

# **Interval Observer Design for Actuator Fault Estimation of Linear Parameter-Varying Systems**

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#### **Example 12 Interval Observer Design for Actuator Fault Interval Observer Design for Actuator Fault ESTIMATION OF LINEAR POST PARAMETER PARAMETER Interval Observer Design for Actuator Fault Figure 1,** *Tarek Rault* **Fault**<br>**Estimation of Linear Parameter-Varying Systems Estimation of Linear Parameter-Varying Systems Estimation of Linear Parameter-Varying Systems**

**Rihab Lamouchi** <sup>∗</sup>, **Tarek Ra¨ıssi** <sup>∗</sup>, **Messaoud Amairi** ∗∗, Rihab Lamouchi<sup>\*</sup>, Tarek Raïssi<sup>\*</sup>, Messaoud Amairi<sup>\*\*</sup>,<br>Mohamed Aoun<sup>\*\*</sup> **Mohamed Aoun** ∗∗ **Mohamed Aoun** ∗∗

scionance Abun<br>Cedric-Lab, Conservatoire National des Arts et Métiers, Paris, France, e-mail: lamouchi.rihab@gmail.com, tarek.raissi@cnam.fr ).<br>\*\* MACS Laboratory (LR16ES22): Modeling, Analysis and Control of\*<br>rams. National Engineering School of Gabes (ENIG). University of Ga MACS Laboratory (EXTOES22). Modeling, Analysis and Control of<br>Systems, National Engineering School of Gabes (ENIG), University of Gabes, *Tunisia (e-mail: amairi.messaoud@ieee.org, mohamed.aoun@gmail.com) Systems, National Engineering School of Gabes (ENIG), University of Gabes,* <sup>∗</sup>*Cedric-Lab, Conservatoire National des Arts et Metiers,Paris, France,* ´ <sup>∗</sup>*Cedric-Lab, Conservatoire National des Arts et Metiers,Paris, France,* ´ *Tunisia (e-mail: amairi.messaoud@ieee.org, mohamed.aoun@gmail.com)* e-mail: lamouchi.rihab@gmail.com, tarek.raissi@cnam.fr ).<br>\*\* MACS Laboratory (LR16ES22): Modeling, Analysis and Control of Tunisia (e-mail: amairi.messaoud@ieee.org, mohamed.aoun@gmail.com) e-mail: lamouchi.rinab@gmail.com, tarek.raissi@cnam.fr ).<br>∗∗ *MACS Laboratory (LR16ES22): Modeling, Analysis and Control of*<br>*stems. National Engineering School of Gabes (ENIG). University of Gab Tunisia (e-mail: amairi.messaoud@ieee.org, mohamed.aoun@gmail.com)*

Abstract: This work is devoted to fault estimation of discrete-time Linear Parameter-Varying (LPV) systems subject to actuator additive faults and external disturbances. Under the assumption that the measurement noises and the disturbances are unknown but bounded, an interval observer is designed, based on decoupling the fault effect, to compute a lower and upper bounds for the unmeasured state and the faults. Stability conditions are expressed in terms of matrices inequalities. A case study is used to illustrate the effectiveness of the proposed approach. *Tunisia (e-mail: amairi.messaoud@ieee.org, mohamed.aoun@gmail.com)*  $\frac{1}{\sqrt{2}}$  in terms of matrices in terms of matrices inequalities. A case study is used to matrices in

© 2018, IFAC (International Federation of Automatic Control) Hosting by Elsevier Ltd. All rights reserved. illustrate the effectiveness of the proposed approach. **Keywords: Fault estimation, Interval of The Company of The Company of The Chief System**  $\odot$  2018, IFAC (International Federation of Automatic

Keywords: Fault estimation, Interval observer, LPV system, Unknown input observer. *Keywords:* Fault estimation, Interval observer, LPV system, Unknown input observer.

#### 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION 1. <del>INTRODUCTION</del>

Industrial systems are subject to several kinds of faults, such as Industrial systems are subject to several kinds of faults, such as Industrial systems are subject to several kinds of faults, such as muustrial systems are subject to several kinds of radiis, such as<br>sensors, actuators or component malfunction, which may lead to performance degradation or even serious human damages. sensors, actuators or component malfunction, which may lead Therefore, it is important to improve system and human safety and reliability. As a result, during the past decades, fault esand reliability. As a result, during the past decades, fault es-<br>timation has been received a great attention; it allows one to determine the size, location and dynamic of the fault. determine the size, location and dynamic of the fault. to performance degradation or even serious human damages. timation has been received a great attention; it allows one to to performance degradation or even serious human damages.<br>Therefore, it is important to improve system and human safety<br>and reliability. As a result, during the past decades, fault estimation has been received a great attention; it allows one to determine the size, location and dynamic of the fault. determine the size, location and dynamic of the fault. timation has been received a great attention; it allows one to determine the size, location and dynamic of the fault.

In reality, most of industrial systems are nonlinear and Linear In reanty, most of muustrial systems are nominear and Emean<br>Parameter-Varying (LPV) models can be used to approximate a large class of nonlinear systems (Shamma [2012]). Many rea large class of nonlinear systems (Shamma [2012]). Many re-<br>searches have been carried out about LPV systems in the filed of fault estimation. For LPV systems, the discrete fault estimation problem has been dealt within many works. In (Abdullah and problem has been dealt whilm many works. In (Abdullah and<br>Zribi [2013]), a fault estimation and compensation scheme for Erior (2013), a raute estimation and compensation scheme for A robust fault estimation and compensation for LPV systems LPV systems, under actuator and sensor faults is presented. under actuator and sensor faults is proposed in (Seron and under actuator and sensor faults is proposed in (Seron and De Don´a [2015]). In (Luspay et al. [2015]), fault estimation for De Don´a [2015]). In (Luspay et al. [2015]), fault estimation for discrete-time LPV systems under noisy scheduling measurediscrete-time LPV systems under noisy scheduling measure-<br>ments is proposed taking into account stochastic and additive scheduling parameter ambiguities. scheduling parameter ambiguities. searches have been carried out about LPV systems in the filed of A robust fault estimation and compensation for LPV systems ments is proposed taking into account stochastic and additive searches have been carried out about LPV systems in the filed of A robust fault estimation and compensation for LPV systems. under actuator and sensor faults is proposed in (Seron and De Doná [2015]). In (Luspay et al. [2015]), fault estimation for ments is proposed taking into account stochastic and additive scheduling parameter ambiguities. scheduling parameter ambiguities. ments is proposed taking into account stochastic and additive ments is proposed taking into account stochastic and additive scheduling parameter ambiguities.

An effective approach based on fault decoupling principle can An effective approach based on fault decoupling principle can<br>be used to estimate the fault. This is obtained by designing an Unknown Input Observer (UIO). Over the past decades, a great<br>deal of general offert has been deveted to the UIO theory. In deal of research effort has been devoted to the UIO theory. In (Sun et al. [2012]), a linear time invariant model-based robust deal of research effort has been devoted to the UIO theory. In fast adaptive fault estimator with unknown input decoupling<br>is against the estimate faults. An UIO decision against in is proposed to estimate faults. An UIO design procedure is is proposed to estimate faults. An UIO design procedure is generalized to LPV descriptor system is presented in (Hamdi et al. [2012]). UIO for LPV systems with parameter varying<br>extent constitution of conclusion in (Jababal at al. [2015]). output equation is developed in (Ichalal et al. [2015]). output equation is developed in (Ichalal et al. [2015]). be used to estimate the fault. This is obtained by designing an (Sun et al.  $[2012]$ ), a linear time invariant model-based robust An effective approach based on fault decoupling principle can<br>be used to estimate the fault. This is obtained by designing an Unknown Input Observer (UIO). Over the past decades, a great Unknown Input Observer (UIO). (Sun et al. [2012]), a linear time invariant model-based robust fast adaptive fault estimator with unknown input decoupling<br>is proposed to estimate faults. An UIO design procedure is fast adaptive fault estimator with unknown input decoupling<br>is proposed to estimate faults. An UIO design procedure is generalized to LPV descriptor system is presented in (Hamdi et al. [2012]). UIO for LPV systems with parameter varying output equation is developed in (Ichalal et al.  $[2015]$ ). output equation is developed in (Ichalal et al.  $[2015]$ ).

