originally proposed by Brook and Evans ³⁵; see Castagliola et al. ² for more details.

As in Castagliola et al.², the design procedure of one-sided EWMA- γ^2 charts is implemented by determining the optimal combinations (λ^{+*}, K^{+*}) or (λ^{-*}, K^{-*}) for particular shifts a and b, such that

• for upward EWMA- γ^2 chart

$$(\lambda^{+*}, K^{+*}) = \underset{(\lambda^{+}, K^{+})}{\operatorname{argmin}} ARL(\gamma_{0}^{*}, \gamma_{1}^{*}, \lambda^{+}, K^{+}, n, m, B, \eta),$$

subject to the constraint

$$ARL(\gamma_0^*, \lambda^*, K^{+*}, n, m, B, \eta) = ARL_0,$$

• for downward EWMA- γ^2 chart

$$(\lambda^{-*}, K^{-*}) = \underset{(\lambda^{-}, K^{-})}{\operatorname{argmin}} ARL(\gamma_{0}^{*}, \gamma_{1}^{*}, \lambda^{-}, K^{-}, n, m, B, \eta),$$

subject to the constraint

$$ARL(\gamma_0^*, \lambda^{-*}, K^{-*}, n, m, B, \eta) = ARL_0.$$

Similarly, the design procedure of two-sided EWMA- γ^2 chart is implemented by determining the optimal combination (λ^*, K^*) for particular shifts a and b, such that

$$(\lambda^*, K^*) = \underset{(\lambda, K)}{\operatorname{argmin}} ARL(\gamma_0^*, \gamma_1^*, \lambda, K, n, m, B, \eta),$$

subject to the constraint

$$ARL(\gamma_0^*, \lambda^*, K^*, n, m, B, \eta) = ARL_0.$$

In this study, we use a non-linear equation solver along with an optimization achieved through an algorithm developed in Scicoslab software; see Tran and Tran ¹¹ for more details.

7 The effect of measurement errors on the EWMA- γ^2 control charts

In this Section, we investigate the performance of the proposed two-sided EWMA- γ^2 and the EWMA- γ^2 control charts proposed by Castagliola et al.² in the presence of measurement errors. When the process is in-control, we set $ARL_0 = 370.4$. Without

loss of generality, we assume in the remaining part of this section that b=1. From Section 4, for fixed values of m, n, B, λ , K, a and η , we can obtain the ARL and SDRL values of the proposed two-sided EWMA- γ^2 and the one-sided EWMA- γ^2 control charts.

Table 6 shows optimal values λ^* and K^* of two-sided EWMA- γ^2 control charts in the presence of measurement errors for the values of $n \in \{5,7,10,15\}$, $\eta \in \{0.1,0.28\}$, $\theta = 0.0.05$, $\gamma_0 \in \{0.05,0.1,0.2\}$, B = 1, m = 1 and $ARL_0 = 370.4$. For the sake of brevity, similar tables showing optimal values λ^* and K^* of two-sided EWMA- γ^2 control charts for other scenarios are not presented here, but are available upon request from the authors. For example, when n = 5, B = 1, $\gamma_0 = 0.05$, $\tau = 0.8$ and $\eta = 0.2$, we have $\lambda^* = 0.0302$, $K^* = 2.2973$ when $\gamma_0 = 0.05$, and $\lambda^* = 0.0274$, $K^* = 2.2738$ when $\gamma_0 = 0.1$. In this case, Table 7 shows the out-of-control ARL_1 values for the two-sided EWMA- γ^2 .

INSERT TABLE 6 ABOUT HERE

INSERT TABLE 7 ABOUT HERE

The obtained results show that the performance of two-sided EWMA- γ^2 control chart is influenced by the values of η with a similar behaviour as for the Shewhart-CV control chart discussed earlier. In most cases, the two-sided EWMA- γ^2 control chart outperforms the Shewhart-CV chart. For example, when $n=5, B=1, \gamma_0=0.05, \tau=0.8$ and $\theta=0.01, \gamma_0=0.05$ and $\eta=0.2$, we have $ARL_1=319.60$ for Shewhart-CV chart and $ARL_1=28.08$ for two-sided EWMA- γ^2 control chart (see Tables 2 and 7).

Table 3 shows the out-of-control ARL_1 values for the two-sided EWMA- γ^2 for different combinations of the *precision* error ratio $\theta \in \{0, 0.01, 0.02, 0.03, 0.04, 0.05\}$, $\gamma_0 \in \{0.05, 0.1, 0.2\}$, $\tau \in \{0.5, 0.65, 0.8, 1.25, 1.5, 2\}$ and $n \in \{5, 7, 10, 15\}$ when m = 1, $\eta = 0.28$ and B = 1.

INSERT TABLE 8 ABOUT HERE

The obtained results show that the performance of the two-sided EWMA- γ^2 control chart is influenced by the values of θ with a similar behaviour as for the Shewhart-CV control chart discussed earlier. In most cases, the two-sided EWMA- γ^2 control chart outperforms the Shewhart-CV chart. For example, when $n=5, B=1, \gamma_0=0.05, \tau=0.8, \eta=0.28, \gamma_0=0.05$ and $\theta=0.02$, we have $ARL_1=312.97$ for Shewhart-CV chart and $ARL_1=27.32$ for two-sided EWMA- γ^2 control chart (see Tables 3 and 8).

INSERT TABLE 9 ABOUT HERE

Table 9 shows the performances of the two-sided EWMA- γ^2 chart under linear covariate error model for different combinations of $B \in \{1, 2, 3, 4, 5\}, \tau \in \{0.5, 0.65, 0.8, 1.25, 1.5, 2\},$

 $\gamma_0 \in \{0.05, 0.1, 0.2\}$ and $n \in \{5, 7, 10, 15\}$ when m = 1 and $\eta = 0.28$, $\theta = 0.05$. It can be noted from Table 9 that the performance of the two-sided EWMA- γ^2 control chart is influenced by the values of B with a similar behaviour as for the Shewhart-CV control chart discussed earlier. Moreover, in most cases, the two-sided EWMA- γ^2 control chart outperforms the Shewhart-CV chart. For example, when n = 5, $\gamma_0 = 0.05$, $\tau = 0.8$, $\eta = 0.28$, $\gamma_0 = 0.05$, $\theta = 0.01$

The performance of the two-sided EWMA- γ^2 chart under linear covariate error model is shown in Table 10 for different combinations of $m \in \{1,3,5,7,10\}$, $\tau \in \{0.5,0.65,0.8,1.25,1.5,2\}$, $\gamma_0 \in \{0.05,0.1,0.2\}$ and $n \in \{3,5,7,9\}$ when B=1 and $\eta=0.28$. For fixed values of n, τ , B and η , as the number m of measurements per item increases, the value of ARL decreases, demonstrating the positive effect of the number of repeated measurements m per item on the performance of the two-sided EWMA- γ^2 chart with similar behaviour as for the Shewhart-CV control chart discussed earlier. Moreover, in most cases, the two-sided EWMA- γ^2 control chart outperforms the Shewhart-CV chart. For instance, when n=5, $\eta=0.28$, $\theta=0.01$, $\tau=0.8$, m=5 and $\gamma_0=0.05$, we have $ARL_1=319.59$ for Shewhart-CV chart and $ARL_1=27.43$ for two-sided EWMA- γ^2 control chart (see Tables 5 and 10).

INSERT TABLE 10 ABOUT HERE

Similar tables showing the effect of measurement errors for the one-sided EWMA- γ^2 charts are not presented here, but are available upon request from the authors. The performance of one-sided EWMA- γ^2 control charts is influenced by measurement errors with a similar behaviour as for the Shewhart-CV and two-sided EWMA- γ^2 control charts discussed earlier. But, in general, quality practitioners often have an interest in detecting a range of shifts $\Omega = [a, b]$, but with no preference for any particular size of the process shift (for instance, see Chen and Chen ³⁶ and Celano et al. ³⁷). In this case, the statistical performance of the corresponding chart can be evaluated through the EARL (Expected Average Run Length) defined as

$$EARL = \int_{\Omega} ARL \times f_{\tau}(\tau) d\tau.$$
 (28)

with $f_{\tau}(\tau) = \frac{1}{b-a}$ for $\tau \in \Omega = [a, b]$ and ARL is as defined in (21). In the following section, we will consider two different ranges of shifts: $\Omega_D = [0.9, 1)$ corresponding to a decreasing case for τ and $\Omega_I = [1, 1.1)$ corresponding to an increasing case for τ .

In this case, we find unique optimal couples (λ^{-*}, K^{-*}) and (λ^{+*}, K^{+*}) of the one-sided EWMA- γ^2 charts such that

$$(\lambda^*, K^*) = \underset{(\lambda, K)}{\operatorname{argmin}} EARL(\gamma_0^*, \gamma_1^*, \lambda, K, n, m, B, \eta),$$

subject to the constraint

$$EARL(\gamma_0^*, \lambda, K, n) = ARL(\gamma_0^*, \lambda, K, n, m, B, \eta) = ARL_0,$$

The optimal design parameters for the one-sided EWMA- γ^2 charts in the presence of measurement errors is presented in Table 11. For example, when n=5, B=1 and $\gamma_0=0.05$, we have $\lambda^*=0.0501$ and $K^*=2.1425$ for the downward EWMA- γ^2 when $(\eta,\theta)=(0.10,0.01)$.

INSERT TABLE 11 ABOUT HERE

Here, in order to evaluate the overall performance of the one-sided EWMA- γ^2 charts with linear covariate error model, we will use EARL values. In the following section, we will consider the specific range of shifts $\Omega = [0.5, 1)$ (decreasing case, denoted by Ω_D) and $\Omega = (1, 2]$ (increasing case, denoted by Ω_I).

The values of EARL of EWMA- γ^2 control charts are plotted in Figure 1 for $\eta \in [0, 1]$, $\theta \in [0, 0.05]$, $\Omega_D = [0.5, 1)$ and $\Omega_I = (1, 2]$, $n \in \{5, 15\}$, m = 1 and B = 1.

INSERT FIGURE 1 ABOUT HERE

The obtained results show that, for fixed values of $n, \gamma_0, m=1$ and B=1, the smaller the precision error ratio η and the accuracy error θ are, the faster the control chart is in detecting the out-of-control condition, demonstrating the negative effect of measurement errors on the performance of one-sided EWMA- γ^2 chart. However, when $\eta \leq 0.3$ and $\theta \leq 0.0115$, the values of EARL in the presence of a precision error are not significantly larger than the value of EARL without measurement error. For instance, when n=5, $B=1, m=1, \gamma_0=0.05$, we have EARL=36.3 for $\eta=0, \theta=0$, and ARL=36.7 for $\eta=0.3, \theta=0.01$ for the downward EWMA- γ^2 (see Figure 1). So, we can conclude that the precision error does not significantly affect the performance of the one-sided EWMA- γ^2 control charts with a normal measurement system. But, the accuracy error significantly affects the performance of the one-sided EWMA- γ^2 control charts for the usual levels of accuracy errors provided by calibrated gauges. For instance, when n=5, $B=1, m=1, \gamma_0=0.05$, we have EARL=36.3 for $\eta=0$ and $\theta=0$, and ARL=38.2 for $\eta=0$ and $\theta=0.05$ for the downward EWMA- γ^2 (see Figure 1).

The values of EARL of the one-sided EWMA- γ^2 control charts are plotted in Figure 2 for $\eta = 0.28$, $\theta = 0.05$, $\Omega_D = [0.5, 1)$ and $\Omega_I = (1, 2]$, $n \in \{3, 5, 7, 9\}$, m = 1 and $B \in [1, 5]$.

INSERT FIGURE 2 ABOUT HERE

It can be noted from Figure 2 that, for fixed values of n, τ , η , θ and m, the value of B significantly affects the performance of the one-sided EWMA- γ^2 control charts. For

instance, when n=5, $\eta=0.28$, $\theta=0.05$, $\gamma_0=0.05$ and m=1, we have EARL=38.2 for B=1, and ARL=36.7 for B=5 for the downward EWMA- γ^2 (see Figure 2).

The values of EARL of EWMA- γ^2 control charts are plotted in Figure 3 for $\eta = 0.28$, $\theta = 0.05$, $\Omega_D = [0.5, 1)$ and $\Omega_I = (1, 2]$, $n \in \{3, 5, 7, 9\}$, B = 1 and $m \in [1, 10]$.

INSERT FIGURE 3 ABOUT HERE

For fixed values of n, B, η and θ , as the number m of measurements per item increases, the values of EARL of the one-sided EWMA- γ^2 control charts slightly decrease. For instance, when n = 5, $\eta = 0.28$, $\theta = 0.05$ and $\gamma_0 = 0.05$, we have ARL = 38.2 for m = 1 and ARL = 38.2 for m = 10 for the downward EWMA- γ^2 (see Figure 3).

8 Illustrative example

In this Section, we discuss the implementation of Shewhart-CV chart in the presence of measurement errors. Let us consider a sintering process in an Italian company that manufactures sintered mechanical parts. The context of the example presented here is similar to the one introduced in Castagliola et al.². As discussed in Castagliola et al.², the process manufactures parts, to ensure a pressure test drop time T_{pd} from 2 bar to 1.5 bar larger than 30 sec, are seen as a quality characteristic related to the pore shrinkage. They stated that the preliminary regression study relating T_{pd} to the quantity Q_C of molten copper has demonstrated the presence of a constant proportionality $\sigma_{pd} = \gamma_{pd} \times \mu_{pd}$ between the standard deviation of the pressure drop time and its mean. The quality practitioner decided to monitor the coefficient of variation $\gamma_{pd} = \sigma_{pd}/\mu_{pd}$ to detect changes in the process variability.

We assume that, from a Phase I dataset, the following quantity has been estimated $\hat{\gamma}_0 = 0.01$. Concerning the parameters of the linear covariate error model, we assume $\eta = 0.28$, $\theta = 0$, B = 1, m = 1. For phase II, the dataset with a sample size n = 5 is simulated and presented in Table 12. The process is assumed to run in-control up to sample #10. Then, between samples #10 and #11, we have simulated the occurrence of an assignable cause shifting γ_{pd} from $\gamma_{pd} = 0.01$ to $\gamma_{pd} = 0.011$, i.e., $\tau = 1.1$.

