

An experimental, theoretical and kinetic-modeling study of the gas-phase oxidation of ammonia

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Supplementary Material

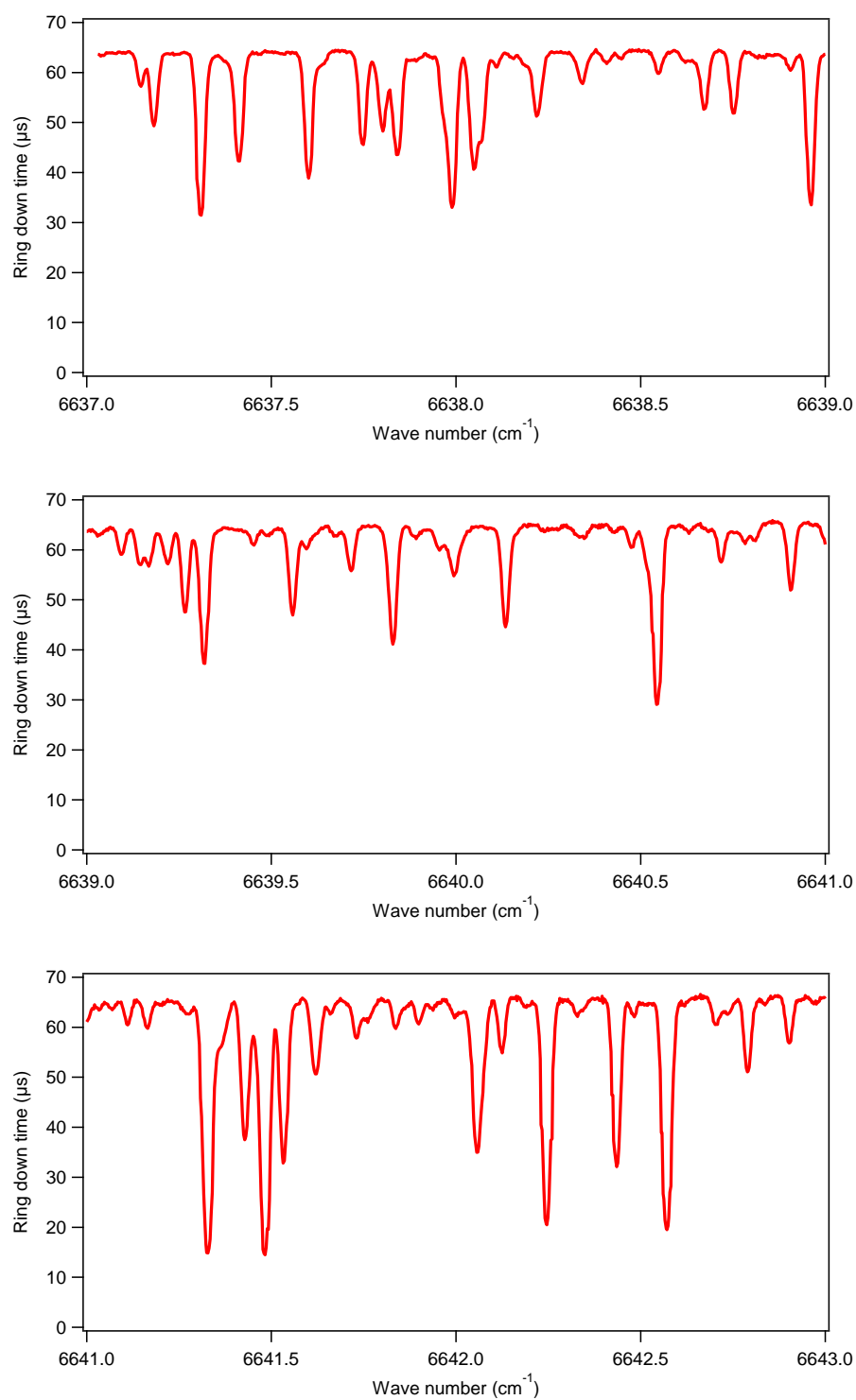
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1 Ammonia CRDS infrared spectrum



CRDS infrared spectrum recorded during the oxidation of ammonia under unreactive conditions ($\varphi = 1$, 500 K) over the range 6637-6643 cm^{-1} .

2 Validation of the kinetic mechanism

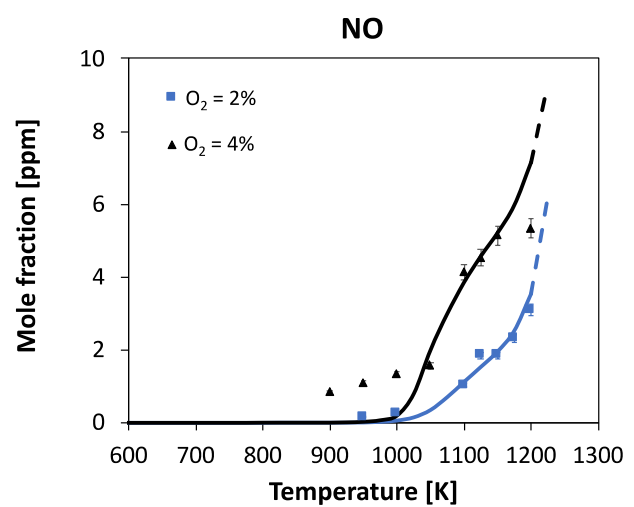
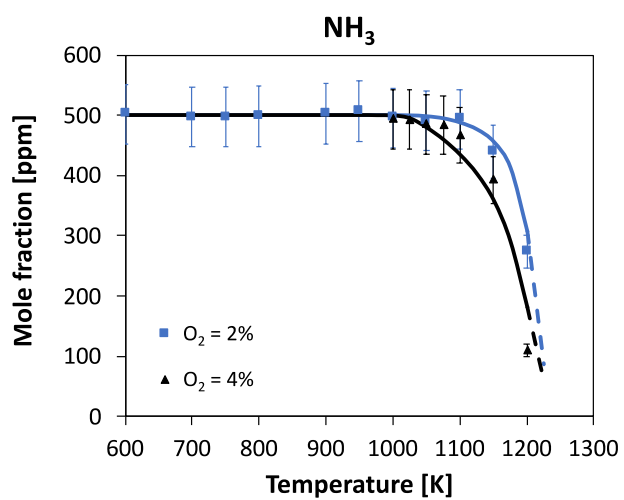
2.1 Jet Stirred Reactor