Usually, an unknown input observer is designed to estimate the fault. However, in presence of uncertainties, classical ob-Usually, an unknown input observer is designed to estimate the fault. However, in presence of uncertainties, classical obthe fault. However, in presence of uncertainties, classical ob-the fault. However, in presence of uncertainties, classical ob-Usually, an unknown input observer is designed to estimate the fault. However, in presence of uncertainties, classical ob-

servers may not be efficient to solve the estimation problem. servers may not be efficient to solve the estimation problem. servers may not be efficient to solve the estimation problem. In this case, interval observer is proposed to compute the set In this case, interval observer is proposed to compute the set<br>of all the admissible values and provides certain lower and upper bounds for the estimate at each instant of time in the expression of the estimate at each instant of time in the presence of bounded uncertainties. Several works have invespresence of bounded uncertainties. Several works have inves-<br>tigated interval observers based on cooperative systems theory regated interval observers based on cooperative systems theory<br>(Raïssi et al. [2010]), (Mazenc et al. [2014]), (Lamouchi et al. (Kaissi et al. [2010]), (Mazenc et al. [2014]), (Lamouchi et al. [2016]) and (Lamouchi et al. [2017]). Few works have consid- $[2010]$  and  $[2010]$  and  $[2017]$ . Few works have considered unknown input interval observers. In  $(Gucik-Derigny et al.$ [2014]), (Gucik-Derigny et al. [2016]), an interval state and un-ered unknown input interval observers. In (Gucik-Derigny et al. known inputs estimation for linear time-invariant continuoustime systems is studied. The work in  $(Xu \text{ et al. } [2017])$  proposes an UIO for LPV systems based on set theoretic approach. poses an OIO for LFV systems based on set theoretic approach.<br>Recently, a new method developed in (Robinson et al. [2017]) has addressed the problem of unknown input interval state nas addressed the problem of unknown liput interval state<br>estimation for Linear Time-Invariant systems. To the best of estimation for Ellicar Time-Invariant systems. To the best of our knowledge, fault estimation problem in discrete-time LPV systems using unknown input interval observer has not been yet fully tackled. fully tackled. of all the admissible values and provides certain lower and<br>wagen hours as far the estimate at each instead of time in the [2014]), (Gucik-Derigny et al. [2016]), an interval state and unour knowledge, fault estimation problem in discrete-time LPV of all the admissible values and provides certain lower and upper bounds for the estimate at each instant of time in the [2014]), (Gucik-Derigny et al. [2016]), an interval state and unknown inputs estimation for linear time-invariant continuoustime systems is studied. The work in (Xu et al. [2017]) proour knowledge, fault estimation problem in discrete-time LPV our knowledge, fault estimation problem in discrete-time LPV<br>systems using unknown input interval observer has not been yet fully tackled. systems using unknown input interval observer has not been yet<br>fully tackled *Keywords:* Fault estimation, Interval observer, LPV system, Unknown input observer. stems using unknown in put in the server has not been yet be

Motivated by the previous explanations and inspired by the previous explanations and inspired by the present method in (Robinson et al. [2017]), an extension of fault es-<br>timetics to a class of discrete time  $\Gamma_{\text{IV}}$  surfaces in a set timation to a class of discrete-time LPV systems in a setmembership framework is proposed in this paper. The idea con-<br>membership framework is proposed in this paper. sists in decoupling the fault effect on the state using transforma-<br>tion of accepting the state using in the state using the state using the state using the state using the state of tion of coordinates. Then, an unknown input interval observer is designed to compute a lower and upper bounds for the state tion of coordinates. Then, an unknown input interval observer and the fault. and the fault. is designed to compute a lower and upper bounds for the state Motivated by the previous explanations and inspired by the method in (Robinson et al.  $[2017]$ ), an extension of fault estimation to a class of discrete-time LPV systems in a setminiation to a class of discrete time Er v systems in a set sists in decoupling the fault effect on the state using transformais designed to compute a lower and upper bounds for the state is designed to compute a lower and upper bounds for the state tion of coordinates. Then, an unknown input interval observer and the fault. and the fault. fully the full set is designed to compute a lower and upper bounds for the state<br>and the fault and the rault.

This paper is organized as follows. Preliminaries are given in<br>Social 2. In Section 2, the preklam attenued is presented Section 2. In Section 3, the problem statement is presented. Section 4, the section 5, the problem statement is presented.<br>Section 4 proposes an interval observer for state and fault estimation. Numerical simulations are presented in Section 5 to show the efficiency of the proposed approach. Finally, the estimation. Numerical simulations are presented in Section 5 paper is concluded in Section 6. paper is concluded in Section 6. to show the efficiency of the proposed approach. Finally, the This paper is organized as follows. Preliminaries are given in Section 2. In Section 3, the problem statement is presented. to show the efficiency of the proposed approach. Finally, the paper is concluded in Section 6. paper is concluded in Section 6. to show the efficiency of the proposed approach. Finally, the paper is concluded in Section 6.

### 2. PRELIMINARIES

A system described by  $x_{k+1} = Ax_k + u_k$ , with  $x_k \in \mathbb{R}^n$  and  $A \in \mathbb{R}^{n \times n}$ , is nonnegative if and only if the matrix *A* is elementwise nonnegative,  $u_k \geq 0$  and  $x_{k_0} \geq 0$ . A matrix  $A \in \mathbb{R}^{n \times n}$  is nonnegative if all its elements are nonnegative. Given a matrix *M* ∈  $\mathbb{R}^{m \times n}$ , define *M*<sup>+</sup> = *max*{0,*M*}, *M<sup>−</sup> = max*{0,−*M*} (similarly for vectors). For two vectors  $x_1, x_2 \in \mathbb{R}^n$  or matrices  $M_1, M_2 \in \mathbb{R}^{n \times n}$ , the relations  $x_1 \leq x_2$  and  $M_1 \leq M_2$  are understood elementwise. The symbol |.| denotes vector or corresponding induced matrix Euclidean norm. For a measurable and locally essentially bounded input  $u : \mathbb{N} \to \mathbb{R}$ , the symbol  $||u||_{[t_0,t_1)}$  denotes its *L*∞-norm where  $||u||_{[t_0,t_1)} = \sup\{|u_t|, t \in$  $[t_0,t_1)$ ,  $||u|| = ||u||_{[0,+\infty)}$ . The set of all inputs *u* with the property  $||u|| < \infty$  is denoted by  $\mathscr{L}_{\infty}$ .

*Lemma 1.* (Chebotarev et al. [2013]) Let  $x, x, \overline{x} \in \mathbb{R}^n$  if  $x \leq x \leq \overline{x}$ then,

$$
\underline{x}^+ \le x^+ \le \overline{x}^+ \text{ and } \overline{x}^- \le x^- \le \underline{x}^- \tag{1}
$$

Similarly, let  $A, A, \overline{A} \in \mathbb{R}^{m \times n}$ , if  $A \leq A \leq \overline{A}$  then

$$
\underline{A}^+ \le A^+ \le \overline{A}^+ \text{ and } \overline{A}^- \le A^- \le \underline{A}^- \tag{2}
$$

*Lemma* 2. (Chebotarev et al. [2013]) Let  $x \in \mathbb{R}^n$  be a vector such that  $\underline{x} \leq x \leq \overline{x}$  for some  $\underline{x}, \overline{x} \in \mathbb{R}^n$ .

