

# Understanding the removal of V, Ni and S in crude oil atmospheric residue hydrodemetallization and hydrodesulfurization

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- <sup>1</sup> Understanding the removal of V, Ni and S in crude
- <sup>2</sup> oil atmospheric residue hydrodemetallization and

# <sup>3</sup> hydrodesulfurization

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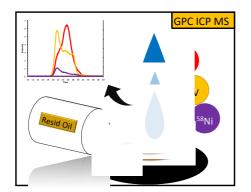
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- 11 KEYWORDS: Vanadium, nickel, sulfur, demetallization, desulfurization, catalysis, residue,
- 12 GPC.
- 13

#### 14 ABSTRACT

This study describes the use of gel permeation chromatography inductively coupled plasma highresolution mass spectrometry (GPC ICP HRMS) to examine and explain two important
petroleum industry catalytic processes: hydrodemetallization (HDM) and hydrodesulfurization
(HDS).

19 The sulfur, nickel and vanadium species size distributions in atmospheric residue fractions were studied to track their evolution during both catalytic processes and examine their mechanisms, 20 especially those mechanisms linked to changes in temperature and initial deactivation via coke 21 22 laydown. Chromatogram shapes as well as peak areas were used to study the V, Ni and S aggregate types and concentrations in the feedstock as well as in the product after varying the 23 24 operating temperature and residence time at a constant temperature. For the V and Ni 25 compounds, the low and medium molecular weight (LMW and MMW, respectively) aggregates are easily hydrotreated under all conditions, while the high molecular weight (HMW) 26 27 compounds are more refractory. For the S compounds, a different reactivity pattern was observed whereby the LMW, MMW and HMW aggregates were more similar in their reactivity, showing 28 29 that the catalyst is less selective towards a certain aggregate size for the S compounds compared 30 to the V or Ni compounds.

31 TOC GRAPHIC



### 33 INTRODUCTION

Hydroprocessing atmospheric residues using fixed-bed reactors is a mature technology that has 34 been extensively studied, and close to 100 units are in operation across the globe.<sup>1</sup> Most of these 35 units are located in Asia and the Middle East, and the total catalyst demand is estimated to be 36 37 approximately 50,000 tons/year. This technology is still relevant for many refineries as it can 38 address key issues faced by the refining industry. For example, environmental specifications are getting stricter for bunker fuels as the revised MARPOL Annex VI will reduce the sulfur cap 39 from 3.5 to 0.5 wt% from 2020 on. Furthermore, heavier crude oils are being processed, and 40 those feedstocks require residue technologies such as atmospheric residue desulfurization 41 (ARDS). 42

Among the numerous elements present in crude oil, the most abundant and undesirable elements are sulfur, vanadium and nickel,<sup>2</sup> which have negative effects, such as catalyst poisoning, fouling and equipment corrosion.<sup>3,4</sup> The presence of sulfur compounds causes environmental and health problems as well, with the emission of toxic S species into the atmosphere.<sup>5,6</sup> With the purpose of reducing these undesirable effects, catalytic removal of these elements is currently carried out in the industry, especially for atmospheric and vacuum residue oils, whose content of these elements is much higher.

50 The ARDS process will be briefly described below, but various detailed reviews and their respective references can be consulted for further information about the process and its 51 evaluation.<sup>1,7,8</sup> The process consists of downflow trickle bed reactors in series with the following 52 catalyst loading distributed across several reactors<sup>9</sup>: large-pore guard hydrodemetallization 53 (HDM) catalyst (whose function is to trap V, Ni and As), a smaller-pore transition catalyst 54 combining HDM and hydrodesulfurization (HDS) activities and a third catalyst with a higher 55 56 HDS activity. The deactivation mechanisms of the catalysts in such a service have also been 57 widely studied over the years.<sup>10</sup> The initial step, which is quite rapid, is mostly due to coke formation.<sup>11</sup> This step is followed by a slower deactivation phase during which metals gradually 58 cover the catalyst surface.<sup>12</sup> The last phase is a rapid loss of activity where the metals and coke 59 create pore plugging or restrict access to the pore structure. 60

Many ARDS units are operated to obtain a fixed sulfur or Conradson carbon residue (CCR) content in the product. However, due to the difficult nature of the feedstock (high amount of metals and coke precursors), many challenges are encountered: short cycle length due to high deactivation rates, pressure-drop issues due to coking, demanding catalyst unloading process, long turnarounds (typically one month), etc. To minimize these issues, it is crucial that the optimal ratio between the HDM, HDM/HDS and HDS catalysts is determined for each specific ARDS unit.