INSERT TABLE 12 ABOUT HERE INSERT FIGURE 4 ABOUT HERE INSERT FIGURE 5 ABOUT HERE

INSERT FIGURE 6 ABOUT HERE

The values of $\hat{\gamma}_i^*$, $\hat{\gamma}_i^{*2}$, Z_i^* (for upward EWMA- γ^2 chart) and S_i^* (for two-sided EWMA- γ^2 chart) are presented in Table 12. Based on (25), the control limits of Shewhart-CV control chart ($ARL_0 = 370.4$) with measurement errors are equal to

$$LCL = 0.00169,$$

 $UCL = 0.02192.$

The optimal parameters λ^* and K^* of upward EWMA- γ^2 chart are found by the optimizing algorithm to be $\lambda^* = 0.05$ and $K^* = 2.6743$. Based on (26), the control limits of upward EWMA- γ^2 chart ($ARL_0 = 370.4$) with measurement errors are equal to

$$UCL_{\text{EWMA}} = 0.000140.$$

The optimal parameters λ^* and K^* of two-sided EWMA- γ^2 chart are found by the optimizing algorithm to be $\lambda^* = 0.064038$ and $K^* = 2.588766$. Based on (14) and (15), the control limits of two-sided EWMA- γ^2 chart ($ARL_0 = 370.4$) with measurement errors are equal to

$$LCL_{\text{EWMA}-\gamma^2} = 0.000072,$$

 $UCL_{\text{EWMA}-\gamma^2} = 0.000144.$

The values of $\hat{\gamma}_i^*$ and the control limits of Shewhart-CV chart are plotted in Figure 4. This figure confirms that from sample #12 onwards, the process is clearly out-of-control. Similarly, the values of Z_i^* and the control limit of upward EWMA- γ^2 are plotted in Figure 5. This figure confirms that from sample #11 onwards, the process is clearly out-of-control. Finally, the values of S_i^* and the control limits of that two-sided EWMA- γ^2 are plotted in Figure 6. This figure confirms that from sample #11 onwards, the process is clearly out-of-control. This once again confirms the effectiveness of the application of EWMA type control charts to monitor production processes.

9 Concluding remarks

In this paper, we have studied the effects of measurement errors on the performance of the Shewhart-CV control chart using a linear covariate error model. We have evaluated the performance of the Shewhart-CV control using the ARL as a performance metric. We have found that the performance of the Shewhart-CV control chart in the presence of measurement errors is influenced by the precision error, i.e., the smaller the value of the precision error is, the faster the Shewhart-CV control chart is in detecting the out-of-control condition. But, the precision error does not significantly affect the performance of the Shewhart-CV control chart with a normal measurement system. The performance of the Shewhart-CV control chart is influenced by the accuracy error, measured by θ and by the value of B. Furthermore, the performance of one-sided and two-sided EWMA- γ^2 control charts are influenced by measurement errors with a similar behaviour as for the Shewhart-CV control chart discussed earlier.

Future research about control charts monitoring the coefficient of variation should be focused on the investigation of their Phase I implementation. We are currently looking into this issue and hope to report the findings in a future paper.

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$\overline{}$	θ	γ_0	n = 5	n = 7	n = 10	n = 15
			B =	1		
0.10	0.01	0.05	0.0081	0.0132	0.0185	0.0238
			0.1053	0.0950	0.0865	0.0791
		0.10	0.0161	0.0263	0.0368	0.0475
			0.2130	0.1917	0.1743	0.1591
		0.15	0.0241	0.0394	0.0550	0.0709
			0.3257	0.2919	0.2646	0.2408
		0.20	0.0320	0.0522	0.0729	0.0940
			0.4464	0.3978	0.3589	0.3253
0.28	0.05	0.05	0.0080	0.0131	0.0183	0.0236
			0.1047	0.0944	0.0860	0.0786
		0.10	0.0160	0.0262	0.0366	0.0472
			0.2117	0.1905	0.1732	0.1581
		0.15	0.0240	0.0391	0.0547	0.0705
			0.3236	0.2901	0.2629	0.2393
		0.20	0.0318	0.0519	0.0725	0.0935
			0.4434	0.3952	0.3565	0.3232
			B =	5		
0.10	0.01	0.05	0.0081	0.0132	0.0185	0.0239
			0.1057	0.0953	0.0868	0.0793
		0.10	0.0162	0.0264	0.0369	0.0476
			0.2137	0.1923	0.1749	0.1596
		0.15	0.0242	0.0395	0.0552	0.0711
			0.3268	0.2929	0.2655	0.2416
		0.20	0.0321	0.0524	0.0732	0.0943
			0.4480	0.3992	0.3601	0.3264
0.28	0.05	0.05	0.0081	0.0132	0.0184	0.0237
			0.1050	0.0947	0.0862	0.0788
		0.10	0.0161	0.0263	0.0367	0.0473
			0.2123	0.1910	0.1737	0.1585
		0.15	0.0240	0.0392	0.0548	0.0707
			0.3245	0.2909	0.2637	0.2400
		0.20	0.0319	0.0520	0.0727	0.0937
			0.4447	0.3963	0.3576	0.3241

Table 1: Values of LCL (first row) and UCL (second row) for the Shewhart-CV control chart in the presence of measurement errors, for different values of η , θ , n, γ_0 , B and m=1.

			n=5			
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(56.34, 56.66, 57.91)	(56.34, 56.66, 57.93)	(56.34, 56.67, 57.98)	(56.35, 56.69, 58.06)	(56.37, 56.76, 58.32)	(56.44, 57.07, 59.56)
0.7	(148.13, 148.80, 151.37)	(148.14, 148.81, 151.41)	(148.14, 148.83, 151.51)	(148.15, 148.88, 151.68)	(148.19, 149.02, 152.22)	(148.36, 149.67, 154.72)
0.8	(319.58, 320.48, 323.77)	(319.58, 320.49, 323.82)	(319.60, 320.52, 323.94)	(319.61, 320.59, 324.16)	(319.66, 320.76, 324.84)	(319.90, 321.60, 327.93)
1.3	(48.70, 49.20, 51.32)	(48.70, 49.21, 51.35)	(48.71, 49.23, 51.44)	(48.72, 49.26, 51.59)	(48.74, 49.37, 52.07)	(48.86, 49.89, 54.42)
1.5	(12.30, 12.49, 13.32)	(12.30, 12.50, 13.33)	(12.30, 12.50, 13.36)	(12.31, 12.52, 13.42)	(12.32, 12.56, 13.61)	(12.37, 12.76, 14.55)
2.0	(3.36, 3.42, 3.70)	(3.36, 3.42, 3.70)	(3.36, 3.43, 3.71)	(3.36, 3.43, 3.73)	(3.37, 3.45, 3.79)	(3.38, 3.51, 4.10)
			n = 7			
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(20.71, 20.89, 21.61)	(20.71, 20.89, 21.62)	(20.72, 20.90, 21.64)	(20.72, 20.91, 21.69)	(20.73, 20.95, 21.84)	(20.77, 21.13, 22.55)
0.7	(75.72, 76.27, 78.42)	(75.72, 76.27, 78.45)	(75.72, 76.30, 78.54)	(75.73, 76.33, 78.68)	(75.76, 76.45, 79.13)	(75.90, 76.99, 81.24)
0.8	(223.38, 224.43, 228.42)	(223.38, 224.44, 228.48)	(223.40, 224.49, 228.63)	(223.41, 224.56, 228.89)	(223.47, 224.77, 229.72)	(223.74, 225.78, 233.50)
1.3	(36.67, 37.16, 39.22)	(36.67, 37.17, 39.25)	(36.68, 37.19, 39.34)	(36.68, 37.22, 39.48)	(36.71, 37.33, 39.94)	(36.83, 37.83, 42.18)
1.5	(8.42, 8.58, 9.27)	(8.42, 8.58, 9.28)	(8.42, 8.59, 9.30)	(8.43, 8.60, 9.35)	(8.43, 8.64, 9.51)	(8.47, 8.80, 10.26)
2.0	(2.36, 2.41, 2.61)	(2.36, 2.41, 2.61)	(2.36, 2.41, 2.62)	(2.36, 2.41, 2.63)	(2.36, 2.42, 2.68)	(2.37, 2.47, 2.91)
			n = 10			
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(7.02, 7.10, 7.41)	(7.02, 7.10, 7.41)	(7.02, 7.10, 7.42)	(7.02, 7.11, 7.44)	(7.03, 7.12, 7.51)	(7.05, 7.20, 7.82)
0.7	(33.76, 34.11, 35.49)	(33.76, 34.11, 35.51)	(33.76, 34.12, 35.57)	(33.77, 34.15, 35.66)	(33.78, 34.22, 35.95)	(33.87, 34.57, 37.32)
0.8	(141.35, 142.36, 146.24)	(141.36, 142.37, 146.29)	(141.37, 142.41, 146.44)	(141.39, 142.48, 146.70)	(141.44, 142.69, 147.50)	(141.69, 143.67, 151.20)
1.3	(26.22, 26.65, 28.44)	(26.22, 26.65, 28.46)	(26.23, 26.67, 28.54)	(26.23, 26.70, 28.66)	(26.26, 26.79, 29.05)	(26.36, 27.23, 30.96)
1.5	(5.58, 5.70, 6.21)	(5.58, 5.70, 6.21)	(5.58, 5.71, 6.23)	(5.58, 5.71, 6.27)	(5.59, 5.74, 6.38)	(5.62, 5.86, 6.93)
2.0	(1.70, 1.73, 1.87)	(1.70, 1.73, 1.87)	(1.70, 1.73, 1.87)	(1.70, 1.74, 1.88)	(1.70, 1.74, 1.91)	(1.71, 1.78, 2.06)
			n = 15			
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(2.44, 2.46, 2.57)	(2.44, 2.46, 2.57)	(2.44, 2.47, 2.57)	(2.44, 2.47, 2.58)	(2.44, 2.47, 2.60)	(2.45, 2.50, 2.70)
0.7	(12.70, 12.87, 13.54)	(12.70, 12.87, 13.55)	(12.70, 12.88, 13.58)	(12.71, 12.89, 13.63)	(12.72, 12.93, 13.77)	(12.76, 13.09, 14.45)
0.8	(76.97, 77.75, 80.80)	(76.98, 77.76, 80.83)	(76.98, 77.79, 80.96)	(77.00, 77.84, 81.15)	(77.04, 78.01, 81.79)	(77.23, 78.78, 84.74)
1.3	(17.13, 17.46, 18.82)	(17.14, 17.47, 18.84)	(17.14, 17.48, 18.90)	(17.14, 17.50, 18.99)	(17.16, 17.57, 19.29)	(17.24, 17.91, 20.74)
1.5	(3.50, 3.57, 3.90)	(3.50, 3.57, 3.90)	(3.50, 3.58, 3.92)	(3.50, 3.58, 3.94)	(3.50, 3.60, 4.01)	(3.52, 3.68, 4.37)
2.0	(1.28, 1.30, 1.37)	(1.28, 1.30, 1.37)	(1.28, 1.30, 1.37)	(1.28, 1.30, 1.38)	(1.28, 1.30, 1.40)	(1.28, 1.32, 1.48)

Table 2: ARL values of Shewhart-CV control chart in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of η , $\theta=0.05$, τ , n, B=1, m=1.

			n=5			
τ	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$
0.5	(51.52, 51.86, 53.24)	(52.48, 52.82, 54.20)	(53.44, 53.78, 55.15)	(54.40, 54.75, 56.11)	(55.37, 55.72, 57.07)	(56.35, 56.69, 58.04)
0.7	(138.93, 139.68, 142.62)	(140.78, 141.53, 144.43)	(142.63, 143.38, 146.24)	(144.48, 145.21, 148.05)	(146.32, 147.04, 149.85)	(148.15, 148.87, 151.64)
0.8	(308.39, 309.45, 313.38)	(310.70, 311.73, 315.58)	(312.97, 313.98, 317.75)	(315.20, 316.21, 319.89)	(317.42, 318.39, 322.02)	(319.61, 320.57, 324.11)
1.3	(43.58, 44.14, 46.53)	(44.60, 45.15, 47.53)	(45.62, 46.17, 48.53)	(46.65, 47.19, 49.53)	(47.68, 48.22, 50.54)	(48.71, 49.25, 51.55)
1.5	(10.58, 10.78, 11.66)	(10.91, 11.12, 12.00)	(11.25, 11.46, 12.34)	(11.60, 11.80, 12.69)	(11.95, 12.16, 13.05)	(12.31, 12.51, 13.41)
2.0	(2.89, 2.96, 3.24)	(2.98, 3.05, 3.33)	(3.07, 3.14, 3.43)	(3.17, 3.23, 3.52)	(3.26, 3.33, 3.62)	(3.36, 3.43, 3.73)
			n = 7			
τ	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$
0.5	(18.45, 18.64, 19.40)	(18.90, 19.09, 19.85)	(19.34, 19.54, 20.30)	(19.80, 19.99, 20.76)	(20.26, 20.45, 21.22)	(20.72, 20.91, 21.68)
0.7	(69.32, 69.93, 72.32)	(70.60, 71.20, 73.58)	(71.88, 72.48, 74.84)	(73.16, 73.76, 76.11)	(74.44, 75.04, 77.38)	(75.73, 76.32, 78.65)
0.8	(212.10, 213.32, 217.97)	(214.39, 215.59, 220.17)	(216.67, 217.86, 222.36)	(218.93, 220.10, 224.53)	(221.18, 222.33, 226.69)	(223.41, 224.54, 228.83)
1.3	(32.45, 32.99, 35.28)	(33.28, 33.82, 36.10)	(34.12, 34.66, 36.93)	(34.97, 35.50, 37.76)	(35.82, 36.35, 38.60)	(36.68, 37.21, 39.45)
1.5	(7.21, 7.38, 8.10)	(7.45, 7.61, 8.34)	(7.68, 7.85, 8.58)	(7.93, 8.10, 8.83)	(8.17, 8.35, 9.08)	(8.43, 8.60, 9.34)
2.0	(2.06, 2.11, 2.32)	(2.12, 2.17, 2.38)	(2.17, 2.22, 2.44)	(2.23, 2.28, 2.50)	(2.30, 2.35, 2.56)	(2.36, 2.41, 2.63)
			n = 10			
τ	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$
0.5	(6.17, 6.25, 6.57)	(6.34, 6.42, 6.74)	(6.51, 6.59, 6.91)	(6.68, 6.76, 7.08)	(6.85, 6.93, 7.26)	(7.02, 7.11, 7.44)
0.7	(30.16, 30.54, 32.03)	(30.87, 31.25, 32.74)	(31.58, 31.96, 33.46)	(32.30, 32.68, 34.18)	(33.03, 33.41, 34.90)	(33.76, 34.14, 35.64)
0.8	(131.70, 132.84, 137.26)	(133.64, 134.77, 139.14)	(135.59, 136.71, 141.02)	(137.52, 138.63, 142.90)	(139.46, 140.55, 144.77)	(141.38, 142.46, 146.64)
1.3	(22.96, 23.42, 25.37)	(23.60, 24.06, 26.01)	(24.25, 24.71, 26.65)	(24.90, 25.36, 27.30)	(25.56, 26.02, 27.96)	(26.23, 26.69, 28.63)
1.5	(4.78, 4.90, 5.43)	(4.93, 5.06, 5.59)	(5.09, 5.22, 5.75)	(5.25, 5.38, 5.92)	(5.42, 5.54, 6.09)	(5.58, 5.71, 6.26)
2.0	(1.52, 1.56, 1.69)	(1.56, 1.59, 1.73)	(1.59, 1.62, 1.76)	(1.63, 1.66, 1.80)	(1.66, 1.70, 1.84)	(1.70, 1.74, 1.88)
			n = 15			
τ	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$
0.5	(2.18, 2.21, 2.31)	(2.23, 2.26, 2.36)	(2.28, 2.31, 2.41)	(2.33, 2.36, 2.47)	(2.39, 2.41, 2.52)	(2.44, 2.47, 2.58)
0.7	(11.13, 11.30, 12.01)	(11.43, 11.61, 12.32)	(11.74, 11.92, 12.64)	(12.06, 12.24, 12.96)	(12.38, 12.56, 13.28)	(12.71, 12.89, 13.62)
0.8	(70.11, 70.98, 74.35)	(71.48, 72.34, 75.70)	(72.85, 73.71, 77.04)	(74.23, 75.08, 78.40)	(75.61, 76.45, 79.75)	(76.99, 77.83, 81.11)
1.3	(14.85, 15.20, 16.65)	(15.29, 15.64, 17.10)	(15.74, 16.10, 17.56)	(16.20, 16.56, 18.02)	(16.67, 17.02, 18.49)	(17.14, 17.50, 18.97)
1.5	(3.02, 3.10, 3.43)	(3.11, 3.19, 3.53)	(3.20, 3.28, 3.63)	(3.30, 3.38, 3.73)	(3.40, 3.48, 3.83)	(3.50, 3.58, 3.93)
2.0	(1.19, 1.21, 1.28)	(1.21, 1.22, 1.30)	(1.22, 1.24, 1.32)	(1.24, 1.26, 1.34)	(1.26, 1.28, 1.36)	(1.28, 1.30, 1.38)