(1) If  $A \in \mathbb{R}^{m \times n}$  is a constant matrix, then

$$
A^+\underline{x} - A^-\overline{x} \leqslant Ax \leqslant A^+\overline{x} - A^-\underline{x} \tag{3}
$$

(2) If  $A \in \mathbb{R}^{m \times n}$  is a matrix satisfying  $A \leq A \leq \overline{A}$  for some  $\underline{A}, \overline{A} \in \mathbb{R}^{m \times n}$ , then

$$
\underline{A}^+\underline{x}^+ - \overline{A}^+\underline{x}^- - \underline{A}^-\overline{x}^+ + \overline{A}^-\overline{x}^- \leq Ax
$$
  
 
$$
\leq \overline{A}^+\overline{x}^+ - \underline{A}^+\overline{x}^- - \overline{A}^-\underline{x}^+ + \underline{A}^-\underline{x}^-.
$$
 (4)

#### 3. PROBLEM STATEMENT

Consider the following discrete-time LPV system:

$$
\begin{cases} x_{k+1} = (A + \Delta A(\rho))x_k + Bu_k + w_k \\ y_k = Cx_k + v_k \end{cases}
$$
 (5)

where  $x_k \in \mathbb{R}^n$  is the state,  $u_k \in \mathbb{R}^q$  is the input,  $y_k \in \mathbb{R}^p$  is the output;  $w_k$ ,  $v_k$  are respectively the bounded disturbance and noise. The vector of scheduling parameters  $\rho \in \Pi$  is considered unknown and only the set of its admissible values  $\Pi$  is given. Δ*A* :  $\Pi$  →  $\mathbb{R}^{n \times n}$  is a known piecewise continuous matrix function.

We assume in the following that an actuator fault can be modelled by an additive term in the system (5). Therefore, the faulty system dynamics are given by:

$$
\begin{cases} x_{k+1} = (A + \Delta A(\rho))x_k + Bu_k + Ff_k + w_k \\ y_k = Cx_k + v_k \end{cases}
$$
 (6)

where  $F \in \mathbb{R}^{n \times q}$  is a known matrix and  $f_k \in \mathbb{R}^q$  is the fault vector.

In the following, it is assumed that the matrix  $\Delta A(\rho)$  belongs into the interval  $[\Delta A, \overline{\Delta A}]$ . The value of the scheduling vector  $\rho$ is not available for measurement but it is easy to compute ∆*A* and  $\overline{\Delta A}$  for a given set  $\Pi$  and a known function  $\Delta A : \Pi \to \mathbb{R}^{n \times n}$ . The disturbance  $w_k$  and the measurement noise  $v_k$  are bounded by two known sequences such that  $w_k \leq w_k \leq \overline{w}_k$  and  $\overline{v}_k \leq v_k \leq \overline{v}_k$  $\overline{v}_k$ .

*Assumption 1.*  $\underline{\Delta A} \leq \Delta A(\rho) \leq \overline{\Delta A}$  for all  $\rho \in \Pi$  and some known  $\Delta A, \overline{\Delta A}$  ∈  $\mathbb{R}^{n \times n}$ .  $\Box$ 

*Assumption 2.* There exist  $\overline{w}$ ,  $\overline{w}$ ,  $\overline{v}$  and  $\overline{v}$  such that:  $w \leq w_k \leq \overline{w}$ and  $\underline{v} \leq v_k \leq \overline{v}$  are satisfied  $\forall k \in \mathbb{N}$ .  $\Box$ .

The methodology presented below is based on two steps. First, an estimation of the state bounds  $x_k, \overline{x}_k \in \mathbb{R}^n$  is described. The second step consists in estimating a lower and upper bounds  $f_k$ ,  $\overline{f}_k \in \mathbb{R}^{\overline{q}}$  for the actuator fault  $f_k$ .

#### 4. MAIN RESULTS

The following assumption is required.

*Assumption 3. C* is full row rank matrix and *F* is a full column rank matrix.

Under Assumption 3, there exists a transformation of coordinates  $z_k = H^T x_k$ ,  $H \in \mathbb{R}^{n \times n}$  such that  $F = H [R_0 \ 0]^T K_0^T$  with  $R_0 \in \mathbb{R}^{q \times q}$  and  $K_0 \in \mathbb{R}^{q \times q}$ .

The system (6) can be rewritten in the coordinates *z* as:

$$
\begin{cases}\nz_{k+1} = (\tilde{A} + \Delta \tilde{A}(\rho))z_k + \tilde{B}u_k + \begin{bmatrix} R_0 \\ 0 \end{bmatrix} \tilde{f}_k + \tilde{w}_k \\
y_k = \tilde{C}z_k + v_k\n\end{cases} (7)
$$
\nwith  $H = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix}$ ,  $\tilde{A} = H^T A H = \begin{bmatrix} \tilde{A}_{11} & \tilde{A}_{12} \\ \tilde{A}_{21} & \tilde{A}_{22} \end{bmatrix}$ ,  
\n
$$
\Delta \tilde{A}(\rho) = H^T \Delta A(\rho) H = \begin{bmatrix} \Delta \tilde{A}_{11}(\rho) & \Delta \tilde{A}_{12}(\rho) \\ \Delta \tilde{A}_{21}(\rho) & \Delta \tilde{A}_{22}(\rho) \end{bmatrix}
$$
,  
\n $\tilde{B} = H^T B = \begin{bmatrix} \tilde{B}_1 & \tilde{B}_2 \end{bmatrix}^T$ ,  $\tilde{C} = CH = \begin{bmatrix} \tilde{C}_1 & \tilde{C}_2 \end{bmatrix}$ ,  $\tilde{f}_k = K_0^T f_k$ ,  $\tilde{w} = H^T w = \begin{bmatrix} \tilde{w}_{1,k} & \tilde{w}_{2,k} \end{bmatrix}^T$ .

*H*<sup>*T*</sup> is assumed to be bounded, then, it follows that  $|\tilde{w}| \leq \overline{\tilde{w}}$ where  $\overline{\tilde{w}}$  is a constant positive vector.

The system (7) can be rewritten as:

$$
\begin{cases} z_{1,k+1} = (\tilde{A}_{11} + \Delta \tilde{A}_{11}(\rho))z_{1,k} + (\tilde{A}_{12} + \Delta \tilde{A}_{12}(\rho))z_{2,k} \\ \quad + \tilde{B}_1 u_k + R_0 \tilde{f}_k + \tilde{w}_{1,k} \\ z_{2,k+1} = (\tilde{A}_{21} + \Delta \tilde{A}_{21}(\rho))z_{1,k} + (\tilde{A}_{22} + \Delta \tilde{A}_{22}(\rho))z_{2,k} \\ \quad + \tilde{B}_2 u_k + \tilde{w}_{2,k} \\ y_k = \tilde{C}_1 z_{1,k} + \tilde{C}_2 z_{2,k} + v_k \end{cases} \tag{8}
$$

 $\tilde{C}_1$  is supposed to be a full column rank matrix (Hou and Muler 1992) and can be decomposed as:  $\tilde{C}_1 = N[R_1 \ 0]^T K_1^T$ with  $N = [N_{11} N_{12}]$  and  $\tilde{y}_k = N^T y_k$ . Then, the measurement equation can be decomposed as:

$$
\begin{cases} \tilde{y}_{1,k} = R_1 K_1^T z_{1,k} + N_{11}^T \tilde{C}_2 z_{2,k} + N_{11}^T v_k \\ \tilde{y}_{2,k} = N_{12}^T \tilde{C}_2 z_{2,k} + N_{12}^T v_k = C_2 z_{2,k} + N_{12}^T v_k \end{cases}
$$
\n(9)

As  $\tilde{y}_{1,k} = G_s^T \tilde{y}_k$  with  $G_s^T = \begin{bmatrix} I_q & O_{q \times (p-q)} \end{bmatrix}$ , the expression of  $z_1$ is extracted from (9):

$$
z_{1,k} = E(y_k - \tilde{C}_2 z_{2,k} - v_k)
$$
 (10)

with  $E = K_1 R_1^{-1} G_s^T N^T$ . By replacing this expression of  $z_{1,k}$  in the second equation of (8) we obtain:

$$
\begin{cases} z_{2,k+1} = A_2 z_{2,k} + \Delta \tilde{A}_2(\rho) z_{2,k} + B_2 u_k + D_2(\rho) y_k \\ - D_2(\rho) v_k + \tilde{w}_{2,k} \\ \tilde{y}_{2,k} = C_2 z_{2,k} + N_{12}^T v_k \end{cases} (11)
$$

with  $A_2 = \tilde{A}_{22} - \tilde{A}_{21} E \tilde{C}_2$ ,  $\Delta \tilde{A}_2(\rho) = \Delta \tilde{A}_{22}(\rho) - \Delta \tilde{A}_{21}(\rho) E \tilde{C}_2$ ,  $B_2 = \tilde{B}_2, D_2(\rho) = \tilde{A}_{21}E + \Delta \tilde{A}_{21}(\rho)E$ , and  $\tilde{C}_2 = N_{12}^T \tilde{C}_2$ .