The total amounts of Ni, V or S are an important piece of information here but do not provide any information about the nature of the molecules containing these elements. Therefore, speciation of the metals in the various feedstocks is an asset in regard to understanding the feed reactivity and the influence on the various deactivation mechanisms and ultimately in optimizing the catalyst loading. One option is to use inorganic speciation in crude oil that has been

73 developed by using size exclusion chromatography in an organic solvent linked with a high-74 resolution mass spectrometer working as the detector. This technique is referred to as gel permeation chromatography (GPC) and employs an organic solvent to perform the analysis, in 75 this case tetrahydrofurane (THF).<sup>4</sup> In this technique, the compounds are separated according to 76 their hydrodynamic volumes, which in the case of these samples follow the molecular weights of 77 the nanoaggregates and molecules that are present in the sample. By dissolving the sample in 78 79 THF, it is possible to obtain a fingerprint of the molecular distribution of the species present in 80 the sample and evaluate how the concentrations of each fraction increase or decrease as a function of the industrial process carried out. 81

Pohl et al.<sup>13</sup> successfully used this method for two crude oils and two residue fractions and 82 managed to map and fingerprint V, Ni, S, Fe, Co, Cr, Zn and Si. The distributions between high 83 molecular weight (HMW) aggregates (possibly asphaltene structures), medium molecular weight 84 85 (MMW) aggregates and low molecular weight (LMW) compounds (possibly free metal porphyrins and nonporphyrinic complexes) differ significantly between these samples, which 86 will affect the HDM and HDS activities and their relative deactivation rates. Gascon et al.<sup>14</sup> used 87 the same approach on the Saturate, Aromatic, Resin and Asphaltene (SARA) fractions of four 88 crude oils, one atmospheric residue and one vacuum residue. The amount of each type of 89 aggregate (HMW, MMW and LMW) was calculated, and significant variations can be observed 90 among the four crude oils and their residue fractions. However, to understand the significance of 91 these variations in the ARDS process, it is necessary to study not only the feedstock but also the 92 93 hydrotreated product to understand the reactivity of the various types of aggregates. With an increasing demand for low-sulfur fuel oil (LSFO), refineries are starting to consider 94

alternative usages for their ARDS units, for example, by coprocessing vacuum residues, which

96 are typically processed in ebullated bed reactors due to the high amount of metals and asphaltenes in this type of feed, which causes an extremely rapid deactivation of the catalyst. A 97 feedstock change often requires changing the operating conditions in the unit (e.g., by lowering 98 the feed rate to lower the liquid hourly space velocity) and redesigning the catalyst loading. The 99 latter is not always straightforward, as it requires a very thorough understanding of the feed and 100 its effect on the catalyst activity throughout the entire cycle to avoid untimely shutdowns. To this 101 102 end, a better understanding of not only the feed properties (contents of sulfur, nitrogen, 103 asphaltene, etc.) but also the molecular composition is invaluable. Thus, in this paper, two ARDS pilot plant studies are reported. In study A, the temperature was adjusted from 375 to 385 °C to 104 105 evaluate its influence on the reactivity of the various sulfur, nickel and vanadium species. In 106 study B, the fate of sulfur, nickel and vanadium nanoaggregates was monitored under constant 107 operating conditions to examine the role of the initial coke laydown on the HDM and HDS 108 reactions.

### 109 MATERIALS AND METHODS

#### 110 Instrumentation

A quantitative analysis of all the feedstocks was carried out with the purpose of determining 111 the mass variations of the target elements by using inductively coupled plasma mass 112 spectrometry (ICP-MS). The principle of the method is to determine the total amount of xylene-113 soluble Ni and V compounds with inductively coupled plasma mass spectrometry (ICP-MS) after 114 suitable dilution of the petroleum/petroleum product sample by weight with xylene. The 115 vanadium and nickel contents are quantified by ICP-MS using a vanadium-isotope mass of 51 116 117 and a nickel-isotope mass of 60 through comparison with calibration curves obtained via 500 wt ppm Conostan organometallic V and Ni standards diluted with xylene. Scandium is used as an 118