Table 3: ARL values of Shewhart-CV control chart in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of θ , $\eta=0.28$, τ , n, B=1, m=1.

			n = 5		
au	B=1	B=2	B=3	B=4	B=5
0.5	(56.35, 56.69, 58.04)	(53.91, 54.24, 55.53)	(53.11, 53.43, 54.71)	(52.71, 53.03, 54.31)	(52.47, 52.79, 54.07)
0.7	(148.15, 148.87, 151.64)	(143.54, 144.24, 146.94)	(142.00, 142.70, 145.39)	(141.23, 141.93, 144.62)	(140.77, 141.46, 144.16)
0.8	(319.61, 320.57, 324.11)	(314.07, 315.03, 318.56)	(312.18, 313.15, 316.71)	(311.24, 312.21, 315.78)	(310.67, 311.64, 315.23)
1.3	(48.71, 49.25, 51.55)	(46.12, 46.64, 48.85)	(45.27, 45.78, 47.98)	(44.84, 45.35, 47.55)	(44.58, 45.10, 47.30)
1.5	(12.31, 12.51, 13.41)	(11.42, 11.62, 12.45)	(11.13, 11.33, 12.15)	(10.99, 11.18, 12.00)	(10.91, 11.10, 11.91)
2.0	(3.36, 3.43, 3.73)	(3.12, 3.18, 3.45)	(3.04, 3.10, 3.37)	(3.00, 3.06, 3.33)	(2.98, 3.04, 3.30)
			n = 7		
au	B=1	B=2	B=3	B=4	B=5
0.5	(20.72, 20.91, 21.68)	(19.57, 19.75, 20.47)	(19.19, 19.37, 20.08)	(19.00, 19.18, 19.89)	(18.89, 19.07, 19.78)
0.7	(75.73, 76.32, 78.65)	(72.51, 73.08, 75.31)	(71.44, 72.00, 74.22)	(70.90, 71.47, 73.68)	(70.58, 71.15, 73.36)
0.8	(223.41, 224.54, 228.83)	(217.78, 218.90, 223.13)	(215.89, 217.00, 221.25)	(214.93, 216.06, 220.32)	(214.36, 215.49, 219.76)
1.3	(36.68, 37.21, 39.45)	(34.54, 35.04, 37.17)	(33.83, 34.33, 36.45)	(33.48, 33.98, 36.09)	(33.27, 33.77, 35.88)
1.5	(8.43, 8.60, 9.34)	(7.80, 7.96, 8.65)	(7.60, 7.76, 8.44)	(7.50, 7.66, 8.33)	(7.44, 7.60, 8.27)
2.0	(2.36, 2.41, 2.63)	(2.20, 2.25, 2.45)	(2.15, 2.20, 2.40)	(2.13, 2.18, 2.37)	(2.11, 2.16, 2.36)
			n = 10		
τ	B=1	B=2	B=3	B=4	B=5
0.5	(7.02, 7.11, 7.44)	(6.59, 6.66, 6.97)	(6.45, 6.52, 6.82)	(6.38, 6.45, 6.75)	(6.34, 6.41, 6.71)
0.7	(33.76, 34.14, 35.64)	(31.94, 32.29, 33.71)	(31.34, 31.69, 33.09)	(31.04, 31.39, 32.78)	(30.86, 31.21, 32.60)
0.8	(141.38, 142.46, 146.64)	(136.53, 137.59, 141.65)	(134.91, 135.97, 140.03)	(134.10, 135.16, 139.22)	(133.62, 134.67, 138.74)
1.3	(26.23, 26.69, 28.63)	(24.56, 25.00, 26.83)	(24.02, 24.45, 26.26)	(23.75, 24.18, 25.99)	(23.59, 24.02, 25.82)
1.5	(5.58, 5.71, 6.26)	(5.17, 5.29, 5.79)	(5.04, 5.15, 5.65)	(4.97, 5.09, 5.58)	(4.93, 5.05, 5.54)
2.0	(1.70, 1.74, 1.88)	(1.61, 1.64, 1.77)	(1.58, 1.61, 1.74)	(1.56, 1.60, 1.72)	(1.56, 1.59, 1.71)
			n = 15		
τ	B=1	B=2	B=3	B=4	B=5
0.5	(2.44, 2.47, 2.58)	(2.31, 2.33, 2.43)	(2.27, 2.29, 2.39)	(2.24, 2.27, 2.37)	(2.23, 2.26, 2.35)
0.7	(12.71, 12.89, 13.62)	(11.90, 12.07, 12.74)	(11.64, 11.80, 12.47)	(11.51, 11.67, 12.33)	(11.43, 11.59, 12.25)
0.8	(76.99, 77.83, 81.11)	(73.53, 74.33, 77.48)	(72.38, 73.18, 76.31)	(71.80, 72.60, 75.73)	(71.46, 72.26, 75.39)
1.3	(17.14, 17.50, 18.97)	(15.97, 16.30, 17.68)	(15.59, 15.91, 17.28)	(15.40, 15.72, 17.08)	(15.28, 15.61, 16.96)
1.5	(3.50, 3.58, 3.93)	(3.25, 3.33, 3.65)	(3.17, 3.25, 3.56)	(3.13, 3.21, 3.52)	(3.11, 3.18, 3.50)
2.0	(1.28, 1.30, 1.38)	(1.23, 1.25, 1.32)	(1.22, 1.23, 1.30)	(1.21, 1.23, 1.30)	(1.21, 1.22, 1.29)

Table 4: ARL values of Shewhart-CV control chart in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of $B,\,\tau,\,n,\,\eta=0.28,\,\theta=0.01,\,m=1.$

			n = 5		
au	m = 1	m = 3	m = 5	m = 7	m = 10
0.5	(56.35, 56.69, 58.04)	(56.34, 56.67, 57.95)	(56.34, 56.66, 57.94)	(56.34, 56.66, 57.93)	(56.34, 56.66, 57.92)
0.7	(148.15, 148.87, 151.64)	(148.14, 148.82, 151.46)	(148.14, 148.81, 151.43)	(148.14, 148.81, 151.41)	(148.14, 148.81, 151.40)
0.8	(319.61, 320.57, 324.11)	(319.59, 320.51, 323.89)	(319.59, 320.50, 323.85)	(319.58, 320.49, 323.82)	(319.59, 320.49, 323.81)
1.3	(48.71, 49.25, 51.55)	(48.71, 49.22, 51.40)	(48.71, 49.21, 51.37)	(48.70, 49.21, 51.35)	(48.71, 49.20, 51.34)
1.5	(12.31, 12.51, 13.41)	(12.30, 12.50, 13.35)	(12.30, 12.50, 13.34)	(12.30, 12.50, 13.33)	(12.30, 12.50, 13.33)
2.0	(3.36, 3.43, 3.73)	(3.36, 3.43, 3.71)	(3.36, 3.42, 3.70)	(3.36, 3.42, 3.70)	(3.36, 3.42, 3.70)
			n = 7		
au	m = 1	m = 3	m = 5	m = 7	m = 10
0.5	(20.72, 20.91, 21.68)	(20.71, 20.90, 21.63)	(20.71, 20.90, 21.62)	(20.71, 20.89, 21.62)	(20.71, 20.89, 21.61)
0.7	(75.73, 76.32, 78.65)	(75.72, 76.29, 78.50)	(75.72, 76.28, 78.47)	(75.72, 76.27, 78.46)	(75.72, 76.27, 78.45)
0.8	(223.41, 224.54, 228.83)	(223.39, 224.47, 228.56)	(223.39, 224.45, 228.51)	(223.38, 224.45, 228.49)	(223.38, 224.44, 228.46)
1.3	(36.68, 37.21, 39.45)	(36.67, 37.18, 39.30)	(36.67, 37.17, 39.27)	(36.67, 37.17, 39.26)	(36.67, 37.16, 39.25)
1.5	(8.43, 8.60, 9.34)	(8.42, 8.59, 9.29)	(8.42, 8.59, 9.28)	(8.42, 8.58, 9.28)	(8.42, 8.58, 9.27)
2.0	(2.36, 2.41, 2.63)	(2.36, 2.41, 2.62)	(2.36, 2.41, 2.61)	(2.36, 2.41, 2.61)	(2.36, 2.41, 2.61)
			n = 10		
τ	m = 1	m = 3	m = 5	m = 7	m = 10
0.5	(7.02, 7.11, 7.44)	(7.02, 7.10, 7.42)	(7.02, 7.10, 7.41)	(7.02, 7.10, 7.41)	(7.02, 7.10, 7.41)
0.7	(33.76, 34.14, 35.64)	(33.76, 34.12, 35.54)	(33.76, 34.11, 35.52)	(33.76, 34.11, 35.51)	(33.76, 34.11, 35.51)
0.8	(141.38, 142.46, 146.64)	(141.36, 142.39, 146.37)	(141.36, 142.38, 146.32)	(141.36, 142.37, 146.30)	(141.36, 142.37, 146.28)
1.3	(26.23, 26.69, 28.63)	(26.22, 26.66, 28.50)	(26.22, 26.66, 28.48)	(26.22, 26.65, 28.47)	(26.22, 26.65, 28.46)
1.5	(5.58, 5.71, 6.26)	(5.58, 5.70, 6.22)	(5.58, 5.70, 6.22)	(5.58, 5.70, 6.21)	(5.58, 5.70, 6.21)
2.0	(1.70, 1.74, 1.88)	(1.70, 1.73, 1.87)	(1.70, 1.73, 1.87)	(1.70, 1.73, 1.87)	(1.70, 1.73, 1.87)
			n = 15		
τ	m = 1	m = 3	m = 5	m = 7	m = 10
0.5	(2.44, 2.47, 2.58)	(2.44, 2.47, 2.57)	(2.44, 2.46, 2.57)	(2.44, 2.46, 2.57)	(2.44, 2.46, 2.57)
0.7	(12.71, 12.89, 13.62)	(12.70, 12.88, 13.57)	(12.70, 12.87, 13.56)	(12.70, 12.87, 13.55)	(12.70, 12.87, 13.55)
0.8	(76.99, 77.83, 81.11)	(76.98, 77.78, 80.90)	(76.98, 77.77, 80.86)	(76.98, 77.76, 80.84)	(76.97, 77.76, 80.83)
1.3	(17.14, 17.50, 18.97)	(17.14, 17.47, 18.87)	(17.14, 17.47, 18.85)	(17.14, 17.47, 18.85)	(17.14, 17.46, 18.84)
1.5	(3.50, 3.58, 3.93)	(3.50, 3.58, 3.91)	(3.50, 3.57, 3.91)	(3.50, 3.57, 3.90)	(3.50, 3.57, 3.90)
2.0	(1.28, 1.30, 1.38)	(1.28, 1.30, 1.37)	(1.28, 1.30, 1.37)	(1.28, 1.30, 1.37)	(1.28, 1.30, 1.37)

Table 5: ARL values of Shewhart-CV control chart in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of m, τ , n, $\eta=0.28$, $\theta=0.05$, B=1.