Assumption 4. The pair 
$$
(A_2, C_2)
$$
 is detectable.  $\Box$ 

*Remark 1.* It is worth to note that it is not always possible to compute a matrix *L* such that  $A_2 - LC_2$  is nonnegative. This restrictive condition can be relaxed by means of a change of coordinates. It has been shown in (Efimov et al. [2013]) that there always exists an transformation matrix  $P$  such that  $R =$  $P(A_2 - LC_2)S$ , with  $S = P^{-1}$ , is nonnegative.

The system (11) can be described in the coordinates  $r_2 = Pz_2$ as follows:

$$
\begin{cases}\nr_{2,k+1} = Rr_{2,k} + P\Delta \tilde{A}_2(\rho) Sr_{2,k} + PB_2 u_k + M(\rho) y_k \\
-M(\rho) v_k + P \tilde{w}_{2,k} \\
\tilde{y}_{2,k} = C_2 P^{-1} r_{2,k} + N_{12}^T v_k\n\end{cases} (12)
$$

where  $M(\rho) = P(D_2(\rho) + LN_{12}^T)$ . In the following, an interval observer design is proposed to estimate the state and the actuator fault.

#### *4.1 State Estimation*

Consider the following observer structure for (12):

$$
\begin{cases}\n\overline{r}_{2,k+1} = R\overline{r}_{2,k} + PB_{2}u_{k} + \overline{\varphi}(\overline{r}_{2,k}, \underline{r}_{2,k}) + \overline{\Gamma}(y_{k}^{+}, y_{k}^{-}) - \\
\underline{\vartheta}(\overline{v}, \underline{v}) + \overline{\Delta}(\overline{\tilde{w}}_{2}, \underline{\tilde{w}}_{2}) \\
\underline{r}_{2,k+1} = R\underline{r}_{2,k} + PB_{2}u_{k} + \underline{\varphi}(\overline{r}_{2,k}, \underline{r}_{2,k}) + \underline{\Gamma}(y_{k}^{+}, y_{k}^{-}) - \\
\overline{\vartheta}(\overline{v}, \underline{v}) + \underline{\Delta}(\overline{\tilde{w}}_{2}, \underline{\tilde{w}}_{2})\n\end{cases} (13)
$$

with

$$
\begin{cases}\n\overline{\varphi}(\overline{r}_{2,k},\underline{r}_{2,k}) = \overline{\sigma}^+ \overline{r}_{2,k}^+ - \underline{\sigma}^+ \overline{r}_{2,k}^- - \overline{\sigma}^- \underline{r}_{2,k}^+ + \underline{\sigma}^- \underline{r}_{2,k}^- \\
\underline{\varphi}(\overline{r}_{2,k},\underline{r}_{2,k}) = \underline{\sigma}^+ \underline{r}_{2,k}^+ - \overline{\sigma}^+ \underline{r}_{2,k}^- - \underline{\sigma}^- \overline{r}_{2,k}^+ + \overline{\sigma}^- \overline{r}_{2,k}^- \\
\overline{\sigma} = (P^+ \Delta \overline{A}_2 - P^- \Delta \overline{A}_2) S^+ - (P^+ \Delta \overline{A}_2 - P^- \Delta \overline{A}_2) S^- \\
\underline{\sigma} = (P^+ \Delta \overline{A}_2 - P^- \Delta \overline{A}_2) S^+ - (P^+ \Delta \overline{A}_2 - P^- \Delta \overline{A}_2) S^- \qquad (14) \\
\overline{\Delta \overline{A}}_2 = \overline{\Delta \overline{A}}_{22} - (\underline{\Delta \overline{A}}_{21} (E \overline{C}_2)^+ - \overline{\Delta \overline{A}}_{21} (E \overline{C}_2)^-) \\
\underline{\Delta \overline{A}}_2 = \underline{\Delta \overline{A}}_{22} - (\overline{\Delta \overline{A}}_{21} (E \overline{C}_2)^+ - \underline{\Delta \overline{A}}_{21} (E \overline{C}_2)^-) \\
\overline{\Gamma}(\overline{y}_k^+, \overline{y}_k^-) = \overline{M} \overline{y}_k^+ - \underline{M} \overline{y}_k^- \cdot \Gamma(\overline{y}_k^+, \overline{y}_k^-) = \underline{M} \overline{y}_k^+ - \overline{M} \overline{y}_k^- \n\end{cases}
$$

and

$$
\begin{cases}\n\overline{M} = (P^+\overline{D}_2 - P^-\underline{D}_2) + PLN_{12}^T \\
\underline{M} = (P^+\underline{D}_2 - P^-\overline{D}_2) + PLN_{12}^T \\
\overline{D}_2 = \tilde{A}_{21}E + (\overline{\Delta A}_{21}E^+ - \underline{\Delta A}_{21}E^-) \\
\underline{D}_2 = \tilde{A}_{21}E + (\underline{\Delta A}_{21}E^+ - \overline{\Delta A}_{21}E^-) \\
\overline{\vartheta}(\overline{v}, \underline{v}) = \overline{M}^+\overline{v}^+ - \underline{M}^+\overline{v}^- - \overline{M}^-\underline{v}^+ + \underline{M}^-\underline{v}^- \\
\underline{\vartheta}(\overline{v}, \underline{v}) = \underline{M}^+\underline{v}^+ - \overline{M}^+\underline{v}^- - \underline{M}^-\overline{v}^+ + \overline{M}^-\overline{v}^- \\
\overline{\Delta}(\overline{\tilde{w}}_2, \overline{\tilde{w}}_2) = P^+\overline{\tilde{w}}_2 - P^-\overline{\tilde{w}}_2 \\
\underline{\Delta}(\overline{\tilde{w}}_2, \overline{\tilde{w}}_2) = P^+\overline{\tilde{w}}_2 - P^-\overline{\tilde{w}}_2\n\end{cases} (15)
$$

Since  $\Delta A(\rho)$  is assumed to be bounded such that  $\Delta A \leq$  $\Delta A(\rho) \leq \overline{\Delta A}$ , it follows that  $\Delta \tilde{A} \leq \Delta \tilde{A}(\rho) = H^T \Delta A(\rho) H \leq$  $\overline{\Delta A}$ , where  $\overline{\Delta A} = ((H^T)^+ \overline{\Delta A} - (H^T)^- \underline{\Delta A})H^+ - ((H^T)^+ \underline{\Delta A} (H^T)^{-} \overline{\Delta A} H^{-}$ ,  $\Delta \tilde{A} = ((H^T)^{+} \Delta A - (H^T)^{-} \overline{\Delta A}) H^{+} - ((H^T)^{+} \overline{\Delta A} (H<sup>T</sup>)<sup>-</sup> ∆*A*)*H*<sup>-</sup>. Therefore,$ 

$$
\overline{\Delta \tilde{A}} = \left[ \frac{\overline{\Delta \tilde{A}}_{11}}{\Delta \tilde{A}_{21}} \frac{\overline{\Delta \tilde{A}}_{12}}{\Delta \tilde{A}_{22}} \right], \underline{\Delta \tilde{A}} = \left[ \frac{\underline{\Delta \tilde{A}}_{11}}{\underline{\Delta \tilde{A}}_{21}} \frac{\Delta \tilde{A}_{12}}{\underline{\Delta \tilde{A}}_{22}} \right]
$$