119 internal standard to correct for drift and matrix effects. The removal of molecular interferences in the ICP-MS analysis was performed with helium kinetic energy discrimination. EnviroMAT 120 used-oil matrix reference material containing V and Ni was analyzed with each sample batch to 121 monitor the analysis accuracy. The physico-chemical properties of the feeds and products were 122 measured using the following standard methods: Nitrogen (ASTM D5762), Sulfur (ASTM D 123 4294, Hydrogen (ASTM D 7171 H), asphaltene (ASTM D6560), microcarbon residue (MCR) 124 125 (ASTM D4530), specific gravity (SG) (ASTM D4052), and simulated distillation (ASTM 126 D7169). Carbon (wt %) content was calculated by difference with 100% with N, S and H content. 127 128 All the speciation analyses were carried out with a Thermo Scientific Element XR double focusing sector field ICP-MS (Thermo Fisher, Germany) instrument accessing the spectrally 129 interfered isotopes of <sup>32</sup>S, <sup>51</sup>V and <sup>58</sup>Ni at a resolution of 4,000 (medium resolution). The mass

interfered isotopes of <sup>32</sup>S, <sup>51</sup>V and <sup>58</sup>Ni at a resolution of 4,000 (medium resolution). The mass
spectrometer was equipped with a quartz injector (1.0 mm inner diameter (i.d.)), a Pt sampler
cone (1.1 mm orifice diameter) and a Pt skimmer cone (0.8 mm orifice diameter). An O<sub>2</sub> gas
flow of 0.08 mL/min was included to avoid carbon deposition. Both the instrument and mass
calibration settings were optimized daily at resolutions of 300 (low resolution) and 4,000. A
medium resolution avoids the spectral interference of O<sub>2</sub> on the <sup>32</sup>S isotope. These optimizations
were carried out using a tuning solution containing 1.0 ng g-1 of Ag, Al, B, Ba, Ca, Cd, Co, Cr,
Cu, Fe, In, K, Li, Mg, Mn, Mo, Na, Ni, P, Pb, Sc, Si, Sn, Ti, V, Zn and Y in tetrahydrofuran

138 (THF). A mass offset was also applied to compensate for the mass drift coming from the sector
139 field magnet.<sup>15,16</sup>

140 The mass spectrometer was equipped with a modified DS-5 microflow total consumption
141 nebulizer (CETAC, Omaha, NE) mounted with a laboratory-made jacketed spray chamber

heated to 60 °C by a water/glycol mixture working with a temperature-controller bath circulator
Neslab RTE-111 (Thermo Fisher Scientific, Waltham, MA).<sup>17</sup>

The chromatographic separation was carried out using three Waters (Waters Corporation, 144 Milford, MA) styrene-divinylbenzene gel permeation columns (7.8 mm i.d. and 300 mm length). 145 These three columns included an HR4 column (particle size of 5 µm with an exclusion limit of 146 600,000 Da of polystyrene equivalent), an HR2 column (particle size of 5 µm with an exclusion 147 148 limit of 20,000 Da) and an HR0.5 column (particle size of 5 µm and an exclusion limit of 1,000 149 Da of polystyrene equivalent). A Dionex high-performance liquid chromatography (HPLC) system fitted with an UltiMate 3,000 microflow pump, an UltiMate 3,000 autosampler and a low 150 151 port-to-port dead-volume microinjection valve were used to deliver the carrier solution and mobile phase. To prevent possible damage to the GPC columns, a Styragel guard column (4.6 152 mm i.d. and 30 mm length) was also fitted between the columns and the pumping system. 153 154 Methodology. One feed, which is a blend of 93% of atmospheric residue (ATM) and 7% vacuum residue (VAC), was hydrotreated under different conditions for the purpose of 155 evaluating and understanding the removal of the target compounds by applying the method 156 optimized by Desprez et al.<sup>16</sup> and Vargas et al.<sup>18</sup>. These researchers studied the size distributions 157 of V, Ni and S and established the integration intervals for HMW, MMW and LMW aggregates 158 in crude oil as follows: 1,100-1,400 s (18 – 23 mL of eluted sample) for HMW compounds, 159 1,400-1,600 s (23 – 27 mL) for MMW compounds and above 1,600 s (< 27 mL) for LMW 160 compounds. The comparison of the different sizes of species will provide useful information 161 about the removal of target compounds. 162

In addition, with the purpose of monitoring the stability of the ICP HR MS intensities, analysis
of known crude oil samples, whose composition had been studied previously, was periodically
carried out.

*Reagents, samples and solutions.* Tetrahydrofuran, multisolvent GPC grade, ACS, stabilized
 with 250 ppm of butylated hydroxytoluene (BHT) (Scharlau, Spain) to prevent the formation of
 peroxides, was used both for sample preparation and for chromatographic elution.