2.1.1 Present work

Type: isothermal Jet Stirred reactor

Model: Isothermal Perfectly-Stirred reactor

- 500 ppm NH_3 – 2-4% O_2
- Balance gas: He
- $P = 800$ torr
- $\tau = 1.5$ s

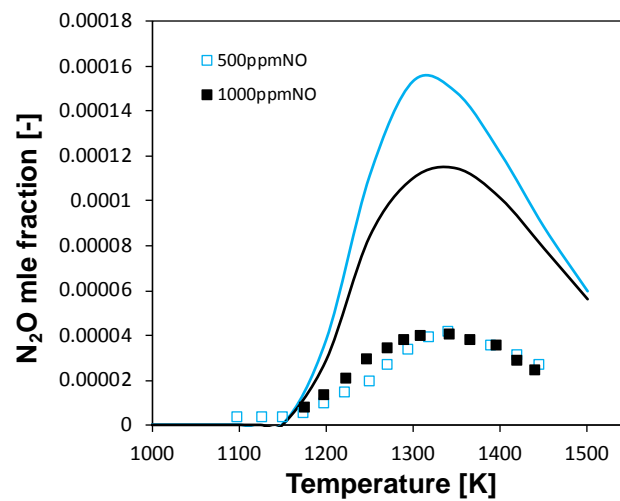
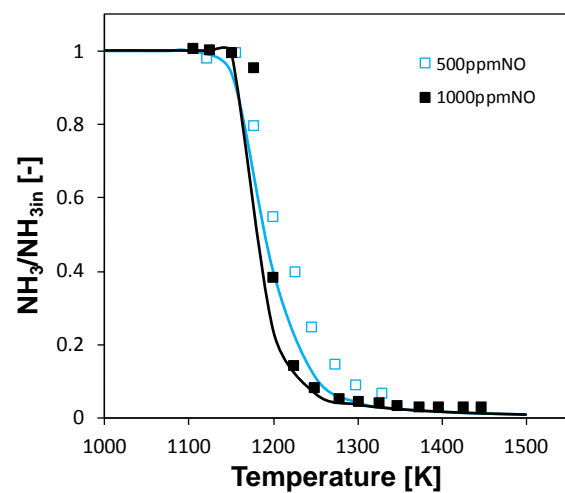
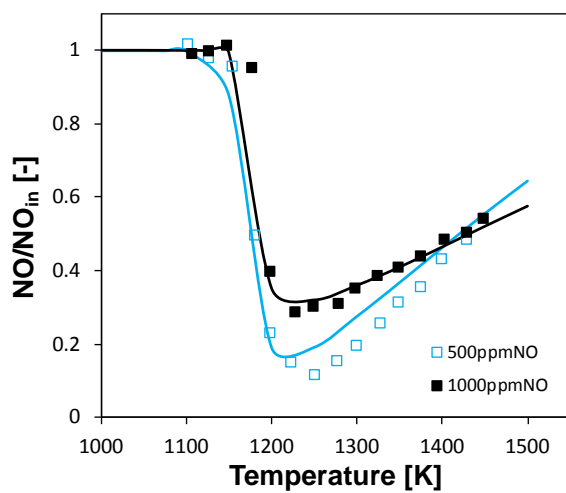


2.1.2 Dagaut et al. [1]

Type: Isothermal Jet Stirred reactor

Model: Isothermal Perfectly-Stirred reactor

- 1000 ppm NH_3 – 12500 ppm O_2 – 500-1000 ppm NO
- Balance gas: N_2
- $P = 800$ torr
- $\tau = 0.1$ s



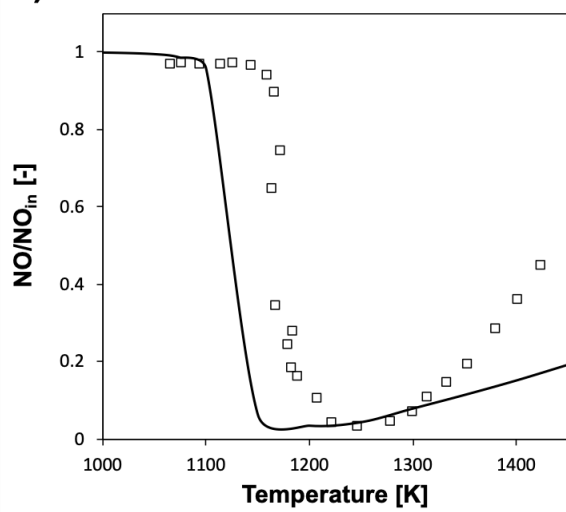
2.1.3 Rota et al. [2]

Type: isothermal Jet Stirred reactor

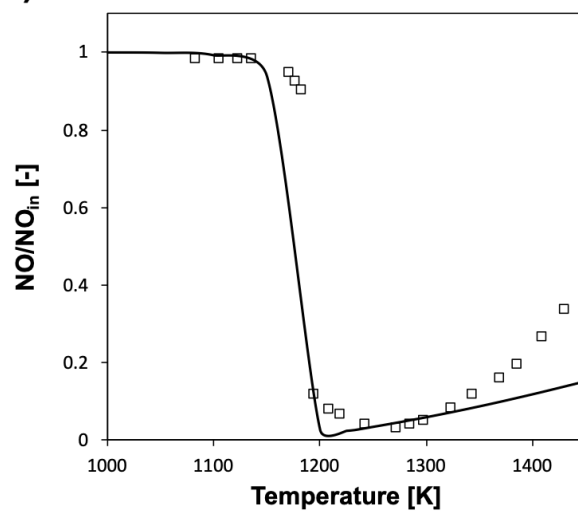
Model: Isothermal Perfectly-Stirred reactor

- Balance gas: N₂
- P = 1 atm
- $\tau = \frac{374}{T[\text{K}]} [\text{s}]$
 - a) 7200 ppm NH₃ – 3000 ppm NO – 6000 ppm O₂
 - b) 7200 ppm NH₃ – 3000 ppm NO – 2000 ppm O₂
 - c) 1920 ppm NH₃ – 800 ppm NO – 2000 ppm O₂
 - d) 1920 ppm NH₃ – 800 ppm NO – 1600 ppm O₂

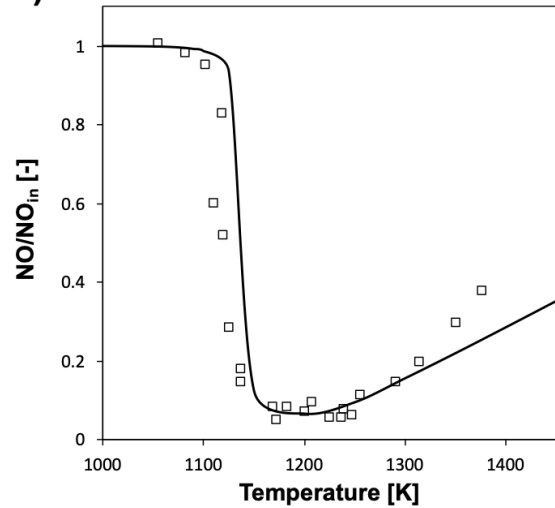
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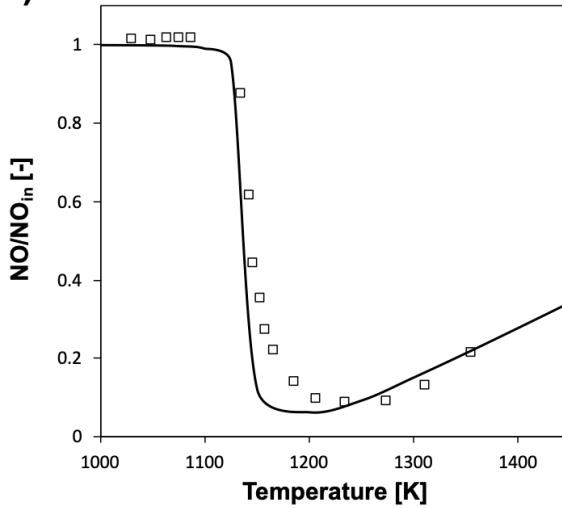
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c)



d)