Denote by  $\overline{e}_{r_{2,k}} = \overline{r}_{2,k} - r_{2,k}$  and  $\underline{e}_{r_{2,k}} = r_{2,k} - \underline{r}_{2,k}$  the interval estimation errors; their dynamics follow:

$$
\begin{cases} \overline{e}_{r_{2,k+1}} = R \overline{e}_{r_{2,k}} + \overline{\phi}_k + \overline{\delta}_k\\ \underline{e}_{r_{2,k+1}} = R \underline{e}_{r_{2,k}} + \underline{\phi}_k + \underline{\delta}_k \end{cases}
$$
(16)

where

$$
\begin{cases}\n\overline{\phi}_k = \overline{\phi}(\overline{r}_{2,k}, \underline{r}_{2,k}) - P\Delta \tilde{A}_2(\rho) S r_{2,k} \\
\frac{\phi_k}{\overline{\delta}_k} = P\Delta \tilde{A}_2(\rho) S r_{2,k} - \underline{\phi}(\overline{r}_{2,k}, \underline{r}_{2,k}) \\
\overline{\delta}_k = \overline{\Gamma}(y_k^+, y_k^-) - M(\rho) y_k - \underline{\vartheta}(\overline{v}, \underline{v}) + M(\rho) v_k \\
+ \overline{\Delta}(\overline{\tilde{w}}_2, \underline{\tilde{w}}_2) - P \tilde{w}_{2,k} \\
\underline{\delta}_k = M(\rho) y_k - \underline{\Gamma}(y_k^+, y_k^-) - M(\rho) v_k + \overline{\vartheta}(\overline{v}, \underline{v}) \\
+ P \tilde{w}_{2,k} - \underline{\Delta}(\overline{\tilde{w}}_2, \underline{\tilde{w}}_2)\n\end{cases} (17)
$$

The functions  $\phi$  and  $\phi$  are globally Lipschitz. Using Lemma 6 in (Zheng et al. [2016]), it follows that for  $\underline{e}_{r_{2,k}} \leq e_{r_{2,k}} \leq \overline{e}_{r_{2,k}}$ and for a chosen submultiplicative norm |.|, there exist positive constants  $a_1$ ,  $a_2$ ,  $a_3$ ,  $b_1$ ,  $b_2$  and  $b_3$  such that:

$$
\begin{cases} |\overline{\phi}_k| \leq a_1 |\overline{e}_{r_{2,k}}| + a_2 |\underline{e}_{r_{2,k}}| + a_3 \\ |\underline{\phi}_k| \leq b_1 |\overline{e}_{r_{2,k}}| + b_2 |\underline{e}_{r_{2,k}}| + b_3 \end{cases}
$$
(18)

*Theorem 1.* Assume that Assumptions 1-4 are satisfied, *R* is nonnegative and the initial state  $r_{2,0}$  verifies  $r_{2,0} \le r_{2,0} \le \overline{r}_{2,0}$ . Then, for all  $k \in \mathbb{R}_+$  the state  $r_{2,k}$  solution of the system (12) satisfies:

$$
\underline{r}_{2,k} \le r_{2,k} \le \overline{r}_{2,k} \tag{19}
$$

In addition, if there exist matrices  $P_1 \in \mathbb{R}^{n \times n}, P_1 = P_1^T \succ 0$ ,  $W \in \mathbb{R}^{n \times n}, W = W^T \succ 0, Q \in \mathbb{R}^{n \times n}, Q = Q^T \succ 0$  and constants  $\gamma > 0$ , such that the following matrix inequality is verified:

$$
\Psi = \begin{bmatrix} \Upsilon & G^T P_1 & G^T P_1 \\ P_1 G & P_1 - \gamma I_n & P_1 \\ P_1 G & P_1 & P_1 - W \end{bmatrix} \prec 0, \tag{20}
$$

$$
\Upsilon = G^T P_1 G - P_1 + \gamma \alpha^2 I_n + Q, G = \begin{bmatrix} R & 0 \\ 0 & R \end{bmatrix},
$$

with  $\alpha = 2 \max\{(a_1 + b_1), (a_2 + b_2)\}\)$ . Then  $\overline{e}_{r_{2,k}}, \underline{e}_{r_{2,k}} \in \mathcal{L}_{\infty}^n$ .  $\Box$ 

**Proof.** Since *R* is assumed to be nonnegative, and by construction  $\overline{\phi}_k$ ,  $\underline{\phi}_k$ ,  $\delta_k$  and  $\underline{\delta}_k$  are nonnegative, then if  $\overline{r}_{2,0}$  and  $\underline{r}_{2,0}$  are chosen such that  $\overline{e}_0$  and  $\underline{e}_0$  are nonnegative, the dynamics of interval estimation errors  $\overline{e}_{r_{2,k}}$  and  $\underline{e}_{r_{2,k}}$  stay nonnegative for all  $k \in \mathbb{N}$ .

For the stability analysis, we introduce the auxiliary system:

$$
\xi_{r_{2,k+1}} = G\xi_{r_{2,k}} + \phi(\xi_{r_{2,k}}) + \delta_k
$$
 (21)

where  $\xi_{r_{2,k}} =$  $\left[e_{r_{2,k}}\right]$  $\overline{e}_{r_{2,k}}$ 1 ,  $\phi_k =$  $\left[\frac{\phi}{k}\right]$  $\phi_k$ 1 ,  $\delta_k =$  $\left[\frac{\delta}{k}\right]$  $\delta_k$  $\Bigg], \delta_k \in \mathscr{L}^{2n}_{\infty}$ . Using equation (18), it is clear that  $|\phi(\xi_{r_{2,k}})| \leq \alpha |\xi_{r_{2,k}}|$ . The constant  $\alpha$  does not depend on  $a_3$  and  $b_3$ . For brevity, the calculus of  $|\phi(\xi_{r2,k})|$  is omitted.

To establish the stability of the system (13), consider the positive definite quadratic Lyapunov function:

$$
V_k = \xi_{r_{2,k}}^T P_1 \xi_{r_{2,k}} \tag{22}
$$

The increment of ∆*V* is given by:

$$
\Delta V = V_{k+1} - V_k
$$
\n
$$
= \xi_{r_{2,k}}^T G^T P_1 G \xi_{r_{2,k}} - \xi_{r_{2,k}}^T P_1 \xi_{r_{2,k}} + \xi_{r_{2,k}}^T G^T P_1 \phi (\xi_{r_{2,k}})
$$
\n
$$
+ \phi^T (\xi_{r_{2,k}}) P_1 G \xi_{r_{2,k}} + \phi^T (\xi_{r_{2,k}}) P_1 \phi (\xi_{r_{2,k}})
$$
\n
$$
+ 2 \xi_{r_{2,k}}^T G^T P_1 \delta_k + 2 \delta_k^T P_1 \phi (\xi_{r_{2,k}}) + \delta_k^T P_1 \delta_k
$$
\n
$$
\leq \xi_{r_{2,k}}^T (G^T P_1 G - P_1) \xi_{r_{2,k}} + \xi_{r_{2,k}}^T G^T P_1 \phi (\xi_{r_{2,k}})
$$
\n
$$
+ \phi^T (\xi_{r_{2,k}}) P_1 G \xi_{r_{2,k}} + \phi^T (\xi_{r_{2,k}}) P_1 \phi (\xi_{r_{2,k}})
$$
\n
$$
+ 2 \xi_{r_{2,k}}^T G^T P_1 \delta_k + 2 \delta_k^T P_1 \phi (\xi_{r_{2,k}}) + \delta_k^T (P_1 - W) \delta_k
$$
\n
$$
+ \gamma \alpha^2 \xi_{r_{2,k}}^T \xi_{r_{2,k}} - \gamma \phi^T (\xi_{r_{2,k}}) \phi (\xi_{r_{2,k}}) + \xi_{r_{2,k}}^T Q \xi_{r_{2,k}}
$$
\n
$$
- \xi_{r_{2,k}}^T Q \xi_{r_{2,k}} + \delta_k^T W \delta_k
$$
\n
$$
\leq \begin{bmatrix} \xi_{r_{2,k}} \\ \phi (\xi_{r_{2,k}}) \end{bmatrix}^T \Psi \begin{bmatrix} \xi_{r_{2,k}} \\ \phi (\xi_{r_{2,k}}) \end{bmatrix} - \xi_{r_{2,k}}^T Q \xi_{r_{2,k}} + \delta_k^T W \delta_k
$$