All the atmospheric residue crude oil feeds were provided by Haldor Topsoe (Denmark), and
the feeds were analyzed by diluting them in THF at dilution factors of 50 for the 93% ATM/7%
VAC feed blend and of 5 for the products.

172 *Pilot plant testing.* The pilot tests were performed in a once-through downflow trickle bed pilot plant located in Haldor Topsoe's R&D facilities. The unit consists of two reactors in series. 173 The product was first separated in a high-pressure separator (HPS). The liquid product from the 174 175 HPS was sent to a low-pressure separator (LPS) and to a stripper for removal of gases and other noncondensed light hydrocarbons. Nitrogen was used as the stripping agent, and once-through 176 pure hydrogen was used. The catalyst was diluted with an inert material (mesh 60 carborundum) 177 using a 25 vol% SiC/75 vol% catalyst ratio. The operating conditions are given in Table 1 for 178 study A (influence of the temperature) and study B (influence of the initial deactivation). The 179 feed properties are listed in Table 2. The results of study A are summarized in Table 3, and the 180 results of study B are provided in Table 4. Note that the catalysts loaded were commercial 181 catalysts used in residue service developed and produced by Haldor Topsoe A/S. 182

184 **Table 1.** Operating Conditions of the Pilot Plant Tests

Inlet pressure hydrogen (barg)	165
H <sub>2</sub> /oil (mL/L)	550
Overall liquid hourly space	0.2

	velocity (LHSV) (h <sup>-1</sup> )
185	
186	
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189	
190	

Table 2. Feed Properties

Property	Method	Atmospheric residue (ATM)	Vacuum residue (VAC)	Blend 93 vol% ATM and 7 vol% VAC
Nitrogen, wt ppm	D 5762	2800	4500	3100
Sulfur, wt%	D 4294	3.985	5.00	4.061
Hydrogen, wt%	D 7171 H	10.75	(11.18)*	10.78
C, wt%	By difference	85.0	83.4	84.8
H/C	-	0.13	0.13	0.13
SG 60/60 °F	D 4052	0.9797	-	0.9847
Density at 40 °C, g/ml	D 4052	0.9621	-	0.9672
Nickel, wt ppm	ICP-MS	21.1	42.4	27.0
Vanadium, wt ppm	ICP-MS	61.1	121	73.0
Carbon Residue, wt%	D 4530	12.02	24.42	12.96
Asphalthenes, wt%	D 6560	5.1	11.0	6.4
Simulated Distilation	D 7169			
0.5 wt% (IBP), °C		221	415	235
5 wt%, °C		341	515	353
10 wt%, °C		378	542	388
30 wt%, °C		454	600	467
50 wt%, °C		535	649	546
70 wt%,°C		614	709	627
80 wt%, °C		665	-	676
85 wt%, °C		698	-	705
90 wt%, °C		736	-	-
95 wt%, °C		-	-	-
99.5 wt% (FBP), °C		-	-	-

\*: H content back-calculated from the properties of the atmospheric residue and of the blend assuming that volume and weight fractions are equivalent as density could not be measured for the vaccum residue.

204	Table 3. Results of Study A (Influence of the Temperature)

Sample type		Feed	Product	Product	Product
Run time, hours			1,003	1,101	1,337
Temperature of the reactor, °C			375	380	385
Sulfur, wt%	ASTM D4294	4.061	0.446	0.349	0.291
Nickel, wt ppm	ICP-MS	27	5.16	4.12	3.62
Vanadium, wt ppm	ICP-MS	73	8.61	6.65	5.85
Asphaltenes, wt%	ASTM D6560	6.4	1.4	1.2	1.6
Simulated Distillation	ASTM D7169				
0.5 wt% (IBP), °C		235	142	142	128
5 wt%, °C		353	258	244	234
10 wt%, °C		388	306	295	285
30 wt%, °C		467	399	391	394
50 wt%, °C		546	466	456	464
70 wt%,°C		627	541	532	542
80 wt%, °C		676	579	572	586
85 wt%, °C		705	603	595	612
90 wt%, °C		-	630	623	641
95 wt%, °C		-	665	658	678
99.5 wt% (FBP), °C		-	721	721	717