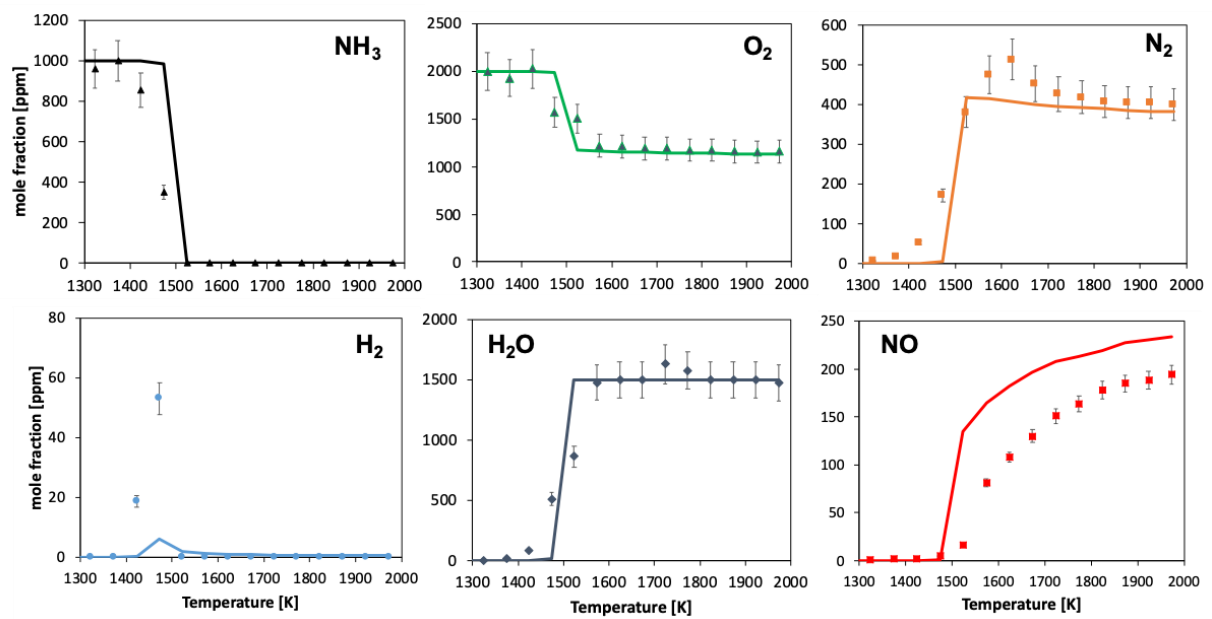
2.2 Flow reactor

2.2.1 Present work

Type: Flow reactor with assigned temperature profile

Model: Plug-flow reactor with assigned temperature profile

- 1000 ppm NH_3 – 2000 ppm O_2
- Balance gas: He
- $P = 925$ torr
- $\tau = 50$ ms (in the reactive zone)

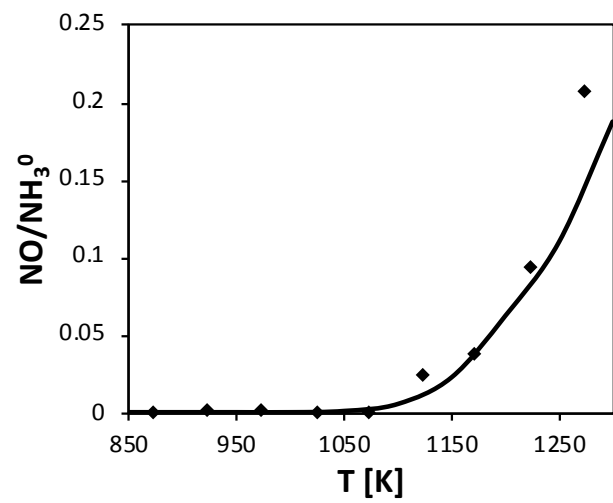
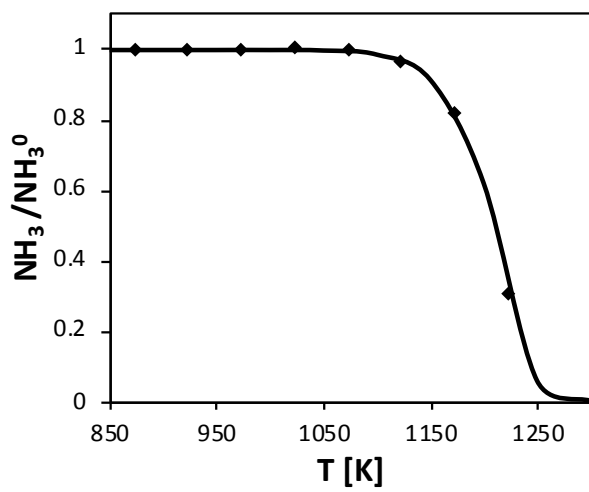


2.2.2 Wargadalam et al. [3]

Type: Isothermal flow reactor

Model: Isothermal Plug-flow reactor

- 242 ppm NH_3 – 10 % O_2
- Balance gas: N_2
- $P = 1 \text{ atm}$
- $\tau = 339/T[\text{K}] \text{ s}$



2.2.3 Song et al. [4]

Type: Flow reactor with assigned temperature profile

Model: Plug-flow reactor with assigned temperature profile

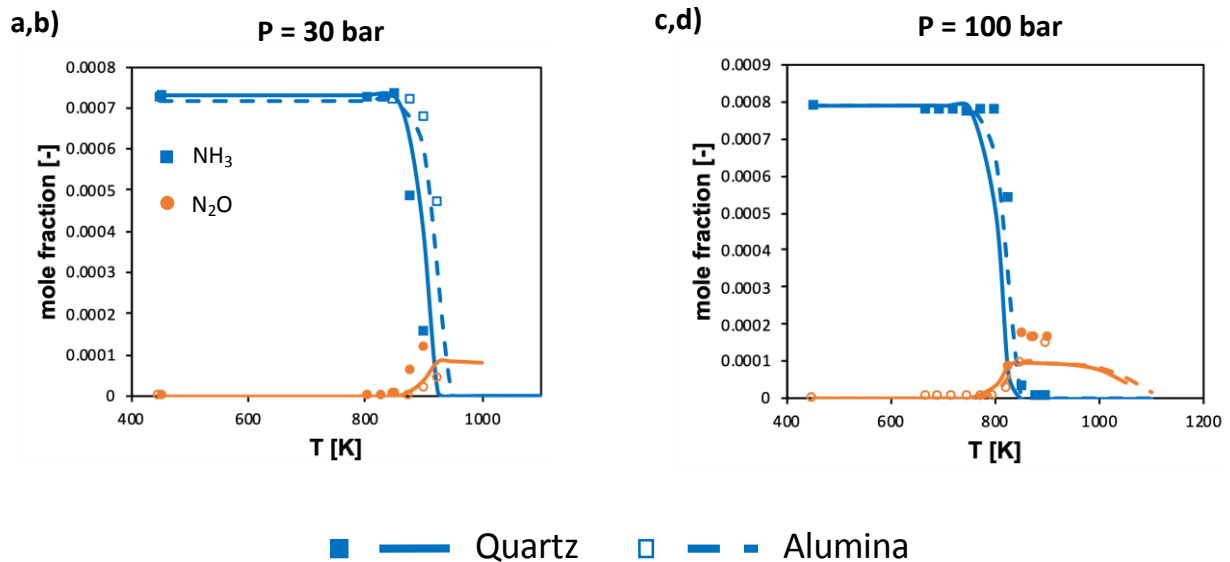
- Balance gas: He

a) $P = 30 \text{ bar} - 729 \text{ ppm NH}_3 - 3.95\% \text{ O}_2 - \tau = \frac{3100}{T[\text{K}]} \text{ [s]} \text{ (in the reactive zone) - Quartz}$