n = 5

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				10 -	- 0		
COPTS, 0.0745, 0.0610 COPTS, 0.0744, 0.0690 COPTS, 0.0751, 0.0580, 0.0591 COPTS, 0.0511, 0.0580, 0.0591 COPTS, 0.0532, 0.0418 COPTS, 0.0532, 0.04190 COPTS, 0.0531, 0.0416 COPTS, 0.0	au	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
COPTS, 0.0745, 0.0610 COPTS, 0.0744, 0.0690 COPTS, 0.0751, 0.0580, 0.0591 COPTS, 0.0511, 0.0580, 0.0591 COPTS, 0.0532, 0.0418 COPTS, 0.0532, 0.04190 COPTS, 0.0531, 0.0416 COPTS, 0.0	0.5	(2.6906, 2.7006, 2.8184)	(2.6908, 2.7008, 2.8208)	(2.6911, 2.7021, 2.8284)	(2.6910, 2.7038, 2.8410)	(2.6933, 2.7028, 2.8829)	(2.6962, 2.7232, 3.1070)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					(0.0792, 0.0742, 0.0600)		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	0.7	, , , , , , , , , , , , , , , , , , , ,	(2.5540, 2.5491, 2.6487)	(2.5543, 2.5495, 2.6561)		(2.5495, 2.5523, 2.7126)	
0.322, 0.2761, 2.3769, 2.3779, 2.2861, 2.9973, 2.2788, 2.2866, 0.2976, 0.2069, 0.0077, 0.0079, 0.0077, 0.0099, 0.0077, 0.0099, 0.0077, 0.0099, 0.0077, 0.0099, 0.0077, 0.0099, 0.0077, 0.0099, 0.0077, 0.0099, 0.0091, 0.00856, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.00988, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.00988, 0.0096, 0.00456, 0.0096, 0.00456, 0.00988, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.00988, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.00456, 0.0096, 0.0096, 0.00456, 0.0096, 0.00986, 0.00986, 0.0096, 0.00986, 0.0		, , ,	, , , ,				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	0.8			, , , ,	, , ,		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.0	, , , , , , , , , , , , , , , , , , , ,	, , , ,			, , , , , , , , , , , , , , , , , , , ,	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	1.9	, , , , , , , , , , , , , , , , , , , ,	' ' '			, , ,	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.5						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 5	, , , , , , , , , , , , , , , , , , , ,	, , , ,				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.0		, , , ,				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.0				, , ,		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2.0	, , ,	, , , ,				' ' '
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		(0.3674, 0.3642, 0.3454)	(0.3664, 0.3625, 0.3444)	, , ,		(0.3688, 0.3642, 0.3354)	(0.3688, 0.3559, 0.3160)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	τ		$\eta = 0.1$		$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
$\begin{array}{c} 0.7 & (2.6744, 2.6784, 2.7494) \\ (0.802, 0.0758, 0.0621) \\ (0.802, 0.0758, 0.0621) \\ (0.807, 0.0756, 0.0620) \\ (0.807, 0.0756, 0.0620) \\ (0.807, 0.0756, 0.0620) \\ (0.807, 0.0756, 0.0620) \\ (0.807, 0.0756, 0.0621) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0423, 0.0391, 0.0308) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1194, 0.1103) \\ (0.2360, 0.2333, 0.2286) \\ (0.2365, 0.2353, 0.2288) \\ (0.2365, 0.2353, 0.2288) \\ (0.2365, 0.2346, 0.2286) \\ (0.2365, 0.2346, 0.2286) \\ (0.2365, 0.2336, 0.3331, 0.2288) \\ (0.4917, 0.4855, 0.4560) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4856, 0.4560) \\ (0.4912, 0.4850, 0.4560) \\ (0.4912$	0.5	(2.8163, 2.8279, 2.9185)	(2.8184, 2.8284, 2.9237)	(2.8180, 2.8304, 2.9287)	(2.8162, 2.8313, 2.9388)	(2.8191, 2.8366, 2.9665)	(2.8207, 2.8523, 3.1201)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		(0.1118, 0.1063, 0.0900)	(0.1123, 0.1063, 0.0905)	(0.1121, 0.1064, 0.0900)	(0.1115, 0.1060, 0.0896)	(0.1118, 0.1054, 0.0870)	(0.1101, 0.1003, 0.0780)
$\begin{array}{c} 0.8 & (2.4318, 2.4203, 2.4657) \\ (2.4318, 2.4205, 2.4565) \\ (2.4318, 2.4205, 2.4565) \\ (2.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0312) \\ (0.0424, 0.0396, 0.0311) \\ (0.0423, 0.0391, 0.0391, 0.0393) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1191, 0.1102) \\ (0.1232, 0.1194, 0.1103) \\ (0.1232, 0.1194, 0.1003) \\ (0.1232, 0.1194, 0.1004) \\ (0.1231, 0.1184, 0.1091) \\ (0.2360, 0.2333, 0.2286) \\ (0.2365, 0.2353, 0.2288) \\ (0.2466, 0.2383, 0.2283) \\ (0.4917, 0.4855, 0.4560) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4560) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4855, 0.4562) \\ (0.4917, 0.4855, 0.4562) \\ (0.4917, 0.4855, 0.4562) \\ (0.4918, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ (0.4917, 0.4852, 0.4852) \\ $	0.7	(2.6744, 2.6784, 2.7494)	(2.6772, 2.6778, 2.7511)	(2.6775, 2.6786, 2.7567)	(2.6764, 2.6799, 2.7663)	(2.6758, 2.6796, 2.7960)	(2.6773, 2.6873, 2.9692)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		(0.0802, 0.0758, 0.0621)	(0.0807, 0.0756, 0.0620)	(0.0807, 0.0755, 0.0617)	(0.0804, 0.0754, 0.0612)	(0.0800, 0.0742, 0.0593)	(0.0791, 0.0698, 0.0526)
$\begin{array}{c} 1.3 & 2.8626, 2.8896, 3.0187 \\ \hline (2.8627, 2.8813, 3.02187) \\ \hline (2.8632, 2.81910, 0.1102) \\ \hline (0.1232, 0.11184, 0.1103) \\ \hline (0.1232, 0.11194, 0.1102) \\ \hline (0.1232, 0.1124, 0.1103) \\ \hline (0.2361, 0.2334, 0.2286) \\ \hline (0.2365, 0.2335, 0.22886) \\ \hline (0.2365, 0.2335, 0.22886) \\ \hline (0.2365, 0.2336, 0.22885) \\ \hline (0.2365, 0.2336, 0.22886) \\ \hline (0.4917, 0.4855, 0.4560) \\ \hline (0.4917, 0.4855, 0.4560) \\ \hline (0.4918, 0.4856, 0.44543) \\ \hline (0.4912, 0.4855, 0.4560) \\ \hline (0.4918, 0.4856, 0.44543) \\ \hline (0.4912, 0.4855, 0.4560) \\ \hline (0.4917, 0.4856, 0.4426) \\ \hline (0.4918, 0.4856, 0.44543) \\ \hline (0.4912, 0.4856, 0.4426) \\ \hline (0.4912, 0.4856, 0.4426) \\ \hline (0.4912, 0.4856, 0.4426) \\ \hline (0.4899, 0.4716, 0.4172) \\ \hline (0.1252, 0.1542, 0.1354) \\ \hline (0.1623, 0.1542, 0.1352) \\ \hline (0.1542, 0.1542, 0.1352) \\ \hline (0.1553, 0.1542, 0.1462) \\ \hline (0.1553, 0.1542, 0.1462) \\ \hline (0.1554, 0.$	0.8	(2.4318, 2.4203, 2.4647)	(2.4318, 2.4205, 2.4650)	(2.4319, 2.4195, 2.4725)	(2.4316, 2.4183, 2.4827)	(2.4322, 2.4164, 2.5153)	(2.4282, 2.4166, 2.7372)
$\begin{array}{c} 1.3 & (2.8626, 2.8896, 3.0187) & (2.8627, 2.8813, 3.0218) \\ (0.1232, 0.1119, 0.1102) & (0.1232, 0.11184, 0.1103) & (0.1232, 0.11184, 0.1109) & (0.1231, 0.1184, 0.1019) & (0.1231, 0.1176, 0.1094) \\ (0.2362, 0.1191, 0.1102) & (0.1232, 0.1184, 0.1103) & (0.1232, 0.1184, 0.1109) & (0.1231, 0.1184, 0.1019) & (0.1231, 0.1176, 0.1094) \\ (0.2360, 0.2333, 0.2286) & (0.2365, 0.2333, 0.2288) & (0.2365, 0.2333, 0.2285) & (0.2365, 0.2333, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2334, 0.2283) & (0.2365, 0.2345, 0.2384) & (0.4914, 0.4855, 0.4519) & (0.4917, 0.4855, 0.4426) & (0.4899, 0.4716, 0.4172) & (0.4917, 0.4855, 0.4426) & (0.4899, 0.4716, 0.4172) & (0.4917, 0.4855, 0.4426) & (0.4899, 0.4716, 0.4172) & (0.1250, 0.1525, 0.1542, 0.1343) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) & (0.1613, 0.1517, 0.1934) $		(0.0424, 0.0396, 0.0314)	(0.0424, 0.0396, 0.0312)	(0.0424, 0.0394, 0.0311)	(0.0423, 0.0391, 0.0308)	(0.0423, 0.0385, 0.0296)	(0.0415, 0.0362, 0.0256)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.3	(2.8626, 2.8836, 3.0187)	(2.8627, 2.8813, 3.0218)	(2.8630, 2.8828, 3.0258)	(2.8634, 2.8852, 3.0361)	(2.8653, 2.8906, 3.0782)	(2.8711, 2.9105, 3.2766)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.5						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$, , , ,	' ' '				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.0	, , , , , , , , , , , , , , , , , , , ,	, , , ,				
$\frac{n=10}{0.5} \frac{\eta=0.1}{(2.9409, 2.9473, 3.0194)} (2.9397, 2.9475, 3.0226) (2.9406, 2.9483, 3.0250) (2.9384, 2.9494, 3.0318) (2.9400, 2.9500, 3.0493) (2.9426, 2.9607, 3.1553) (0.1625, 0.1542, 0.1348) (0.1621, 0.1542, 0.1352) (0.1623, 0.1540, 0.1342) (0.1613, 0.1537, 0.1334) (0.1613, 0.1517, 0.1296) (0.1596, 0.1448, 0.1174) (0.7 (2.7899, 2.7924, 2.8496) (2.7904, 2.7945, 2.8498) (2.7868, 2.7937, 2.8549) (2.7876, 2.7945, 2.8593) (2.7876, 2.7973, 2.8778) (2.7899, 2.8078, 2.9896) (0.1134, 0.1074, 0.0920) (0.1135, 0.1079, 0.0916) (0.1124, 0.1074, 0.0915) (0.1125, 0.1071, 0.0904) (0.1121, 0.1064, 0.0877) (0.1112, 0.1014, 0.1074, 0.0915) (0.1125, 0.1071, 0.0904) (0.1121, 0.1064, 0.0877) (0.1112, 0.1014, 0.1074, 0.0915) (0.1586, 2.5542, 2.5889) (2.5568, 2.5524, 2.5788) (2.5501, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5510, 2.5512, 2.5821) (2.5608, 2.5528, 2.5828) (2.5500, 2.5514, 2.6105) (2.5572, 2.5502, 2.7473) (0.0596, 0.0567, 0.0466) (0.0602, 0.0565, 0.0466) (0.0593, 0.0566, 0.0462) (0.0603, 0.0565, 0.0458) (0.0595, 0.0554, 0.0446) (0.0590, 0.0527, 0.0393) (0.1589, 0.1542, 0.1420) (0.1583, 0.15412, 0.1418) (0.1594, 0.1541, 0.1420) (0.1586, 0.1539, 0.1416) (0.1594, 0.1529, 0.1398) (0.1574, 0.1481, 0.1397) (0.3195, 0.3156, 0.3010) (0.3186, 0.3159, 0.3020) (0.3176, 0.3146, 0.3000) (0.3186, 0.3156, 0.3954, 3.2563, 3.8487) (3.6954, 3.7266, 3.8499) (3.6974, 3.7273, 3.8564) (3.6906, 3.7285, 3.3785, 3.3806, 3.3487) (3.6954, 3.7266, 3.8499) (3.6974, 3.7273, 3.8564) (3.6906, 3.7285, 3.3785, 3.3806, 3.3812) (3.6980, 3.7285, 3.3806, 3.4812) (0.6418, 0.6339, 0.2946) (0.6418, 0.6339, 0.2946) (0.6418, 0.6339, 0.2946) (0.6418, 0.6339, 0.2948) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2458, 0.2399, 0.2031) (0.2466, 0.2895, 0.0886, 0.0881, 0.0717, 0.1339) (0.1634, 0.1528, 0.1399) (0.1644, 0.1590, 0.1389) (0.1643, 0.1586, 0.1376) (0.1650$	2.0					, , ,	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		(0.4317, 0.4000, 0.4000)	(0.4310, 0.4004, 0.4049)	, , ,		(0.4312, 0.4000, 0.4420)	(0.4033, 0.4110, 0.4112)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	τ	n = 0	n = 0.1			n = 0.5	n = 1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		<u> </u>	<u> </u>	<u>'</u>	<u> </u>	<u>'</u>	
$\begin{array}{c} 0.7 & (2.7899, 2.7924, 2.8496) & (2.7904, 2.7945, 2.8498) & (2.7868, 2.7937, 2.8549) & (2.7876, 2.7945, 2.8593) & (2.7876, 2.7973, 2.8778) & (2.7899, 2.8078, 2.9896) \\ & (0.1134, 0.1074, 0.0920) & (0.1135, 0.1079, 0.0916) & (0.1124, 0.1074, 0.0915) & (0.1125, 0.1071, 0.0904) & (0.1121, 0.1064, 0.0877) & (0.1112, 0.1021, 0.0781) \\ & (0.8568, 2.5524, 2.5778) & (2.5601, 2.5510, 2.5596) & (2.5547, 2.5525, 2.5821) & (2.5608, 2.5528, 2.5880) & (2.5570, 2.5491, 2.6105) & (2.5572, 2.5502, 2.7473) \\ & (0.0596, 0.0567, 0.0466) & (0.0602, 0.0565, 0.0466) & (0.0593, 0.0566, 0.0462) & (0.0603, 0.0565, 0.0458) & (0.0595, 0.0554, 0.0446) & (0.0599, 0.0527, 0.0393) \\ & (0.1589, 0.1542, 0.1441) & (2.9289, 2.9475, 3.0452) & (2.9323, 2.9486, 3.0518) & (2.9307, 2.9500, 3.0598) & (2.9344, 2.9538, 3.0851) & (2.9361, 2.9715, 3.2329) \\ & (0.1589, 0.1542, 0.1442) & (0.1584, 0.1542, 0.14418) & (0.1594, 0.1544, 0.1420) & (0.1586, 0.1539, 0.1416) & (0.1594, 0.1529, 0.1388) & (0.1574, 0.1481, 0.1397) \\ & (0.3195, 0.3156, 0.3010) & (0.3186, 0.3159, 0.3200) & (0.3176, 0.3146, 0.3000) & (0.3186, 0.3156, 0.2985) & (0.3195, 0.3137, 0.2938) & (0.3186, 0.3082, 0.2825) \\ & (0.36953, 3.7285, 3.8487) & (3.6954, 3.7266, 3.8499) & (3.6974, 3.7273, 3.8564) & (3.6960, 3.7298, 3.8633) & (3.6980, 3.7360, 3.8926) & (3.7071, 3.7672, 4.0163) \\ & (0.6418, 0.6359, 0.5966) & (0.6418, 0.6330, 0.5958) & (0.6438, 0.6320, 0.5959) & (0.6413, 0.6320, 0.5922) & (0.6413, 0.6296, 0.5877) & (0.6408, 0.6212, 0.5526) \\ & & & & & & & & & & & & & & & & & & $	0.0	, , ,	, , , ,				
$ \begin{array}{c} (0.1134, 0.1074, 0.0920) \\ (0.1134, 0.1079, 0.0916) \\ (0.1124, 0.1074, 0.0915) \\ (0.2568, 2.5524, 2.5778) \\ (2.5568, 2.5524, 2.5778) \\ (2.5560, 2.5510, 2.5796) \\ (2.5570, 2.510, 2.5796) \\ (2.5574, 2.5525, 2.5821) \\ (2.5566, 0.0665, 0.0466) \\ (0.0693, 0.0566, 0.0466) \\ (0.0692, 0.0565, 0.0466) \\ (0.0593, 0.0566, 0.0462) \\ (0.0593, 0.0566, 0.0463) \\ (0.0693, 0.0565, 0.0458) \\ (0.0693, 0.0565, 0.0458) \\ (0.0595, 0.0554, 0.0446) \\ (0.0590, 0.0527, 0.0393) \\ (0.1589, 0.1542, 0.1420) \\ (0.1589, 0.1542, 0.1420) \\ (0.1583, 0.1542, 0.1418) \\ (0.1594, 0.1541, 0.1420) \\ (0.1594, 0.1541, 0.1420) \\ (0.1584, 0.3260, 3.3417) \\ (0.3195, 0.3156, 0.3010) \\ (0.3186, 0.3159, 0.3200) \\ (0.3166, 0.3159, 0.3200) \\ (0.3176, 0.3166, 0.3010) \\ (0.418, 0.6359, 0.5966) \\ (0.6418, 0.6359, 0.5966) \\ (0.6418, 0.6330, 0.5958) \\ (0.6438, 0.6320, 0.5959) \\ (0.6438, 0.6320, 0.5959) \\ (0.6413, 0.6320, 0.5922) \\ (0.6413, 0.6320, 0.5922) \\ (0.6413, 0.6296, 0.5877) \\ (0.6408, 0.6212, 0.5526) \\ \hline \\ \hline{ \hline $\eta = 0$ } \hline { \eta = 0.1 } \hline { \eta = 0.2 } \hline { \eta = 0.3 } \hline { \eta = 0.5 } \hline { \eta = 1} \\ \hline \\ \hline 0.5 \\ (0.2448, 0.2390, 0.2043) \\ (0.2448, 0.2390, 0.2043) \\ (0.2448, 0.2399, 0.2031) \\ (0.2458, 0.2399, 0.2931) \\ (0.2458, 0.2399, 0.2931) \\ (0.2458, 0.2399, 0.2931) \\ (0.2468, 0.2399, 0.2931) \\ (0.2468, 0.2399, 0.2931) \\ (0.2468, 0.2399, 0.1392) \\ (0.1650, 0.1599, 0.1392) \\ (0.1650, 0.1599, 0.1392) \\ (0.1650, 0.1599, 0.1392) \\ (0.16650, 0.1599, 0.1392) \\ $	0.7						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.7	, , , , , , , , , , , , , , , , , , , ,	, , , ,				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.8	, , , , , , , , , , , , , , , , , , , ,	, , , ,				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.0			, , , ,			