217 Table 4. Results of Study B (Influence of the Initial Deactivation Due to Coke Laydown)

Sample type		Feed	Product	Product	Product	Product
Run time, hours			23	52	76	100
Temperature of the rea	ctor, °C		375	375	375	375
Sulfur, wt%	ASTM D4294	4.061	0.098	0.179	0.212	0.282
Nickel, wt ppm	ICP-MS	27	1.18	1.74	2.08	2.89
Vanadium, wt ppm	ICP-MS	73	2.02	2.84	3.25	4.32
Simulated Distillation	ASTM D7169					
0.5 wt% (IBP), °C		235	142	67	142	155
5 wt%, °C		353	249	247	260	272
10 wt%, °C		388	301	300	313	323
30 wt%, °C		467	407	403	415	421
50 wt%, °C		546	482	474	491	497
70 wt%,°C		627	572	553	577	583
80 wt%, °C		676	632	598	632	639
85 wt%, °C		705	675	626	668	676
90 wt%, °C		-	-	659	716	721
95 wt%, °C		_	-	702	-	-
99.5 wt% (FBP), °C		-	-	-	-	-

### 220 RESULTS AND DISCUSSION

### 221 Feedstock properties and fingerprints of the metal complexes in the feedstocks

222 The physico-chemical properties of the atmospheric and vacuum residues as well as those of 223 the blends are listed in Table 2. The properties are in line with those of the typical atmospheric and vacuum residues reported in the literature.<sup>1</sup> It is interesting to note that there is a factor of 2 224 difference between the two residues with respect to the Ni, V, asphaltene and MCR contents. 225 When two feeds are blended, it is important to check whether aggregation phenomena occur as 226 these aggregates may influence the asphaltene stability and thereby the residue hydrotreating 227 228 process. As shown in Figure 1, the theoretical blend (i.e., the calculated profile based on the 229 analysis of the atmospheric and vacuum residues) and the physical blend show the same distribution, indicating that no nanoaggregation occurs. It should be noted that this finding could 230 231 be a consequence of the fractions stemming from the same crude oil. Indeed, trimodal size distributions are observed for both the V and Ni compounds present in these feedstocks, while a 232 less pronounced trimodal distribution, much richer in MMW aggregates, is observed for the 233 234 sulfur compounds.

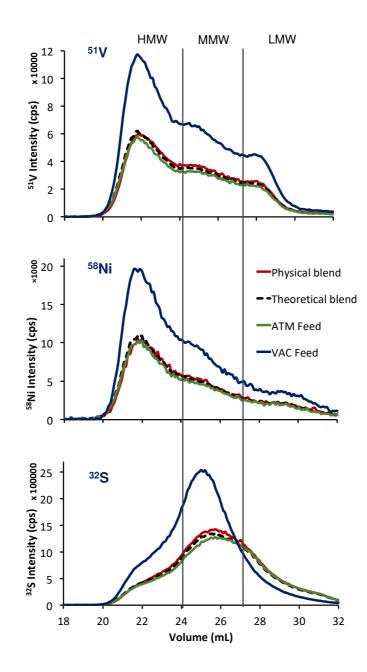
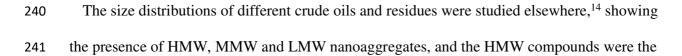


Figure 1. GPC ICP HR MS chromatograms of the V, Ni and S species in the atmospheric residue feedstock (ATM, green line),
 vacuum residue (VAC, blue line), blend of 93 vol% ATM and 7% VAC (physical blend, red line) and theoretically reconstructed
 blend of 93 vol% ATM and 7 vol% VAC (black dashed line) based on individual ATM and VAC chromatograms.



242 most abundant in Ni and V, while the MMW nanoaggregates were most abundant in S. The

results obtained in this study are consistent with these previous results.

244 Study A – influence of the temperature

Behavior of V and Ni. The evolution of the V and Ni species present in the feed after having
been through the hydrotreating process at different temperatures has been studied. The samples
were hydrotreated at the three different temperatures previously mentioned: 375 °C, 380 °C and
385 °C.