b) $P = 30 \text{ bar} - 719 \text{ ppm NH}_3 - 4.03\% \text{ O}_2 - \tau = \frac{1984}{T[\text{K}]} \text{ [s]} \text{ (in the reactive zone) - Alumina}$

c) $P = 100 \text{ bar} - 789 \text{ ppm NH}_3 - 4.07\% \text{ O}_2 - \tau = \frac{10330}{T[\text{K}]} \text{ [s]} \text{ (in the reactive zone) - Quartz}$

d) $P = 100 \text{ bar} - 789 \text{ ppm NH}_3 - 4.07\% \text{ O}_2 - \tau = \frac{6610}{T[\text{K}]} \text{ [s]} \text{ (in the reactive zone) - Alumina}$

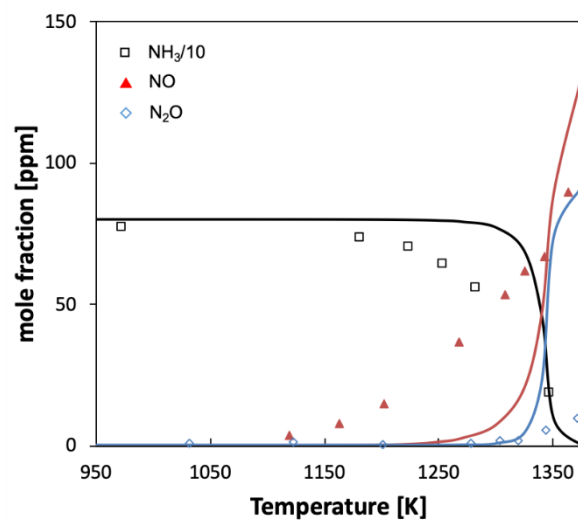


2.2.4 Hulgaard and Dam-Johansen [5]

Type: Isothermal flow reactor

Model: isothermal plug-flow reactor

- 800 ppm NH_3 – 2.5 % O_2
- Balance gas: N_2
- $P = 106 \text{ kPa}$
- $\tau = 71/T[\text{K}] \text{ s}$

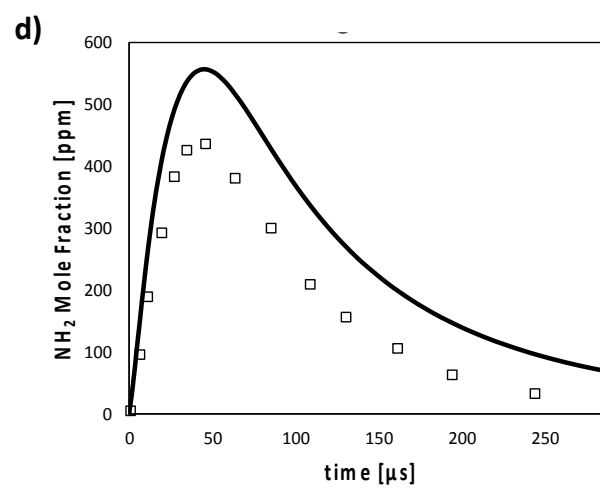
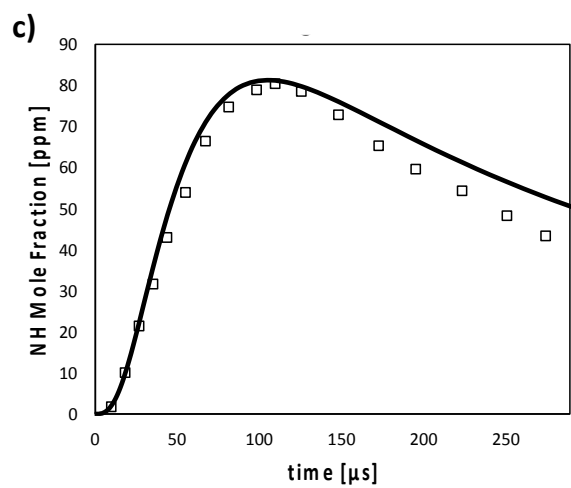
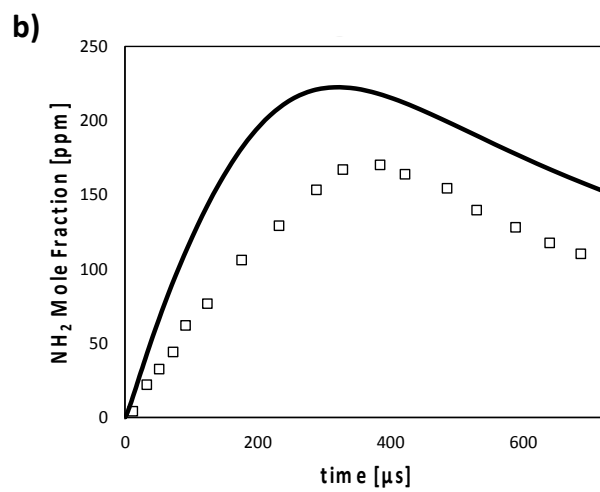
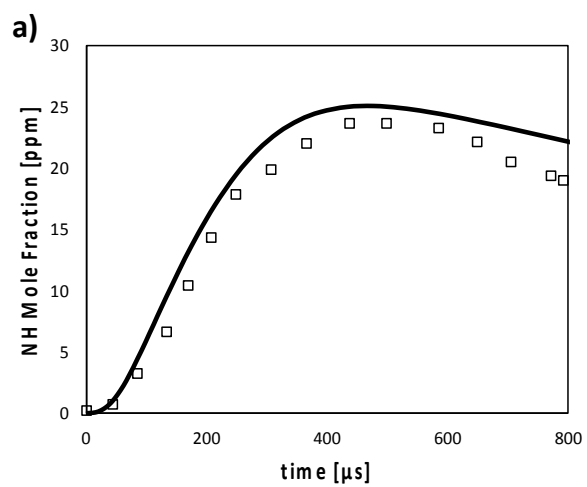