$ \begin{array}{c} (0.1589, 0.1542, 0.1420) \\ (0.1583, 0.1542, 0.1418) \\ (0.1594, 0.1541, 0.1420) \\ (0.1594, 0.1541, 0.1420) \\ (0.1586, 0.1539, 0.1416) \\ (0.1594, 0.1529, 0.1398) \\ (0.1574, 0.1481, 0.1397) \\ (0.32966, 3.34417) \\ (0.32960, 3.3260, 3.4417) \\ (0.3195, 0.3156, 0.3010) \\ (0.3186, 0.3010) \\ (0.3186, 0.3159, 0.3020) \\ (0.3176, 0.3146, 0.3000) \\ (0.3176, 0.3146, 0.3000) \\ (0.3186, 0.3156, 0.2985) \\ (0.3186, 0.3159, 0.3137, 0.2938) \\ (0.6418, 0.6359, 0.5966) \\ (0.6418, 0.6359, 0.5966) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6330, 0.5958) \\ (0.6418, 0.6320, 0.5959) \\ (0.6418, 0.6320, 0.5922) \\ (0.6413, 0.6320, 0.5922) \\ (0.6413, 0.6296, 0.5877) \\ (0.6413, 0.6296, 0.5877) \\ (0.6413, 0.6296, 0.5877) \\ (0.6408, 0.6212, 0.5526) \\ \hline \\ $	1.0		, , , ,				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.3		, , , , , , , , , , , , , , , , , , , ,				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.5				, , ,		, , , ,
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$, , , , , , , , , , , , , , , , , , , ,	, , , ,				
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	2.0				, , ,		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		(0.6418, 0.6359, 0.5966)	(0.6418, 0.6330, 0.5958)		(/ /	(0.6413, 0.6296, 0.5877)	(0.6408, 0.6212, 0.5526)
$\begin{array}{c} 0.5 (3.0561, 3.0710, 3.1077) (3.0579, 3.0732, 3.1065) (3.0582, 3.0751, 3.1071) (3.0560, 3.0732, 3.1117) (3.0578, 3.0806, 3.1220) (3.0601, 3.0926, 3.2109) \\ (0.2448, 0.2390, 0.2043) (0.2458, 0.2399, 0.2031) (0.2458, 0.2404, 0.2014) (0.2443, 0.2385, 0.2001) (0.2446, 0.2395, 0.1943) (0.2424, 0.2319, 0.1845) \\ 0.7 (2.8987, 2.9072, 2.9467) (2.8993, 2.9049, 2.9484) (2.8976, 2.9063, 2.9511) (2.8978, 2.9068, 2.9544) (2.8987, 2.9090, 2.9659) (2.9017, 2.9190, 3.0384) \\ (0.1650, 0.1599, 0.1392) (0.1652, 0.1588, 0.1394) (0.1644, 0.1590, 0.1389) (0.1643, 0.1586, 0.1376) (0.1643, 0.1577, 0.1339) (0.1634, 0.1528, 0.1213) \\ 0.8 (2.6805, 2.6778, 2.6949) (2.6777, 2.6784, 2.6958) (2.6797, 2.6790, 2.6948) (2.6799, 2.6779, 2.6995) (2.6786, 2.6768, 2.7129) (2.6791, 2.6776, 2.7853) \\ (0.0869, 0.0831, 0.0711) (0.0861, 0.0832, 0.0710) (0.0866, 0.0832, 0.0701) (0.0866, 0.0827, 0.0698) (0.0861, 0.0817, 0.0683) (0.0855, 0.0784, 0.0603) \\ 1.3 (2.9936, 3.0094, 3.0806) (2.9956, 3.0095, 3.0787) (2.9939, 3.0097, 3.0808) (2.9962, 3.0119, 3.0869) (2.9945, 3.0123, 3.1045) (2.9970, 3.0285, 3.2039) \\ (0.2110, 0.2070, 0.1921) (0.2120, 0.2069, 0.1906) (0.2110, 0.2065, 0.1896) (0.2120, 0.2068, 0.1892) (0.2105, 0.2044, 0.1867) (0.2088, 0.2002, 0.1816) \\ 1.5 (3.3332, 3.3560, 3.4441) (3.3311, 3.3553, 3.4423) (3.3347, 3.3559, 3.4451) (3.3341, 3.3561, 3.4519) (3.3356, 3.3617, 3.4735) (3.3395, 3.3838, 3.5575) \\ (0.4396, 0.4343, 0.4111) (0.4377, 0.4333, 0.4084) (0.4406, 0.4328, 0.4069) (0.4396, 0.4313, 0.4062) (0.4396, 0.4309, 0.4038) (0.4367, 0.4250, 0.3800) \\ 2.0 (3.6038, 3.6315, 3.7431) (3.6035, 3.6319, 3.7422) (3.6059, 3.6329, 3.7479) (3.6043, 3.6350, 3.7546) (3.6065, 3.6411, 3.7774) (3.6139, 3.6684, 3.8887) \\ \end{array}$							
$ \begin{array}{c} (0.2448, 0.2390, 0.2043) \\ 0.7 \\ (2.8987, 2.9072, 2.9467) \\ (2.8993, 2.9049, 2.9484) \\ (0.1650, 0.1599, 0.1392) \\ (0.8896, 2.9049, 2.9484) \\ (0.1650, 0.1599, 0.1392) \\ (0.8897, 2.9072, 2.6784, 2.6958) \\ (2.6797, 2.6784, 2.6958) \\ (2.6797, 2.6790, 2.6948) \\ (2.6797, 2.6790, 2.6948) \\ (2.8987, 2.9068, 2.9544) \\ (2.8987, 2.9068, 2.9544) \\ (2.8987, 2.9090, 2.9659) \\ (2.8987, 2.9090, 2.9659) \\ (2.8987, 2.9090, 2.9659) \\ (2.9017, 2.9190, 3.0384) \\ (0.1634, 0.1528, 0.1213) \\ (0.0869, 0.0831, 0.0711) \\ (0.0861, 0.0832, 0.0710) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.2110, 0.2070, 0.1921) \\ (0.2110, 0.2070, 0.1921) \\ (0.2120, 0.2069, 0.1906) \\ (0.2110, 0.2070, 0.4333, 0.4084) \\ (0.4396, 0.4343, 0.4111) \\ (0.4377, 0.4333, 0.4084) \\ (0.4396, 0.4343, 0.4311) \\ (0.4397, 0.4333, 0.4084) \\ (0.4396, 0.4343, 0.4311) \\ (0.4397, 0.4333, 0.4084) \\ (0.4406, 0.4328, 0.4069) \\ (0.2104, 0.2014) \\ (0.2443, 0.2345, 0.2001) \\ (0.2443, 0.2385, 0.2001) \\ (0.2897, 2.6968, 2.9544) \\ (0.2897, 2.6995) \\ (2.6799, 2.6779, 2.6995) \\ (2.6799, 2.6779, 2.6995) \\ (2.6799, 2.6779, 2.6995) \\ (2.6786, 2.6768, 2.7129) \\ (0.0866, 0.0827, 0.0698) \\ (0.0861, 0.0817, 0.0683) \\ (0.0861, 0.0817, 0.0683) \\ (0.0861, 0.0817, 0.0683) \\ (0.0855, 0.0784, 0.0603) \\ (0.29970, 3.0285, 3.2039) \\ (0.2110, 0.2070, 0.1921) \\ (0.2120, 0.2068, 0.1892) \\ (0.2110, 0.2070, 0.1921) \\ (0.2120, 0.2068, 0.1892) \\ (0.213$	τ	<u> </u>		<u>'</u>	<u>'</u>		<u> </u>
$\begin{array}{c} 0.7 & (2.8987, 2.9072, 2.9467) \\ (0.1650, 0.1599, 0.1392) \\ (0.1652, 0.1588, 0.1394) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0869, 0.0831, 0.0711) \\ (0.861, 0.0832, 0.0710) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0827, 0.0698) \\ (0.08110, 0.0861, 0.0817, 0.0683) \\ (0.08110, 0.0817, 0.0683) \\ (0.08110, 0.0817, 0.0683) \\ (0.08110, 0.0817, 0.0683) \\ (0.08110, 0.0817, 0.0683) \\ (0.08110, 0.0817, 0.0683) \\ (0.081110, 0.0817, 0.0683) \\ (0$	0.5	(3.0561, 3.0710, 3.1077)	(3.0579, 3.0732, 3.1065)	(3.0582, 3.0751, 3.1071)	(3.0560, 3.0732, 3.1117)	(3.0578, 3.0806, 3.1220)	(3.0601, 3.0926, 3.2109)
$ \begin{array}{c} (0.1650, 0.1599, 0.1392) \\ 0.8 \\ (2.6805, 2.6778, 2.6949) \\ (0.0869, 0.0831, 0.0711) \\ 0.8 \\ (2.6950, 2.6949) \\ (0.0861, 0.0832, 0.0710) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0827, 0.0698) \\ (0.2110, 0.2070, 0.1921) \\ (0.2110, 0.2070, 0.1921) \\ (0.2120, 0.2069, 0.1906) \\ (0.213332, 3.3560, 3.4441) \\ (0.33311, 3.3553, 3.4423) \\ (0.4396, 0.4343, 0.4111) \\ (0.4377, 0.4333, 0.4084) \\ (0.4406, 0.4328, 0.4069) \\ (0.2106, 0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4052) \\ (0.4396, 0.4343, 0.4111) \\ (0.4377, 0.4333, 0.4084) \\ (0.4406, 0.4328, 0.4069) \\ (0.2010, 0.2063, 0.3747) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4052) \\ (0.4396, 0.4396, 0.4309, 0.4038) \\ (0.4406, 0.4328, 0.4069) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4052) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, $		(0.2448, 0.2390, 0.2043)	(0.2458, 0.2399, 0.2031)	(0.2458, 0.2404, 0.2014)	(0.2443, 0.2385, 0.2001)	(0.2446, 0.2395, 0.1943)	(0.2424, 0.2319, 0.1845)
$\begin{array}{c} 0.8 & (2.6805, 2.6778, 2.6949) \\ & (0.0869, 0.0831, 0.0711) \\ & (0.0861, 0.0832, 0.0710) \\ & (0.0866, 0.0832, 0.0701) \\ & (0.0866, 0.0832, 0.0701) \\ & (0.0866, 0.0832, 0.0701) \\ & (0.0866, 0.0832, 0.0701) \\ & (0.0866, 0.0832, 0.0701) \\ & (0.0866, 0.0827, 0.0698) \\ & (0.0866, 0.0827, 0.0698) \\ & (0.0861, 0.0817, 0.0683) \\ & (0.0861, 0.0817, 0.0683) \\ & (0.0855, 0.0784, 0.0603) \\ & (0.29970, 3.0285, 3.2039) \\ & (0.2110, 0.2070, 0.1921) \\ & (0.2120, 0.2069, 0.1906) \\ & (0.2110, 0.2065, 0.1896) \\ & (0.2110, 0.2068, 0.1892) \\ & (0.2130, 0.2068, 0.1892) \\ & (0.2130, 0.2068, 0.3441) \\ & (0.3331, 3.3553, 3.4423) \\ & (0.4396, 0.4343, 0.4111) \\ & (0.4377, 0.4333, 0.4084) \\ & (0.4406, 0.4328, 0.4069) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4309, 0.4038) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4313, 0.4062) \\ & (0.4396, 0.4396, 0.4313, 0.4084) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062) \\ & (0.4496, 0.4398, 0.4313, 0.4062)$	0.7	(2.8987, 2.9072, 2.9467)	(2.8993, 2.9049, 2.9484)	(2.8976, 2.9063, 2.9511)	(2.8978, 2.9068, 2.9544)	(2.8987, 2.9090, 2.9659)	(2.9017, 2.9190, 3.0384)
$ \begin{array}{c} (0.0869, 0.0831, 0.0711) \\ (0.0861, 0.0832, 0.0710) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0827, 0.0698) \\ (0.0866, 0.0827, 0.0698) \\ (0.0861, 0.0817, 0.0683) \\ (0.0861, 0.0817, 0.0683) \\ (0.0855, 0.0784, 0.0603) \\ (0.29970, 3.0285, 3.2039) \\ (0.2110, 0.2070, 0.1921) \\ (0.2120, 0.2069, 0.1906) \\ (0.2110, 0.2065, 0.1896) \\ (0.2110, 0.2068, 0.1892) \\ (0.2120, 0.2068, 0.1892) \\ (0.2105, 0.2044, 0.1867) \\ (0.2088, 0.2002, 0.1816) \\ (0.2088, 0.2$		(0.1650, 0.1599, 0.1392)	(0.1652, 0.1588, 0.1394)	(0.1644, 0.1590, 0.1389)	(0.1643, 0.1586, 0.1376)	(0.1643, 0.1577, 0.1339)	(0.1634, 0.1528, 0.1213)
$ \begin{array}{c} (0.0869, 0.0831, 0.0711) \\ (0.0861, 0.0832, 0.0710) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0832, 0.0701) \\ (0.0866, 0.0827, 0.0698) \\ (0.0866, 0.0827, 0.0698) \\ (0.0861, 0.0817, 0.0683) \\ (0.0861, 0.0817, 0.0683) \\ (0.0855, 0.0784, 0.0603) \\ (0.29970, 3.0285, 3.2039) \\ (0.2110, 0.2070, 0.1921) \\ (0.2120, 0.2069, 0.1906) \\ (0.2110, 0.2065, 0.1896) \\ (0.2110, 0.2068, 0.1892) \\ (0.2120, 0.2068, 0.1892) \\ (0.2105, 0.2044, 0.1867) \\ (0.2088, 0.2002, 0.1816) \\ (0.3332, 3.3560, 3.4441) \\ (0.4396, 0.4343, 0.4111) \\ (0.4377, 0.4333, 0.4084) \\ (0.4406, 0.4328, 0.4069) \\ (0.4406, 0.4328, 0.4069) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.402) \\ (0.4396, 0.4309, 0.4309, 0.4038) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4313, 0.4062) \\ (0.4396, 0.4396, 0.4309, 0.4038) \\ (0.4396, 0.4396, 0.4396, 0.4398, 0.4089) \\ (0.4396, 0.4396, 0.4396, 0.4396, 0.4398, 0.4089) \\ (0.4496, 0.4396, 0.4396, 0.4396, 0.4398, 0.4089) \\ (0.4496, 0.4396, 0.4396, 0.4396, 0.4398, 0.4089) \\ (0.4496, 0.4396, 0.4396, 0.4396, 0.4396, 0.4398, 0.4089) \\ (0.4496, 0.4396, 0.4396, 0.4396, 0.4396, 0.4398, 0.4398, 0.4398, 0.4398) \\ (0.4496, 0.4396, 0.4396, 0.4398, 0.4$	0.8	(2.6805, 2.6778, 2.6949)	(2.6777, 2.6784, 2.6958)	(2.6797, 2.6790, 2.6948)	(2.6799, 2.6779, 2.6995)	(2.6786, 2.6768, 2.7129)	(2.6791, 2.6776, 2.7853)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			(0.0001.0.0000.0.0710)	(0.0866, 0.0832, 0.0701)	(0.0866, 0.0827, 0.0698)		
		(0.0869, 0.0831, 0.0711)	(0.0801, 0.0832, 0.0710)	(0.0000, 0.0002, 0.0101)			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.3					(2.9945, 3.0123, 3.1045)	(2.9970, 3.0285, 3.2039)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1.3	(2.9936, 3.0094, 3.0806)	(2.9956, 3.0095, 3.0787)	(2.9939, 3.0097, 3.0808)	(2.9962, 3.0119, 3.0869)		
2.0 (3.6038, 3.6315, 3.7431) (3.6035, 3.6319, 3.7422) (3.6059, 3.6329, 3.7479) (3.6043, 3.6350, 3.7546) (3.6065, 3.6411, 3.7774) (3.6139, 3.6684, 3.8887)		(2.9936, 3.0094, 3.0806) (0.2110, 0.2070, 0.1921)	(2.9956, 3.0095, 3.0787) (0.2120, 0.2069, 0.1906)	(2.9939, 3.0097, 3.0808) (0.2110, 0.2065, 0.1896)	(2.9962, 3.0119, 3.0869) (0.2120, 0.2068, 0.1892)	(0.2105, 0.2044, 0.1867)	(0.2088, 0.2002, 0.1816)
		(2.9936, 3.0094, 3.0806) (0.2110, 0.2070, 0.1921) (3.3332, 3.3560, 3.4441)	(2.9956, 3.0095, 3.0787) (0.2120, 0.2069, 0.1906) (3.3311, 3.3553, 3.4423)	(2.9939, 3.0097, 3.0808) (0.2110, 0.2065, 0.1896) (3.3347, 3.3559, 3.4451)	(2.9962, 3.0119, 3.0869) (0.2120, 0.2068, 0.1892) (3.3341, 3.3561, 3.4519)	(0.2105, 0.2044, 0.1867) (3.3356, 3.3617, 3.4735)	(0.2088, 0.2002, 0.1816) (3.3395, 3.3838, 3.5575)
(0.0100, 0.0112, 0.1024) (0.0110, 0.0111, 0.1100) (0.0204, 0.0100, 0.1101) (0.0110, 0.0101, 0.1140) (0.0120, 0.0000, 0.1004) (0.0100, 0.0111, 0.1100)	1.5	(2.9936, 3.0094, 3.0806) (0.2110, 0.2070, 0.1921) (3.3332, 3.3560, 3.4441) (0.4396, 0.4343, 0.4111)	$ \begin{array}{c} (2.9956, 3.0095, 3.0787) \\ (0.2120, 0.2069, 0.1906) \\ (3.3311, 3.3553, 3.4423) \\ (0.4377, 0.4333, 0.4084) \end{array} $	(2.9939, 3.0097, 3.0808) (0.2110, 0.2065, 0.1896) (3.3347, 3.3559, 3.4451) (0.4406, 0.4328, 0.4069)	(2.9962, 3.0119, 3.0869) (0.2120, 0.2068, 0.1892) (3.3341, 3.3561, 3.4519) (0.4396, 0.4313, 0.4062)	(0.2105, 0.2044, 0.1867) (3.3356, 3.3617, 3.4735) (0.4396, 0.4309, 0.4038)	(0.2088, 0.2002, 0.1816) (3.3395, 3.3838, 3.5575) (0.4367, 0.4250, 0.3800)
	1.5	(2.9936, 3.0094, 3.0806) (0.2110, 0.2070, 0.1921) (3.3332, 3.3560, 3.4441) (0.4396, 0.4343, 0.4111) (3.6038, 3.6315, 3.7431)	(2.9956, 3.0095, 3.0787) (0.2120, 0.2069, 0.1906) (3.3311, 3.3553, 3.4423) (0.4377, 0.4333, 0.4084) (3.6035, 3.6319, 3.7422)	(2.9939, 3.0097, 3.0808) (0.2110, 0.2065, 0.1896) (3.3347, 3.3559, 3.4451) (0.4406, 0.4328, 0.4069) (3.6059, 3.6329, 3.7479)	(2.9962, 3.0119, 3.0869) (0.2120, 0.2068, 0.1892) (3.3341, 3.3561, 3.4519) (0.4396, 0.4313, 0.4062) (3.6043, 3.6350, 3.7546)	(0.2105, 0.2044, 0.1867) (3.3356, 3.3617, 3.4735) (0.4396, 0.4309, 0.4038) (3.6065, 3.6411, 3.7774)	(0.2088, 0.2002, 0.1816) (3.3395, 3.3838, 3.5575) (0.4367, 0.4250, 0.3800) (3.6139, 3.6684, 3.8887)