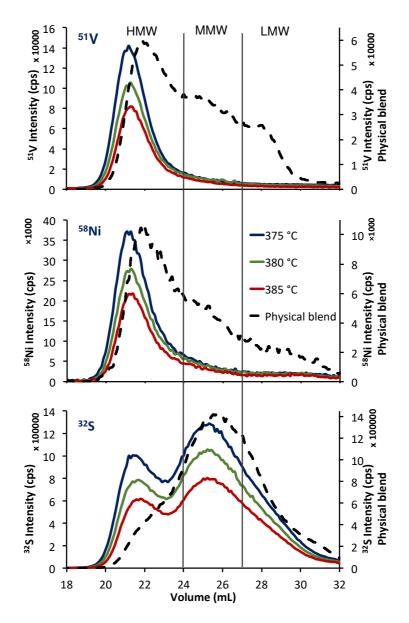


Figure 2. GPC ICP HR MS chromatograms of the V, Ni and S species in the feed (black dashed line) and the product after having
 been hydrotreated at different temperatures (the hydrotreatments at 375 °C, 380 °C and 385 °C correspond to the blue, green
 and red lines, respectively).

253

Figure 2 shows that, as expected, at higher temperatures, more V, Ni and S species are 254 removed. For V and Ni, the LMW and MMW aggregates are easily hydrotreated even at low 255 temperatures, and as the temperature is increased, only the remaining HMW aggregates are 256 hydrotreated. This phenomenon can be quantitatively observed in Figure 3, where the 257 258 concentration of each nanoaggregate size is determined based on the areas of the peaks (details 259 of the integration method are available in the open literature).<sup>15</sup> The concentration of LMW and MMW aggregates is negligibly small at all temperatures, while the concentration of HMW 260 aggregates shows a linear decrease as a function of the temperature. The correlation coefficient 261 262 of the slope is better for the regression of the HMW nanoaggregates compared to those of the MMW and LMW nanoaggregates, confirming that the temperature is driving the HMW 263 264 hydrotreatment. From the slopes of these linear trends, as listed in Table 5, it can be readily observed that the HMW V aggregates are hydrotreated faster than the Ni aggregates. This 265 observation is in agreement with previous results in the open literature.<sup>19</sup> 266

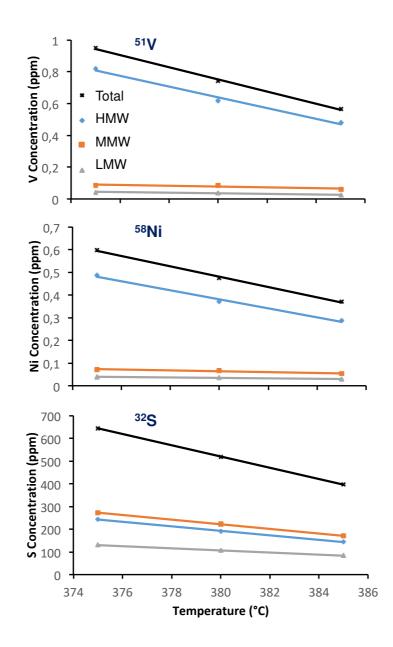


Figure 3. The concentrations of V, Ni and S (total in black, HMW in blue, MMW in orange and LMW in gray) in the products that
 were hydrotreated at different temperatures quantified based on the total concentration and the GPC ICP HR MS
 chromatograms.

276	Table 5. Slopes and Regress.	on Coefficients for the Varia	tion in V, Ni and S Concentrations vs.	Temperature
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	Total		Total HMW		MMW		LMW	
	Slope	r <sup>2</sup>	Slope	r <sup>2</sup>	Slope	r <sup>2</sup>	Slope	r <sup>2</sup>
V	-3.82 E-02	0.998	-3.39 E-02	0.988	-0.25 E -02	0.733	-0.19 E -02	0,965
Ni	-2.28 E-02	0.998	-1.98 E -02	0.992	-0.19 E -02	0.957	-0.10 E -02	0,879
S	-24.84	0.999	-9.955	0.997	-10.21	0.999	-4.678	0,999

278

279 Behavior of S. Interestingly, the fate of the S aggregates differs from that observed for the V 280 and Ni aggregates. Figures 2 and 3 show that the LMW and MMW S aggregates are not fully hydrotreated at the lowest temperatures. This phenomenon indicates that these LMW and MMW 281 compounds are more refractory compared to the size-similar V and Ni compounds. It is also 282 worth noting that a bimodal HMW-MMW S distribution is observed in the hydrotreated 283 products, while this distribution was not clearly present in the feedstock. It is likely that a 284 285 trimodal distribution occurs in the feedstock but is hidden due to the high concentration of 286 aggregates eluting in the MMW range. These results show that S compounds/nanoaggregates with molecular weights between HMW and MMW are more easily removed, indicating that the 287 catalyst possesses a higher efficiency for these kinds of nanoaggregates. 288