2.3 Shock tube

2.3.1 Davidson et al. [6]

Model: constant-volume batch reactor

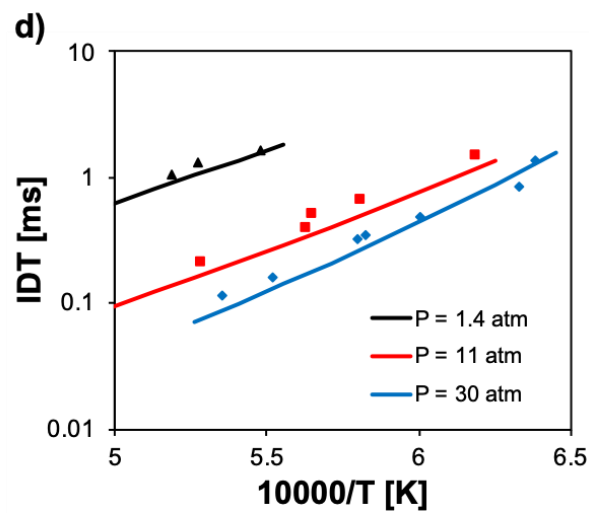
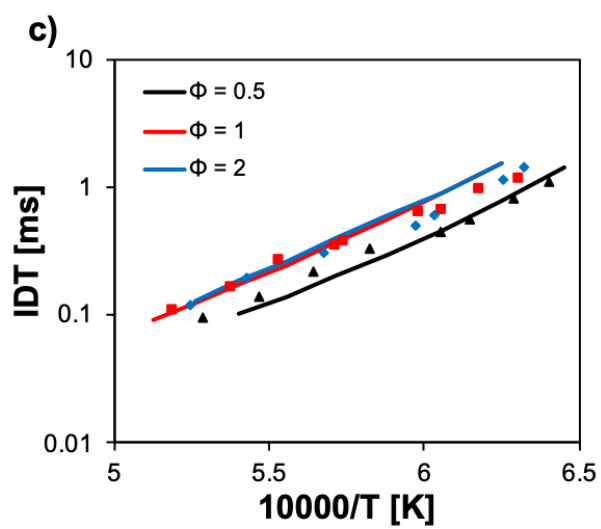
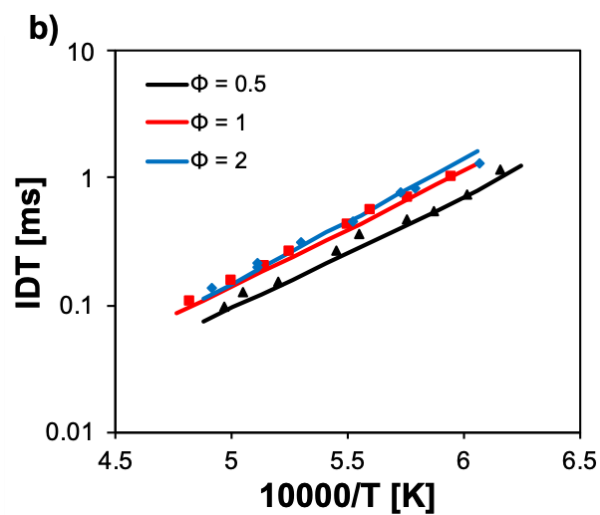
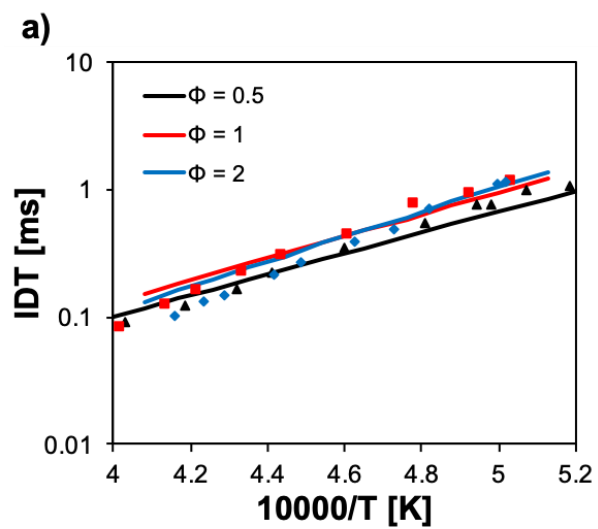
- Ammonia pyrolysis
- Balance gas: Ar
 - a) $T = 2294 \text{ K} - P = 0.986 \text{ atm} - 3000 \text{ ppm NH}_3$
 - b) $T = 2301 \text{ K} - P = 1.028 \text{ atm} - 2700 \text{ ppm NH}_3$
 - c) $T = 2652 \text{ K} - P = 0.876 \text{ atm} - 3000 \text{ ppm NH}_3$
 - d) $T = 2781 \text{ K} - P = 0.902 \text{ atm} - 2700 \text{ ppm NH}_3$



2.3.2 Mathieu and Petersen [7]

Model: constant-volume batch reactor

- Balance gas: Ar
 - a) $P = 1.4 \text{ atm} - 99\% \text{ Ar}$
 - b) $P = 11 \text{ atm} - 99\% \text{ Ar}$
 - c) $P = 30 \text{ atm} - 99\% \text{ Ar}$
 - d) $\phi = 1 - 98\% \text{ Ar}$

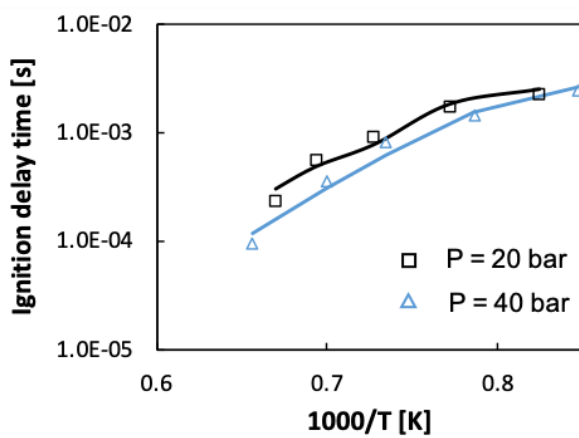


2.3.3 Shu et al. [8]

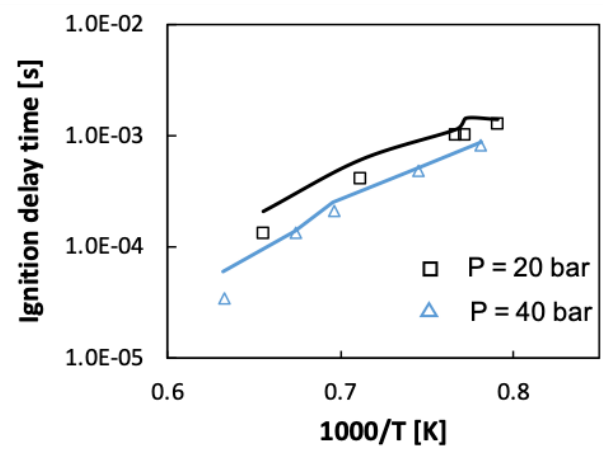
Model: Batch reactor with assigned volume profile (converted from experimental pressure trace)

- NH_3/Air
 - a) $\phi = 0.5 - P = 20\text{-}40$ bar
 - b) $\phi = 1 - P = 20\text{-}40$ bar
 - c) $\phi = 2 - P = 20\text{-}40$ bar