Table 6: Optimal values λ^* (first row of each block) and K^* (second row of each block) of two-sided EWMA- γ^2 control charts in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of η , $\theta=0.05$, τ , η , $\theta=1$, $\eta=1$.

				= 5		
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(9.50, 9.95, 12.32)	(9.50, 9.96, 12.36)	(9.51, 9.98, 12.47)	(9.51, 10.01, 12.67)	(9.54, 10.12, 13.32)	(9.65, 10.64, 17.04)
0.7	(14.07, 14.75, 18.63)	(14.08, 14.76, 18.69)	(14.08, 14.79, 18.89)	(14.09, 14.84, 19.24)	(14.13, 15.00, 20.42)	(14.29, 15.81, 27.51)
0.8	(28.07, 29.55, 39.49)	(28.07, 29.57, 39.69)	(28.08, 29.63, 40.28)	(28.11, 29.74, 41.30)	(28.18, 30.11, 44.89)	(28.53, 32.04, 69.81)
1.3	(15.06, 15.21, 16.08)	(15.06, 15.21, 16.09)	(15.06, 15.22, 16.13)	(15.06, 15.23, 16.20)	(15.07, 15.27, 16.41)	(15.11, 15.46, 17.44)
1.5	(5.93, 6.02, 6.38)	(5.93, 6.02, 6.39)	(5.93, 6.03, 6.40)	(5.94, 6.03, 6.43)	(5.94, 6.05, 6.51)	(5.96, 6.14, 6.90)
2.0	(2.55, 2.59, 2.75)	(2.55, 2.59, 2.75)	(2.56, 2.59, 2.76)	(2.56, 2.60, 2.77)	(2.56, 2.61, 2.80)	(2.57, 2.64, 2.97)
			n =	= 7		
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(6.99, 7.27, 8.60)	(6.99, 7.27, 8.62)	(7.00, 7.28, 8.68)	(7.00, 7.30, 8.78)	(7.01, 7.36, 9.13)	(7.08, 7.67, 10.98)
0.7	(10.39, 10.81, 12.96)	(10.39, 10.81, 12.99)	(10.39, 10.83, 13.10)	(10.40, 10.86, 13.27)	(10.42, 10.95, 13.87)	(10.52, 11.43, 17.26)
0.8	(20.99, 21.90, 27.22)	(20.99, 21.91, 27.32)	(21.00, 21.95, 27.61)	(21.02, 22.02, 28.10)	(21.06, 22.23, 29.80)	(21.28, 23.34, 40.69)
1.3	(11.40, 11.52, 12.16)	(11.40, 11.52, 12.17)	(11.40, 11.53, 12.20)	(11.40, 11.54, 12.25)	(11.41, 11.57, 12.40)	(11.44, 11.71, 13.16)
1.5	(4.45, 4.51, 4.79)	(4.45, 4.51, 4.79)	(4.45, 4.52, 4.80)	(4.45, 4.52, 4.82)	(4.45, 4.53, 4.88)	(4.47, 4.60, 5.18)
2.0	(1.95, 1.98, 2.10)	(1.95, 1.98, 2.11)	(1.95, 1.98, 2.11)	(1.95, 1.98, 2.12)	(1.95, 1.99, 2.15)	(1.96, 2.02, 2.28)
			n =			
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(5.13, 5.30, 6.04)	(5.13, 5.30, 6.05)	(5.13, 5.31, 6.09)	(5.14, 5.32, 6.15)	(5.14, 5.35, 6.33)	(5.19, 5.52, 7.29)
0.7	(7.63, 7.88, 9.09)	(7.63, 7.88, 9.10)	(7.63, 7.89, 9.16)	(7.63, 7.91, 9.25)	(7.65, 7.97, 9.56)	(7.71, 8.24, 11.25)
0.8	(15.58, 16.13, 19.02)	(15.58, 16.13, 19.07)	(15.58, 16.16, 19.21)	(15.59, 16.20, 19.46)	(15.62, 16.32, 20.29)	(15.75, 16.96, 25.21)
1.3	(8.57, 8.67, 9.14)	(8.57, 8.67, 9.14)	(8.57, 8.67, 9.16)	(8.57, 8.68, 9.20)	(8.58, 8.70, 9.31)	(8.60, 8.81, 9.85)
1.5	(3.33, 3.38, 3.58)	(3.33, 3.38, 3.59)	(3.33, 3.38, 3.60)	(3.33, 3.39, 3.61)	(3.33, 3.40, 3.65)	(3.35, 3.45, 3.87)
2.0	(1.52, 1.54, 1.63)	(1.52, 1.54, 1.63)	(1.52, 1.54, 1.64)	(1.52, 1.54, 1.64)	(1.52, 1.55, 1.66)	(1.53, 1.57, 1.76)
			n =	-		
τ	$\eta = 0$	$\eta = 0.1$	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.5$	$\eta = 1$
0.5	(3.62, 3.74, 4.17)	(3.62, 3.74, 4.17)	(3.62, 3.74, 4.19)	(3.62, 3.75, 4.21)	(3.63, 3.77, 4.30)	(3.66, 3.89, 4.79)
0.7	(5.42, 5.56, 6.23)	(5.42, 5.57, 6.24)	(5.42, 5.57, 6.26)	(5.42, 5.58, 6.31)	(5.43, 5.61, 6.47)	(5.47, 5.77, 7.30)
0.8	(11.17, 11.49, 13.02)	(11.17, 11.49, 13.04)	(11.17, 11.51, 13.12)	(11.18, 11.53, 13.24)	(11.19, 11.60, 13.64)	(11.27, 11.95, 15.85)
1.3	(6.25, 6.32, 6.65)	(6.25, 6.32, 6.66)	(6.25, 6.33, 6.67)	(6.25, 6.33, 6.70)	(6.25, 6.35, 6.77)	(6.27, 6.43, 7.14)
1.5	(2.44, 2.47, 2.62)	(2.44, 2.47, 2.62)	(2.44, 2.47, 2.63)	(2.44, 2.48, 2.64)	(2.44, 2.48, 2.67)	(2.45, 2.52, 2.82)
2.0	(1.21, 1.23, 1.28)	(1.21, 1.23, 1.28)	(1.21, 1.23, 1.28)	(1.21, 1.23, 1.29)	(1.21, 1.23, 1.30)	(1.22, 1.24, 1.36)

Table 7: ARL values of two-sided EWMA- γ^2 control charts in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of η , $\theta=0.05$, τ , n, B=1, m=1.

