

Large-Eddy Simulation of Flame Dynamics during Ignition of a Swirling Injector Unit and Comparison with Experiments

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HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés. A safe and reliable ignition of combustion chambers must be ensured for aeronautical applications and gas turbines. A flame flashback has been observed experimentally [1] during the ignition of spray flames which might have a damaging effect on the injection unit. Large eddy simulations (LES) can help to investigate and better understand the dynamic flame behaviour during ignition.

Scope

The SICCA combustor is a swirled single-injector spray combustor operated at ambient pressure.

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^[2] Safran Tech, E&P, Châteaufort, CS 80112, 78772 Magny-Les-Hameaux, France

• Content - C

and Comparison with Experiments

- $\mathbf{P}_{th} \approx 5 \,\mathrm{kW}$
- Fuel: liquid n-heptane (C_7H_{16}) at T = 298 K Global equivalence ratio: $\Phi = 0.89$





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Numerical Setup

The numerical domain and the sover setup are based on previous work published in [2].

- LES solver: AVBP (CERFACS/IFPEN)
- SGS model: Wall Adapting Local Eddy-Viscosity (WALE) model
- Combustion model: Dynamic TFLES with PEA
- Two phase modeling: monodisperse Eulerian-Eulerian model ($d_{inj} = 15.3 \,\mu m$)







(b) 12.5 ms (C) 20.8 ms (d) 29.2 ms (e) 37.5 ms (a) 4.17 ms Experimental ignition sequence recorded by a high-speed camera with OH*-filter [1].

⁴ LES Ignition Sequence –

- Ignition with a spherical volume of high temperature burnt gases
- Penetration into the swirler
- Flame edge attached to the swirler
- After a characteristic time: quenching of the lower flame part
- Flame lift-off and stabilization at a distance from the swirler





Evaporation model: Abramzon-Sirignano

Prescribed temperature profile ranging between *T* = 773 and *T* = 1173 K

Penetration into the Injector

Phase I: Stabilization and anchoring

- Growth of the initial flame kernel [I]
- Burnt gas expansion causes acoustic pressure disturbance [II]
- Temporary stagnation of the mass flow rate [III]
- Flame flashback and anchoring attached to the swirler, despite pre-ignition mass flow rates are re-established [IV]
- Transient stabilization in qualitative agreement with experimental data [V]







(a) 4.2 ms (b) 12.5 ms Line of sight integrated heat release [V].

Flame Lift-Off

Phase II: Flame lift-off and shape transition

- Lower flame part quenched after a characteristic time related to the cooling of the recirculating burnt gases near the combustor walls [VI]
- Flame lift-off and stabilization detached from the swirler [VII]
- Detached flame shape different with respect to attached flame [VIII]
- Lift-off delay qualitatively retrieves experimental trends [IX]

of Heat Release

Level

MIN





(k) 28 ms

Flame shape based on progress variable c = 0.5colored by temperature.

4 Conclusion -

- Capability of LES to properly capture the flame dynamics during ignition including:
 - the stabilization of the flame attached to the swirler
 - the lift-off after a characteristic time
- Good qualitative agreement of the governing mechanisms in each phase with experimental data

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Heat release rate $[Js^{-1}m^{-1}]$

Heat release rate and contour of the progress variable c = 0.5 at the combustor mid-plane.

(a) $t = 23.5 \,\mathrm{ms}$

Line of sight integrated heat release at 25.1 ms [IX].

Cooling of the IRZ and ORZ [VI].

References

[1] K. Prieur, D. Durox, G. Vignat, T. Schuller, S. Candel, Proceedings of ASME Turbo Expo, 4B, (GT2018-76840) (2018).

(b) t = 24 ms

[2] T. Lancien, K. Prieur, D. Durox, S. Candel, R. Vicquelin, Journal of Engineering for Gas Turbines and Power 140 (2017).

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