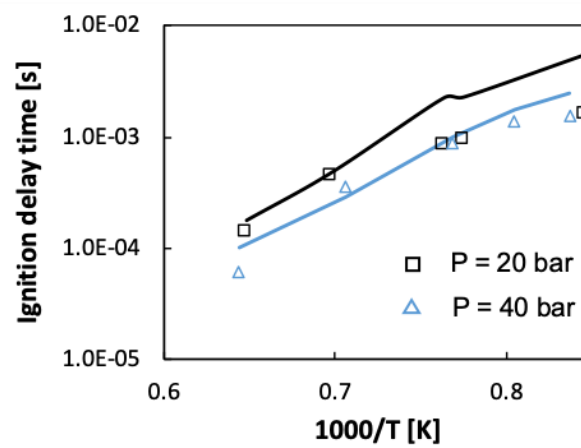
a)



b)



c)

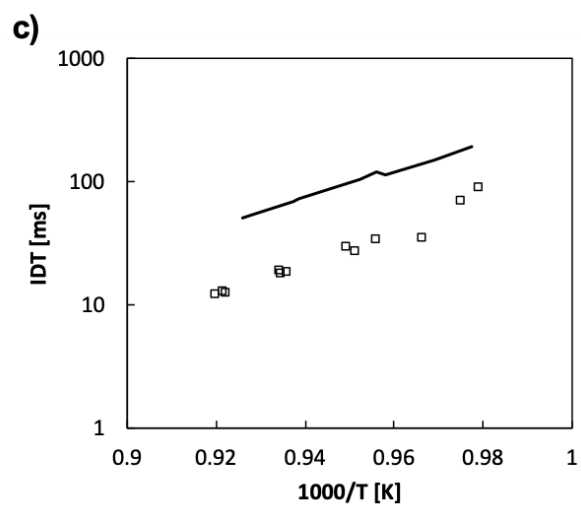
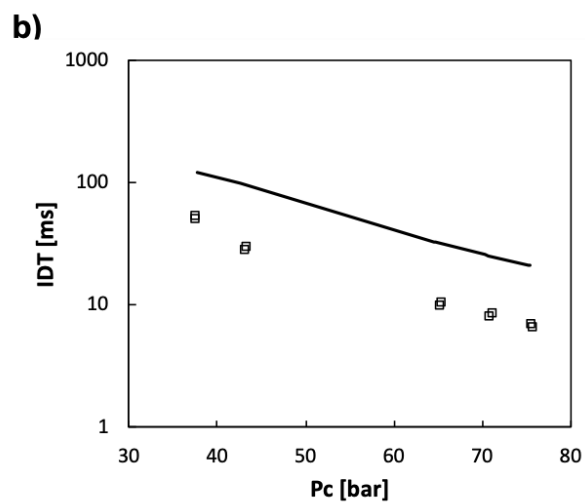
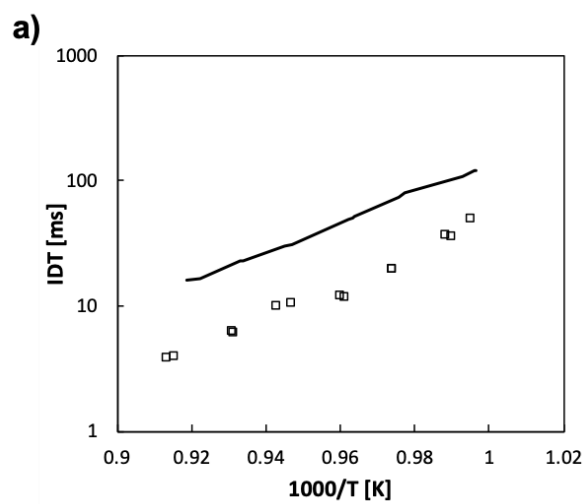


2.4 Rapid-compression machine

2.4.1 Pochet et al. [9]

Model: Batch reactor with assigned volume profile (converted from experimental pressure trace)

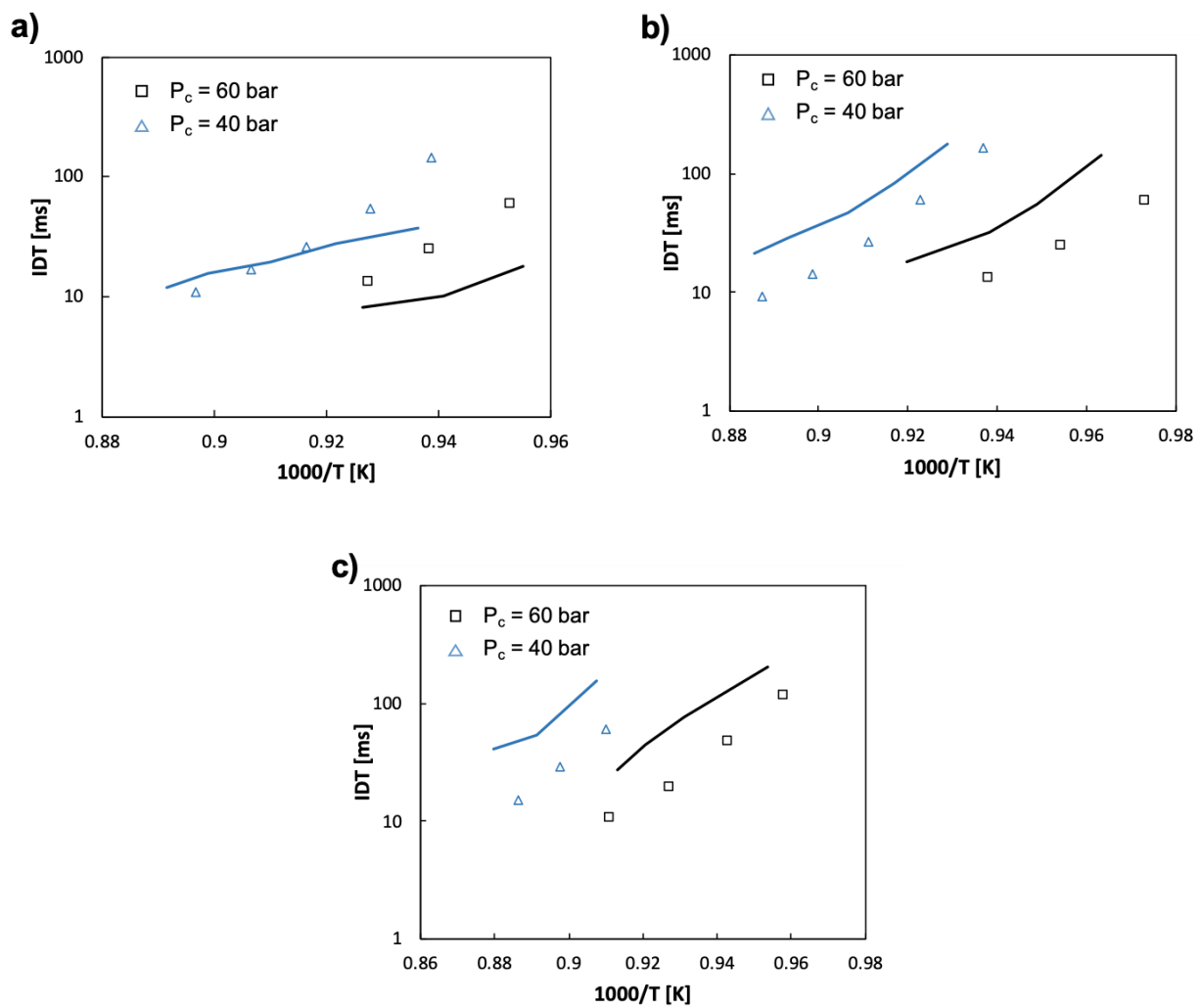
- 8.93% NH_3 – 19.13% O_2 – 61.15% N_2 – 10.79% Ar
 - a) $P_c = 65.5$ bar
 - b) $T_{\text{in}} = 353$ K
 - c) $P_c = 43.4$ bar