	n = 5							
au	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$		
0.5	(9.30, 9.84, 12.73)	(9.34, 9.87, 12.71)	(9.39, 9.90, 12.68)	(9.43, 9.94, 12.66)	(9.47, 9.97, 12.64)	(9.51, 10.00, 12.62)		
0.7	(13.60, 14.40, 19.17)	(13.70, 14.48, 19.16)	(13.80, 14.57, 19.15)	(13.90, 14.65, 19.15)	(13.99, 14.74, 19.15)	(14.09, 14.83, 19.16)		
0.8	(26.81, 28.52, 41.04)	(27.06, 28.75, 41.03)	(27.32, 28.99, 41.02)	(27.58, 29.23, 41.02)	(27.84, 29.47, 41.04)	(28.10, 29.72, 41.06)		
1.3	(13.85, 14.04, 15.05)	(14.09, 14.27, 15.27)	(14.33, 14.51, 15.50)	(14.57, 14.75, 15.73)	(14.82, 14.99, 15.95)	(15.06, 15.23, 16.18)		
1.5	(5.39, 5.49, 5.88)	(5.50, 5.60, 5.99)	(5.61, 5.70, 6.10)	(5.72, 5.81, 6.20)	(5.83, 5.92, 6.31)	(5.94, 6.03, 6.42)		
2.0	(2.30, 2.34, 2.51)	(2.35, 2.39, 2.56)	(2.40, 2.44, 2.61)	(2.45, 2.49, 2.66)	(2.50, 2.54, 2.71)	(2.56, 2.60, 2.77)		
			n =	= 7				
au	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$		
0.5	(6.84, 7.16, 8.77)	(6.87, 7.19, 8.76)	(6.90, 7.22, 8.76)	(6.94, 7.24, 8.76)	(6.97, 7.27, 8.76)	(7.00, 7.30, 8.76)		
0.7	(10.03, 10.52, 13.11)	(10.11, 10.58, 13.13)	(10.18, 10.65, 13.15)	(10.25, 10.72, 13.18)	(10.33, 10.78, 13.20)	(10.40, 10.85, 13.23)		
0.8	(20.01, 21.06, 27.55)	(20.21, 21.24, 27.63)	(20.41, 21.43, 27.71)	(20.61, 21.62, 27.80)	(20.81, 21.81, 27.89)	(21.01, 22.00, 27.98)		
1.3	(10.47, 10.62, 11.36)	(10.65, 10.80, 11.53)	(10.84, 10.98, 11.70)	(11.02, 11.16, 11.88)	(11.21, 11.35, 12.06)	(11.40, 11.54, 12.23)		
1.5	(4.04, 4.11, 4.41)	(4.12, 4.19, 4.49)	(4.20, 4.27, 4.57)	(4.28, 4.36, 4.65)	(4.36, 4.44, 4.73)	(4.45, 4.52, 4.82)		
2.0	(1.77, 1.80, 1.94)	(1.81, 1.84, 1.97)	(1.84, 1.87, 2.01)	(1.88, 1.91, 2.04)	(1.91, 1.95, 2.08)	(1.95, 1.98, 2.12)		
			n =					
τ	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$		
0.5	(5.02, 5.22, 6.11)	(5.04, 5.24, 6.11)	(5.07, 5.25, 6.11)	(5.09, 5.27, 6.12)	(5.11, 5.29, 6.13)	(5.13, 5.31, 6.13)		
0.7	(7.36, 7.65, 9.08)	(7.41, 7.70, 9.11)	(7.47, 7.75, 9.14)	(7.52, 7.80, 9.17)	(7.58, 7.85, 9.20)	(7.63, 7.91, 9.23)		
0.8	(14.83, 15.46, 18.90)	(14.98, 15.60, 19.00)	(15.13, 15.75, 19.09)	(15.28, 15.89, 19.19)	(15.44, 16.04, 19.29)	(15.59, 16.19, 19.40)		
1.3	(7.86, 7.98, 8.51)	(8.00, 8.12, 8.65)	(8.14, 8.26, 8.78)	(8.28, 8.40, 8.92)	(8.43, 8.54, 9.05)	(8.57, 8.68, 9.19)		
1.5	(3.03, 3.08, 3.31)	(3.09, 3.14, 3.37)	(3.15, 3.20, 3.43)	(3.21, 3.26, 3.49)	(3.27, 3.32, 3.55)	(3.33, 3.38, 3.61)		
2.0	(1.40, 1.42, 1.52)	(1.42, 1.45, 1.54)	(1.45, 1.47, 1.57)	(1.47, 1.49, 1.59)	(1.49, 1.52, 1.62)	(1.52, 1.54, 1.64)		
			n =	-				
$_{-}\tau$	$\theta = 0$	$\theta = 0.01$	$\theta = 0.02$	$\theta = 0.03$	$\theta = 0.04$	$\theta = 0.05$		
0.5	(3.52, 3.66, 4.17)	(3.54, 3.68, 4.18)	(3.56, 3.70, 4.19)	(3.58, 3.71, 4.19)	(3.60, 3.73, 4.20)	(3.62, 3.75, 4.21)		
0.7	(5.22, 5.39, 6.17)	(5.26, 5.43, 6.19)	(5.30, 5.47, 6.22)	(5.34, 5.50, 6.25)	(5.38, 5.54, 6.27)	(5.42, 5.58, 6.30)		
0.8	(10.62, 10.98, 12.77)	(10.73, 11.09, 12.86)	(10.84, 11.20, 12.94)	(10.95, 11.30, 13.03)	(11.06, 11.41, 13.12)	(11.18, 11.52, 13.21)		
1.3	(5.73, 5.82, 6.19)	(5.83, 5.92, 6.29)	(5.94, 6.02, 6.39)	(6.04, 6.12, 6.49)	(6.14, 6.23, 6.59)	(6.25, 6.33, 6.69)		
1.5	(2.22, 2.26, 2.42)	(2.27, 2.30, 2.46)	(2.31, 2.35, 2.51)	(2.35, 2.39, 2.55)	(2.39, 2.43, 2.59)	(2.44, 2.48, 2.63)		
2.0	(1.15, 1.16, 1.22)	(1.16, 1.17, 1.23)	(1.17, 1.19, 1.24)	(1.19, 1.20, 1.26)	(1.20, 1.21, 1.27)	(1.21, 1.23, 1.29)		

Table 8: ARL values of two-sided EWMA- γ^2 control charts in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of θ , $\eta=0.28$, τ , n, B=1, m=1.

			n = 5		
au	B=1	B=2	B=3	B=4	B=5
0.5	(9.51, 10.00, 12.62)	(9.40, 9.88, 12.43)	(9.36, 9.84, 12.40)	(9.34, 9.83, 12.39)	(9.33, 9.82, 12.39)
0.7	(14.09, 14.83, 19.16)	(13.83, 14.55, 18.73)	(13.75, 14.47, 18.65)	(13.71, 14.43, 18.62)	(13.68, 14.40, 18.60)
0.8	(28.10, 29.72, 41.06)	(27.43, 28.98, 39.77)	(27.20, 28.75, 39.52)	(27.10, 28.64, 39.43)	(27.03, 28.58, 39.38)
1.3	(15.06, 15.23, 16.18)	(14.45, 14.61, 15.53)	(14.25, 14.41, 15.33)	(14.15, 14.31, 15.23)	(14.09, 14.25, 15.17)
1.5	(5.94, 6.03, 6.42)	(5.66, 5.75, 6.12)	(5.57, 5.66, 6.02)	(5.53, 5.61, 5.98)	(5.50, 5.59, 5.95)
2.0	(2.56, 2.60, 2.77)	(2.43, 2.46, 2.62)	(2.38, 2.42, 2.58)	(2.36, 2.40, 2.56)	(2.35, 2.39, 2.54)
			n = 7		
τ	B=1	B=2	B=3	B=4	B=5
0.5	(7.00, 7.30, 8.76)	(6.91, 7.21, 8.63)	(6.89, 7.18, 8.61)	(6.87, 7.17, 8.60)	(6.87, 7.16, 8.60)
0.7	(10.40, 10.85, 13.23)	(10.21, 10.65, 12.95)	(10.14, 10.58, 12.88)	(10.11, 10.55, 12.86)	(10.10, 10.54, 12.85)
0.8	(21.01, 22.00, 27.98)	(20.49, 21.45, 27.15)	(20.33, 21.27, 26.96)	(20.24, 21.19, 26.89)	(20.19, 21.14, 26.84)
1.3	(11.40, 11.54, 12.23)	(10.93, 11.06, 11.74)	(10.77, 10.91, 11.58)	(10.69, 10.83, 11.50)	(10.65, 10.78, 11.46)
1.5	(4.45, 4.52, 4.82)	(4.24, 4.31, 4.59)	(4.17, 4.24, 4.52)	(4.14, 4.21, 4.48)	(4.12, 4.19, 4.46)
2.0	(1.95, 1.98, 2.12)	(1.86, 1.89, 2.02)	(1.83, 1.86, 1.98)	(1.81, 1.84, 1.97)	(1.81, 1.84, 1.96)
			n = 10		
τ	B=1	B=2	B=3	B=4	B=5
0.5	(5.13, 5.31, 6.13)	(5.07, 5.25, 6.05)	(5.05, 5.23, 6.03)	(5.04, 5.22, 6.02)	(5.04, 5.22, 6.02)
0.7	(7.63, 7.91, 9.23)	(7.49, 7.76, 9.04)	(7.44, 7.71, 8.99)	(7.42, 7.69, 8.97)	(7.41, 7.67, 8.96)
0.8	(15.59, 16.19, 19.40)	(15.20, 15.77, 18.85)	(15.07, 15.64, 18.70)	(15.00, 15.58, 18.64)	(14.97, 15.54, 18.61)
1.3	(8.57, 8.68, 9.19)	(8.21, 8.32, 8.81)	(8.09, 8.20, 8.69)	(8.03, 8.14, 8.63)	(8.00, 8.11, 8.59)
1.5	(3.33, 3.38, 3.61)	(3.18, 3.23, 3.44)	(3.13, 3.18, 3.39)	(3.10, 3.15, 3.36)	(3.09, 3.14, 3.35)
2.0	(1.52, 1.54, 1.64)	(1.46, 1.48, 1.57)	(1.44, 1.46, 1.55)	(1.43, 1.45, 1.54)	(1.42, 1.44, 1.53)
			n = 15		
τ	B=1	B=2	B=3	B=4	B=5
0.5	(3.62, 3.75, 4.21)	(3.57, 3.70, 4.16)	(3.55, 3.68, 4.15)	(3.55, 3.67, 4.14)	(3.54, 3.67, 4.14)
0.7	(5.42, 5.58, 6.30)	(5.32, 5.47, 6.17)	(5.29, 5.44, 6.14)	(5.27, 5.42, 6.12)	(5.26, 5.41, 6.12)
0.8	(11.18, 11.52, 13.21)	(10.89, 11.22, 12.84)	(10.80, 11.13, 12.74)	(10.75, 11.08, 12.69)	(10.72, 11.05, 12.67)
1.3	(6.25, 6.33, 6.69)	(5.99, 6.07, 6.41)	(5.90, 5.98, 6.32)	(5.86, 5.94, 6.28)	(5.83, 5.91, 6.25)
1.5	(2.44, 2.48, 2.63)	(2.33, 2.37, 2.52)	(2.29, 2.33, 2.48)	(2.27, 2.31, 2.46)	(2.26, 2.30, 2.45)
2.0	(1.21, 1.23, 1.29)	(1.18, 1.19, 1.25)	(1.17, 1.18, 1.23)	(1.16, 1.18, 1.23)	(1.16, 1.17, 1.22)

Table 9: ARL values of two-sided EWMA- γ^2 control charts in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of $B,\,\tau,\,n,\,\eta=0.28,\,\theta=0.01,\,m=1.$

			n = 5		
au	m = 1	m = 3	m=5	m = 7	m = 10
0.5	(9.51, 10.00, 12.62)	(9.51, 9.97, 12.42)	(9.50, 9.96, 12.38)	(9.50, 9.96, 12.36)	(9.50, 9.96, 12.35)
0.7	(14.09, 14.83, 19.16)	(14.08, 14.78, 18.80)	(14.08, 14.77, 18.73)	(14.08, 14.76, 18.70)	(14.08, 14.76, 18.68)
0.8	(28.10, 29.72, 41.06)	(28.08, 29.60, 40.00)	(28.07, 29.58, 39.80)	(28.07, 29.57, 39.71)	(28.07, 29.56, 39.64)
1.3	(15.06, 15.23, 16.18)	(15.06, 15.21, 16.11)	(15.06, 15.21, 16.10)	(15.06, 15.21, 16.09)	(15.06, 15.21, 16.09)
1.5	(5.94, 6.03, 6.42)	(5.93, 6.02, 6.40)	(5.93, 6.02, 6.39)	(5.93, 6.02, 6.39)	(5.93, 6.02, 6.39)
2.0	(2.56, 2.60, 2.77)	(2.56, 2.59, 2.75)	(2.56, 2.59, 2.75)	(2.56, 2.59, 2.75)	(2.55, 2.59, 2.75)
			n = 7		
τ	m = 1	m = 3	m = 5	m = 7	m = 10
0.5	(7.00, 7.30, 8.76)	(6.99, 7.28, 8.65)	(6.99, 7.27, 8.63)	(6.99, 7.27, 8.62)	(6.99, 7.27, 8.61)
0.7	(10.40, 10.85, 13.23)	(10.39, 10.82, 13.05)	(10.39, 10.81, 13.01)	(10.39, 10.81, 12.99)	(10.39, 10.81, 12.98)
0.8	(21.01, 22.00, 27.98)	(21.00, 21.93, 27.47)	(20.99, 21.92, 27.37)	(20.99, 21.91, 27.33)	(20.99, 21.91, 27.30)
1.3	(11.40, 11.54, 12.23)	(11.40, 11.53, 12.18)	(11.40, 11.52, 12.17)	(11.40, 11.52, 12.17)	(11.40, 11.52, 12.17)
1.5	(4.45, 4.52, 4.82)	(4.45, 4.51, 4.80)	(4.45, 4.51, 4.79)	(4.45, 4.51, 4.79)	(4.45, 4.51, 4.79)
2.0	(1.95, 1.98, 2.12)	(1.95, 1.98, 2.11)	(1.95, 1.98, 2.11)	(1.95, 1.98, 2.11)	(1.95, 1.98, 2.11)
			n = 10		
τ	m = 1	m = 3	m = 5	m = 7	m = 10
0.5	(5.13, 5.31, 6.13)	(5.13, 5.30, 6.07)	(5.13, 5.30, 6.06)	(5.13, 5.30, 6.06)	(5.13, 5.30, 6.05)
0.7	(7.63, 7.91, 9.23)	(7.63, 7.89, 9.13)	(7.63, 7.88, 9.11)	(7.63, 7.88, 9.11)	(7.63, 7.88, 9.10)
0.8	(15.59, 16.19, 19.40)	(15.58, 16.15, 19.14)	(15.58, 16.14, 19.09)	(15.58, 16.13, 19.07)	(15.58, 16.13, 19.06)
1.3	(8.57, 8.68, 9.19)	(8.57, 8.67, 9.15)	(8.57, 8.67, 9.15)	(8.57, 8.67, 9.14)	(8.57, 8.67, 9.14)
1.5	(3.33, 3.38, 3.61)	(3.33, 3.38, 3.59)	(3.33, 3.38, 3.59)	(3.33, 3.38, 3.59)	(3.33, 3.38, 3.59)
2.0	(1.52, 1.54, 1.64)	(1.52, 1.54, 1.64)	(1.52, 1.54, 1.63)	(1.52, 1.54, 1.63)	(1.52, 1.54, 1.63)
			n = 15		
τ	m = 1	m = 3	m=5	m = 7	m = 10
0.5	(3.62, 3.75, 4.21)	(3.62, 3.74, 4.18)	(3.62, 3.74, 4.18)	(3.62, 3.74, 4.17)	(3.62, 3.74, 4.17)
0.7	(5.42, 5.58, 6.30)	(5.42, 5.57, 6.25)	(5.42, 5.57, 6.24)	(5.42, 5.57, 6.24)	(5.42, 5.57, 6.23)
0.8	(11.18, 11.52, 13.21)	(11.17, 11.50, 13.08)	(11.17, 11.49, 13.06)	(11.17, 11.49, 13.05)	(11.17, 11.49, 13.04)
1.3	(6.25, 6.33, 6.69)	(6.25, 6.33, 6.67)	(6.25, 6.33, 6.66)	(6.25, 6.32, 6.66)	(6.25, 6.32, 6.66)
1.5	(2.44, 2.48, 2.63)	(2.44, 2.47, 2.62)	(2.44, 2.47, 2.62)	(2.44, 2.47, 2.62)	(2.44, 2.47, 2.62)
2.0	(1.21, 1.23, 1.29)	(1.21, 1.23, 1.28)	(1.21, 1.23, 1.28)	(1.21, 1.23, 1.28)	(1.21, 1.23, 1.28)