### 289 Study B - initial deactivation due to coke laydown

The initial and fast deactivation during ARDS tests is due to coking and, more specifically, the strong initial adsorption of polyaromatic compounds, including N-containing molecules onto the surface of the catalyst.<sup>11</sup> In commercial units, the impact of the initial coke laydown on HDS and HDM is not simple to evaluate. For some units, it is clear that the HDM activity is more affected than the HDS activity during the first hundred hours. For other units, the initial deactivations of

the HDS and HDM activities are equal, which depends on the catalyst loading, feed properties
and operating conditions. Therefore, the goal of this study was to evaluate how the initial
deactivation (which is due to coke laydown) affected the hydrotreatment rates of the various
aggregates and if certain differences between the initial deactivations of HDM and HDS could be
observed, which could be related to the aggregate distribution. For this purpose, the temperature
of the process was kept constant at 375 °C to evaluate the changes due to the initial catalyst
deactivation (at 23, 52, 76 and 100 run hours).

302 Behavior of V and Ni. The evolution of the V and Ni species present in the feed after having been through the hydrotreating process at different times has been studied. As shown in Figure 4, 303 304 initially, the concentration of V and Ni species is very low, but during the first hours of the test, a steady increase in the total concentration of V and N is observed. Figure 5 shows the quantitative 305 description of this increase. This increase is almost entirely ascribed to an increase in the HMW 306 307 fraction. It should be noted that most of the LMW and MMW aggregates are removed throughout the test despite the increasing deactivation (Table 6) of the catalyst, as indicated by 308 309 the total product Ni and V contents listed in Table 4.

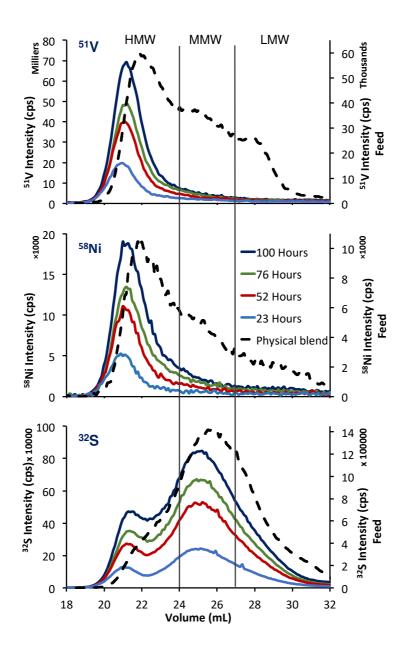


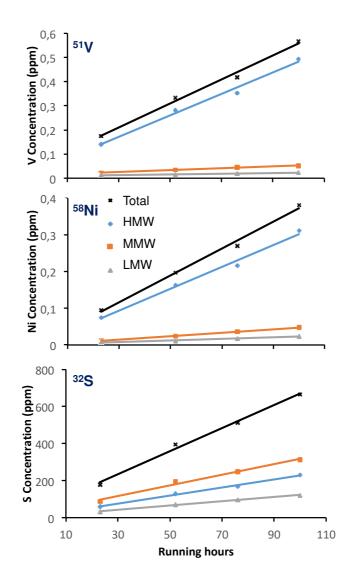
Figure 4. GPC ICP HR MS chromatograms of the V, Ni and S species in the feed (black dashed line) and the product for different
 run times after having been hydrotreated at the same temperature (the run times of 23 h, 52 h, 76 h and 100 h correspond to
 the light blue, red, green and blue lines, respectively).

319	Table 6. Slopes and Regression Coefficients for the Variation in V, Ni and S Concentration vs. Run Time (Hours).

	Total		Total HMW		MMW		LMW	
	Slope	r <sup>2</sup>	Slope	r <sup>2</sup>	Slope	r <sup>2</sup>	Slope	r <sup>2</sup>
V	4.96 E-03	0.991	4.44 E-03	0.987	0.38 E -03	0.989	0.14 E -03	0,997
Ni	3.66 E-03	0.993	2.98 E -03	0.989	0.46 E -03	0.997	0.22 E -03	0,966
S	6,22	0.994	2.19	0.994	2.87	0.990	1.16	0,995

321

322 *Behavior of S.* In Figure 4, it is observed that the sulfur species follow a different evolution. A 323 bimodal distribution of the HMW and MMW peaks is observed, and its ratio has been calculated, 324 resulting in an almost constant value. As shown more clearly in Figure 5, the increase in S 325 species is similar for the three groups of hydrodynamic volume distributions, which could 326 indicate either a higher preference of the catalyst for the HMW species (if we compare the 327 behavior of S with the behavior of V and Ni) or a more refractory behavior from the S species 328 with the catalyst.