2.4.2 He et al. [10]

Model: Batch reactor with assigned volume profile (converted from experimental pressure trace)

- Balance gas: Ar
- $T_c = 310\text{-}370\text{ K}$
 - a) $\phi = 0.5$
 - b) $\phi = 1$
 - c) $\phi = 1.5$

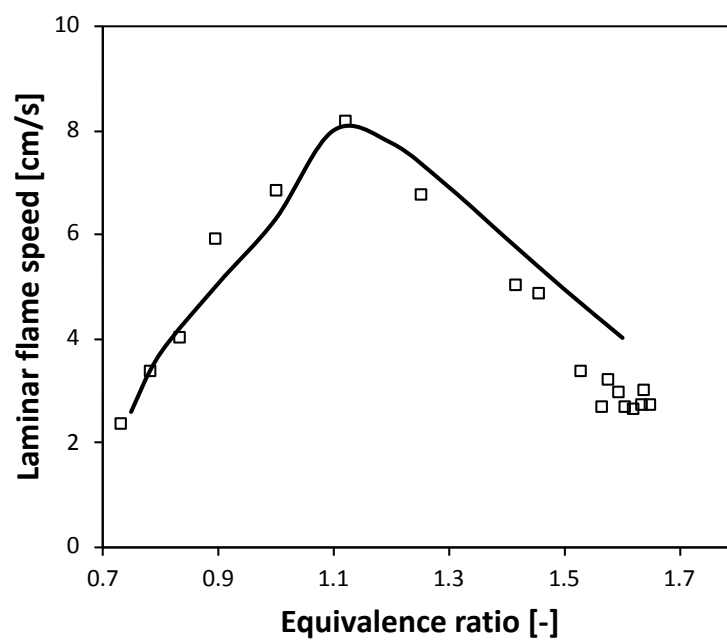


2.5 Laminar flame speed

2.5.1 Ronney [11]

Model: Premixed 1D laminar flame – radiation accounted for by optically-thin model

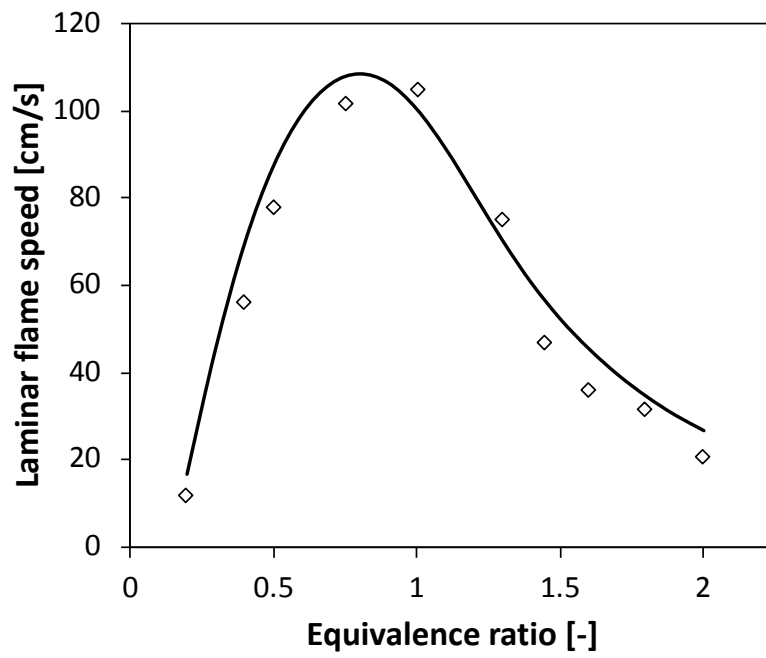
- NH_3/Air
- $T_{\text{in}} = 298 \text{ K}$
- $P = 1 \text{ atm}$



2.5.2 Liu et al. [12]

Model: Premixed 1D laminar flame – radiation accounted for by optically-thin model

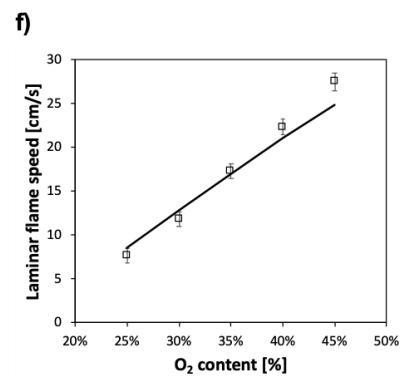
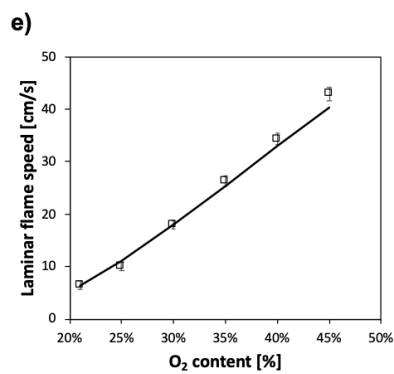
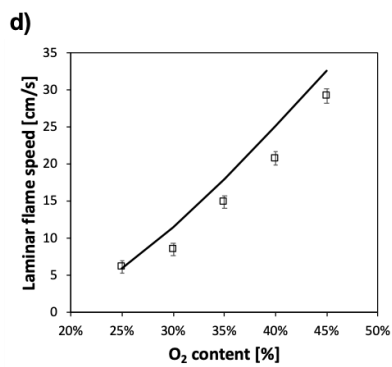
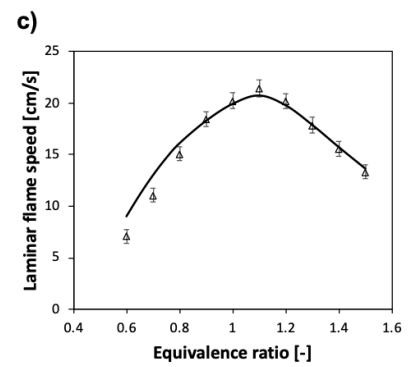
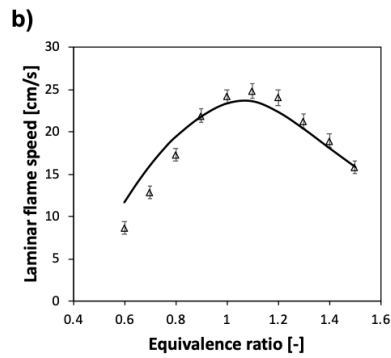
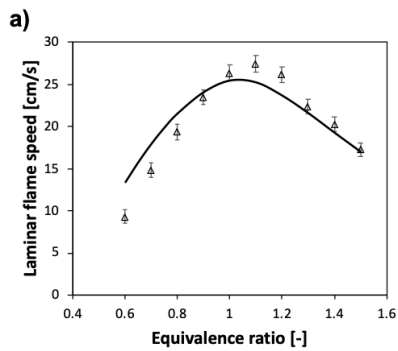
- NH_3/O_2
- $T_{\text{in}} = 298 \text{ K}$
- $P = 1 \text{ atm}$