Table 10: ARL values of two-sided EWMA- γ^2 control charts in the presence of measurement errors for $\gamma_0=0.05$ (left side), $\gamma_0=0.1$ (middle) and $\gamma_0=0.2$ (right side), for different values of $m,\,\tau,\,n,\,\eta=0.28,\,\theta=0.05,\,B=1.$

$\overline{\eta}$	θ	γ_0	n = 5	n = 7	n = 10	n = 15
0.10	0.01	0.05	(0.0501, 2.1425)	(0.0502, 2.1942)	(0.0578, 2.2619)	(0.0690, 2.3348)
			(0.0501, 2.6910)	(0.0502, 2.6473)	(0.0579, 2.6755)	(0.0720, 2.7294)
		0.10	(0.0500, 2.0801)	(0.0501, 2.1401)	(0.0552, 2.2101)	(0.0683, 2.2989)
			(0.0500, 2.7439)	(0.0509, 2.7007)	(0.0598, 2.7286)	(0.0725, 2.7632)
		0.15	(0.0500, 1.9813)	(0.0500, 2.0545)	(0.0530, 2.1307)	(0.0651, 2.2344)
			(0.0500, 2.8353)	(0.0531, 2.7996)	(0.0610, 2.8025)	(0.0732, 2.8188)
		0.20	(0.0500, 1.8526)	(0.0500, 1.9425)	(0.0502, 2.0234)	(0.0610, 2.1454)
			(0.0501, 2.9688)	(0.0556, 2.9316)	(0.0634, 2.9100)	(0.0740, 2.8951)
0.28	0.05	0.05	(0.0500, 2.1426)	(0.0501, 2.1940)	(0.0560, 2.2566)	(0.0675, 2.3311)
			(0.0501, 2.6908)	(0.0502, 2.6471)	(0.0574, 2.6714)	(0.0696, 2.7150)
		0.10	(0.0500, 2.0811)	(0.0501, 2.1409)	(0.0540, 2.2065)	(0.0656, 2.2924)
			(0.0500, 2.7430)	(0.0501, 2.6929)	(0.0588, 2.7205)	(0.0704, 2.7505)
		0.15	(0.0500, 1.9833)	(0.0500, 2.0563)	(0.0520, 2.1279)	(0.0627, 2.2281)
			(0.0500, 2.8333)	(0.0519, 2.7876)	(0.0593, 2.7887)	(0.0710, 2.8054)
		0.20	(0.0500, 1.8560)	(0.0500, 1.9455)	(0.0500, 2.0248)	(0.0595, 2.1419)
			(0.0501, 2.9650)	(0.0545, 2.9199)	(0.0615, 2.8945)	(0.0725, 2.8848)

Table 11: Optimal couples (λ^*, K^*) for downward EWMA- γ^2 (first row of each block) and optimal couples (λ^*, K^*) for upward EWMA- γ^2 (second row of each block), in the presence of measurement errors, for different values of η , θ , n, γ_0 , B=1 and m=1.

		Phase	II								
\overline{k}	X_1^*	X_2^*	X_3^*	X_4^*	X_5^*	S_i^*	\bar{X}_i^*	$\hat{\gamma}^*$	$\hat{\gamma}^{*2}$	Z_i^*	S_i^*
1	50.67	49.45	49.88	49.91	50.26	0.4571	50.0320	0.0091	0.00008	0.000108	0.000106
2	49.59	50.21	50.23	49.58	49.76	0.3240	49.8757	0.0065	0.00004	0.000108	0.000102
3	49.69	50.46	49.21	50.26	50.08	0.4969	49.9386	0.0100	0.00010	0.000108	0.000102
4	49.48	50.71	50.04	49.99	50.54	0.4898	50.1502	0.0098	0.00010	0.000108	0.000102
5	50.73	50.00	51.16	49.76	50.52	0.5624	50.4334	0.0112	0.00013	0.000109	0.000103
6	49.42	51.25	50.28	51.85	49.45	1.0830	50.4510	0.0215	0.00046	0.000126	0.000126
7	49.17	49.95	48.98	49.72	49.86	0.4307	49.5358	0.0087	0.00008	0.000124	0.000123
8	50.09	50.43	50.02	49.77	49.41	0.3800	49.9448	0.0076	0.00006	0.000121	0.000119
9	50.40	49.27	50.01	50.58	50.25	0.5100	50.1019	0.0102	0.00010	0.000120	0.000118
10	49.11	50.28	51.22	49.79	51.21	0.9145	50.3215	0.0182	0.00033	0.000130	0.000131
11	48.48	50.49	50.65	49.78	51.03	1.0047	50.0863	0.0201	0.00040	0.000144	0.000149
12	48.01	49.34	50.71	48.00	49.21	1.1244	49.0523	0.0229	0.00052	0.000163	0.000173
13	50.22	50.25	49.89	51.80	51.64	0.8886	50.7615	0.0175	0.00031	0.000170	0.000181
14	51.01	49.21	49.24	50.81	49.37	0.9035	49.9282	0.0181	0.00033	0.000178	0.000191
15	49.33	48.82	49.02	50.28	49.67	0.5734	49.4236	0.0116	0.00013	0.000176	0.000187
16	51.16	50.11	48.63	50.64	50.32	0.9481	50.1721	0.0189	0.00036	0.000185	0.000198
17	51.04	49.48	50.35	49.19	50.22	0.7336	50.0560	0.0147	0.00022	0.000186	0.000199
18	49.22	50.91	50.43	51.80	51.35	0.9919	50.7413	0.0195	0.00038	0.000196	0.000211
19	49.99	49.58	50.38	50.07	49.44	0.3815	49.8924	0.0076	0.00006	0.000189	0.000201
_20	49.26	49.01	50.17	49.55	51.07	0.8249	49.8131	0.0166	0.00028	0.000194	0.000206

Table 12: Illustrative example of Phase II dataset.

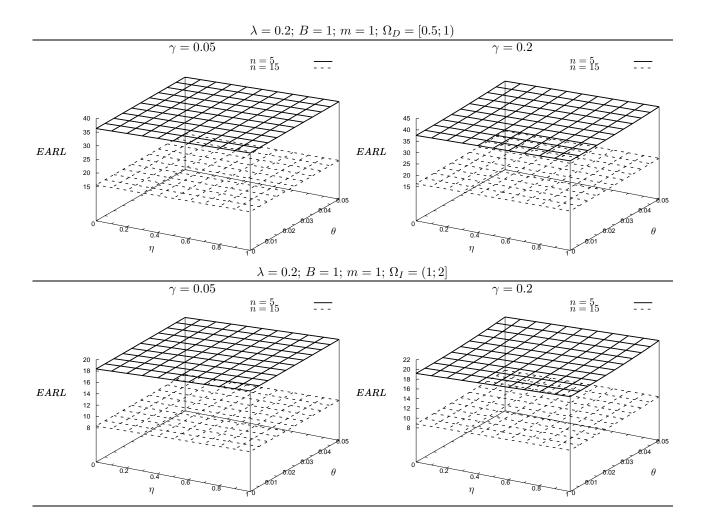


Figure 1: The effect of η and θ on the overall performance of the EWMA- γ^2 control charts in the presence of measurement errors for $\lambda=0.2,\,ARL_0=370.4,\,B=1,\,m=1,\,n\in\{5,15\},\,\gamma_0\in\{0.05,0.2\}$

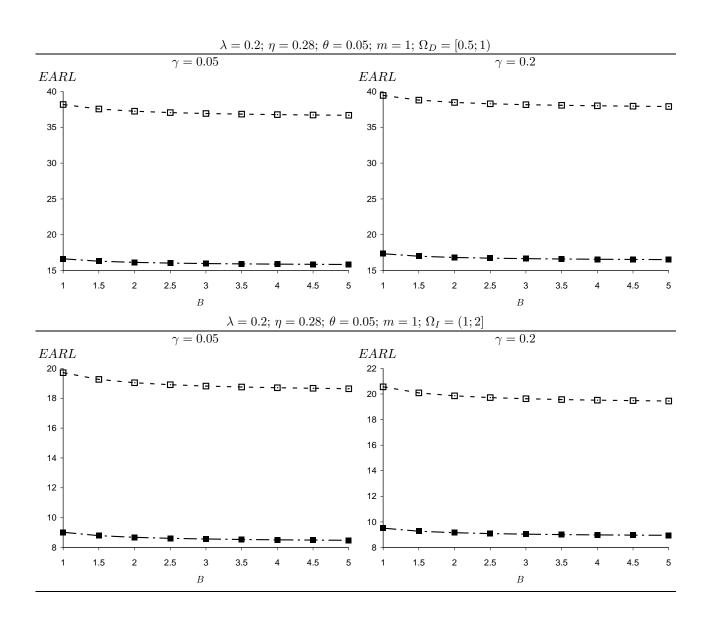


Figure 2: The effect of B on the overall performance of the EWMA- γ^2 control charts in the presence of measurement errors for n=5 (- \square -) and n=15 (- \square -), $\lambda=0.2,\ m=1,\ ARL_0=370.4,\ \eta=0.28,\ \theta=0.05,\ n\in\{1,15\},\ \gamma_0\in\{0.05,0.2\}$

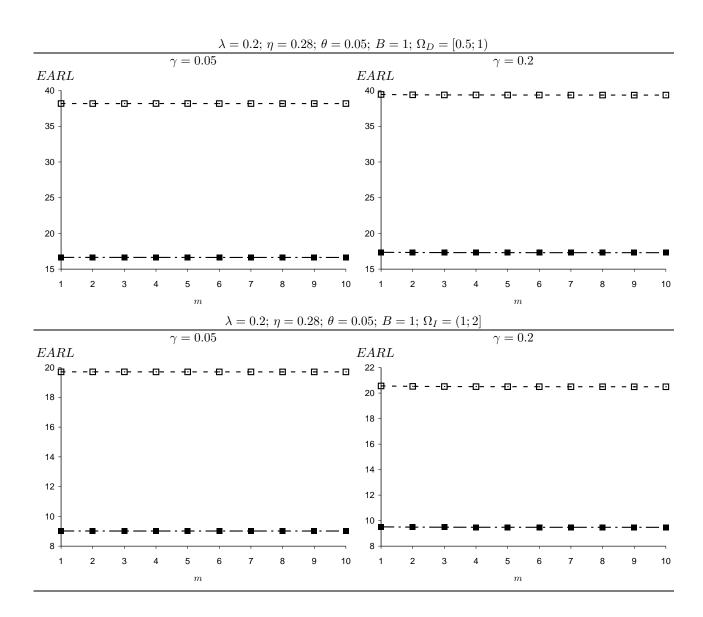


Figure 3: The effect of m on the overall performance of the EWMA- γ^2 control charts in the presence of measurement errors for n=5 (- \square -) and n=15 (- \blacksquare -), $\lambda=0.2,\ B=1,\ ARL_0=370.4,\ \eta=0.28,\ \theta=0.05,\ n\in\{1,15\},\ \gamma_0\in\{0.05,0.2\}$

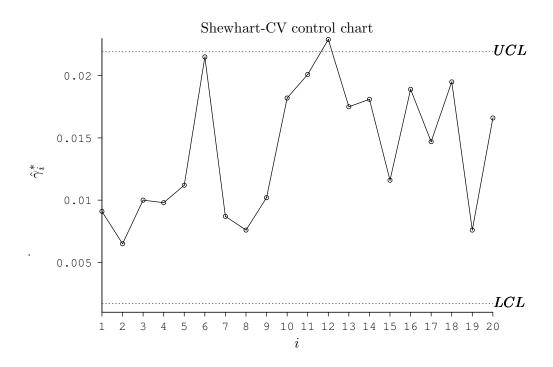


Figure 4: Shewhart-CV control chart applied to the sintering process (Phase II).

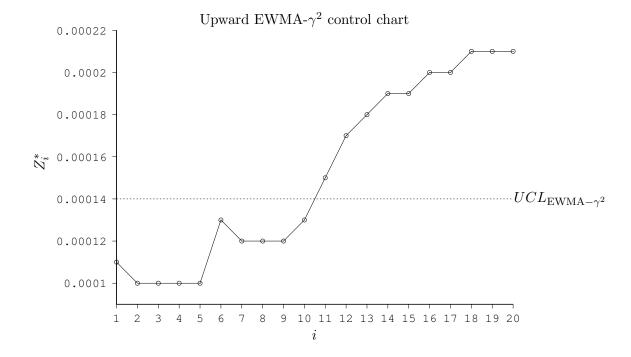


Figure 5: Upward EWMA- γ^2 control chart applied to the sintering process (Phase II).

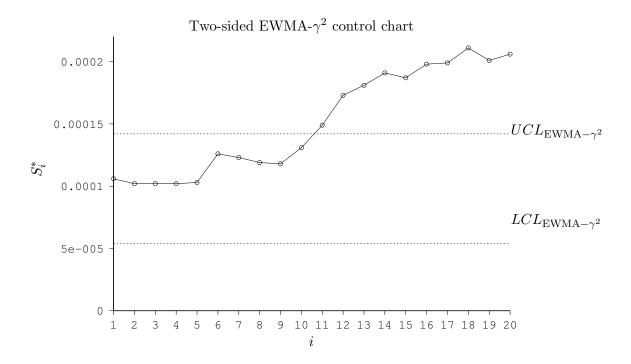


Figure 6: Two-sided EWMA- γ^2 control chart applied to the sintering process (Phase II).