329

Figure 5. The concentrations of V, Ni and S (total in black, HMW in blue, MMW in orange and LMW in gray) in the products that
 were hydrotreated for different run times quantified based on the total concentration and the GPC ICP HR MS chromatograms.

### 333 CONCLUSION

334 This study has provided innovative and valuable information related to the size distributions of

the different species present in atmospheric residue feedstocks and how these distributions vary

- during HDS and HDM processes. Obtaining fingerprints of the metal aggregates in these
- 337 feedstocks has provided us with a better understanding of their speciation in S, Ni and V. For the

Ni and V aggregates, it was found that the HMW compounds are more refractory compared to
the LMW and MMW compounds, which are removed at low temperatures or even after long run
hours.

For the S aggregates, a slightly different behavior was observed whereby the LMW and MMW 341 aggregates are not as easily hydrotreated, and in fact, the MMW nanoaggregates/compounds are 342 slightly less easily hydrotreated compared to the HMW aggregates. This phenomenon illustrates 343 344 the inherent difference in chemical composition of the metallo-organic compounds compared to 345 the sulfur-containing compounds and their reactivity. In a previous study<sup>15,20,21</sup> free porphyrinic compounds were easily removed, possibly via easy access of the molecules to the catalyzer. Of 346 347 the HMW nanoaggregate part, only a small portion can be easily removed, which can be the porphyrins linked at the surface of the nanoaggregates,<sup>15</sup> but the Ni and V compounds that are 348 located deeper in the nanoaggregates are more difficult to remove as the shell of the 349 350 nanoaggregates has to be removed first before the V and Ni compounds can access the catalyst. In regard to the S compounds, the observed behavior seems to me driven more by the types of S 351 compounds than by the aggregation states of the S compounds. Here, the molecular 352 conformation of the S compounds needs to be studied. More in-depth molecular studies have to 353 be conducted. 354

Nevertheless, this study provides insights into the catalyst preference towards these
compounds/nanoaggregates, which is an important factor for future optimization of the balance
between the HDM and HDS catalysts for those ARDS units processing different feedstocks with
different V, Ni and S nanoaggregate distributions.

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- **364** The authors declare no competing financial interest.

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### 434 TABLE CAPTIONS

- **Table 1.** Operating Conditions of the Pilot Plant Tests
- 436 **Table 2.** Feed Properties
- 437 **Table 3.** Results of Study A (Influence of the Temperature)
- **Table 4.** Results of Study B (Influence of the Initial Deactivation Due to Coke Laydown)
- 439 **Table 5.** Slopes and Regression Coefficients for the Variation in V, Ni and S Concentrations vs.
- 440 Temperature
- 441 **Table 6.** Slopes and Regression Coefficients for the Variation in V, Ni and S Concentration vs.
- 442 Run Time (Hours)

#### 444 FIGURE CAPTIONS

Figure 1. GPC ICP HR MS chromatograms of the V, Ni and S species in the atmospheric

residue feedstock (ATM, green line), vacuum residue feedstock (VAC, blue line), blend of 93

447 vol% ATM and 7% VAC (physical blend, red line) and theoretically reconstructed blend of 93

448 vol% ATM and 7 vol% VAC (black dashed line) based on individual ATM and VAC

449 chromatograms.

450 Figure 2. GPC ICP HR MS chromatograms of the V, Ni and S species in the feed (black dashed

451 line) and product after hydrotreatment at different temperatures (the hydrotreatments at 375 °C,

452 380 °C and 385 °C correspond to the blue, green and red lines, respectively).

Figure 3. The concentrations of V, Ni and S (total in black, HMW in blue, MMW in orange and
LMW in gray) in the products that were hydrotreated at different temperatures quantified based
on the total concentration and the GPC ICP HR MS chromatograms.

Figure 4. GPC ICP HR MS chromatograms of the V, Ni and S species in the feed (black dashed
line) and the product for different run times after having been hydrotreated at the same
temperature (the run times of 23 h, 52 h, 76 h and 100 h correspond to the light blue, red, green
and blue lines, respectively).

Figure 5. The concentrations of V, Ni and S (total in black, HMW in blue, MMW in orange and
LMW in gray) in the products that were hydrotreated for different run times quantified based on
the total concentration and the GPC ICP HR MS chromatograms.