Then, the system (13) is ISS stable and  $\zeta_{r_{2,k}}$  is bounded.  $\Box$ 

Since  $r_2 = Pz_2$ , it follows that  $z_{2,k} \leq z_{2,k} \leq \overline{z}_{2,k}$  with:

$$
\begin{cases} \overline{z}_{2,k} = S^+ \overline{r}_{2,k} - S^- \underline{r}_{2,k} \\ \underline{z}_{2,k} = S^+ \underline{r}_{2,k} - S^- \overline{r}_{2,k} \end{cases}
$$
(23)

As  $x_k = Hz_k$  and based on (10), it follows that:

$$
\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix} \begin{bmatrix} E(y_k - \tilde{C}_{2}z_{2,k} - v_k) \\ z_{2,k} \end{bmatrix}
$$
 (24)

Therefore

 $\begin{bmatrix} \phantom{-} \end{bmatrix}$ 

$$
\begin{cases} x_{1,k} = H_{11} E y_k + E_{122,k} + H_{122,k} - E_{2} v_k \\ x_{2,k} = H_{21} E y_k + E_{322,k} + H_{222,k} - E_4 v_k \end{cases}
$$
 (25)

The bounds of the state  $x_k$  are given by:

$$
\begin{cases}\n\overline{x}_{1,k} = H_{11}E y_k + H_{12}^+ \overline{z}_{2,k} - H_{12}^- \underline{z}_{2,k} + (-E_1)^+ \overline{z}_{2,k} \\
-(-E_1)^- \underline{z}_{2,k} + (-E_2)^+ \overline{v} - (-E_2)^- \underline{v} \\
\underline{x}_{1,k} = H_{11}E y_k + H_{12}^+ \underline{z}_{2,k} - H_{12}^- \overline{z}_{2,k} + (-E_1)^+ \underline{z}_{2,k} \\
-(-E_1)^- \overline{z}_{2,k} + (-E_2)^+ \underline{v} - (-E_2)^- \overline{v} \\
\overline{x}_{2,k} = H_{21}E y_k + H_{22}^+ \overline{z}_{2,k} - H_{22}^- \underline{z}_{2,k} + (-E_3)^+ \overline{z}_{2,k} \\
-(-E_3)^- \underline{z}_{2,k} + (-E_4)^+ \overline{v} - (-E_4)^- \underline{v} \\
\underline{x}_{2,k} = H_{21}E y_k + H_{22}^+ \underline{z}_{2,k} - H_{22}^- \overline{z}_{2,k} + (-E_3)^+ \underline{z}_{2,k} \\
-(-E_3)^- \overline{z}_{2,k} + (-E_4)^+ \underline{v} - (-E_4)^- \overline{v} \\
E_k + H_k^- \overline{E}_k - H_k^- \overline{E}_k^* \overline{v} + H_k^- \overline{E}_k - H_k^- \overline{E}_k^* \overline{v} + H_k^- \overline{E}_k - H_k^- \overline{v} + H_k^+ \overline{v} + H_k^- \overline{v} + H_k^- \overline{v} + H
$$

with  $E_1 = H_{11}E\tilde{C}_2$ ,  $E_2 = H_{11}E$ ,  $E_3 = H_{21}E\tilde{C}_2$  and  $E_4 = H_{21}E$ .

*Theorem 2.* Assume that the conditions of Theorem 1 are satisfied and  $x_0 \le x_0 \le \overline{x}_0$ . Then, for all  $k \in \mathbb{Z}_+$  the estimates  $x_k = \left[\frac{x_{1,k}}{x_{2,k}}\right]$ *x*2,*<sup>k</sup>* and  $\overline{x}_k = \left[\frac{\overline{x}_{1,k}}{\overline{x}_{2,k}}\right]$ *x*2,*<sup>k</sup>* � satisfies:  $x_k \le x_k \le \overline{x}_k.$  (27)

where  $x_k$  and  $\overline{x}_k$  are given by (26).

**Proof.** Introducing the observation errors for the state *xk*:

$$
\begin{cases}\n\overline{e}_{x_1,k} = \overline{x}_{1,k} - x_{1,k} \\
\underline{e}_{x_1,k} = x_{1,k} - \underline{x}_{1,k} \\
\overline{e}_{x_2,k} = \overline{x}_{2,k} - x_{2,k} \\
\underline{e}_{x_2,k} = x_{2,k} - \underline{x}_{2,k}\n\end{cases} (28)
$$

Then, we obtain:

$$
\begin{cases}\n\overline{e}_{x_1,k} = (H_{12}^+ + (-E_1)^+) \overline{e}_{z_2} - (H_{12}^- + (-E_1)^-) \underline{e}_{z_2} \\
+ (-E_2)^+ (\overline{v} - v_k) - (-E_2)^- (\overline{v} + v_k) \\
\underline{e}_{x_1,k} = (H_{12}^+ + (-E_1)^+) \underline{e}_{z_2} - (H_{12}^- + (-E_1)^-) \overline{e}_{z_2} \\
+ (-E_2)^+ (\overline{v} + v_k) - (-E_2)^- (\overline{v} - v_k) \\
\overline{e}_{x_2,k} = (H_{22}^+ + (-E_1)^+) \overline{e}_{z_2} - (H_{22}^- + (-E_1)^-) \underline{e}_{z_2} \\
+ (-E_2)^+ (\overline{v} - v_k) - (-E_2)^- (\overline{v} + v_k) \\
\underline{e}_{x_2,k} = (H_{22}^+ + (-E_3)^+) \underline{e}_{z_2} - (H_{22}^- + (-E_3)^-) \overline{e}_{z_2} \\
+ (-E_4)^+ (\overline{v} + v_k) - (-E_4)^- (\overline{v} - v_k)\n\end{cases} (29)
$$

Similarly to Proof 1, the observation errors (29) are nonnegative. Therefore,  $\underline{x}_k \le x_k \le \overline{x}_k$ ,  $\forall k \ge k_0$ . By defining  $\xi_x =$  $\left[\overline{e}_{x_1}^T \ \underline{e}_{x_1}^T \ \overline{e}_{x_1}^T \ \underline{e}_{x_1}^T \right]^T$  and the matrices

$$
\mathfrak{F} = \begin{bmatrix}\nH_{12}^+ + (-E_1)^+ & H_{12}^- + (-E_1)^- \\
H_{12}^- + (-E_1)^- & H_{12}^+ + (-E_1)^+ \\
H_{22}^+ + (-E_3)^+ & H_{22}^- + (-E_3)^- \\
H_{22}^- + (-E_3)^- & H_{22}^+ + (-E_3)^+ \\
H_{22}^- + (-E_2)^+ - (-E_2)^- \\
-(-E_2)^+ + (-E_2)^+ \\
(-E_4)^+ - (-E_4)^-\n\end{bmatrix},
$$

Therefore,  $\xi_x \leq \mathfrak{F}\xi_{z_2} + 2\mathfrak{J}\overline{\nu}$ . We have  $\xi_{z_2} = \mathfrak{R}\xi_{r_{2,k}}$  with  $\mathfrak{R} =$  $\begin{bmatrix} R^+ & -R^- \end{bmatrix}$ −*R*<sup>−</sup> *R*<sup>+</sup> . It follows that  $\xi_x \leq \mathfrak{F} \mathfrak{R} \xi_{r_{2,k}} + 2 \mathfrak{J} \overline{\nu}$ . Since  $\xi_{r_{2,k}}$  is bounded, it can be deduced that  $\xi_x$  is bounded as well.  $\Box$ 