2.5.3 Mei et al. [13]

Model: Premixed 1D laminar flame – radiation accounted for by optically-thin model

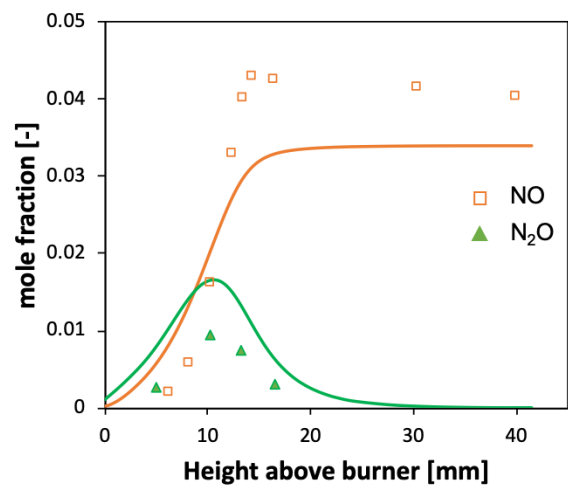
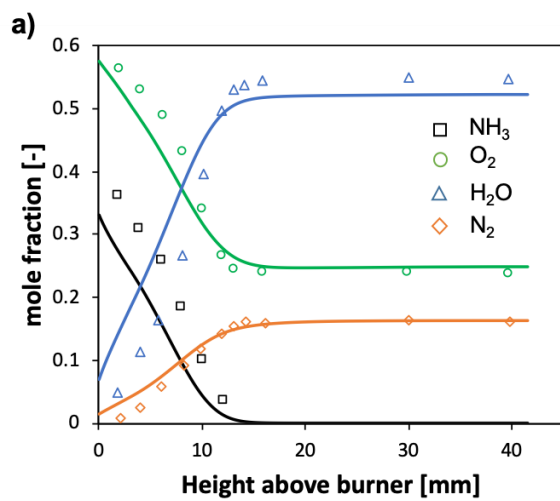
- NH_3/O_2
- $T_{\text{in}} = 298 \text{ K}$
 - a) 35% O_2 – 1 atm
 - b) 35% O_2 – 21 atm
 - c) 35% O_2 – 5 atm
 - d) $\phi = 0.7$ – 1 atm
 - e) $\phi = 1$ – 1 atm
 - f) $\phi = 1.5$ – 1 atm

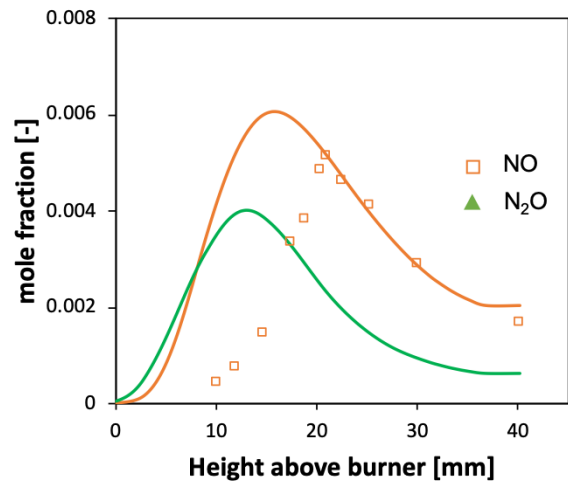
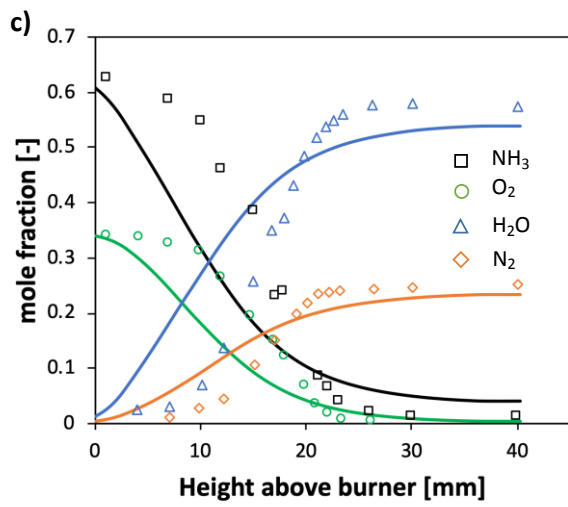
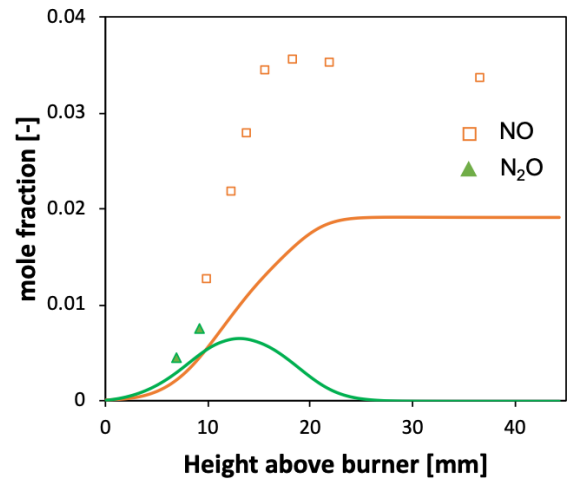
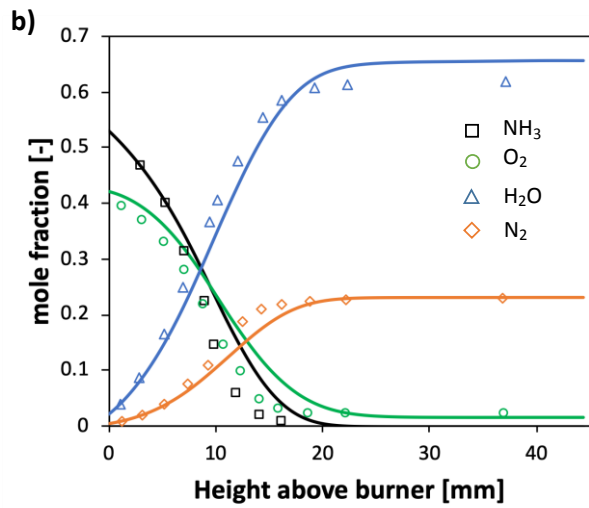


2.6 Burner-stabilized flame

2.6.1 MacLean et al. [14]

- NH_3/O_2
- $P = 20 \text{ torr}$
- $v_0 = 60.5 \text{ cm/s}$
 - a) 40% NH_3 – 60% O_2
 - b) 57% NH_3 – 43% O_2
 - c) 65% NH_3 – 35% O_2





3 References

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