# *4.2 Fault Estimation*

From equation (9), the fault vector can be expressed as:

$$
f_k = K_0 R_0^{-1} [z_{1,k+1} - \tilde{A}_{11} z_{1,k} - \Delta \tilde{A}_{11}(\rho) z_{1,k} - \tilde{A}_{12} z_{2,k} - \Delta \tilde{A}_{12}(\rho) z_{2,k} - \tilde{B}_1 u_k - \tilde{w}_{1,k}]
$$
(30)

Replacing  $z_1$  with its expression in (10), equation (30) becomes:

$$
f_k = K_0 R_0^{-1} [E y_{k+1} + G_{1Z} z_{k+1} + (-E) v_{k+1} - G_2(\rho) y_k + G_3 z_{2,k} + G_4(\rho) z_{2,k} + G_2(\rho) v_k - \tilde{B}_1 u_k - \tilde{w}_{1,k}]
$$
(31)

with  $G_1 = -E\tilde{C}_2$ ,  $G_2(\rho) = (\tilde{A}_{11} + \Delta \tilde{A}_{11}(\rho))E$ ,  $G_3 = \tilde{A}_{11}E\tilde{C}_2$  $\tilde{A}_{12}$  and  $G_4(\rho) = \Delta \tilde{A}_{11}(\rho) E \tilde{C}_2 - \Delta \tilde{A}_{12}(\rho)$ . The bounds of the actuator fault vector are given by:

$$
\begin{cases}\n\overline{f}_k = K_0 R_0^{-1} [E y_{k+1} - \underline{\Gamma}_f (y_{k+1}^+, y_{k+1}^-) + \overline{\varphi}_1 (\overline{z}_{2,k+1}, \underline{z}_{2,k+1}) \\
+ \overline{\vartheta}_1 (\overline{v}, \underline{v}) + \overline{\varphi}_2 (\overline{z}_{2,k}, \underline{z}_{2,k}) + \overline{\vartheta}_2 (\overline{v}, \underline{v}) + \overline{\varphi}_3 (\overline{z}_{2,k}, \underline{z}_{2,k}) \\
-\tilde{B}_1 u_k - \underline{\tilde{w}}_1] \\
\underline{f}_k = K_0 R_0^{-1} [E y_{k+1} - \overline{\Gamma}_f (y_{k+1}^+, y_{k+1}^-) + \underline{\varphi}_1 (\overline{z}_{2,k+1}, \underline{z}_{2,k+1}) \\
+ \overline{\vartheta}_1 (\overline{v}, \underline{v}) + \underline{\varphi}_2 (\overline{z}_{2,k}, \underline{z}_{2,k}) + \underline{\vartheta}_2 (\overline{v}, \underline{v}) + \underline{\varphi}_3 (\overline{z}_{2,k}, \underline{z}_{2,k}) \\
-\tilde{B}_1 u_k - \overline{\tilde{w}}_1]\n\end{cases}
$$
\n(32)

with

$$
\begin{cases}\n\Gamma_f(y_{k+1}^+, y_{k+1}^-) = \overline{G}_2 y_{k+1}^+ - \underline{G}_2 y_{k+1}^- \\
\Gamma_f(y_{k+1}^+, y_{k+1}^-) = \underline{G}_2 y_{k+1}^+ - \overline{G}_2 y_{k+1}^- \\
\overline{\varphi}_1(\overline{z}_{2,k+1}, \underline{z}_{2,k+1}) = G_1^+ \overline{z}_{2,k+1} - G_1^- \underline{z}_{2,k+1}^- \\
\underline{\varphi}_1(\overline{z}_{2,k+1}, \underline{z}_{2,k+1}) = G_1^+ \underline{z}_{2,k+1} - G_1^- \overline{z}_{2,k+1}^-\n\end{cases}
$$
\n(33)  
\n
$$
\begin{cases}\n\overline{\varphi}_2(\overline{z}_{2,k}, \underline{z}_{2,k}) = G_3^+ \overline{z}_{2,k} - G_3^- \overline{z}_{2,k}^-\n\end{cases}
$$
\n(33)  
\n
$$
\begin{cases}\n\overline{\varphi}_2(\overline{z}_{2,k}, \underline{z}_{2,k}) = G_3^+ \underline{z}_{2,k} - G_3^- \overline{z}_{2,k}^-\n\end{cases}
$$
\n(34)  
\n
$$
\overline{\varphi}_3(\overline{z}_{2,k}, \underline{z}_{2,k}) = \overline{G_4}^+ \overline{z}_{2,k}^+ - \overline{G_4}^+ \overline{z}_{2,k}^- - \overline{G_4}^- \overline{z}_{2,k}^+ + \overline{G_4}^- \overline{z}_{2,k}^- \\
\underline{\varphi}_3(\overline{z}_{2,k}, \underline{z}_{2,k}) = \underline{G_4}^+ \underline{z}_{2,k}^+ - \overline{G_4}^+ \underline{z}_{2,k}^- - \overline{G_4}^- \overline{z}_{2,k}^+ + \overline{G_4}^- \overline{z}_{2,k}^-\n\end{cases}
$$

and

$$
\begin{cases}\n\overline{\vartheta}_{1}(\overline{v},\underline{v}) = (-E)^{+}\overline{v} - (-E)^{-}\underline{v} \\
\frac{\vartheta}{\vartheta}_{1}(\overline{v},\underline{v}) = (-E)^{+}\underline{v} - (-E)^{-}\overline{v} \\
\overline{\vartheta}_{2}(\overline{v},\underline{v}) = \overline{G_{2}}^{+}\overline{v}^{+} - \underline{G_{2}}^{+}\overline{v}^{-} - \overline{G_{2}}^{-}\underline{v}^{+} + \underline{G_{2}}^{-}\underline{v}^{-} \\
\frac{\vartheta}{\vartheta}_{2}(\overline{v},\underline{v}) = \underline{G_{2}}^{+}\underline{v}^{+} - \overline{G_{2}}^{+}\underline{v}^{-} - \underline{G_{2}}^{-}\overline{v}^{+} + \overline{G_{2}}^{-}\overline{v}^{-} \\
\overline{G}_{4} = (\overline{\Delta A}_{11}(E\tilde{C}_{2})^{+} - \underline{\Delta A}_{11}(E\tilde{C}_{2})^{-}) - \underline{\Delta A}_{12} \\
\underline{G}_{4} = (\underline{\Delta A}_{11}(E\tilde{C}_{2})^{+} - \overline{\Delta A}_{11}(E\tilde{C}_{2})^{-}) - \overline{\Delta A}_{12} \\
\overline{G}_{2} = \tilde{A}_{11}E + (\overline{\Delta A}_{11}E^{+} - \underline{\Delta A}_{11}E^{-}) \\
\underline{G}_{2} = \tilde{A}_{11}E + (\underline{\Delta A}_{11}E^{+} - \overline{\Delta A}_{11}E^{-})\n\end{cases} (34)
$$

*Theorem 3.* Assume that the conditions of Theorem 1 are satisfied. Then, for all  $k \in \mathbb{Z}_+$  the estimates  $\overline{f}_k$  and  $\underline{f}_k$  satisfies:

$$
\underline{f}_k \le f_k \le \overline{f}_k. \tag{35}
$$

where  $\underline{f}_k$  and  $\overline{f}_k$  are given by (32).

**Proof.** The lower and upper observation errors of the fault vector are given by:  $\overline{e}_{f,k} = \overline{f}_k - f_k$  and  $\underline{e}_{f,k} = f_k - \underline{f}_k$ . Then, we obtain:

$$
\begin{cases} \overline{e}_{f,k} = K_0 R_0^{-1} [G_1^+ \overline{e}_{z_{2,k+1}} - G_1^- \underline{e}_{z_{2,k+1}} + G_3^+ \overline{e}_{z_{2,k}} - G_3^- \underline{e}_{z_{2,k}} \\ + \overline{\varphi}_3 - \varphi_3 + \overline{\delta}_{f,k}] \\ \underline{e}_{f,k} = K_0 R_0^{-1} [G_1^+ \underline{e}_{z_{2,k+1}} - G_1^- \overline{e}_{z_{2,k+1}} + G_3^+ \underline{e}_{z_{2,k}} - G_3^- \overline{e}_{z_{2,k}} \\ - \underline{\varphi}_3 + \varphi_3 + \underline{\delta}_{f,k}] \end{cases} \tag{36}
$$

with  $\varphi_3 = G_4(\rho)z_{2,k}, \ \overline{\delta}_{f,k} = (-E)^+(\overline{\nu}-\nu_{k+1}) - (-E)^-(\overline{\nu}+$  $v_{k+1}) + (\overline{\tilde{w}}_1 + \tilde{w}_1) + \overline{\vartheta}_2 - G_2v_k - \underline{\Gamma} + G_2y_k, \underline{\delta}_{f,k} = (-E)^+(\overline{v} + \overline{\zeta})$  $(v_{k+1}) - (-E)^{-}(\overline{v} - v_{k+1}) + (\overline{\tilde{w}}_1 - \tilde{w}_1) + G_2v_k - \underline{\vartheta}_2 + \overline{\Gamma} - G_2y_k.$ With the same reasoning as in the proof of Theorem 1, it is deduced from (36) that the fault observation errors are positive. Since  $\overline{e}_{z_2}, \underline{e}_{z_2}, v$  and  $\tilde{w}_1$  are bounded, then  $\overline{f}$  and  $f$  are bounded as well.

The functions  $\overline{\varphi}_3$  and  $\varphi_3$  are globally Lipschitz. Using Lemma 6 in (Zheng et al. [2016]), it follows that for  $\underline{e}_{z_2,k} \leq e_{z_2,k} \leq \overline{e}_{r,k}$ and for a chosen submultiplicative norm |.|, there exist positive constants  $c_1$ ,  $c_2$ ,  $c_3$ ,  $d_1$ ,  $d_2$  and  $d_3$  such that:

$$
\begin{cases} |\overline{\varphi}_k - \varphi_k| \leqslant c_1 |\overline{e}_{z_2,k}| + c_2 |\underline{e}_{z_2,k}| + c_3 \\ |\underline{\varphi}_k - \varphi_k| \leqslant d_1 |\overline{e}_{z_2,k}| + d_2 |\underline{e}_{z_2,k}| + d_3 \end{cases} \tag{37}
$$

If we define 
$$
\xi_f = \begin{bmatrix} \overline{e}_f \\ \frac{e}{f} \end{bmatrix}
$$
,  $\mathfrak{F}_1 = \begin{bmatrix} |G_1^+| & |-G_1^-| \\ |-G_1^-| & |G_1^+| \end{bmatrix}$ ,  $\mathfrak{F}_2 = \begin{bmatrix} |G_3^+| & |-G_3^-| \\ |-G_3^-| & |G_3^+| \end{bmatrix}$ ,  $\mathfrak{F}_3 = \begin{bmatrix} c_1 & c_2 \\ d_1 & d_2 \end{bmatrix}$ ,  $\overline{\delta} = |\overline{\delta}_{f,k}| + c_3$  and  $\underline{\delta} = |\underline{\delta}_{f,k}| + d_3$ . It follows that

$$
|\xi_f| \le |K_0 R_0^{-1}|(\mathfrak{F}_1 + \mathfrak{F}_2 + \mathfrak{F}_3)|\xi_z| + \left[\frac{\overline{\delta}}{\underline{\delta}}_{f,k}\right]
$$
(38)

 $\operatorname{As} |\xi_{z_2}| = |\Re| |\xi_{r_2,k}|$ , we obtain

$$
|\xi_f| \le |K_0 R_0^{-1}|(\mathfrak{F}_1 + \mathfrak{F}_2 + \mathfrak{F}_3)|\mathfrak{R}||\xi_{r_{2,k}}| + \begin{bmatrix} \overline{\tilde{\delta}}_{f,k} \\ \underline{\tilde{\delta}}_{f,k} \end{bmatrix}
$$
(39)

As  $\xi_{r_{2,k}}$  is bounded, it follows that  $\xi_f$  as well.  $\Box$ 

### 5. NUMERICAL EXAMPLE

Consider an LPV system described by:

$$
\begin{cases}\n x_{k+1} = (A + \Delta A(\rho))x_k + Bu_k + Ff_k + w_k \\
 y_k = Cx_k + v_k\n\end{cases}
$$
\n(40)\nwhere:  $A = \begin{bmatrix} -1 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & -1 & -1 \end{bmatrix}$ ,  $C = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$ ,  $B = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$ ,  $F = \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix}$ \n
$$
\begin{bmatrix} 0.1\rho_{1,k} & 0.5 & 0.1 \end{bmatrix}
$$

$$
\Delta A(\rho) = \begin{bmatrix} 0.1\rho_{1,k} & 0.5 & 0.1 \\ 0.1 & 0.2 & 0.4 \\ 0.3 & 0.5 & 0.05\rho_{2,k} \end{bmatrix}.
$$

with  $\rho_{1,k} = \sin(0.2 k)$  and  $\rho_{2,k} = \cos(0.1 k)$ . The disturbance  $v_k$  and the measurement noise  $w_k$  are uniformly distributed signals assumed to belong to the interval [−0.01 0.01] and [−0.01 0.01], respectively. The actuator fault is simulated by  $f_k = cos(0.5 k)$ .

Since *F* is full column rank matrix and *C* is a full row rank matrix, Assumption 3 is satisfied and a transformation of coordinates  $z_k = H^T x_k$  is required with  $H =$  $\lceil -100 \rceil$ 0 10  $\left[\begin{smallmatrix} -1 & 0 & 0 \ 0 & 1 & 0 \ 0 & 0 & 1 \end{smallmatrix}\right]$ ,  $K_0 = 1, R_0 =$ 1. Then, the system (40) can be described in the coordinates *z*

by equation (8).

The matrix  $\tilde{C}_1$  can be decomposed as:  $\tilde{C}_1 = N [R_1 \ 0]^T K_1^T$ , with  $N = \begin{bmatrix} -1 & 0 \ 0 & 1 \end{bmatrix}, R_1 = 1, K_1 = 1.$ 

 $\text{For } L = [-0.3 \quad -2.1]^T, A_2 = \begin{bmatrix} 0 & 0 \\ 1 & 1 \end{bmatrix}$  $-1 -1$ and  $C_2 = \begin{bmatrix} 0 & 1 \end{bmatrix}$ , the matrix  $A_2 - LC_2 = \begin{bmatrix} 0 & 0.3 \\ 1 & 1.1 \end{bmatrix}$ −1 1.1 � is not nonnegative. Thus, using a transformation of coordinates  $P = \begin{bmatrix} 10 & -5 \\ -10 & 6 \end{bmatrix}$ , the matrix  $R = P(A_2 - LC_2)P^{-1} = \begin{bmatrix} 0.5 & 0 \\ 0 & 0 \end{bmatrix}$ 0 0.6 � is nonnegative. Then, all the conditions of Theorem 1 are satisfied with  $\alpha = 0.057$  and the matrix inequality (20) is feasible.

The initial states are chosen as  $x_0 = [1 \ 1 \ 1]^T$ ,  $\overline{x}_0 = [1.5 \ 1.5 \ 1.5]^T$ ,  $x_0 = [0.5 \, 0.5 \, 0.5]^T$ . The state and fault estimation bounds are computed using (26) and (32), respectively, and the results are given in Figure 1, Figure 2 and Figure 3.



Fig. 1. Evolution of the second component of state  $x_2$ .



Fig. 2. Evolution of the third component of state  $x_3$ .



Fig. 3. Evolution of the fault *fk*.

The simulation results show that the upper and the lower bounds of the state and fault estimation converge to an interval despite the presence of measurement noise and disturbances.

## 6. CONCLUSION

A methodology for actuator fault estimation for discrete-time LPV systems has been proposed in this paper. The actuator fault is considered as an unknown input. An unknown input interval observer is designed to estimate the system state and the fault under the assumption that the exogenous disturbances and the measurement noises are bounded. Based on Lyapunov theory, stability conditions are given in terms of matrices inequality. Simulation results show the robustness of the proposed approach.

The design of Active Fault Tolerant Control and its interaction with fault identification module will be investigated in further works.

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